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Technical Basis for Regulatory Guidance on the Alternate Pressurized Thermal Shock Rule

Final Report

Office of Nuclear Regulatory Research

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Prepared by:
G. Stevens[1]
M. Kirk
M. Modarres[2]

[1] Structural Integrity Associates, Inc.
11515 Vanstory Drive, Suite 125
Huntersville, NC 28078

[2] University of Maryland
Clark School of Engineering
College Park, MD 20742-7531

Mark Kirk, NRC Project Manager

Office of Nuclear Regulatory Research

ABSTRACT

During plant operation, the walls of reactor pressure vessels (RPVs) are exposed to neutron radiation, resulting in embrittlement of the vessel steel and weld materials in the area of the RPV adjacent to the core. If an embrittled RPV had a flaw of critical size and if certain severe system transients were to occur, the flaw could rapidly propagate through the vessel, resulting in a through-wall crack that could challenge the integrity of the RPV. The severe transients of concern, known as pressurized thermal shock (PTS), are characterized by a rapid cooling of the internal RPV surface in combination with repressurization of the RPV. Advances in understanding material behavior, the ability to realistically model plant systems and operational characteristics, and the ability to better evaluate PTS transients to estimate loads on vessel walls led the U.S. Nuclear Regulatory Commission (NRC) to develop a risk-informed revision of the existing PTS Rule in Title 10 of the *Code of Federal Regulations* (10 CFR) 50.61a, "Alternate Fracture Toughness Requirements for Protection against Pressurized Thermal Shock Events."

This report explains the basis for the requirements that establish the entry conditions to permit the use of 10 CFR 50.61a and describes methods that licensees can use to meet the following four requirements:

(1) criteria related to the date of construction and design requirements
(2) criteria related to the evaluation of plant-specific surveillance data
(3) criteria related to inservice inspection data and nondestructive examination requirements
(4) criteria related to alternate screening criteria on embrittlement

FOREWORD

The reactor pressure vessel (RPV) is exposed to neutron radiation during normal operation. Over time, the RPV steel becomes progressively more brittle in the region adjacent to the core. If a vessel has a preexisting flaw of critical size and if certain severe system transients occur, this flaw could propagate rapidly through the vessel, resulting in a through-wall crack. The severe transients of concern, known as pressurized thermal shock (PTS), are characterized by rapid cooling (i.e., thermal shock) of the internal RPV surface that may be combined with repressurization. The simultaneous occurrence of flaws of critical size, embrittled steel, and a severe PTS transient is a low-probability event. U.S. pressurized-water reactors (PWRs) are not projected to approach the levels of embrittlement that would make them susceptible to PTS failure, even during extended operation beyond the original 40-year design life.

Advances in understanding material behavior, the ability to realistically model plant systems and operational characteristics, and the ability to better evaluate PTS transients to estimate loads on vessel walls led the U.S. Nuclear Regulatory Commission to develop a risk-informed revision of the existing PTS Rule in Title 10 of the *Code of Federal Regulations* (10 CFR) 50.61a, "Alternate Fracture Toughness Requirements for Protection against Pressurized Thermal Shock Events" (Alternate PTS Rule).

The Alternate PTS Rule provides revised PTS screening criteria in the form of an embrittlement reference temperature, RT_{MAX-X}, which characterizes the RPV material's resistance to flaw-initiated fractures. The Alternate PTS Rule is based on more comprehensive analysis methods than the existing PTS Rule in 10 CFR 50.61, "Fracture Toughness Requirements for Protection against Pressurized Thermal Shock Events." This alternate rule became desirable because the existing requirements, such as those in 10 CFR 50.61, are based on unnecessarily conservative assumptions. The Alternate PTS Rule reduces regulatory burden for those PWR licensees that expect to exceed the 10 CFR 50.61 embrittlement requirements before the expiration of their operating licenses while still maintaining adequate safety margins. PWR licensees may choose to comply with the Alternate PTS Rule as a voluntary alternative to complying with the requirements in 10 CFR 50.61.

This document explains the basis for the requirements that establish the entry conditions that allow licensees to use the Alternate PTS Rule. It also describes methods that licensees can use to meet the following four requirements:

(1) criteria related to the date of construction and design requirements
(2) criteria related to the evaluation of plant-specific surveillance data
(3) criteria related to inservice inspection data and nondestructive examination requirements
(4) criteria related to alternate screening criteria on embrittlement

Raymond Furstenau, Director
Director of Nuclear Regulatory Research
U.S. Nuclear Regulatory Commission

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EXECUTIVE SUMMARY

In early 2010, the U.S. Nuclear Regulatory Commission (NRC) promulgated Title 10 of the *Code of Federal Regulations* (10 CFR) 50.61a, “Alternate Fracture Toughness Requirements for Protection against Pressurized Thermal Shock Events” (Alternate Pressurized Thermal Shock (PTS) Rule) to amend existing regulations to provide alternate embrittlement requirements for protection against PTS events in pressurized-water reactor (PWR) pressure vessels. These requirements are based on more comprehensive, accurate, and realistic analysis methods than those used by the NRC to establish the screening criteria in 10 CFR 50.61, “Fracture Toughness Requirements for Protection against Pressurized Thermal Shock Events.” This alternate rule became desirable because the existing requirements in 10 CFR 50.61 are based on unnecessarily conservative assumptions. The Alternate PTS Rule reduces regulatory burden for those PWR licensees that expect to exceed the 10 CFR 50.61 embrittlement requirements before the expiration of their operating licenses while still maintaining adequate safety margins. PWR licensees may choose to comply with the Alternate PTS Rule as a voluntary alternative to complying with the requirements in 10 CFR 50.61.

The Alternate PTS Rule provides revised PTS screening criteria in the form of embrittlement reference temperatures, RT_{MAX-X}, that characterize the RPV material’s resistance to fracture initiating from flaws. Licensees may use the RT_{MAX-X} embrittlement screening criteria as long as they meet the following four criteria:

(1) criteria related to the date of construction and design requirements

The Alternate PTS Rule applies to licensees whose construction permits were issued before February 3, 2010, and whose RPVs were designed and fabricated to the standards in the 1998 edition (or an earlier edition) of the American Society of Mechanical Engineers Boiler and Pressure Vessel Code (ASME Code). The NRC applied this restriction because the structural and thermal-hydraulic analyses that established the basis for the Alternate PTS Rule embrittlement screening criteria represented only plants constructed before this date. Licensees are responsible for demonstrating that their technical-basis calculations, developed in support of the Alternate PTS Rule, address the risk-significant factors that control PTS for any plant constructed after February 3, 2010. Chapter 4 of this document describes methods by which licensees can satisfy these criteria and identifies factors to be considered in such an evaluation.

(2) criteria related to evaluation of plant-specific surveillance data

The Alternate PTS Rule includes statistical tests that licensees must perform on RPV surveillance data to determine whether the surveillance data are sufficiently close to the predictions of an embrittlement trend curve (ETC) that the ETC predictions are valid for use. Of particular interest from a regulatory perspective is the use of these statistical tests to determine whether plant-specific surveillance data deviate significantly from the ETC predictions in a manner that suggests the ETC is likely to underpredict plant-specific data trends. Chapter 5 of this document describes guidance on assessing the closeness of plant-specific data to the ETC using statistical tests, including the following:

- a detailed description of the mathematical procedures for use in assessing the licensee's compliance with the three statistical tests in the Alternate PTS Rule

- a list of factors to consider in diagnosing the reason why a particular surveillance dataset might fail these statistical tests

- a description of certain situations under which the licensee can adjust the ETC predictions

(3) criteria related to inservice inspection (ISI) data and nondestructive examination (NDE) requirements

The Alternate PTS Rule describes a number of tests of and conditions on the collection and analysis of ISI data that should provide reasonable assurance that the distribution of flaws assumed to exist in the probabilistic fracture mechanics (PFM) calculations, which provide the basis for the RT_{MAX-X} screening criteria, provides an acceptable model of the population of flaws in the RPV of interest. Chapter 6 of this document provides guidance to help licensees satisfy these criteria. This document discusses the following guidance:

- guidance for initial evaluation of NDE data obtained from qualified ISI examinations

- guidance for further evaluation of NDE data obtained from qualified ISI examinations, including the following:

  - elements and NDE techniques associated with the qualified ISI examinations in Mandatory Appendix VIII, "Performance Demonstration for Ultrasonic Examination Systems," to Section XI, "Rules for Inservice Inspection of Nuclear Power Plant Components," of the ASME Code that are performed to assess compliance with the requirements of the Alternate PTS Rule

  - a mathematical procedure that can be used to adjust NDE data to account for flaw detection and sizing errors and comparison of the adjusted data to the population of flaws assumed in the PFM technical basis for the Alternate PTS Rule

- guidance for plants with RPV flaws that fall outside the applicability of the flaw tables in the Alternate PTS Rule, including the following:

  - a mathematical procedure that licensees can use to preclude brittle fracture based on RT_{NDT} information

  - a mathematical procedure that licensees can use to combine the NDE data with the population of flaws assumed in the PFM calculations to estimate the total flaw distribution that is predicted to exist in the RPV and guidance on how to apply this total flaw distribution as part of a PFM calculation using the Fracture Analysis of Vessels–Oak Ridge computer code

(4) criteria related to alternate screening criteria on embrittlement

Guidance is provided to help licensees estimate a plant-specific value of through-wall cracking frequency for cases that do not satisfy the RT_{MAX-X} screening criteria of the Alternate PTS Rule. Chapter 7 of this document describes the two sets of guidance on satisfying the embrittlement acceptability criteria.

This document provides guidance and the associated technical basis for methods that licensees can use to meet these requirements.

ABBREVIATIONS AND ACRONYMS

ADAMS	Agencywide Documents Access and Management System
AP	Advanced Passive
APWR	Advanced Pressurized Water Reactor
ASME	American Society of Mechanical Engineers
ASME Code	American Society of Mechanical Engineers Boiler and Pressure Vessel Code
BWR	Boiling Water Reactor
CFR	Code of Federal Regulations
CVN	Charpy V-Notch
E	Energy
EPR	Evolutionary Power Reactor
EPRI	Electric Power Research Institute
ETC	Embrittlement Trend Curve
F	Degrees Fahrenheit
FAVOR	Fracture Analysis of Vessels–Oak Ridge
HAZ	Heat-Affected Zone
ISI	Inservice Inspection
Mev	Million Electron Volts
MRP	Materials Reliability Program
N/cm^2	Neutrons Per Square Centimeter
NDE	Nondestructive Examination
NRC	U.S. Nuclear Regulatory Commission
NRR	Office Of Nuclear Reactor Regulation
ORNL	Oak Ridge National Laboratory
PFM	Probabilistic Fracture Mechanics
PNNL	Pacific Northwest National Laboratory
POD	Probability Of Detection
PRA	Probabilistic Risk Assessment
PTS	Pressurized Thermal Shock
PVRUF	Pressure Vessel Research User Facility
PWR	Pressurized Water Reactor
RPV	Reactor Pressure Vessel
SCD	Surveillance Capsule Data
TWCF	Through Wall Cracking Frequency
TWE	Through Wall Extent
UT	Ultrasonic Testing

SYMBOLS AND EXPRESSIONS

A	Multiplier for determining ΔT_{30} based on the product form
ADJ	An adjustment in the embrittlement prediction to account for a failure of the mean test
B	Multiplier for determining ΔT_{30} based on the product form
C_1 and C_2	Critical values of the outlier test
CRP	Intermediate term for determining ΔT_{30} in degrees Fahrenheit or Celsius
Cu	Copper content in weight percent
Cu_e	Effective copper content in weight percent
$f(Cu_e,P)$	Intermediate term for determining ΔT_{30} based on effective copper content and phosphorus content
$g(Cu_e,Ni, \phi t_e)$	Intermediate term for determining ΔT_{30} based on the effective copper content, nickel content, and effective fluence
m	Slope of ΔT_{30} prediction residuals plotted versus the base-10 logarithm of fluence
MATLAB	Matrix laboratory
$Max(Cu_e)$	Intermediate term for determining ΔT_{30} based on the effective copper content
MD	Intermediate term for determining ΔT_{30} based on degrees Fahrenheit or Celsius
Mn	Manganese content in weight-percent
n	Number of ΔT_{30} observations in a plant specific surveillance dataset
Ni	Nickel content in weight-percent
P	Phosphorus content in weight-percent
r*	Normalized residual
r^*_1 and r^*_2	Calculated values of residuals for the outlier test
$r_{LIMIT(1)}$ and $r_{LIMIT(2)}$	Critical values of the outlier test (the same as C_1 and C_2)
r_{max}	Maximum permissible ΔT_{30} prediction residual
r_{mean}	Mean ΔT_{30} prediction residual for a plant specific surveillance dataset
$R_{(max1)}$	The largest ΔT_{30} prediction residual for a plant specific surveillance dataset
$R_{(max2)}$	The second largest ΔT_{30} prediction residual for a plant specific surveillance dataset
$RT_{MAX\ X}$	Any or all of the values $RT_{MAX\text{–}AW}$, $RT_{MAX\text{–}PL}$, $RT_{MAX\text{–}FO}$, $RT_{MAX\text{–}CW}$, or sum of $RT_{MAX\text{–}AW}$ and $RT_{MAX\text{–}PL}$ for a particular reactor vessel, expressed as a temperature in degrees Fahrenheit or Celsius
$RT_{MAX\ AW}$	A value, expressed as a temperature in degrees Fahrenheit or Celsius, which characterizes the reactor vessel's resistance to fracture initiating from flaws found along axial weld fusion lines
$RT_{MAX\ PL}$	A value, expressed as a temperature in degrees Fahrenheit or Celsius, which characterizes the reactor vessel's resistance to fracture initiating from flaws found in plates remote from welds

$RT_{MAX\ FO}$	A value, expressed as a temperature in degrees Fahrenheit or Celsius, which characterizes the reactor vessel’s resistance to fracture initiating from flaws in forgings remote from welds
$RT_{MAX\ CW}$	A value, expressed as a temperature in degrees Fahrenheit or Celsius, which characterizes the reactor vessel’s resistance to fracture initiating from flaws found along circumferential weld fusion lines
RT_{NDT}	Nil ductility transition temperature in degrees Fahrenheit or Celsius
$RT_{NDT(u)}$	Unirradiated nil ductility transition temperature in degrees Fahrenheit or Celsius
RT_{PTS}	The RT_{NDT} value at the end of a license, as defined in 10 CFR 50.61, in degrees Fahrenheit or Celsius
S	Distance of flaw below surface in inches or millimeters
se(m)	Standard error of m
t_e	Effective time in seconds
T_C	Irradiated (coolant) temperature in degrees Fahrenheit or Celsius
$T_{CRIT(\alpha)}$	Critical value of Student’s t distribution
T_m	T statistic for m
t, T_{WALL}	Wall thickness in inches or millimeters
t(...)	Student’s t distribution
TWE	Through wall extent in inches or millimeters
TWE_{MAX}	Maximum through wall extent in inches or millimeters
TWE_{MIN}	Minimum through wall extent in inches or millimeters
VFLAW	Vessel flaw
α	Statistical significance level
ΔT_{30}	Increase in the Charpy V notch energy transition temperature in degrees Fahrenheit or Celsius at 30 foot pounds or 41 joules caused by neutron irradiation embrittlement
$\Delta T_{30(ADJ)}$	An adjusted value of ΔT_{30} in degrees Fahrenheit or Celsius that accounts for a failure in the mean slope test
$\Delta T_{30i(measured)}$	A measured value of ΔT_{30} in degrees Fahrenheit or Celsius
$\Delta T_{30i(ETC\ mean)}$	A value of ΔT_{30} predicted by Equation (1) in degrees Fahrenheit or Celsius
ΔYS	Change in yield strength in thousands of pounds per square inch or megapascals
ϕ	Flux in neutrons per square centimeter per second
ϕt	Fluence in neutrons per square centimeter
ϕt_e	Effective fluence in neutrons per square centimeter
σ	Standard deviation in degrees Fahrenheit or Celsius

1 INTRODUCTION

1.1 Background

The U.S. Nuclear Regulatory Commission (NRC) promulgated Title 10 of the *Code of Federal Regulations* (10 CFR) 50.61a, “Alternate Fracture Toughness Requirements for Protection against Pressurized Thermal Shock Events” (the Alternative Pressurized Thermal Shock (PTS) Rule) [1], on January 4, 2010 (Volume 75 of the *Federal Register*, pages 13–29 (75 FR 13–29) [2]). The regulations at 10 CFR 50.61a amend existing regulations to provide alternate fracture toughness requirements for protection against PTS events for pressurized-water reactor (PWR) pressure vessels.

The Alternate PTS Rule provides alternate embrittlement requirements that are based on more comprehensive analysis methods. This regulatory action became desirable because the existing requirements, such as those in 10 CFR 50.61, “Fracture Toughness Requirements for Protection against Pressurized Thermal Shock Events” [3], are based on unnecessarily conservative assumptions. The Alternate PTS Rule reduces regulatory burden, while maintaining adequate safety, for those PWR licensees that expect to exceed the 10 CFR 50.61 embrittlement requirements before the expiration of their operating licenses. PWR licensees may choose to comply with the Alternate PTS Rule as a voluntary alternative to complying with the requirements in 10 CFR 50.61.

The Alternate PTS Rule provides revised PTS screening criteria in the form of embrittlement reference temperatures, RT_{MAX-X}, that characterize the resistance of the material in the reactor pressure vessel (RPV) to fracture initiating from flaws. Table 1 of the Alternate PTS Rule and Table 1-1 of this document list the PTS screening criteria. The values in Table 1-1 of this document are based on up-to-date understandings and models of the many factors that affect the operating safety of PWRs. Chapter 2 of this report further discusses the provisions and use of the Alternate PTS Rule.

Table 1-1 $RT_{MAX\text{-}X}$ PTS Embrittlement Screening Criteria from the Alternate PTS Rule [1]

Product form and RT_{MAX-X} Values	RT_{MAX-X} limits [°F] for different vessel wall thicknesses[6] (T_{WALL})		
	$T_{WALL} \leq 9.5$ in.	9.5 in. $< T_{WALL} \leq 10.5$ in.	10.5 in. $< T_{WALL} \leq 11.5$ in.
Axial Weld RT_{MAX-AW}	269	230	222
Plate RT_{MAX-PL}	356	305	293
Forging without underclad cracks RT_{MAX-FO}[7]	356	305	293
Axial Weld and Plate $RT_{MAX-AW} + RT_{MAX-PL}$	538	476	445
Circumferential Weld RT_{MAX-CW}[8]	312	277	269
Forging with underclad cracks RT_{MAX-FO}[9]	246	241	239

[6] Wall thickness is the beltline wall thickness including the clad thickness.

[7] Forgings without underclad cracks apply to forgings for which no underclad cracks have been detected and that were fabricated in accordance with Regulatory Guide 1.43.

[8] RT_{PTS} limits contribute 1×10^{-8} per reactor year to the reactor vessel TWCF.

[9] Forgings with underclad cracks apply to forgings that have detected underclad cracking or were not fabricated in accordance with Regulatory Guide 1.43.

1.2 Scope of this Report

Licensees may use the RT_{MAX-X} embrittlement screening criteria shown in Table 1-1 as long as their RPV meets certain criteria outlined in the Alternate PTS Rule. This document explains the bases for the criteria that establish the entry conditions that allow licensees to use the Alternate PTS Rule and describes methods that licensees can use to meet the following four criteria:

(1) criteria related to the date of construction and design requirements

The regulation at 10 CFR 50.61a(b) restricts the applicability of the Alternate PTS Rule to reactors for which construction permits were issued before February 3, 2010, and that have RPVs designed and fabricated to the 1998 edition (or an earlier edition) of the ASME American Society of Mechanical Engineers Boiler and Pressure Vessel Code (ASME Code). Chapter 4 describes the criteria related to the date of plant construction by which licensees can use the Alternate PTS Rule.

(2) criteria related to the evaluation of plant-specific surveillance data

Under 10 CFR 50.61a(f), the NRC requires licensees to verify that their plant-specific surveillance data for the RPV in question satisfy three statistical tests described in the Alternate PTS Rule. These tests assess whether the embrittlement trend curve (ETC) used in the Alternate PTS Rule adequately predicts these plant-specific surveillance data. If the licensee cannot verify these predictions, it must submit an evaluation of plant-specific surveillance data to the Director of the NRC Office of Nuclear Reactor Regulation (NRR) that proposes a method to account for plant-specific surveillance data when assessing the subject RPV relative to the Alternate PTS Rule screening criteria on RT_{MAX-X}. Chapter 5 of this document describes methods by which licensees can satisfy these criteria.

(3) criteria related to inservice inspection (ISI) data and nondestructive examination (NDE) requirements

Under 10 CFR 50.61a(e), the NRC requires the licensee to verify that the flaw density and size distributions detected within the beltline region of the RPV during a qualified examination under Section XI, “Rules for Inservice Inspection of Nuclear Power Plant Components,” of the ASME Code [4] are bounded by flaw tables in the Alternate PTS Rule. The Alternate PTS Rule requires that any flaws detected within the inner 1 inch or 10 percent of the wall thickness of the vessel base material, whichever is greater, do not exceed the limits shown in Table 1-2. If the licensee cannot make this verification, it must demonstrate that the RPV will have a through-wall cracking frequency (TWCF) of less than $1x10^{-6}$ per reactor year. Chapter 6 of this document describes methods by which licensees can satisfy these criteria.

(4) criteria related to alternate screening criteria on embrittlement

Chapter 7 of this document describes criteria by which licensees can assess plant-specific TWCF for cases that do not satisfy the RT_{MAX-X} screening criteria of the Alternate PTS Rule.

References to the “beltline” region of the RPV throughout this report refer to all regions of the RPV adjacent to the reactor core that are exposed to a fluence of $1x10^{17}$ neutrons per square centimeter (n/cm^2) or higher during the operating lifetime of the reactor [24]. Fluence values should be determined using a methodology consistent with that specified in Regulatory Guide 1.190, “Calculational and Dosimetry Methods for Determining Pressure Vessel Neutron Fluence,” issued March 2001 [26], or by using methods otherwise acceptable to the staff.

The NRC solicited input from interested stakeholders regarding an alternate PTS regulation during three public meetings in 2011 [16]. The Electric Power Research Institute’s (EPRI’s) Materials Reliability Program (MRP) developed recommended technical methods or approaches in seven areas. MRP-334, “Materials Reliability Program: Proposed Resolutions to the Analytical Challenges of Alternate PTS Rule (10 CFR 50.61a) Implementation,” issued January 2012 [10], describes those recommended technical methods. These methods reduce the resources needed by utilities and the NRC to implement the Alternate PTS Rule and provide a consistent and acceptable level of safety subsequent to implementation of the rule, especially in those instances in which a licensee must perform alternate evaluations to demonstrate its compliance with the Alternate PTS Rule. Chapter 3 of this document discusses the NRC’s responses to the recommendations made in MRP-334.

Table 1-2 Allowable Flaw Tables from the Alternate PTS Rule [2]

Through–wall extent, TWE [in.]		Maximum number of flaws per 1000-inches of weld length in the inspection volume that are greater than or equal to TWE_{MIN} and less than TWE_{MAX}
TWE_{MIN}	TWE_{MAX}	
0	0.075	No Limit
0.075	0.475	166.70
0.125	0.475	90.80
0.175	0.475	22.82
0.225	0.475	8.66
0.275	0.475	4.01
0.325	0.475	3.01
0.375	0.475	1.49
0.425	0.475	1.00
0.475	Infinite	0.00

Through-wall extent, TWE [in.]		Maximum number of flaws per 1000 square-inches of inside surface area in the inspection volume that are greater than or equal to TWE_{MIN} and less than TWE_{MAX}. This flaw density does not include underclad cracks in forgings.
TWE_{MIN}	TWE_{MAX}	
0	0.075	No Limit
0.075	0.375	8.05
0.125	0.375	3.15
0.175	0.375	0.85
0.225	0.375	0.29
0.275	0.375	0.08
0.325	0.375	0.01
0.375	Infinite	0.00

2 OVERVIEW OF THE ALTERNATE PRESSURIZED THERMAL SHOCK RULE

2.1 Background

PTS events are system transients in a PWR during which the RPV rapidly cools down, resulting in cold vessel temperatures with or without repressurization of the RPV. The rapid cooling of the inside surface of the RPV causes thermal stresses that can combine with stresses caused by high pressure. The aggregate effect of these stresses is an increase in the potential for fracture if a preexisting flaw is present in a region of the RPV that has significant embrittlement.

The PTS Rule in 10 CFR 50.61 establishes screening criteria below which the potential for an RPV to fail because of a PTS event is deemed to be acceptably low. These screening criteria effectively define a level of embrittlement beyond which operation cannot continue without further plant-specific compensatory action or analysis. Compensatory actions include (1) reducing the neutron flux, (2) modifying the plant to reduce the PTS event probability or severity, and (3) RPV annealing. The regulations in 10 CFR 50.61(b)(3), (b)(4), and (b)(7) and in 10 CFR 50.66, "Requirements for Thermal Annealing of the Reactor Pressure Vessel," address these actions [5].

Currently, no operating PWR RPV is projected to exceed the 10 CFR 50.61 screening criteria before the expiration of its original 40-year operating license. However, several PWR RPVs are approaching the screening criteria, whereas others are likely to exceed the screening criteria during the period of license renewal.

The NRC developed technical bases that support updating the PTS regulations ([6], [7], [8], [9], [14]). These technical bases conclude that the risk of through-wall cracking because of a PTS event is much lower than previously estimated. This finding indicates that the screening criteria in 10 CFR 50.61 are unnecessarily conservative. Therefore, the NRC developed 10 CFR 50.61a, the Alternate PTS Rule, to provide alternate screening criteria based on the updated technical bases. These technical bases covered the following topics:

- applicability of the Alternate PTS Rule
- updated embrittlement correlation
- ISI volumetric examination and flaw assessments
- NDE-related uncertainties
- surveillance data

The following sections present a brief overview of these topics.

In addition, 10 CFR 50.61a(d) defines seven subsequent requirements that licensees must satisfy as a part of their implementation of the Alternate PTS Rule.

2.2 Applicability of the Alternate Pressurized Thermal Shock Rule

The Alternate PTS Rule is based, in part, on analysis of information from three currently operating PWRs. Because factors that are generally common to PWRs control the severity of the risk-significant transient classes (e.g., primary-side pipe breaks and stuck-open valves on the primary side that may later reclose), the NRC concluded that the results and screening criteria developed from these analyses could be applied with confidence to the entire fleet of operating PWRs. The NRC based this conclusion on an understanding of the characteristics of the dominant transients that drive their risk significance and on an evaluation of a larger population of high-embrittlement PWRs. This evaluation revealed no design, operational, training, or procedural factors that could credibly increase either the severity of these transients or the frequency of their occurrence in the general PWR population above the severity and frequency characteristic of the three plants that were modeled in detail. The NRC also concluded that PTS events that were insignificant risk contributors in these analyses are not expected to become dominant contributors in other plants.

The Alternate PTS Rule applies to licensees whose construction permits were issued before February 3, 2010, and whose RPVs were designed and fabricated to the 1998 edition or an earlier edition of the ASME Code.

2.3 Updated Embrittlement Correlation

The technical basis for the Alternate PTS Rule used many different models and parameters to estimate the yearly probability that a PWR will develop a through-wall crack as a consequence of PTS loading. One of these models was a revised ETC that uses information on the chemical composition and neutron exposure of low-alloy steels in the RPV beltline region to estimate the fracture-mode transition temperature of these materials. Although the general trends predicted by the embrittlement models in 10 CFR 50.61 and the Alternate PTS Rule are similar, the mathematical form of the revised ETC in the Alternate PTS Rule differs substantially from the ETC in 10 CFR 50.61. The NRC updated the ETC in the Alternate PTS Rule to more accurately represent the substantial amount of RPV surveillance data that has accumulated between the last revision of the 10 CFR 50.61 ETC in the mid-1980s and the database supporting the 10 CFR 50.61a ETC, which was finalized in 2002. Section 5.1 discusses the specifics of the updated ETC used in the Alternate PTS Rule.

2.4 Inservice Inspection Volumetric Examination and Flaw Assessments

The Alternate PTS Rule differs from 10 CFR 50.61 in that it requires licensees that choose to follow its requirements to analyze the results from ISI volumetric examinations done in accordance with ASME Code, Section XI. The analyses of ISI volumetric examinations may be used to determine whether the flaw density and size distribution in the licensee's RPV beltline region are bounded by the flaw density and size distribution used in the development of the Alternate PTS Rule.

The NRC developed the Alternate PTS Rule using flaw density, spatial, and size distributions determined from experimental data, from physical models, and from expert judgment. The experimental data were obtained by taking samples from RPV materials from canceled plants (i.e., from the Shoreham Nuclear Power Plant and the Pressure Vessel Research Users' Facility (PVRUF) vessels). The NRC believes that a comparison of the results from qualified ASME Code, Section XI, ISI volumetric examinations is necessary to confirm that the flaw density and size distributions in the RPV to which the Alternate PTS Rule may be applied are consistent with the flaw density and size distributions used in the development of the Alternate PTS Rule.

Under 10 CFR 50.55a(g)(6)(ii)(C) [11], the NRC requires licensees to implement ISI examinations in accordance with Supplements 4 and 6 [12] to Mandatory Appendix VIII, "Performance Demonstration for Ultrasonic Examination Systems," to Section XI of the ASME

Code. Supplement 4 contains qualification requirements for the RPV ISI volume from the clad-to-base-metal interface to the inner 15 percent of the RPV base material wall thickness. Supplement 6 contains qualification requirements for RPV weld volumes that lie within the outer 85 percent of the RPV base material wall thickness.

A simplified representation of the flaw density and size distributions used in the development of the Alternate PTS Rule is summarized by numerical values in Tables 2 and 3 of the Alternate PTS Rule for weld and plate/forging materials, respectively, as duplicated here in Table 1-2. Hereafter, Tables 2 and 3 of the Alternate PTS Rule are collectively referred to as "the flaw tables." These tables provide the number of flaws in each size range that were evaluated in the underlying technical bases. If the RPV has a distribution of flaws that have sizes and densities greater than those in the flaw tables, the licensee must evaluate those flaws to ensure that they are not causing the TWCF to exceed a value of $1x10^{-6}$.

The technical basis for the Alternate PTS Rule also indicated that flaws buried more deeply than 1 inch from the clad-to-base interface are not as susceptible to brittle fracture as flaws of similar size located closer to the inner surface. Therefore, the Alternate PTS Rule does not require an assessment of the density of these flaws, but the rule still requires large flaws, if discovered, to be evaluated for contributions to TWCF if they are within the inner three-eighths (3/8t) of the vessel base material wall thickness. Section II, "Discussion," of 75 FR 13–29 [2] for the Alternate PTS Rule indicates that the limitation for flaw acceptance, as specified in ASME Code, Section XI, Table IWB-3510-1, approximately corresponds to the threshold for the sizes of flaws that can contribute significantly to TWCF if they are present in RPV material at this depth. Therefore, the Alternate PTS Rule requires the licensee to evaluate flaws within the inner 3/8t of the vessel thickness that exceed the size limits in Table IWB-3510-1 for their contribution to TWCF, in addition to the other evaluations for such flaws that are prescribed in the ASME Code.

The Alternate PTS Rule also clarifies that, for consistency with ASME Code, Section XI, Mandatory Appendix VIII, the smallest flaws that must be sized are 0.075 inch in through-wall extent (TWE). For each flaw detected that has a TWE equal to or greater than 0.075 inch, the licensee is required to document the dimensions of the flaw, its orientation, its location within the RPV, and its depth from the clad-to-base-metal interface. Those planar flaws for which the major axis of the flaw is identified by a circumferentially oriented ultrasonic transducer must be categorized as ''axial.'' All other planar flaws may be categorized as ''circumferential.'' If the licensee is uncertain about which flaw dimension constitutes the major axis for a given flaw identified with an ultrasonic transducer oriented in the circumferential direction, the licensee should consider it an axial flaw. The NRC may also use this information to evaluate whether plant-specific information gathered suggests that the NRC staff should generically reexamine the technical basis for the Alternate PTS Rule.

The technical basis for the Alternate PTS Rule did not include surface cracks that penetrate through the RPV stainless steel clad and more than 0.070 inch into the welds or the adjacent RPV base metal because these types of flaws have not been observed in the beltline of any operating PWR vessel. However, flaws of this type were observed in a boiling-water reactor (BWR) RPV head in 1990 and were attributed to intergranular stress-corrosion cracking of the stainless steel cladding. BWRs are not susceptible to PTS events and, therefore, are not subject to the requirements in 10 CFR 50.61. However, if similar cracks were found in the beltline region of a PWR, they would be a significant contributor to TWCF because of their size and location. As a result, the Alternate PTS Rule requires licensees to determine whether cracks of this type exist in the beltline weld region as a part of each required ASME Code, Section XI, ultrasonic examination.

2.5 Uncertainties Related to Nondestructive Examination

The flaw sizes shown in Table 1-2 represent actual flaw dimensions, whereas the results from ASME Code, Section XI, examinations are estimated dimensions. The available information indicates that, for most flaw sizes in Table 1-2, qualified inspectors will oversize flaws. Comparing oversized flaws to the size and density distributions in Table 1-2 is conservative but not necessary.

As a result of stakeholder feedback received during the NRC's solicitation for public comments on a preliminary draft of the Alternate PTS Rule, the final published Alternate PTS Rule permits licensees to adjust the flaw sizes estimated by inspectors qualified under ASME Code, Section XI, Mandatory Appendix VIII, Supplements 4 and 6. The NRC also determined that a licensee should be allowed to consider other NDE uncertainties, such as probability of detection (POD) and flaw density and location, because these uncertainties may affect the ability of the licensee to demonstrate compliance with the Alternate PTS Rule. As a result, the language in 10 CFR 50.61a(e) allows licensees to account for the effects of NDE-related uncertainties in meeting the flaw size and density requirements of Table 1-2. The Alternate PTS Rule does not provide specific guidance on a methodology to account for the effects of NDE-related uncertainties, but the rule notes that accounting for such uncertainties may be based on data collected from ASME Code inspector-qualification tests or any other tests that measure the difference between the actual flaw size and the size determined from the ultrasonic examination. Because collecting, evaluating, and using data from ASME Code inspector-qualification tests requires extensive engineering judgment, the Alternate PTS Rule requires that the Director of NRR review and approve the methodology used to adjust flaw sizes to account for the effects of NDE-related uncertainties.

2.6 Surveillance Data

The regulation at 10 CFR 50.61a(f) defines the process for calculating the values for the reference temperature, RT_{MAX-X}, for a particular RPV material. These values may be based on the RPV material's copper (Cu), manganese (Mn), phosphorus (P), and nickel (Ni) weight percentages; reactor cold-leg coolant temperature; fast neutron flux and fluence values, and unirradiated nil-ductility transition reference temperature, RT_{NDT}.

The Alternate PTS Rule includes a procedure by which the RT_{MAX-X} values, which are predicted for plant-specific RPV materials using an ETC, are compared to heat-specific surveillance data that are collected as part of surveillance programs under Appendix H, "Reactor Vessel Material Surveillance Program Requirements," [13] to 10 CFR Part 50, "Domestic Licensing of Production and Utilization Facilities." The purpose of this comparison is to assess how well the ETC represents the surveillance data. If the surveillance data are close (closeness is assessed statistically) to the ETC, the predictions of this ETC are used, which is most often expected to be the case. However, a significant and nonconservative deviation of heat-specific surveillance data from the predictions of the ETC indicates a need for alternative methods (i.e., other than the ETC) to reliably predict the temperature-shift trend (and to estimate RT_{MAX-X}) for the conditions being assessed. Therefore, the Alternate PTS Rule includes three statistical tests to determine the significance of the differences between heat-specific surveillance data and the ETC.

3 RESPONSES TO STAKEHOLDER FEEDBACK

The NRC solicited input from interested stakeholders regarding an alternate PTS implementation regulatory guide during three public meetings in 2011 [16]. Based on those meetings, the EPRI's MRP developed recommendations for technical methods or approaches that would be useful for Alternate PTS Rule implementation in seven areas.
MRP-334 describes those recommended technical methods [10] and provides 15 specific recommendations that might reduce the resources that utilities and the NRC need to implement the Alternate PTS Rule. In addition, EPRI stated in MRP-334 that the recommendations would provide a consistent and acceptable level of safety subsequent to implementation of the Alternate PTS Rule, especially for those instances in which licensees must perform evaluations to demonstrate their compliance with the Alternate PTS Rule.

Table 3-1 includes EPRI's recommendations from MRP-334. The last column of Table 3-1 includes the NRC's responses to EPRI's recommendations. As indicated by some of the responses to EPRI's recommendations, the NRC further clarified some of the guidance in this document.

Table 3-1 EPRI Recommendations for Addressing Alternate PTS Rule Requirements [10]

No.	10 CFR 50.61a Paragraph	MRP-334 Recommendation	MRP-334 Justification	NRC Response
1	(f)(6), (a)(10)	Adjustments should not be made to sister-plant ΔT_{30} values for the purpose of performing the surveillance data tests in 10 CFR 50.61a.	The 10 CFR 50.61a ETC directly considers the material properties and the irradiation temperature in the calculation of ΔT_{30} and the residual for each point of plant or sister-plant data. Section 3.1 provides additional information.	The NRC agrees with the comment. Sister-plant data are used as part of the surveillance dataset (see Step 1a of the surveillance procedure), but no adjustments to the data are made.
2	(f)(6), (a)(10)	Limitations should be placed on the variation in chemistry within a weld heat that must be considered when considering sister-plant data.	Appendix A to this report includes an example of a weld heat with significant variation. Section 3.1 provides additional information.	The NRC agrees that the licensee should consider variations in composition if there is a need to explain or understand deviations that the statistical tests require for surveillance data. This is pointed out in Step 2(d)(ii)(a) in the section titled "Factors to Consider When the Statistical Tests of Step 2 Are Failed" under the heading "Composition and Exposure Variables." Specific limits are not provided but should be justified on a case-specific basis.
3	(f)(6)(vi), (a)(11)	If the licensee cannot meet the surveillance data tests using exact time-weighted average T_C values, it should consider a tolerance that is equivalent to plus or minus one-half of the range of the operating temperatures over the irradiation time. If the surveillance data tests can be satisfied by using a temperature within this tolerance range on T_C, ΔT_{30} values should not require an adjustment.	Large differences in irradiation temperature can also have significant effects on the calculated ΔT_{30} values. The regulation at 10 CFR 50.61a defines T_C as a time-weighted average of the cold-leg temperature under normal full-power operating conditions. However, the values used in the development of the ETC may not have reflected an accurate time-weighted average for each specific plant. This tolerance accounts for the uncertainty in the actual operating temperature when the largest changes in the embrittlement index occurred. Section 3.1 provides additional information.	The NRC agrees that the licensee should consider variations in cold-leg temperature if there is a need to explain or understand deviations identified by the statistical tests that are required for surveillance data. This is pointed out in Step 2(d)(ii)(a) in the section titled "Factors to Consider When the Statistical Tests of Step 2 Are Failed" under the heading "Composition and Exposure Variables." Specific limits are not provided but should be justified on a case-specific basis.

No.	10 CFR 50.61a Paragraph	MRP-334 Recommendation	MRP-334 Justification	NRC Response
4	(f)(6)(vi), (f)(6)(v)(A), (f)(6)(v)(C)	Section 3.2 of the report recommends a procedure to calculate the ΔT_{30} adjustment to meet the requirements of 10 CFR 50.61a(f)(6)(vi) when either the mean or outlier statistical tests are failed when the requirements in 10 CFR 50.61a(f)(6)(v) are applied.	The surveillance capsule data (SCD) statistical tests in 10 CFR 50.61a(f)(6) can be overly conservative; therefore, any needed adjustments to ΔT_{30} and RT_{MAX-X} for failing the SCD statistical tests should be minimal. The proposed procedure is simple to implement and addresses the concerns with deviation from the ETC without excessive conservatism. Section 3.2 provides additional information.	The NRC adopted this recommendation to address failures of the mean test. Refer to Step 2(b)(i). The NRC adopted a different approach to address outlier failures caused by a low-fluence datum. Refer to Step 2(b)(ii). The NRC does not disagree with the proposed procedure for outlier failures but believes that use of this procedure should be justified on a case-specific basis.
5	(f)(6)(vi), (f)(6)(v)(B)	An industry-consensus ETC that addresses irradiation-induced shifts caused by fluence values up to $1x10^{20}$ n/cm^2 (E > 1 million electron volts (MeV)) should be used to calculate the predicted values of ΔT_{30} if the slope test is not satisfied.	Data from several plants with fluence exposures of up to $8.5x10^{19}$ n/cm^2 have been evaluated, and no slope-test deviations were encountered. High-fluence SCD could possibly fail the statistical slope test. The industry has developed a coordinated surveillance program to obtain high-fluence data from power reactors for use in developing an industry-consensus ETC that addresses irradiation-induced shifts caused by fluence values up to $1x10^{20}$ n/cm^2 (E > 1 MeV). Section 3.3 provides additional information.	As of the current date, an ETC agreed on by broad consensus between the NRC and industry stakeholders does not exist. In addition, the data from the coordinated surveillance program will not be available in large quantities until 2025. The NRC agrees that, in the event of a slope-test failure, the best current understanding of irradiation damage mechanics should be used to help explain the failure and suggest corrective actions. However, because technical consensus on this matter has not been reached, the NRC is not providing guidance on this matter.

No.	10 CFR 50.61a Paragraph	MRP-334 Recommendation	MRP-334 Justification	NRC Response
6	(f)(6)(vi), (f)(6)(v)(A), (f)(6)(v)(B), (f)(6)(v)(C)	Section 3.4 provides recommendations for possible criteria for not adjusting ΔT_{30} values in accordance with 10 CFR 50.61a(f)(6)(vi) when the test requirements in 10 CFR 50.61a(f)(6)(v)(A), (B), and (C) cannot be satisfied.	There are several scenarios where an adjustment to ΔT_{30} values would not be appropriate. Section 3.4 discusses these scenarios and criteria.	As discussed in Step 2(d) of this regulatory guide, the NRC agrees that there are many situations in which adjustment of the ΔT_{30} values is neither needed nor justifiable. Step 2(d) discusses some of these situations but does not provide specific exceptions. These exceptions should be justified on a case-specific basis.
7	(d)(4), (c)(3)	A provision should be included in the proposed regulatory guide for the direct calculation of $TWCF_{95\text{-}TOTAL}$ using the plant-specific $RT_{MAX\text{-}X}$ values for cases in which the $RT_{MAX\text{-}X}$ limits in Table 1 of 10 CFR 50.61a cannot be met.	There are some conservatisms in the $RT_{MAX\text{-}XX}$ screening limits. In addition, plate and forging limited plants are likely to reach the more restrictive limit for circumferential welds before reaching the plate or forging limits. Section 3.5 provides additional information.	The NRC agrees with this recommendation. The NRC added guidance to this regulatory guide as Position 4, which refers to the appropriate formula and methods in Section 3.5.1, “Limitation on TWCF,” of NUREG-1874, “Recommended Screening Limits for Pressurized Thermal Shock (PTS),” issued March 2010.
8	(e)(1)	Any small flaws detected by ISI within +0.5 inch of the outer boundaries of the ASME Code, Section XI, inspection volume can be treated as potential plate flaws. All other flaws within the inspection volume should be treated as weld flaws.	The plate flaw limits in Table 3 of 10 CFR 50.61a should be evaluated only for RPV base metal flaws that are not affected by welding but are detected by ISI. Section 3.6 provides additional information.	The NRC agrees, in part, with this comment. This NUREG includes guidance for establishing whether the flaws are in the plate or in the weld (see Section 6.3, Step D).

No.	10 CFR 50.61a Paragraph	MRP-334 Recommendation	MRP-334 Justification	NRC Response
9	(e)(1)	Plate flaws that have a depth (TWE) of 0.4 inch or more should be evaluated as weld flaws.	This is necessary to ensure that the small flaws created during fabrication of the plates and forgings, which is what was simulated in the FAVOR probabilistic fracture mechanics analysis code, have not been expanded to larger sized flaws by the effects of welding, which were simulated by FAVOR as weld flaws. Section 3.6 provides additional information.	The NRC disagrees with this recommendation because it is arbitrary. A case-specific justification is needed to demonstrate why a plate flaw should be recategorized as a weld flaw.
10	(e)(4)(i)	The proposed regulatory guide should provide criteria or methods for determining whether the deviation in flaw limits will have a detrimental effect on the applicability of the PTS screening criteria in Table 1 of 10 CFR 50.61a.	Such criteria would reduce burden on both the NRC and industry while providing an acceptable level of safety and quality. Section 3.7 and Appendix E provide additional information.	The NRC agrees with this comment. Step 3(i) of this regulatory guide provides both simplified and more detailed procedures that address evaluations that may be performed when the flaw limits are exceeded. The industry may choose to justify alternatives to these procedures on a case-specific basis.
11	(e)(4)(i)	Deviations to the flaw limits for plants that have low embrittlement should be generically allowed. Low embrittlement can be defined as having RT_{MAX-X} values that are equivalent to or less than a TWCF of 1% of the PTS risk objective or approximately $1x10^{-8}$ events per year.	The vessel material at these plants would still have high enough fracture toughness that even large increases in the number of flaws above the 10 CFR 50.61a limits would not result in a plant reaching the PTS risk objective of $1x10^{-6}$ events per year. Section 3.7 provides additional information.	The NRC disagrees with this recommendation and the associated justification. If the flaw limits are failed, it would be inappropriate to use the relationships between TWCF and RT_{MAX-X} that depend on these limits being correct to address the issue. This regulatory guide provides simplified criteria for assessing brittle fracture that may be used in this situation, or another valid alternative case-specific solution may be proposed.

12	(e)(1)	The flaw limits in Tables 2 and 3 of 10 CFR 50.61a should be applied to axial flaws only.	This proposed approach addresses the real technical concern (i.e., the maximum number of axial flaws that could lead to potential vessel failure). The flaw-orientation discussion in Section 3.7.1 provides additional information.	The NRC disagrees with this comment. The comparison to Tables 2 and 3 in 10 CFR 50.61a considers all flaws, whether such flaws are axial or circumferential, because under 10 CFR 50.61a(e), “Examination and Flaw Assessment Requirements,” paragraph (e)(1)(iii), states the following: For each flaw detected in the inspection volume described in paragraph (e)(1) with a TWE equal to or greater than 0.075 inches, the licensee shall document the dimensions of the flaw, including TWE and length, whether the flaw is axial or circumferential in orientation and its location within the reactor vessel, including its azimuthal and axial positions and its depth embedded from the clad-to-base-metal interface. 10 CFR 50.61a(e)(4) states, in part, the following: The licensee shall perform analyses to demonstrate that the reactor vessel will have a TWCF of less than $1x10^{-6}$ per reactor year if the ASME Code, Section XI, volumetric examination required by paragraph (c)(2) or (d)(2) of this section indicates any of the following: (i) The flaw density and size in the inspection volume described in paragraph (e)(1) exceed the limits in Tables 2 or 3 of this section.

No.	10 CFR 50.61a Paragraph	MRP-334 Recommendation	MRP-334 Justification	NRC Response
13	(e)(1), (e)(4)	A qualitative assessment process should be provided for addressing a flaw that exceeds the maximum size allowed in the flaw limit tables but is less than 0.875 inch in TWE.	Section 3.7.1 proposes a qualitative process that considers flaw orientation, flaw location, flaw size, and material properties.	The NRC agrees with this comment. Step I of this regulatory guide addresses the recommendation.
14	(e)(1), (e)(4), (e)(5)	A quantitative assessment process should be provided (1) for instances in which multiple flaws exceed the flaw limit tables or (2) if the requirements of the qualitative process cannot be satisfied.	Section 3.7.2 provides a quantitative process that considers the contribution of individual flaws to the total vessel TWCF. If needed, Appendix F provides an additional process that reduces some of the conservatisms in the Section 3.7.2 process.	The NRC agrees with this comment. Step I of this regulatory guide addresses the recommendation.
15	(e)(1)	When assessing the flaw-limit tables, multiple flaws that are combined into one flaw in accordance with the ASME Code, Section XI, proximity rules should not be counted as multiple ISI flaws.	The ASME Code, Section XI, proximity rules were considered in the development of the flaw distributions used in the technical basis for 10 CFR 50.61a. Section 3.7.2 provides additional information.	The NRC agrees with this comment. The regulatory guide considers flaw proximity, as indicated in Figure 5-2.

4 GUIDANCE FOR CRITERIA RELATED TO THE DATE OF CONSTRUCTION AND DESIGN REQUIREMENTS

The Alternate PTS Rule applies to plants with construction permits issued before February 3, 2010, and with RPVs designed and fabricated in accordance with the 1998 edition or an earlier edition of the ASME Code. This chapter provides guidelines and supporting bases for this requirement.

4.1 Requirements in the Alternate Pressurized Thermal Shock Rule

The regulation at 10 CFR 50.61a(b), "Applicability," states that the Alternate PTS Rule applies to plants that were issued a construction permit after February 3, 2010. Section II of 75 FR 13–29 [2] states the following:

> The final rule is applicable to licensees whose construction permits were issued before February 3, 2010 and whose reactor vessels were designed and fabricated to the American Society of Mechanical Engineers Boiler and Pressure Vessel Code (ASME Code), 1998 Edition or earlier. This would include applicants for plants such as Watts Bar Unit 2 who have not yet received an operating license. However, it cannot be demonstrated, *a priori*, that reactor vessels that were not designed and fabricated to the specified ASME Code editions will have material properties, operating characteristics, PTS event sequences and thermal hydraulic responses consistent with those evaluated as part of the technical basis for this rule. Therefore, the NRC determined that it would not be prudent at this time to extend the use of the rule to future PWR plants and plant designs such as the Advanced Passive (AP) 1000, Evolutionary Power Reactor (EPR) and U.S. Advanced Pressurized Water Reactor (US APWR). These designs have different reactor vessels than those in the currently operating plants, and the fabrication of the vessels based on these designs may differ from the vessels evaluated in the analyses that form the bases for the final rule. Licensees of reactors who commence commercial power operation after the effective date of this rule or licensees with reactor vessels that were not designed and fabricated to the 1998 Edition or earlier of the ASME Code may, under the provisions of § 50.12, seek an exemption from § 50.61a(b) to apply this rule if a plant specific basis analyzing their plant operating characteristics, materials of fabrication, and welding methods is provided.

Section 4.2 discusses the regulatory guidance for the above requirements.

4.2 Regulatory Guidance

The NRC applied the restriction in Section 4.1 on the applicability of the Alternate PTS Rule embrittlement screening criteria because the structural and thermal-hydraulic analyses that established the basis for the Alternate PTS Rule represented only plants constructed before February 3, 2010. A licensee that applies the Alternate PTS Rule to a plant with a construction permit issued after February 3, 2010, must demonstrate that the technical bases calculations in NUREG 1806, "Technical Basis for Revision of the Pressurized Thermal Shock (PTS) Screening Limit in the PTS Rule," issued August 2007 [6], and its supporting technical reference adequately address the risk significant factors that control PTS for the plant in question. The factors that this evaluation should consider include, but might not be limited to, the following:

- the event sequences that may lead to overcooling of the RPV

- the thermal hydraulic response of the nuclear steam supply system in response to such sequences

- characteristics of the RPV design (e.g., vessel diameter, vessel wall thickness, and operating pressure) that influence the stresses that develop in the beltline region of the vessel (as defined in Section 1.2) in response to the event sequences

- characteristics of the RPV materials and their embrittlement behavior

5 GUIDANCE FOR CRITERIA RELATED TO THE EVALUATION OF PLANT SPECIFIC SURVEILLANCE DATA

The NRC staff developed and published the information in this chapter to support the development of the Alternate PTS Rule. Chapter 5 repeats relevant information from this work for completeness and clarity [14] and, in some cases, further clarifies the information in Reference [14] compared to the technical bases supporting the Alternate PTS Rule. Additionally, the information presented in this chapter adds to the information in Reference [14] in two respects: (1) Section 5.2 describes procedures for grouping data (e.g., treatment of "sister plant" data) before performing the statistical tests, and (2) Section 5.6.2 describes procedures that can be used if the statistical tests are failed.

This chapter describes procedures that licensees can use to analyze the plant-specific surveillance data collected through surveillance programs (in accordance with 10 CFR Part 50, Appendix H) to assess how well the ETC represents these data . If the surveillance data are "close" (closeness is assessed statistically) to the prediction of the ETC, the predictions of the ETC are used. Statistically significant differences between plant-specific datasets and the ETC prediction identify situations that warrant more focused attention and are an indication that methods other than, or in addition to, the ETC may be needed to predict ΔT_{30} trends. Although standard statistical procedures exist to assess the significance of differences between individual datasets and ETC predictions, similarly standard procedures are not as commonly available to assess the practical importance of such differences or to adjust the data to account for these differences. This chapter concludes by discussing (1) factors that licensees may consider if the statistical tests are failed and (2) procedures that licensees could use to adjust the predictions of the ETC in certain circumstances.

The remainder of this chapter is divided into six sections:

- Section 5.1 describes the ΔT_{30} ETC. Oak Ridge National Laboratory (ORNL) TM-2006/530, "A Physically Based Correlation of Irradiation-Induced Transition Temperature Shifts for RPV Steels," issued November 2007, describes the development of this ETC [9].

- Section 5.2 describes entry conditions that licensees must meet to use the proposed surveillance assessment procedure.

- Section 5.3 describes different types of deviations between plant-specific surveillance data and the trends represented by the ΔT_{30} ETC from Reference [9].

- Section 5.4 describes procedures that statistically assess the deviations described in Section 5.3.

- Section 5.5 applies the procedures of Section 5.4 to the surveillance database that supported the development of the ETC [9].

- Section 5.6 discusses factors that licensees should consider if the statistical tests of Section 5.4 are failed. In addition, it describes procedures that licensees could use to adjust the predictions of the ETC in certain circumstances.

5.1 Embrittlement Trend Curve

As detailed in ORNL/TM-2006/530 [9], the numerical coefficients in the following equations were determined by fitting them to the ΔT_{30} data collected through the 10 CFR Part 50, Appendix H, surveillance programs that licensees have submitted to the NRC through approximately 2002. This ΔT_{30} ETC, which is used in the Alternate PTS Rule, has the following form:

$$\Delta T_{30} = MD + CRP \quad (5\text{-}1)$$

$$MD = \mathrm{A} \cdot (1 - 0.001718\, T_c)(1 + 6.13\, \mathrm{P}\, \mathrm{Mn}^{2.471})\varphi t_e^{\,0.5} \quad (5\text{-}2)$$

$$A = \begin{cases} 1.14\text{x}10^{-7} \text{ for forgings} \\ 1.561\text{x}10^{-7} \text{ for plates} \\ 1.417\text{x}10^{-7} \text{ for welds} \end{cases} \quad (5\text{-}3)$$

$$CRP = \mathrm{B} \cdot \left[1 + 3.77\, \mathrm{Ni}^{1.191}\right] \mathrm{f}(\mathrm{Cu_e}, \mathrm{P}) \cdot \mathrm{g}\left(\mathrm{Cu_e}, \mathrm{Ni}, \varphi t_e\right) \quad (5\text{-}4)$$

$$B = \begin{cases} 102.3 \text{ for forgings} \\ 102.5 \text{ for plates in non-Combustion Engineering vessels} \\ 135.2 \text{ for plates in Combustion Engineering vessels} \\ 155.0 \text{ for welds} \end{cases} \quad (5\text{-}5)$$

$$\mathrm{Cu_e} = \begin{cases} 0 \text{ if Cu} \leq 0.072 \\ min\left[\mathrm{Cu}, \mathrm{MAX}(\mathrm{Cu_e})\right] \text{ if Cu} > 0.072 \end{cases} \quad (5\text{-}6)$$

$$\mathrm{MAX}(\mathrm{Cu_e}) = \begin{cases} 0.243 \text{ for Linde 80 welds} \\ 0.301 \text{ for all other materials} \end{cases} \quad (5\text{-}7)$$

$$f(Cu_e, P) = \begin{cases} 0 \text{ for } Cu \leq 0.072 \\ (Cu_e - 0.072)^{0.668} \text{ for } Cu > 0.072 \text{ and } P \leq 0.008 \\ [(Cu_e - 0.072) + 1.359(P - 0.008)\,]^{0.668} \text{ for } Cu > 0.072 \text{ and } P > 0.008 \end{cases} \quad (5\text{-}8)$$

$$g(Cu_e, Ni, \varphi t_e) = 0.5 + 0.5 \times tanh\left\{\frac{log_{10}(\varphi t_e) + 1.1390 \times Cu_e - 0.448 \times Ni - 18.120}{0.629}\right\} \quad (5\text{-}9)$$

$$f(Cu_e, P) = \begin{cases} 0 \text{ for } Cu \leq 0.072 \\ (Cu_e - 0.072)^{0.668} \text{ for } Cu > 0.072 \text{ and } P \leq 0.008 \\ [(Cu_e - 0.072) + 1.359(P - 0.008)\,]^{0.668} \text{ for } Cu > 0.072 \text{ and } P > 0.008 \end{cases} \quad (5\text{-}10)$$

Equation (1) estimates the dependent variable, ΔT_{30}, in degrees Fahrenheit (F). Table 5-1 lists the standard deviation of residuals about Equation (1) for different product forms and Cu contents. Table 5-2 provides the units and descriptions of independent variables in these equations. As with any equation calibrated to empirical data, inaccuracies have a greater tendency to occur at the extremes of, or beyond the limits of, the calibration dataset. Users of Equation (1) should therefore exercise caution when applying it to conditions near or beyond the extremes of its calibration dataset, which appears in Table 5-2. For example, for materials that have Cu contents below 0.072 weight percent (wt%), Equation (1) predicts negative ΔT_{30} values when the irradiation temperature exceeds 582.1 degrees F. Clearly, negative shift values are incorrect.

Table 5-1 Standard Deviation of Residuals about Equation (1)

Product Form	Standard Deviation, σ (°F)	
	Cu ≤ 0.072 wt%	Cu > 0.072 wt%
Weld	18.6	26.4
Plate		21.2
Forging		19.6

Table 5-2 Independent Variables in the Equation (1) ETC and the Ranges and Mean Values of the Calibration Dataset

Variable	Symbol	Units	Values of Surveillance Database			
			Average	Standard Deviation	Minimum	Maximum
Neutron Fluence (E > 1 MeV)	ϕt	n/cm^2	$1.24\text{x}10^{+19}$	$1.19\text{x}10^{+19}$	$9.26\text{x}10^{+15}$	$1.07\text{x}10^{+20}$
Neutron Flux (E > 1 MeV)	ϕ	n/cm^2/s	$8.69\text{x}10^{+10}$	$9.96\text{x}10^{+10}$	$2.62\text{x}10^{+08}$	$1.63\text{x}10^{+12}$
Irradiation Temperature	T_c	°F	545	11	522	570
Copper Content	Cu	wt%	0.140	0.084	0.010	0.410
Nickel Content	Ni	wt%	0.56	0.23	0.04	1.26
Manganese Content	Mn	wt%	1.31	0.26	0.58	1.96
Phosphorus Content	P	wt%	0.012	0.004	0.003	0.031

5.2 Data Used in Statistical Tests

Licensees should apply the following requirements for the use of surveillance data to perform the statistical tests outlined in this chapter:

(1) Materials Evaluated (i.e., the Meaning of "Plant Specific")

- When performing the statistical tests required by the Alternate PTS Rule, the licensee should evaluate each shell and weld material in the RPV beltline region for which 10 CFR Part 50, Appendix H, surveillance data exist. The statistical tests should be performed separately for each heat.

- For each heat that has available data, the ΔT_{30} values used in the statistical tests should include data from the following sources:

  - data obtained for the heat of material in question as part of a 10 CFR Part 50, Appendix H, surveillance program conducted for the plant in question

  - data obtained for the heat of material in question as part of a 10 CFR Part 50, Appendix H, surveillance program conducted for any other plant that is operating, or has operated, under a license issued by the NRC

    Data from this source is often referred to as having come from a "sister plant." Such data may have different best-estimate chemistry values and different irradiation temperatures (e.g., the Cu and T_c values for heat "123" at plant "XYZ" may be 0.23 and 553 degrees F, respectively, whereas the Cu and T_c values for heat "123" at plant "ABC" may be 0.21 and 544 degrees F, respectively). The statistical tests described in Sections 5.3 and 5.4 operate on the residuals (i.e., the difference between the surveillance measurement of ΔT_{30} and the prediction of the ETC). In so doing, the ETC takes account of these plant-specific variations in chemistry and/or temperature, so there is no need to make further adjustments to account for so-called "sister plant" data (see Reference [10]).

(2) Data Quantity Requirements

To perform these statistical tests, at least three plant-specific ΔT_{30} values, each measured at a unique fluence value, should be available. If this condition is not met, the licensee should use the ETC described in the Alternate PTS Rule to estimate ΔT_{30}.

(3) Data Binning Requirements

- As discussed in item 1, these statistical evaluations should bin together and consider data obtained for the heat of material in question as part of a 10 CFR Part 50, Appendix H, surveillance program conducted for any plant that is operating, or has operated, under a license issued by the NRC.

- For plates and forgings, Charpy data are often obtained for different orientations of the notch relative to the primary working direction of the plate or forging. For these statistical tests, ΔT_{30} values for a particular plate or forging should be computed from unirradiated specimens that have the same notch orientation. Once ΔT_{30} values are calculated, different notch orientation data from the same heat of material should be binned together for the statistical tests described in Sections 5.3 and 5.4. This is appropriate because the differences in unirradiated transition temperature caused by notch orientation will be subtracted out when ΔT_{30} values are calculated.

(4) Data Characterization Requirements

For all materials meeting the requirements of the three preceding items, the following information is needed:

- heat identification
- plant identification
- capsule identification
- product form
- notch orientation
- the unirradiated reference temperature, $RT_{NDT(U)}$
- ΔT_{30}
- Charpy V-notch (CVN) energy data used to estimate ΔT_{30}
- fluence
- flux
- operating time
- cold-leg temperature under normal full-power operating conditions (T_c) (i.e., T_c (degrees F) is determined as the time-weighted average coolant temperature of the reactor coolant system cold leg that covers the time period when the capsule was in the reactor)
- Cu content
- Ni content
- P content
- Mn content
- citation (i.e., the reference, or references, for all of the information listed above)

The values of Cu, Ni, P, and Mn are the best-estimate values for the material. For a plate or forging, the best-estimate value is normally the mean of the measured values for that plate or forging. For a weld, the best-estimate value is normally the mean of the measured values for a weld deposit that are obtained using the same weld wire heat number as the critical vessel weld. If these values are not available, the licensee should use either the upper limiting values given in the material specifications to which the vessel material was fabricated or conservative estimates (i.e., mean plus one standard deviation) based on generic data. Table 4 of 10 CFR 50.61a provides the upper-bound estimates for P and Mn. Similarly, 10 CFR 50.61 provides the upper-bound estimates for Cu and Ni.

5.3 Statistical Evaluation of Surveillance Data

In developing this surveillance assessment procedure, consideration was given to the development of statistical tests capable of detecting the four types of deviations between heat-specific surveillance data and the ΔT_{30} ETC expressed by Equations (1) through (10). Figure 5-1 illustrates these deviations and identifies them as Type A, B, C, and D. The list below describes the potential origins and implications of these types of statistical deviations. Figure 5-1 illustrates only situations in which the data suggest that the ΔT_{30} ETC may provide a nonconservative prediction (i.e., situations in which the data exceed the ETC prediction). The opposite situation is also possible (i.e., situations in which the ETC underestimates the data). However, only nonconservative predictions are important from a regulatory viewpoint.

- Type A Deviations. For Type A deviations, measurements differ from the mean ETC prediction more or less uniformly at all fluence levels. Additionally, the magnitude of this deviation is larger than would be expected based on the population of data used to calibrate the ETC. Potential origins of Type A deviations may include, but are not limited to, errors in the chemical composition values or errors in the unirradiated ΔT_{30} value associated with the surveillance sample. A statistically significant Type A deviation (Section 5.4.1 describes procedures for evaluating statistical significance) implies that the ETC may systematically underestimate the value of ΔT_{30} for the heat of steel being evaluated.

- Type B Deviations. For Type B deviations, measurements differ from the mean ETC prediction by an amount that increases as fluence increases. Additionally, the magnitude of this deviation is larger than would be expected based on the population of data used to calibrate the ETC. Potential origins of Type B deviations may include, but are not limited to, (1) errors in the temperature value associated with the surveillance sample or (2) the existence of an embrittlement mechanism that is not represented in the ETC calibration dataset. A statistically significant Type B deviation (Section 5.4.2 describes procedures for evaluating statistical significance) implies that the ETC may systematically underestimate the value of ΔT_{30} for the heat of steel being evaluated and that the magnitude of this underestimation will increase as the plant operation continues.

- Type C Deviations. For Type C deviations, measurements differ from the mean ETC by exhibiting more scatter than would be expected based on the population of data used to calibrate the ETC. Potential origins of Type C deviations may include, but are not limited to, errors made in testing, labeling, or controlling the notch orientation of surveillance specimens. Statistically significant Type C deviations do not imply that the ETC may systematically underpredict the true embrittlement; instead, such deviations imply that the ability of the surveillance data to provide insight into embrittlement trends is called into question for a specific heat of material.

- Type D Deviations. For Type D deviations, one or more of the ΔT_{30} measurements differ significantly from the mean ETC prediction even though all other measurements for the heat of steel being evaluated agree well with that prediction. The magnitude of the deviation of these outliers is larger than would be expected based on the population of data used to calibrate the ETC. Potential origins of Type D deviations may include, but are not limited to, (1) a large measurement error in the single datum or (2) the rapid emergence of an embrittlement mechanism in the surveillance sample that is not represented in the calibration dataset (e.g., rapid emergence of a Type B deviation). A statistically significant Type D deviation (Section 5.4.3 describes procedures for evaluating statistical significance) implies that the ETC may systematically underestimate the value of ΔT_{30} for the heat of steel being evaluated.

If they are statistically significant, Type A, B, and D deviations all give rise to concerns that the embrittlement trends predicted by the ETC may produce nonconservative estimates of the embrittlement experienced by materials that are used to construct the RPV under evaluation. For this reason, Sections 5.4.1 through 5.4.3 describe the methods used to assess the statistical significance of these deviations. Type C deviations, if they are statistically significant, suggest that the surveillance program for the material in question may not reliably indicate embrittlement trends for that material. Because 10 CFR Part 50, Appendix H, requires the performance of surveillance on the “limiting” (meaning “most irradiation-sensitive”) materials used to construct the RPV beltline, the existence of a Type C deviation is important from a regulatory viewpoint but not in the context of indicating a potential nonconservatism in the predictions of the ΔT_{30} ETC adopted in the Alternate PTS Rule. For this reason, the Alternate PTS Rule does not include statistical procedures to detect Type C deviations (see Reference [1]); therefore, Section 5.4 does not describe such procedures.

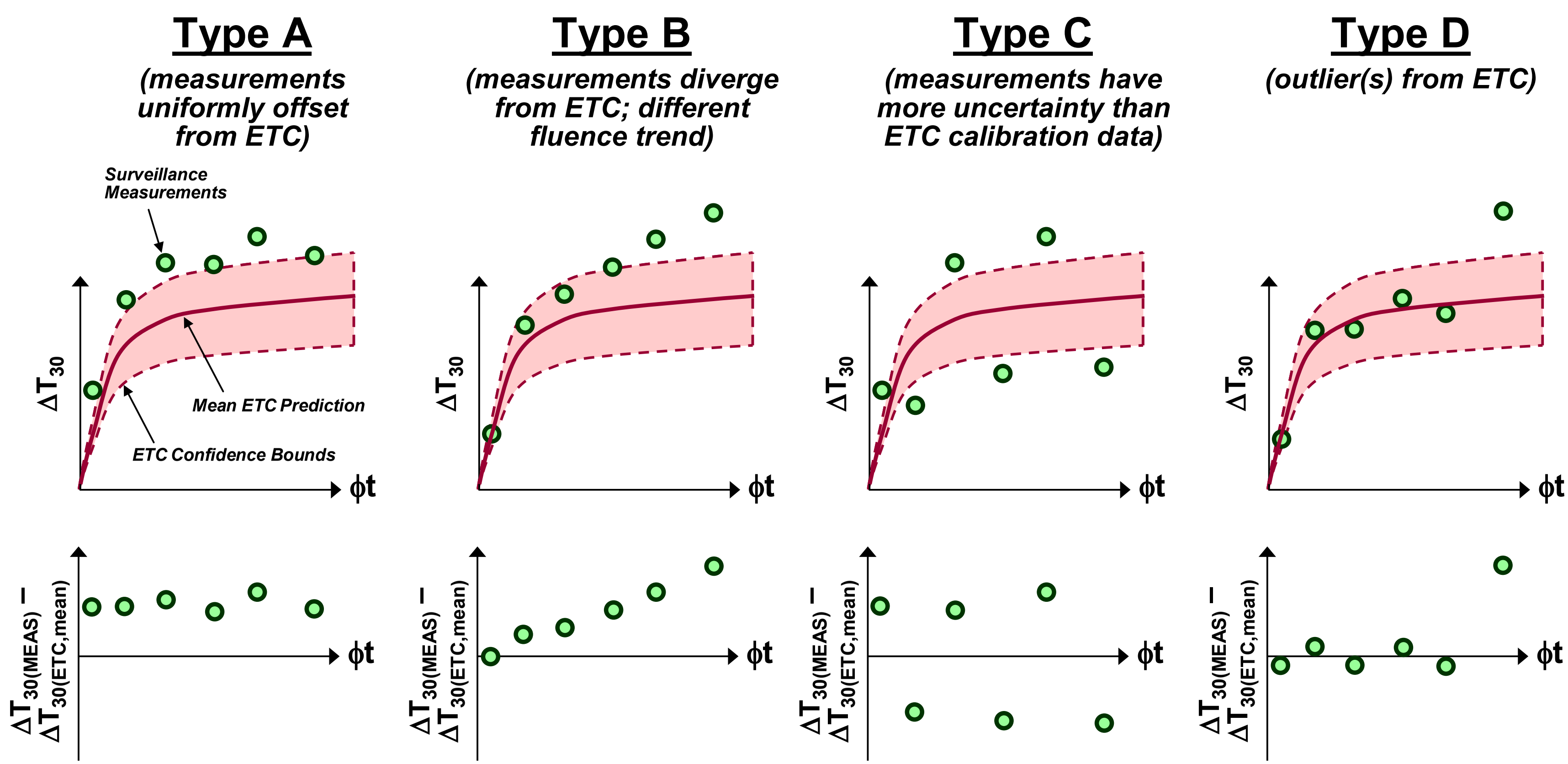

Figure 5-1 Four types of deviations between heat specific surveillance data and a ΔT_{30} ETC

5.4 How to Perform Statistical Tests of Surveillance Data

This section describes how to perform the Type A (mean test), Type B (slope test), and Type D (outlier test) assessments of surveillance data are required by the Alternate PTS Rule.

5.4.1 Type A Deviations

As illustrated by Figure 5-1, Type A deviations are characterized by measurements that differ from the mean ETC prediction more or less uniformly at all fluence levels. The following procedure can be used to detect Type A deviations when the ΔT_{30} measurements for a specific heat of material are uniformly underpredicted by Equation (1). A statistical significance level of α = 1% (i.e., 2.33 standard deviations) is recommended for this one-sided test. Section 5.4.4 discusses the rationale for this selection.

A-1. Ensure that the entry conditions of Section 5.2 have been met.

A-2. Estimate the residual (r) for each datum using the following formula:

$$r = \Delta T_{30(Measured)} - \Delta T_{30(Predicted)}, \quad (5\text{-}11)$$

where $\Delta T_{30(measured)}$ represents each individual measurement, and $\Delta T_{30(predicted)}$ is the value of ΔT_{30} predicted by Equation (1) using the best-estimate composition for the surveillance material and the best-estimate exposure values for the plant from which the companion $\Delta T_{30(measured)}$ value was obtained.

A-3. Estimate the mean residual (r_{mean}) for the ΔT_{30} dataset using the following formula:

$$r_{mean} = \frac{1}{n}\sum_{i=1}^{n}\{r_i\}, \quad (5\text{-}12)$$

where n is the number of ΔT_{30} measurements for the specific heat of material under assessment.

A-4. Estimate the maximum allowable residual (r_{max}) using the following formula:

$$r_{max} = \frac{2.33\sigma}{\sqrt{n}}, \quad (5\text{-}13)$$

where n is the number of ΔT_{30} measurements for the specific heat of material under assessment and σ is the population standard deviation taken from Table 5-1.

A-5. If r_{mean} exceeds r_{max}, the subject dataset shows a Type A deviation.

5.4.2 Type B Deviations

As illustrated by Figure 5-1, Type B deviations are characterized by measurements that differ from the ETC prediction by an amount that increases as fluence increases. The following procedure is used to detect Type B deviations. Similar to the test for Type A deviations, a statistical significance level of α = 1% is recommended for this one-sided test. Section 5.4.4 discusses the rationale for this selection.

B-1. Ensure that the entry conditions of Section 5.2 have been met.

B-2. For each measured ΔT_{30} value, calculate the difference between the measured and predicted value of ΔT_{30} using Equation (11). As illustrated in Figure 5-2, plot r versus the $\log_{10}$ value of fluence. The abscissa is expressed in this manner because embrittlement, as quantified by ΔT_{30}, increases approximately linearly with the logarithm of fluence.

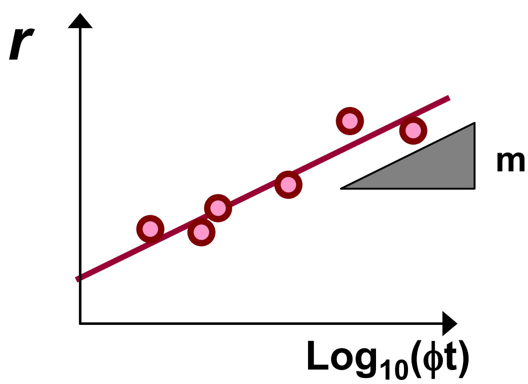

Figure 5-2 Procedure used to assess Type B deviations

B-3. Using the method of least squares, estimate the slope (m) of the data plotted as shown in Figure 5-2. In addition, estimate the standard error of the estimated value of the slope, se(m).

B-4. Estimate the T-statistic for the slope as follows:

$$T_{SURV} = \frac{m}{se(m)} \quad (5\text{-}14)$$

B-5. Establish the critical T-value as follows:

$$T_{CRIT(\alpha)} = t(\alpha, n-2), \quad (5\text{-}15)$$

where t(…) represents Student's t-distribution, α is the selected significance level, and n is the number of $\Delta T_{30(Measured)}$ values. Adoption of α = 1% is recommended for regulatory implementation of this procedure. Section 5.4.4 discusses the rationale for this selection. Table 5-3 provides values of $T_{CRIT(1\%)}$.

Table 5-3 α = 1% Student's t-Values

Number of ΔT_{30} Values, n	n-2	One-Tailed T_{CRIT} (1%, n-2)
3	1	31.82
4	2	6.96
5	3	4.54
6	4	3.75
7	5	3.36
8	6	3.14
9	7	3.00
10	8	2.90
11	9	2.82
12	10	2.76
13	11	2.72
14	12	2.68
15	13	2.65

B-6. If T_m exceeds $T_{CRIT(\alpha)}$, the subject dataset shows a Type B deviation.

5.4.3 Type D Deviations

As illustrated by Figure 5-1, Type D deviations are characterized by one or more of the ΔT_{30} measurements differing significantly from the mean ETC prediction even though all other measurements for the heat of steel under evaluation agree well with the ETC. Similar to the tests for both Type A and Type B deviations, a statistical significance level of α = 1% is recommended for this one-sided test. Section 5.4.4 discusses the rationale for this selection.

D-1. Ensure that the entry conditions of Section 5.2 have been met.

D-2. Estimate the normalized residual, *r**, for each or the n observations in the ΔT_{30} dataset using the following formula:

$$r^* = \frac{r}{\sigma} \qquad (5\text{-}16)$$

where r is defined from Equation (11) and σ is the population standard deviation taken from Table 5-1.

D-3. Find the largest and second largest r* values from Step D-2; designate these as r^*_1 and r^*_2, respectively.

D-4. Find the limit values $r_{LIMIT(1)}$ and $r_{LIMIT(2)}$ corresponding to n in Table 5-4. These threshold values correspond to a significance level of α = 1%. Appendix A to this document describes how the values of C_1 and C_2 in Table 5-4 were derived.

D-5. If $r^*_1 \le r_{LIMIT(1)}$ and $r^*_2 \le r_{LIMIT(2)}$, the dataset is judged to not show a Type D deviation. Otherwise the surveillance dataset is judged to show a Type D deviation.

Table 5-4 α = 1% Threshold Value for the Outlier Test

n	$r_{LIMIT(2)}$	$r_{LIMIT(1)}$
3	1.55	2.71
4	1.73	2.81
5	1.84	2.88
6	1.93	2.93
7	2.00	2.98
8	2.05	3.02
9	2.11	3.06
10	2.16	3.09
11	2.19	3.12
12	2.23	3.14
13	2.26	3.17
14	2.29	3.19
15	2.32	3.21
17	2.37	3.24
26	2.53	3.36
64	2.83	3.62

Note that Appendix A refers to $r_{LIMIT(1)}$ as C_2 and $r_{LIMIT(2)}$ as C_1. The notation is changed here to improve clarity.

5.4.4 Comments on the Statistical Tests

The significance level recommended for regulatory implementation of the Type A, B, and D tests is α = 1%. At this significance level, there is less than a 1-percent chance that the underlying cause of the detected difference (Type A, B, or D) between the plant-specific surveillance data and the value of ΔT_{30} predicted by Equation (1) has occurred as a result of chance alone. The following considerations informed this recommendation:

- A 1-percent significance level makes it more difficult for plant-specific surveillance data to be declared "different" from the predictions of the ETC than has traditionally been the case. For example, both 10 CFR 50.61 [3] and Regulatory Guide 1.99, "Radiation Embrittlement of Reactor Vessel Materials," Revision 2, issued May 1988 [15], use a "2σ" criterion which, for a one-sided test, implies an α = 2.5% significance level. The staff views this change in significance level from 2.5 percent to 1 percent as appropriate in view of the greater physical and empirical support of Equation (1) than that available when the NRC adopted both 10 CFR 50.61 and Regulatory Guide 1.99, Revision 2.

- The selection of the α = 1% significance level represents a conscious tradeoff between the competing goals of providing high confidence in the determination of a statistically significant difference between plant-specific surveillance data and the predictions of Equation (1) versus limiting the risk of judging that a particular set of plant-specific surveillance data are similar to the ΔT_{30} ETC when, in fact, they are not. The former goal is achieved by adopting a small value for α, whereas the latter goal is achieved by increasing the α value.

- If a plant-specific dataset is determined by these statistical tests to be "different" from the predictions of Equation (1), the alternatives that are available to licensees to either troubleshoot the cause of the difference or develop new/replacement data are limited, expensive, or have long lead times. Consequently, although the NRC recognizes the importance of comparing plant-specific data to generic trends and taking action when such comparisons show differences, the agency believes that reserving such actions to cases in which the differences are the clearest and are the most practically significant is justified.

Considering all of these factors, the Alternate PTS Rule adopted a significance level for Type A, B, and D deviations of α = 1%.

5.5 Evaluation of Plant Data Relative to the Statistical Tests

This section presents information that appeared previously in Reference [14]. It is repeated here for clarity and completeness.

The plant surveillance data used in ORNL/TM-2006/530 [9] to calibrate Equation (1) were evaluated according to the statistical tests detailed in Section 5.4. After filtering the data to remove heats having less than three ΔT_{30} observations at three different fluence values, 159 datasets remained for evaluation. These sets included data from both PWRs and BWRs and from plants that are no longer in operation. Although the BWR and ex-plant data are not directly pertinent to the Alternate PTS Rule, this analysis retained them for information. Appendix B contains the detailed results of these analyses.

Table 5-5 summarizes the 14 heats of material from 12 plants that show a statistically significant deviation of Type A, B, or D, whereas Table 5-6 summarizes the proportion of heats in the surveillance database that exhibit statistically significant deviations at the α = 1% level. The information in Table 5-6 demonstrates that both the mean and the outlier tests exhibit a rate of deviation above the expected value for a population of 159 datasets (i.e., 1 percent of 159, or 1.59), whereas the deviation rate of the slope test is close to this expected value. These observations suggest that, for the mean and outlier tests, the assumption that the residuals are distributed normally about the ETC (Equation (1)) may be incorrect. One possible explanation for this situation could be the presence of systematic biases in some of the unirradiated T_{30} values (e.g., arising from measurement error or imprecision). Such biases, if present, would have no effect on the detection rate of the slope test because it operates on the differences between ΔT_{30} residuals, not on their absolute values. Therefore, any systematic biases in the unirradiated ΔT_{30} values would be subtracted from the ΔT_{30} difference values that are used to perform the slope test and, consequently, could not affect the outcome of the test. Conversely, the mean and outlier tests both operate on the absolute values of ΔT_{30} residuals. Consequently, systematic biases in the unirradiated values of ΔT_{30} could affect the normalcy of the ΔT_{30} residuals and, thereby, the detection rate of the mean and outlier tests.

Table 5-5 Heats of Material That Exhibit Statistically Significant Deviations (α = 1%) of Type A, B, or D

Plant Name	Heat ID	Product Form	Population σ (°F)	Number of ΔT_{30} Values	Test Results		
					A - Mean Test	B - Slope Test	D - Outlier Test
Operating PWRs							
San Onofre Unit 3	PSO301	Plate	18.6	3	FAIL	PASS	FAIL
D.C. Cook, Unit 2	PCK201	Plate	21.2	8	FAIL	PASS	PASS
Beaver Valley, Unit 1	PBV101	Plate	21.2	8	FAIL	PASS	FAIL
Callaway	WCL101	Weld	18.6	4	FAIL	PASS	FAIL
Surry, Unit 1	WSU101	Weld	26.4	3	FAIL	PASS	FAIL
Indian Point, Unit 2	PIP203	Plate	21.2	3	FAIL	PASS	PASS
Sequoyah, Unit 1	FSQ101	Forging	19.6	8	FAIL	PASS	PASS
Sequoyah, Unit 1	WSQ101	Weld	26.4	4	FAIL	PASS	PASS
Sequoyah, Unit 2	WSQ201	Weld	26.4	4	PASS	PASS	FAIL
Operating BWRs							
River Bend, Unit 1 and Oyster Creek	WRB01	Weld	18.6	3	FAIL	PASS	FAIL
Decommissioned PWRs							
Maine Yankee	PMY01	Plate	21.2	6	FAIL	PASS	PASS
Zion, Unit 1	WZN101	Weld	18.6	5	PASS	FAIL	PASS
Decommissioned BWRs							
Big Rock Point	PBR01	Plate	21.2	5	FAIL	FAIL	FAIL

Table 5-6 Proportion of Material Heats in the Current Surveillance Database That Exhibit Statistically Significant Deviations (α = 1%) of Type A, B, or D

Test Type		Datasets that Show Statistically Significant (α = 1%) Deviation	
		Count	Percent
A	Mean Test	11	6.9%
B	Slope Test	2	1.3%
D	Outlier Test	7	4.4%

5.6 Considerations When Statistical Tests Are Failed

Failure of plant-specific surveillance data to pass any of these statistical tests indicates a situation in which Equation (1) may underestimate the embrittlement magnitude. Using Equation (1) in such situations without additional justification is not advisable. Such failures warrant a more focused assessment of the surveillance data and indicate that methods other than, or in addition to, the ETC may be necessary to reliably predict ΔT_{30} trends. However, the most appropriate approach may not be a heat-specific adjustment of the ETC predictions in all cases. For example, statistically significant differences may indicate situations in which the available data (i.e., the ΔT_{30} measurements or the composition and exposure values associated with the ΔT_{30} measurements, or both) are incorrect; therefore, adjusting the ETC predictions to match these data would be unwise.

This section divides the discussion into two parts. First, it lists the factors that could help in diagnosing the reason why the surveillance data failed the statistical tests. Second, it discusses situations in which adjustments of the ETC predictions may be made using simple procedures.

5.6.1 Factors To Consider When Statistical Tests Are Failed

Before the licensee considers adjusting the ETC predictions to match surveillance data, the NRC suggests that the licensee conduct a detailed assessment of the accuracy and appropriateness of the ΔT_{30} data. Such an assessment should consider, but not be limited to, the following factors:

- Unirradiated RT_{NDT} Value. As noted in Section 5.5, the occurrence of mean and outlier failures in the available surveillance data exceeds the statistically expected value. Both of these tests are sensitive to the accuracy of the unirradiated RT_{NDT} value. In these cases, a records investigation of the unirradiated RT_{NDT} value or the performance of additional testing of archival material, or both, may provide a more accurate estimate of RT_{NDT}, which may explain the reason for failure of the mean test or outlier test, or both.

- Irradiated ΔT_{30} Values. Although most CVN energy versus temperature curves from which ΔT_{30} values are estimated are based on 8 to 12 individual measurements, some datasets are more limited and, therefore, can increase uncertainty in the ΔT_{30} estimate. If any of the statistical tests are not satisfied, a review of the individual CVN energy versus temperature curves may help to reveal the cause of the failure.

- Composition and Exposure Variables. The input variables to Equation (1) are subject to variability and are often based on limited data. However, the predictions of Equation (1) depend on these input variables, particularly Cu content, fluence, temperature, and Ni content. If a sensitivity analysis reveals that small variations of the values input to Equation (1) rationalize the failure of the statistical tests, this might indicate that more refined information concerning input values (e.g., additional measurements) could explain the reason for the failure of the statistical tests.

- Notch Orientation. The ΔT_{30} value for plate and forging materials is sensitive to the orientation of the notch in the CVN specimen relative to the primary working direction of the plate or forging. Differences in notch orientation between the unirradiated ΔT_{30} value and the ΔT_{30} value of all the irradiated specimens could explain why the mean test is not satisfied. Similarly, differences in notch orientation between the unirradiated ΔT_{30} value and the ΔT_{30} value of the irradiated specimens in a single capsule could explain why the outlier test is not satisfied. In these situations, the outcome of a records search or metallurgical investigation of the tested specimens might be useful to explain the reason for the failure of the statistical tests.

- Comparative Trends Analysis. In addition to CVN specimens, surveillance capsules also contain tensile specimens that are part of the capsule testing program. Like ΔT_{30}, the increase in yield strength with irradiation (ΔYS) also follows certain trends. If the ΔYS data for a particular material that failed the statistical tests follow the trends exhibited by ΔYS data for a similar composition, this information might indicate that the CVN specimens were taken from the wrong material or have been somehow mislabeled.

5.6.2 Specific Procedures

If a statistical test is failed, licensees may use any of the following three procedures:

(1) Mean Test (Type A) Failure. Figure 5-3 (left side) illustrates the following procedure used to adjust ETC predictions to account for a failure of the mean test:

- Calculate the value ADJ as follows:

$$ADJ = r_{mean} - r_{max} \quad (5\text{-}17)$$

- Adjust the prediction of Equation (1) as follows:

$$\Delta T_{30(ADJ)} = MD + CRP + ADJ \quad (5\text{-}18)$$

- Use the value $\Delta T_{30(ADJ)}$ in place of ΔT_{30} in all calculations required by the Alternate PTS Rule for the material that failed the mean test.

(2) Slope Test (Type B) Failure. One procedure for adjusting ETC predictions to account for a failure of the slope test is to adjust the ETC predictions, Equation (1), based on the greater increase of embrittlement with fluence suggested by the plant-specific data. The licensee should technically justify and document the specific procedure used.

(3) Outlier Test (Type D) Failure (Not Satisfied at Low Fluence). Figure 5-3 (right side) illustrates a situation in which a ΔT_{30} value measured at low fluence is the cause of failing the outlier test. Such a failure is not considered structurally relevant to a PTS evaluation and, therefore, may be ignored as long as both of the following conditions are satisfied:

- The fluence of the datum that caused the outlier test failure, ϕt_{LOW}, is less than 10 percent of the fluence at which the PTS evaluation is being performed, ϕt_{EVAL}

- After elimination of the datum measured at ϕt_{LOW}, the entry conditions for the surveillance tests are still met (i.e., at least three data points measured at three different fluence levels remain), and all three statistical tests are satisfied with the reduced dataset.

Other approaches to assessment of surveillance data in which all surveillance measurements are bounded are subject to review and approval by the NRC.

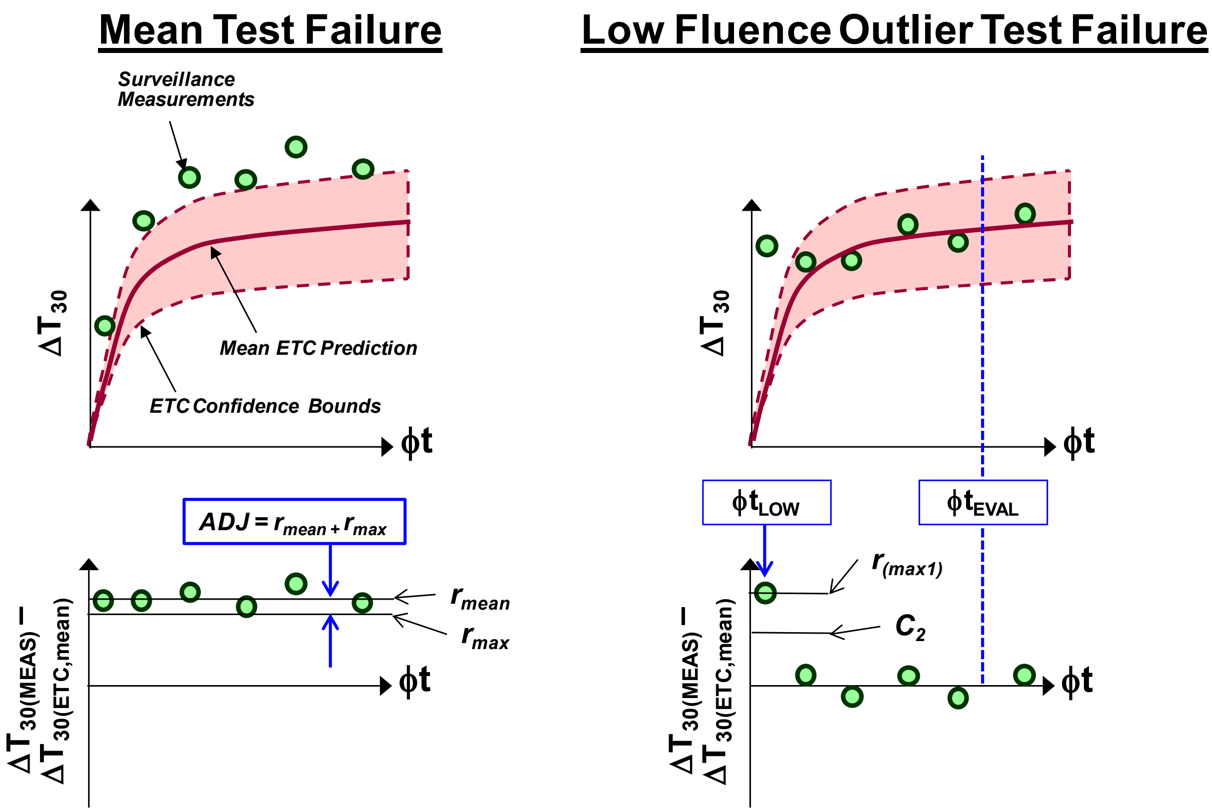

Figure 5-3 Specific procedures to account for failure of the mean test (left) or low-fluence outlier statistical test (right)

5.7 Summary and Conclusions

This chapter discussed the three statistical tests required by the Alternate PTS Rule and methods by which data can be evaluated relative to these tests. The aim of these tests is to determine whether the surveillance data are sufficiently "close" to the predictions of the ETC to allow use of the ETC predictions. From a regulatory perspective, it is of particular interest to determine whether plant-specific surveillance data deviate significantly from the predictions of the ETC in a manner that suggests that the ETC is likely to underpredict plant-specific trends. To this end, a statistical significance level of α = 1% was adopted, which represents a conscious tradeoff between the competing goals of providing high confidence in the determination of a statistically significant difference between plant-specific surveillance data and the ΔT_{30} ETC versus limiting the risk of judging that a particular set of plant-specific surveillance data are similar to the ETC when, in fact, they are not. The α = 1% tests will show fewer statistically significant deviations than did 10 CFR 50.61 or Regulatory Guide 1.99, Revision 2, both of which use a "2σ" criterion that, for a one-sided test, implies a significance level of α = 2.5%. The staff views this change in significance level (from 2.5 percent to 1 percent) as appropriate in view of the greater empirical support for the ETC used in the Alternate PTS Rule than that available when the NRC adopted 10 CFR 50.61 or Regulatory Guide 1.99, Revision 2.

The Alternate PTS Rule adopted three statistical tests because, collectively, they indicate when an underprediction of embrittlement magnitude by the ETC may have occurred. Appendix B applies these statistical tests to the operating plant surveillance database assembled through (approximately) 2002. Of the heats of material considered, only 14 heats from 12 plants failed one or more of the three statistical tests. Failure of plant-specific surveillance data to pass any of the statistical tests indicates a situation in which the ETC may underestimate the embrittlement magnitude. Using Equation (1) in such situations without additional justification is not advisable. Such failures warrant a more focused assessment of the surveillance data and indicate that methods other than, or in addition to, the ETC may be necessary to reliably predict ΔT_{30} trends. However, the most appropriate approach may not be a heat-specific adjustment of the ETC predictions in all cases. For example, statistically significant differences may indicate situations in which the available data (i.e., the ΔT_{30} measurements or the composition and exposure values associated with the ΔT_{30} measurements, or both) are incorrect; therefore, adjusting the ETC predictions to match these data would be unwise. This chapter listed the factors that could help in diagnosing the reason why the surveillance data failed the statistical tests and discusses certain situations for which adjustments of the ETC predictions can be made.

6 GUIDANCE RELATED TO INSERVICE INSPECTION DATA AND NONDESTRUCTIVE EXAMINATION REQUIREMENTS

6.1 Background

The technical basis for the Alternate PTS Rule concludes that flaws as small as 0.1 inch in TWE contribute to the TWCF, and nearly all of the contributions come from flaws buried less than 1 inch below the inner diameter surface of the reactor vessel wall. Therefore, the Alternate PTS Rule specifies flaw limits for such flaws as indicated in Table 1-2 in this document. For weld flaws that exceed the sizes and numbers prescribed in Table 1-2, the risk analyses indicated that a single flaw contributes a significant fraction of the 1×10^{-6} per reactor year screening criteria on TWCF. Therefore, if a flaw that exceeds the sizes and quantities described in the flaw tables is found in a reactor vessel, it is important to assess it individually.

The technical basis for the Alternate PTS Rule also indicated that flaws buried deeper than 1 inch from the clad-to-base interface did not contribute as significantly to total risk as flaws of similar size located closer to the inner surface. Therefore, the Alternate PTS Rule does not require a comparison of the density of these flaws, but the rule still requires an evaluation of large flaws, if any are discovered, for their contributions to TWCF if they are within the inner 3/8t of the vessel wall thickness. Because flaws greater than 3/8t of the vessel wall thickness from the inside surface do not contribute to TWCF, the rule does not require an analysis of larger flaws.

The limitation for flaw acceptance, specified in ASME Code, Section XI, Table IWB-3510-1, approximately corresponds to the threshold for flaw sizes that can contribute significantly to TWCF if flaws of such sizes are present in reactor vessel material at this depth. Therefore, the final rule requires that flaws exceeding the size limits in Table IWB-3510-1 be evaluated for their contribution to TWCF in addition to the other evaluations for such flaws that are prescribed in the ASME Code.

The regulation at 10 CFR 50.61a(e) describes a number of tests and conditions on the collection and analysis of NDE data. These data provide reasonable assurance that the distribution of flaws assumed to exist in the probabilistic fracture mechanics (PFM) calculations, which provided the basis for the RT_{MAX-X} screening criteria in Table 1-1 of this document, provides an appropriate, or bounding, model of the population of flaws in the RPV of interest. These tests and conditions, the totality of which the diagram in Figure 6-1 illustrates, go beyond a simple comparison of the NDE data to the flaw table limits in Table 1-2.

The steps below summarize the process depicted in Figure 6-1. For each step in Figure 6-1, reference is made to the paragraph in the Alternate PTS Rule that contains the requirement addressed by that step.

Step A. All recordable flaw data (see Figure 6-2) should be collected for the inner 3/8t of the wall thickness for the base material and weld metal examination volumes within the RPV beltline region using procedures, equipment, and personnel as required by ASME Code, Section XI, Mandatory Appendix VIII, Supplements 4 and 6 [7], using ultrasonic testing (UT) volumetric examinations. (Note that the evaluation required by the flaw tables in 10 CFR 50.61a should include any flaws that are detected within the ultrasonic transducer scan paths. This includes any flaws located outside of the required ASME Code, Section XI, examination volume (see Step D of this procedure)).

Step B. The plant-specific flaw data from Step A should be evaluated for axial flaw surface connection. Any flaws with a TWE greater than or equal to 0.075 inch that are axially oriented and located at the clad-to-base metal interface should be assessed to determine whether they connect to the RPV inner surface using examination techniques that can detect and characterize service-induced cracking of the RPV cladding. Eddy current and visual examination methods are acceptable to the staff for detecting cladding cracks. The licensee shall implement an appropriate quality standard to ensure that these examinations can effectively identify surface cracking as required by 10 CFR Part 50, Appendix B, "Quality Assurance Criteria for Nuclear Power Plants and Fuel Reprocessing Plants," Criterion IX, "Control of Special Processes." Criterion IX requires the licensee to establish measures to ensure that special processes, including nondestructive testing, are controlled and accomplished by qualified personnel using qualified procedures in accordance with applicable codes, standards, specifications, criteria, and other special requirements. Appropriate quality standards for surface examinations are identified in the ASME Code, Section XI, or ASME Code, Section V, "Nondestructive Examination," or both.

- If surface connected flaws *do not exist* then proceed to Step C.

- Conversely, if surface connected flaws *do exist* then proceed to Step G.

  - If the outcome of Step G is a pass, proceed to Step C.
  - If the outcome of Step G is a failure, proceed to Step H.

Step C. The plant-specific flaw data from Step A should be evaluated for acceptability in accordance with the ASME Code, Section XI, Table IWB-3510-1, flaw acceptance standards.

- If all flaws are acceptable in accordance with the flaw acceptance standards, proceed to Step D.

- Conversely, if some flaws are not acceptable in accordance with the ASME flaw acceptance standards, proceed to Step G.

  - If the outcome of Step G is a pass, proceed to Step D.

  - If the outcome of Step G is a failure, proceed to Step H. Additionally, the licensee must demonstrate that it has satisfied the requirements of ASME Code, Section XI, before the vessel could be approved for a return to service.

Step D. The plant-specific flaw data should be compared to Tables 2 and 3 of 10 CFR 50.61a. Section 6.3 of this document provides an example of how this step may be performed and explains how the plant-specific flaw data are categorized as weld flaws or plate flaws.

- If all flaws are acceptable in accordance with the flaw tables of 10 CFR 50.61a, proceed to Step I.

- Conversely, if some flaws are not acceptable in accordance with the flaw tables, proceed to Step E.

Step E. The evaluation may account for NDE uncertainties such as flaw sizing errors, a flaw detection threshold, or POD. Appendix C to this document describes the development and application of one methodology acceptable to the NRC that accounts for uncertainties in NDE data. The licensee may use this method to develop more realistic vessel-specific flaw depth and density distributions for comparison to Tables 2 and 3 of 10 CFR 50.61a and may use them in a plant-specific PFM analysis. The methodology considers flaw sizing errors, a flaw detection threshold, POD, and a prior flaw distribution assumption. It applies a Bayesian updating methodology to combine the observed NDE data with the available flaw data and models used as part of the PTS reevaluation effort. The licensee must submit the adjustments made to the volumetric test data to account for NDE-related uncertainties, as described in 10 CFR 50.61a(c)(2).

- At the conclusion of this step, proceed to Step F.

Step F. The revised flaw distribution results of Step E should be compared to Tables 2 and 3 of 10 CFR 50.61a.

- If all flaws are acceptable in accordance with the flaw tables of 10 CFR 50.61a, proceed to Step I.

- Conversely, if some flaws are not acceptable in accordance with the flaw tables, proceed to Step G.

Step G. A demonstration that the TWCF is less than 1×10^{-6} events per reactor year is necessary to satisfy 10 CFR 50.61a(e)(4). The staff considers the two approaches described below to be acceptable for providing assurance that the TWCF is less than 1×10^{-6} events per reactor year. Therefore, all flaws should be evaluated for acceptability using one of the following two approaches:

(1) Preclusion of Brittle Fracture. The licensee can satisfactorily demonstrate upper-shelf behavior, which precludes brittle fracture, by maintaining temperature above RT_{NDT} + 60 degrees F using the following steps:

- Compute the irradiated RT_{NDT} for all flaws as follows:
  - Determine the unirradiated value of RT_{NDT} and $RT_{NDT(U)}$ for the material at each flaw location.
  - Determine the fluence at each flaw location.
  - Compute ΔT_{30} for each flaw using Equation (5) and the fluence at each flaw location.
  - Compute the flaw-specific value of RT_{NDT} as $RT_{NDT(U)} + \Delta T_{30}$ for each flaw.
- Assuming a lower bound PTS transient temperature of 75 degrees F, upper-shelf behavior is assured if $RT_{NDT} + 60 \leq 75°$ F. Therefore, the flaw-specific value of RT_{NDT} should be less than or equal to 15° F. This evaluation is considered acceptable if the flaw-specific values of RT_{NDT} are less than or equal to 15° F for all flaws.

(2) Calculation of the Plant-Specific TWCF Using a Plant-Specific PFM Analysis. A plant-specific PFM analysis to calculate TWCF is complex, and many variations of inputs are possible for such an analysis. Therefore, guidance for plant-specific PFM analysis to calculate TWCF is not provided. Section 6.2.2 provides general considerations for a plant-specific PFM analysis. Several sources discuss the methodology used in performing TWCF calculations for PTS. These include NUREG-1806; NUREG-1807, "Probabilistic Fracture Mechanics—Models, Parameters, and Uncertainty Treatment Used in FAVOR Version 04.1," issued June 2007 [20]; and NUREG/CR-6854, "Fracture Analysis of Vessels—Oak Ridge FAVOR, v04.1, Computer Code: Theory and Implementation of Algorithms, Methods, and Correlations," issued August 2007 [21]. The steps associated with conducting a plant-specific PFM calculation are as follows:

- Perform a Bayesian update of the flaw distribution:
  - Apply the procedures of Appendix C to this document and obtain revised flaw depth and density parameters (similar to those shown in Table 6-2 below).
- Calculate the TWCF using a PFM computer code (e.g., ORNL/TM-2012/566, "Fracture Analysis of Vessels—Oak Ridge (FAVOR), v12.1, Computer Code: User's Guide," issued 2012) [19]:
  - Run the generalized procedure for generating flaw-related inputs (see Ref. 12) using the revised flaw depth and density parameters.
  - Develop necessary plant-specific inputs using the guidance in NUREG-1806, NUREG-1807, and NUREG/CR-6854.
  - Run a plant-specific PFM analysis.
  - Calculate the TWCF.
- Compare the plant-specific TWCF to the TWCF screening criteria specified in 10 CFR 50.61a:
  - The evaluation associated with Step I is acceptable if the calculated TWCF is less than or equal to the $1x10^{-6}$ events per reactor year screening criteria specified in 10 CFR 50.61a.
- If the outcome of this step is a pass, proceed to Step I.
- If the outcome of this step is a failure, proceed to Step H.

Step H. The licensee should perform a plant-specific assessment for PTS and submit the assessment to the Director of NRR for review and approval as required by 10 CFR 50.61a(d)(4).

Step I. The screening criteria in Table 1 of 10 CFR 50.61a may be applied to the plant in question. Under 10 CFR 50.61a(c), the NRC requires licensees to submit their plant-specific assessments, including explicit details and results, to the Director of NRR for review and approval in the form of a license amendment at least three years before RT_{MAX-X} is projected to exceed the Alternate PTS Rule screening criteria.

Based on this process, the guidelines discussed in this chapter include the following three components:

(1) guidance for plants in which RPV flaws fall outside the applicability of the flaw tables in the Alternate PTS Rule, including the following:

- guidance on a procedure to preclude brittle fracture
- guidance on considerations to include in a plant-specific PFM analysis

(2) guidance for initial evaluation of NDE data obtained from qualified ISI examinations

(3) guidance on methods for further evaluation of NDE data obtained from qualified ISI examinations, including the following:

- guidance on the elements and NDE techniques associated with the qualified ISI examinations performed in accordance with ASME Code, Section XI, Mandatory Appendix VIII, to assess compliance with the requirements of the Alternate PTS Rule

- guidance on a mathematical procedure that can be used to adjust NDE data to account for flaw detection errors and sizing errors and guidance on comparison of the adjusted data to the population of flaws assumed in the PFM analysis used to develop the Alternate PTS Rule

The sections below describe guidance for these topics.

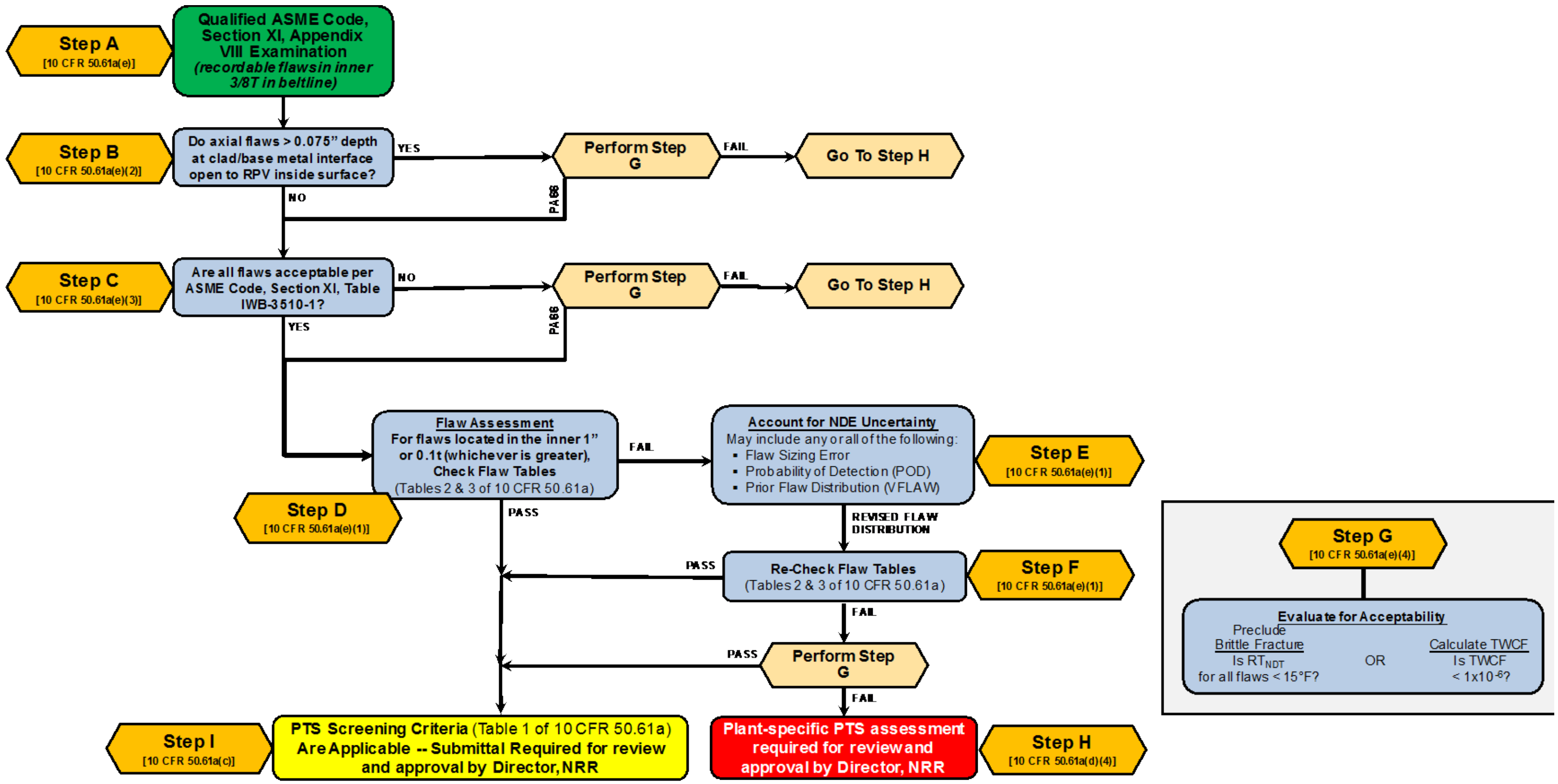

Figure 6-1 Flow diagram with recommendations for meeting the requirements of the Alternate PTS Rule

6.2 Guidance on Criteria Related to Alternate Screening Criteria on Embrittlement

This section describes guidance for situations in which plant-specific NDE results do not meet the acceptance standards of ASME Code, Section XI, Table IWB-3510-1, or are not within the limits prescribed by the flaw tables in the Alternate PTS Rule. In such situations, additional efforts beyond those described in Section 6.1 may still allow application of the PTS screening criteria in Table 1-1 of this document.

The guidelines discussed in this section include the following components:

- guidance on a procedure that can be used to preclude brittle fracture based on RT_{NDT} information for RPV flaws that fall outside the applicability of the Alternate PTS Rule flaw tables

- guidance on a procedure that can be used to combine the NDE data with the population of flaws assumed in the TWCF calculations to estimate a total flaw distribution that is predicted to exist in the RPV and guidance on the use of the total flaw distribution if a licensee chooses to conduct a PFM calculation

The sections below discuss these topics in detail.

6.2.1 Guidance on a Procedure To Preclude Brittle Fracture

This section provides guidance on a mathematical procedure to preclude brittle fracture for flaws that exceed the acceptance standards of ASME Code, Section XI, Table IWB-3510-1, as identified by Step I in Figure 6-1 of this document. Such guidance is based on information in Section II of 75 FR 13–29 [2], which states the following in regard to ISI volumetric examination and flaw assessments:

> The technical basis for the final rule also indicates that flaws buried deeper than 1 inch from the clad-to-base interface are not as susceptible to brittle fracture as similar size flaws located closer to the inner surface. Therefore, the final rule does not require the comparison of the density of these flaws, but still requires large flaws, if discovered, to be evaluated for contributions to TWCF if they are within the inner three-eighths of the vessel thickness. The limitation for flaw acceptance, specified in ASME Code, Section XI, Table IWB-3510-1, approximately corresponds to the threshold for flaw sizes that can make a significant contribution to TWCF if present in reactor vessel material at this depth. Therefore, the final rule requires that flaws exceeding the size limits in ASME Code, Section XI, Table IWB-3510-1 be evaluated for contribution to TWCF in addition to the other evaluations for such flaws that are prescribed in the ASME Code.

This section describes a simplified procedure for the situation in which the as-found NDE data for a plant reveal that one or more flaws fall outside the maximum range of the flaw tables in the Alternate PTS Rule and that the flaws do not satisfy the flaw-acceptance criteria of ASME Code, Section XI. Therefore, the following situations occur:

- The NDE data were obtained using a qualified examination in accordance with ASME Code, Section XI, Mandatory Appendix VIII, thereby satisfying Step A in Figure 6-1.

- All recordable flaws are located away from the clad-to-base-metal interface. Therefore, Step B is satisfied with a result of “NO” in Figure 6-1.

- Some of the recordable flaws do not meet the flaw-acceptance criteria of ASME Code, Section XI. Therefore, Step C is not satisfied with a result of “NO” in Figure 6-1.

Thus, based on the above information, Step F in Figure 6-1 requires the licensee to perform a flaw evaluation with acceptable results in accordance with ASME Code, Section XI, for those recordable flaws that do not meet the flaw-acceptance criteria of ASME Code, Section XI. In addition, further evaluation for acceptability using Step I is required. For the purposes of this example, a flaw evaluation in accordance with ASME Code, Section XI, is assumed to be successful and, therefore, is not described in the assessment that follows.

For the further evaluation required by Step I in Figure 6-1, one approach is to determine whether brittle fracture can be precluded. For this situation, a recommended evaluation could be the following:

<u>Step I—Preclude Brittle Fracture Option</u>

- The licensee can satisfactorily demonstrate upper-shelf behavior, which precludes brittle fracture, by maintaining temperature above RT_{NDT} + 60 degrees F [22].

- The licensee should compute the irradiated RT_{NDT} for all flaws as follows:

  - Determine the unirradiated value of RT_{NDT} and $RT_{NDT(u)}$ for the material at each flaw location.

  - Determine the fluence at each flaw location.

  - Compute ΔT_{30} for each flaw using Equation (1) and the fluence at each flaw location.

  - Compute the flaw-specific value of RT_{NDT} as $RT_{NDT(u)} + \Delta T_{30}$ for each flaw.

- Assuming a lower-bound PTS transient temperature of 75° F, upper-shelf behavior is assured if $RT_{NDT} + 60 \leq 75°$ F. Therefore, the flaw-specific value of RT_{NDT} should be less than or equal to 15° F.

- Flaws are acceptable if the flaw-specific value of RT_{NDT} is less than or equal to 15° F. For this situation, the decision at Step F is “ACCEPTABLE” in Figure 6-1.

- Flaws are not acceptable if the flaw-specific value of RT_{NDT} is greater than 15° F. For this situation, the decision at Step F is “NOT ACCEPTABLE” in Figure 6-1, another assessment is required (Step E in Figure 6-1), and the provisions of the Alternate PTS Rule may not be used.

- For the case in which Step F is “ACCEPTABLE,” all recordable flaws less than the maximum of 0.1 times the vessel wall thickness or 1 inch must be checked against the flaw tables (Step D in Figure 6-1).

- If the result of Step D is “PASS,” the RT_{MAX-X} screening criteria of the Alternate PTS Rule may be used (Step K in Figure 6-1).

Table 6-1 provides a sample calculation that demonstrates acceptability by Step I above.

Table 6-1 Sample Brittle Fracture Assessment

STEP D: Preclude Brittle Fracture for J-2 Flaws

Flaw No.	Flaw Position			Fluence at Clad/Base Metal Interface at Flaw Location (n/cm^2)[a]	Attenuation Factor, $e^{-0.24x}$	Attenuated Fluence at Flaw Location (n/cm^2)	End-of-Life Effective Full Power Years (EFPY)	Attenuated Flux at Flaw Location (n/cm^2-sec)
	Height on RPV (inches)	RPV Circumferential Position (°)	Depth Below Clad, x (inches)					
X	235.00	150.1	1.66	1.02E+19	0.6714	6.85E+18	54.0	4.02E+09
Y	235.14	157.7	2.70	1.02E+19	0.5231	5.34E+18	54.0	3.13E+09

Flaw No.	LINDE 80 Weld Chemistry[b]				
	$RT_{NDT(u)}$ (°F)	Cu (wt %)	Ni (wt %)	Mn (wt%)	P (wt%)
X	-40	0.09	0.48	1.300	0.004
Y	-40	0.09	0.48	1.300	0.004

Flaw No.	Temperature (°F)	ϕt_e Effective Fluence (n/cm^2)	A	B	Max(Cu_e)	Cu_e	f(Cu_e,P)	g(Cu_e,Ni,ϕt_e)	Mfterm (°F)	CRPterm (°F)	ΔT_{30} (°F)	RT_{NDT} (°F)
X	550.0	1.272E+19	1.417E-07	155.0	0.2430	0.0900	0.0683	9.412E-01	29.2	25.6	54.8	14.8
Y	550.0	1.057E+19	1.417E-07	155.0	0.2430	0.0900	0.0683	9.253E-01	26.6	25.2	51.8	11.8

Notes: a. Determined from a plant-specific fluence map.
b. From RPV surveillance program.

6.2.2 Guidance on Considerations To Include in a Plant-Specific Probabilistic Fracture Mechanics Analysis

This section provides guidance on the key considerations that should be included in a plant-specific PFM analysis to calculate TWCF, as identified by Step I in Figure 6-1. Such guidance includes a mathematical procedure to combine NDE data with the PFM flaw distribution used to develop the Alternate PTS Rule. A plant-specific TWCF analysis might be necessary based on 10 CFR 50.61a(d)(4) [1], which states the following:

> (4) If the analysis required by paragraph (d)(3) of this section indicates that no reasonably practicable flux reduction program will prevent the RT_{MAX-X} value for one or more reactor vessel beltline materials from exceeding the PTS screening criteria, then the licensee shall perform a safety analysis to determine what, if any, modifications to equipment, systems, and operation are necessary to prevent the potential for an unacceptably high probability of failure of the reactor vessel as a result of postulated PTS events. In the analysis, the licensee may determine the properties of the reactor vessel materials based on available information, research results and plant surveillance data, and may use probabilistic fracture mechanics techniques.

The PFM computer code, FAVOR [19], was developed by ORNL with NRC funding to predict failure probabilities for embrittled vessels subject to PTS transients. The NRC used FAVOR in the underlying TWCF analyses for the development of the Alternate PTS Rule. Critical inputs to FAVOR are the number and sizes of fabrication flaws in the RPVs of interest and the characteristics of cooldown scenarios. The TWCF analysis further requires the expected frequencies of the cooldown scenarios. Work on flaw distributions was coordinated with another NRC research program conducted by Pacific Northwest National Laboratory (PNNL) to perform examinations of RPV materials to detect and measure the numbers and sizes of fabrication flaws in welds and base metal. To supplement the limited data from flaw detection and measurements, PNNL applied an expert judgment elicitation process and the PRODIGAL flaw simulation model developed in the United Kingdom by Rolls-Royce and Associates. PNNL's experimental work on flaw distributions provided fabrication flaw data from NDE and destructive examinations, which were used to develop statistical distributions to characterize the numbers and sizes of flaws in the various regions of RPVs. Based on these statistical distributions, PNNL developed the computer program VFLAW, which generated flaw distributions that were used as inputs to the FAVOR computer code [18]. These input files for FAVOR describe flaw distributions based on PNNL's research activities. Therefore, the VFLAW program and the incorporation of plant-specific NDE data are critical input elements for performing plant-specific TWCF analyses.

Appendix C provides a recommended methodology for combining plant-specific NDE data with the PFM flaw distribution used to develop the Alternate PTS Rule. For the sample application to Beaver Valley Power Station, Unit 2 (Beaver Valley), discussed in Appendix C (Table C-4), Table 6-2 lists the revised flaw parameters that represent a plant-specific flaw distribution. The revised parameters on the flaw uncertainty distribution may be used to generate a revised flaw distribution for Beaver Valley, Unit 2, that is consistent with the flaw distribution used in the PTS FAVOR analyses. The revised parameters will lead to revised flaw distributions that may be input to a FAVOR PFM analysis. These parameters have been customized using the Appendix C procedure based on the specific geometry of Beaver Valley, Unit 2, and as-found NDE data. The revised flaw distributions may be generated and used as input to FAVOR by re-running the VFLAW program with the revised parameters listed in Table 6-2. Re-running the

VFLAW program allows adjustment of the generic VFLAW flaw distribution used to develop the Alternate PTS Rule into a plant-specific flaw distribution based on the updated knowledge of flaws obtained from plant-specific ISI. As shown in Table 6-2, this yields a Bayesian updated flaw distribution for use in the plant-specific PFM required at Step I in Figure 6-1.

As described in Appendix C, it is important to note that, although the VFLAW data represent generic values of flaw characteristics (based on expert judgment and the PVRUF and Shoreham RPVs), such data should be specialized to a specific RPV by using RPV-specific weld length, weld bead thickness, geometry, and other weld characteristics. Therefore, the specialized VFLAW data that result from this evaluation are the most representative information that can be used to describe a prior distribution of flaw depth and flaw density for a plant-specific PFM assessment. If other prior information is available, such information may also be used instead of, or in addition to, the specialized VFLAW data.

A PFM analysis that calculates TWCF also requires (1) the thermal-hydraulic characteristics of the cooldown scenarios as input to FAVOR and (2) the frequency of those scenarios as input to the TWCF calculation. The characteristics and frequency of excessive cooldown scenarios are not developed by existing probabilistic risk assessments (PRAs), which model only the end states of core damage and containment failure. The PTS rulemaking relied on extensive PRA analyses to explore, identify, and characterize excessive cooldown end states.

A plant-specific PFM analysis that calculates TWCF is complex, and many variations of inputs are possible for such an analysis. Therefore, this report does not include guidance for a plant-specific PFM analysis to calculate TWCF. NUREG-1806 [6], NUREG-1807 [21], and NUREG/CR-6854 [22] discuss the methodology used in performing a PFM analysis to calculate TWCF for PTS. As indicated in the Alternate PTS Rule, the plant-specific PFM analysis used to calculate TWCF and the description of the modifications made to the plant-specific inputs must be submitted to the Director of NRR in the form of a license amendment at least 3 years before RT_{MAX-X} is projected to exceed the PTS screening criteria.

The steps associated with conducting a plant-specific PFM evaluation are as follows:

(1) Perform the Bayesian update of the flaw distribution.

- Apply the procedures of Appendix C and obtain revised flaw depth and density parameters (similar to those shown in Table 6-2).

(2) Calculate the TWCF using FAVOR.

- Run VFLAW using the revised flaw depth and density parameters.
- Develop necessary plant-specific input using the guidance in NUREG-1806, NUREG-1807, and NUREG/CR-6854.
- Run a plant-specific FAVOR analysis.
- Calculate the TWCF.

(3) Compare the plant-specific TWCF from the FAVOR analysis to the screening criteria.

- If the calculated TWCF value is less than or equal to the screening criteria of 1×10^{-6} per reactor year as specified in the Alternate PTS Rule, the NDE data are acceptable, and the licensee may use the PTS screening criteria in Table 1-1 (Step K in Figure 6-1).
- If the TWCF value is greater than the screening criteria of 1×10^{-6} per reactor year as specified in the Alternate PTS Rule, the NDE data are unacceptable, and the PTS screening criteria in Table 1-1 may not be used. Alternate actions are required to resolve PTS embrittlement issues; such actions may include changes to the facility to reduce the likelihood or severity of the cooldown transients. The licensee must submit its plant-specific PTS assessment to the Director of NRR for review and approval (Step J in Figure 6-1).

Table 6-2 Summary of the Revised Flaw Depth and Density VFLAW Parameters To Be Used in a Revised PFM Analysis for Beaver Valley, Unit 2 (from Appendix C)

Case	Flaw Size Category	Original VFLAW Parameters of Uncertainty Distribution Used in PTS Work (Flaw Depth Parameters Specialized to Beaver Valley, Unit 2)	Revised Parameters of Uncertainty Distribution Based on Beaver Valley, Unit 2, NDE Data
1	Small ($a \leq \Delta$)	$\alpha_3 = 0.180$ $\alpha_4 = 1{,}419$	$\alpha'_3 = 0.230$ $\alpha'_4 = 1{,}909$
2	Large ($a > \Delta$)	$\alpha_3 = 0.180$ $\alpha_4 = 4$	$\alpha'_3 = 0.230$ $\alpha'_4 = 5$
3	Small ($a \leq \Delta$)	$U_1 = 34$ $U_2 = 8$ $U_3 = 1$	$U'_1 = 513.75$ $U'_2 = 17.71$ $U'_3 = 1.54$
4	Large ($a > \Delta$)	$\alpha_1 = 4.615$ $\alpha_2 = 4$	$\alpha'_1 = 4.563$ $\alpha'_2 = 5$

6.3 Guidance for Initial Evaluation of Nondestructive Examination Data

This section provides guidance for initial evaluation of NDE data obtained from qualified ISI examinations, as identified in Steps A through F in Figure 6-1. These steps are expected to be the most common use of the Alternate PTS Rule, and they represent a comparison of the as-reported NDE results with the flaw tables. Successful comparison of the NDE data to the flaw tables provides reasonable assurance that the plant-specific flaw distribution is bounded by the flaw distribution used in the development of the Alternate PTS Rule, therefore justifying application of the alternate PTS screening criteria in Table 1-1 to the plant in question.

As indicated under 10 CFR 50.61a(e), the licensee must acquire volumetric examination results evaluated under 10 CFR 50.61a(e)(1), (e)(2), and (e)(3) using procedures, equipment, and personnel qualified under ASME Code, Section XI, Mandatory Appendix VIII, Supplements 4 and 6, as specified in 10 CFR 50.55a(b)(2)(xv). Under 10 CFR 50.55a(g)(6)(ii)(C), the NRC requires licensees to implement ASME Code, Section XI, Mandatory Appendix VIII, Supplements 4 and 6. Supplement 4 contains qualification requirements for the RPV ISI volume from the clad-to-base-metal interface to the inner 15% of the RPV base-metal wall thickness. Supplement 6 contains qualification requirements for RPV weld volumes that lie within the outer 85% of the RPV base-metal wall thickness.

Figure 6-2 shows the examination and flaw evaluation process in ASME Code, Section XI, and identifies the flaws from that process that should be used for comparison to the flaw tables in the Alternate PTS Rule. As noted in Figure 6-2, the process used to identify flaws for comparison to the flaw tables is a subset of the process outlined in the ASME Code. All recordable flaws, subsequent to application of the flaw proximity rules of ASME Code, Section XI, Subarticle IWA-3300 (Flaw Characterization), are used for comparison to the flaw tables in the Alternate PTS Rule [16b].

A letter from N.A. Palm and M.G. Semmler (Westinghouse Electric Company) to A. Csontos (NRC), dated September 7, 2011, includes a sampling of RPV weld examinations from 13 PWR RPVs, conducted in accordance with ASME Code, Section XI, Mandatory Appendix VIII [17]. This sampling is a compilation of several RPV beltline weld examinations performed since 2000 that were provided by Westinghouse Electric Company in response to a request from the NRC. These results form the basis for the example comparison to the flaw tables shown in Figure 6-3 and Table 6-3 through Table 6-6 in this document. The following paragraphs discuss this figure and these tables.

The following evaluation process was used (Steps A through D and Step K in Figure 6-1) for the example shown in Figure 6-3 and Table 6-3 through Table 6-6:

Step A. Perform a qualified examination in accordance with ASME Code, Section XI, Mandatory Appendix VIII.

- Figure 6-3 shows the ASME Code, Section XI, Appendix VIII, examination results for Plant J.
- Eleven welds (two girth welds and nine intersecting axial welds) were examined in the RPV beltline region. A total of eight combined recordable flaws (as defined by the process shown in Figure 6-2) were detected.

Step B. Do axial flaws greater than 0.075 inch in depth at the clad-to-base-metal interface open to the RPV inside surface?

- Based on the S dimension (distance of flaw below the clad-to-base-metal interface) shown in Figure 6-3 for all flaws, no flaws at the clad-to-base-metal interface require supplemental examination to confirm that they are not connected to the RPV inside surface.
- If supplemental examination is required, perform a demonstrated surface or visual examination of the clad surface within the examination volume required by ASME Code, Section XI (e.g., Figures IWB-2500-1 and IWB-2500-2) to identify potential axial indications in the cladding surface that may extend into the base metal. A demonstrated visual or surface examination is capable of detecting and characterizing inservice cracking in a clad surface representative of the reactor vessel cladding process. An eddy current test is one acceptable examination method for performing this verification.
- The licensee shall document the method that it used for determining the uncertainty in locating the position of axial flaws identified by surface or visual examination and the location of axial flaws identified by UT examination. Any axial flaws located by UT within the uncertainty bounds of an axial crack shall be considered to be the same axial flaw.
- If the licensee confirms that no axial flaws are connected to the RPV inside surface, Step B is “NO” in Figure 6-1.

Step C. Are all flaws acceptable according to ASME Code, Section XI, Table IWB-3510-1?

- As indicated in Figure 6-3 in the column titled, “ASME Code Disposition,” in the second table, all recordable flaws are acceptable for meeting the requirements of ASME Code, Section XI, Table IWB-3510-1. The details of this determination are not shown.
- Therefore, the outcome of Step C is “YES” in Figure 6-1.

Step D. Check the flaw tables for flaws located in the inner 1 inch or 0.1t (whichever is greater).

- Compute the total weld length examined. The total weld examination length is determined in Table 6-3 based on the circumference of the RPV and the percentage of the weld examined (i.e., the coverage amount) for each of the 11 welds.
- Compute the total plate surface area examined. Table 6-4 lists the total plate surface area examined based on the surface area of the ASME Code, Section XI, examination volume less the surface area of the weld for each of the 11 welds examined.

- Determine the position of flaws. The position of all flaws is determined (Table 6-5) as follows:

  - Determine whether the flaw resides in plate or weld material. This determination is based on the flaw position with respect to the weld centerline and the maximum weld crown width[1] on either surface of the inspected weld. If the flaw position resides within the span of the weld centerline ± one-half of the weld crown width, the flaw was considered to be a WELD flaw. Otherwise, it was treated as a PLATE flaw.

  - Determine whether the flaw resides within the inner 1 inch or 10% of the base-metal wall thickness, whichever is greater, for comparison to the flaw tables in the Alternate PTS Rule.

  - Determine whether the flaw resides between the inner 1 inch or 10% of the base-metal thickness, whichever is greater, and the inner 37.5% of the base-metal wall thickness (3/8t) for potential evaluation of brittle fracture.

  - Based on the results shown in Table 6-5, two flaws should be compared to Table 2 (the weld flaw table) of the Alternate PTS Rule, and one flaw should be compared to Table 3 (the plate/forging flaw table) of the Alternate PTS Rule. Although two flaws reside between the inner 1 inch or 10 percent of the base-metal thickness (whichever is greater) and the inner 37.5% of the base-metal wall thickness (3/8t) from the clad-base-metal interface, they do not require further assessment for acceptability because they were found to be acceptable in accordance with ASME Code, Section XI, Table IWB-3510-1.

- Assess flaws.

  - The flaws determined in the previous step to be located in the inner 1 inch or 10% of the base-metal wall thickness (whichever is greater) are compared to the flaw tables from the Alternate PTS Rule in Table 6-6 and are found to be acceptable.

  - The remaining two flaws located between the inner 1 inch or 10% of the base-metal thickness (whichever is greater) and the inner 37.5% of the base-metal wall thickness (3/8t) from the clad-base-metal interface are acceptable in accordance with ASME Code, Section XI, Table IWB-3510-1.

  - Therefore, the outcome of Step D is “PASS” in Figure 6-1.

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1 The weld crown width was used in this example for the entire RPV base-metal wall thickness, which can potentially classify flaws located midwall as weld flaws rather than plate flaws in single-groove or double-V-groove weld configurations. This approach is conservative with respect to the flaw limits in Table 1-2. Consideration should also be given to the proximity of the flaw to the weld’s heat-affected zone (HAZ). For example, the licensee should consider that any flaw located in the plate material but within some technically justified minimum distance from the edge of the weld is affected by the HAZ and, therefore, is a weld flaw. In addition, if there are any weld-repair areas located within the examination volume, the licensee should classify any flaws detected within those areas as weld flaws.

<u>Step K</u>. Plant J can apply the PTS screening criteria in Table 1 of 10 CFR 50.61a. The licensee must submit the PTS evaluation to the NRC for review and approval.

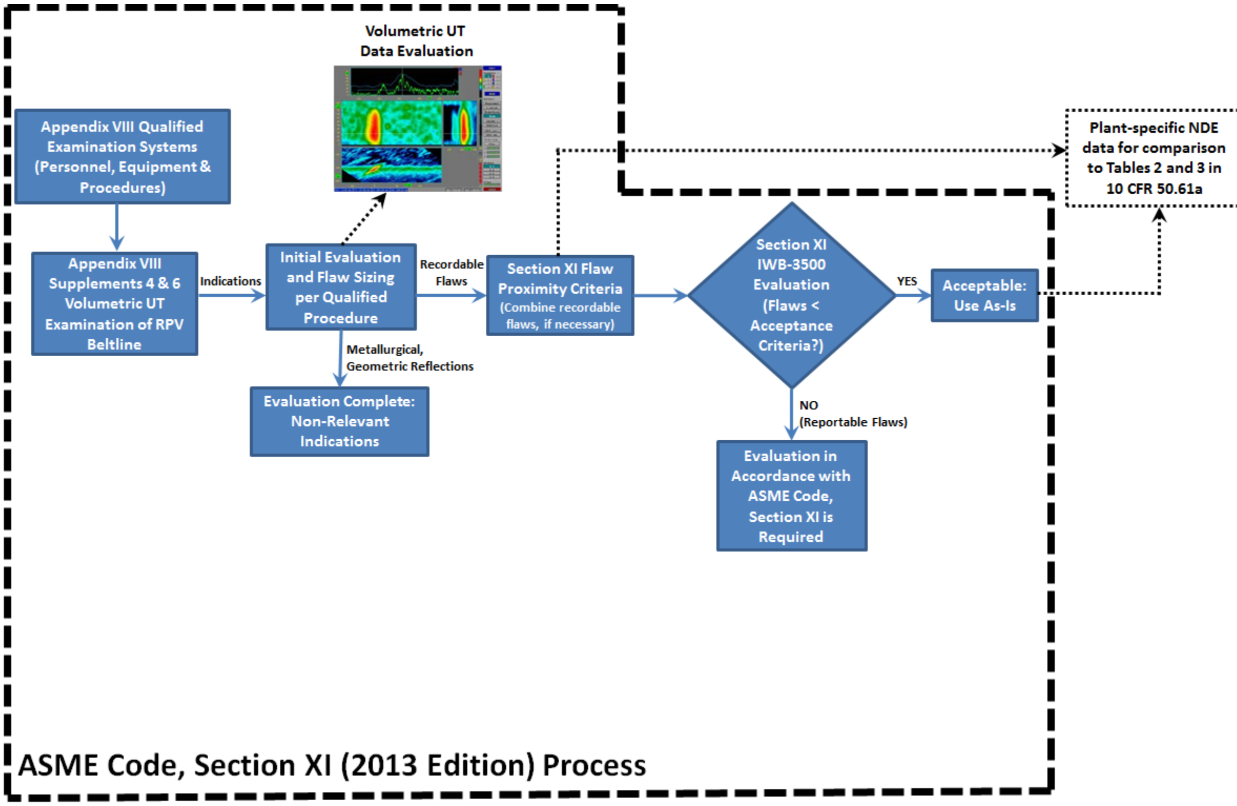


Figure 6-2 ASME Code, Section XI, examination and flaw evaluation process and identification of flaws for comparison to the Alternate PTS Rule

Step A: Plant J Examination Results: (see Westinghouse Letter LTR-AMLRS-11-71 [18])

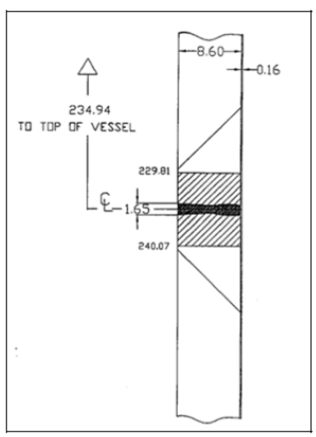
Reactor Vessel ISI History for Plant J Beltline Materials					
Weld ID	**Description**	**Date Last Inspected**	**Percent Coverage Obtained**	**Number of Recordable Indications**	**Number of Reportable Indications**
J-1	Nozzle Shell to Intermediate Shell Circ. Weld	2004	100	None	None
J-2	Intermediate Shell to Lower Shell Circ.	2004	100	4	None
J-3	Nozzle Shell Longitudinal Seam	2004	100	None	None
J-4	Nozzle Shell Longitudinal Seam	2004	100	None	None
J-5	Nozzle Shell Longitudinal Seam	2004	100	None	None
J-6	Intermediate Shell Longitudinal Seam	2004	100	None	None
J-7	Intermediate Shell Longitudinal Seam	2004	100	1	None
J-8	Intermediate Shell Longitudinal Seam	2004	100	None	None
J-9	Lower Shell Longitudinal Seam	2004	77.80[1]	2	None
J-10	Lower Shell Longitudinal Seam	2004	77.80[1]	None	None
J-11	Lower Shell Longitudinal Seam	2004	77.80[1]	1	None

Note 1: Limitations exist due to core support lugs at bottom of lower shell longitudinal welds.

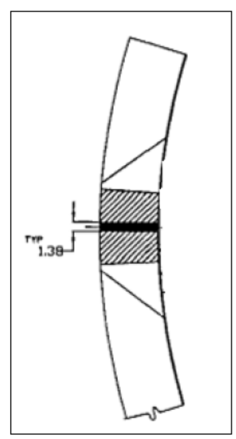
Reactor Vessel ISI Information for Potential Beltline Flaws Plant J																
Weld Number	Indication No.	Beam Direction	Weld Centerline (in.) or (º)	Weld width (in)	x (in)	θ (°)	2a (in)	a (in)	L (in)	t (in)	S (in)	a/L	AR	a/t (%)	Code Allowable a/t (%)	ASME Code Disposition
J-2	1	DN	235.00 in.	1.65	235.00	150.1	0.16	0.08	2.10	8.60	1.66	0.04	25.0	0.9	2.0	Allowable
	2	UP		1.65	235.14	157.7	0.12	0.06	1.25	8.60	2.70	0.05	20.0	0.7	2.2	Allowable
	3	UP		1.65	235.80	129.3	N/A	0.25	1.00	8.60	0.00[1]	.25	4	2.9	3.3	Allowable
	4	UP		1.65	235.50	332.1	0.24	0.12	1.75	8.60	4.49	0.07	14.3	1.4	2.2	Allowable
J-7	1	CCW	120°	1.38	123.6	123.6	0.22	0.11	2.10	8.60	0.63	0.05	20.0	1.3	7.6	Allowable
J-9	1	DN	60°	1.38	256.50	60.3	0.25	0.13	1.60	8.60	0.11	0.08	12.5	1.5	1.87	Allowable
	2	CCW		1.38	240.30	60.4	0.34	0.17	1.60	8.60	0.79	0.11	9.1	2.0	2.5	Allowable
J-11	1	CCW	300°	1.38	312.61	300.3	0.27	0.14	1.75	8.60	3.60	0.08	12.5	1.6	2.2	Allowable

Note 1: S dimension is from outside diameter surface so this is an OD surface flaw.

Top of core position x=149.1 in.
Bottom of core position x=292.6 in.
Reactor Vessel Inner Diameter (without cladding)= 173 in.
Cladding Thickness= 0.156 in.



Circumferential Weld



Axial Weld

Figure 6-3 Sample ASME Code, Section XI, MandatoryAppendix VIII, examination results for Plant J

Table 6-3 Determination of Total Weld Length Examined for Plant J

STEP D: Compute Total Weld Length Examined

Weld ID	Direction	Radius, R_i (inches)	Length (inches)	Comments	Examination Coverage	Examined Length, L = Length * Coverage (inches)
J-1	Circumferential	86.5	543.5	Length computed as $2\pi R_i$	100%	543.5
J-2	Circumferential	86.5	543.5	Length computed as $2\pi R_i$	100%	543.5
J-3	Axial	N/A	70	Length assumed	100%	70.0
J-4	Axial	N/A	70	Length assumed	100%	70.0
J-5	Axial	N/A	70	Length assumed	100%	70.0
J-6	Axial	N/A	70	Length assumed	100%	70.0
J-7	Axial	N/A	70	Length assumed	100%	70.0
J-8	Axial	N/A	70	Length assumed	100%	70.0
J-9	Axial	N/A	70	Length assumed	77.8%	54.5
J-10	Axial	N/A	70	Length assumed	77.8%	54.5
J-11	Axial	N/A	70	Length assumed	77.8%	54.5
					Total, L =	**1,670.4**

Table 6-4 Determination of Total Plate Surface Area Examined for Plant J

STEP D: Compute Total Plate Surface Area Examined

Weld ID	Examined Length, L	Weld Width, W_W (1) (inches)	Examination Width, W_E (2) (inches)	Comments	Plate Surface Area (inches^2)
J-1	543.5	1.65	8.60	Plate surface area computed as L x $(W_E - W_W)$	3,777.29
J-2	543.5	1.65	8.60	Plate surface area computed as L x $(W_E - W_W)$	3,777.29
J-3	70.0	1.38	8.60	Plate surface area computed as L x $(W_E - W_W)$	505.40
J-4	70.0	1.38	8.60	Plate surface area computed as L x $(W_E - W_W)$	505.40
J-5	70.0	1.38	8.60	Plate surface area computed as L x $(W_E - W_W)$	505.40
J-6	70.0	1.38	8.60	Plate surface area computed as L x $(W_E - W_W)$	505.40
J-7	70.0	1.38	8.60	Plate surface area computed as L x $(W_E - W_W)$	505.40
J-8	70.0	1.38	8.60	Plate surface area computed as L x $(W_E - W_W)$	505.40
J-9	54.5	1.38	8.60	Plate surface area computed as L x $(W_E - W_W)$	393.20
J-10	54.5	1.38	8.60	Plate surface area computed as L x $(W_E - W_W)$	393.20
J-11	54.5	1.38	8.60	Plate surface area computed as L x $(W_E - W_W)$	393.20
				Total, A =	**11,766.6**

Notes: (1) The weld width, W_W, is defined as the maximum weld crown width from both sides of the RPV wall. From Figure 6-3, W_W is 1.65 inches for circumferential welds and 1.38 inches for axial welds.

(2) The examination width, W_E, is defined as the ASME Code, Section XI, examination volume width, which is one-half of the wall thickness on both sides of the weld. From Figure 6-3, the RPV base-metal wall thickness, which is equal to W_E, is 8.60 inches.

Table 6-5 Determination of the Flaw Positions for Plant J

STEP D: **Determine Position of Flaws**

Weld No.	Indication No.	Weld Centerline		Weld Width (inches)	Flaw Position: Height on RPV (inches)	Flaw Position: RPV Circumferential Position (°)	Flaw Position: Depth Below Clad (inches)	Weld or Plate Flaw?	Is Flaw Within First 1.0" or 0.10t?	Is Flaw Within First 3/8t?	Through Wall Extent (TWE) = 2a (inches)	Evaluation Required
J-2	1	235	in	1.65	235.00	150.1	1.66	WELD	NO	YES	0.16	Acceptable per ASME XI Table IWB-3510-1
	2	235	in	1.65	235.14	157.7	2.70	WELD	NO	YES	0.12	Acceptable per ASME XI Table IWB-3510-1
	3	235	in	1.65	235.80	129.3	8.60	WELD	NO	NO	0.50	No evaluation for 50.61a required
	4	235	in	1.65	235.50	332.1	4.49	WELD	NO	NO	0.24	No evaluation for 50.61a required
J-7	1	120	°	1.38	123.60	123.6	0.63	PLATE	YES	N/A	0.22	Compare to Plate Flaw Table
J-9	1	60	°	1.38	256.50	60.3	0.11	WELD	YES	N/A	0.25	Compare to Weld Flaw Table
	2	60	°	1.38	240.30	60.4	0.79	WELD	YES	N/A	0.34	Compare to Weld Flaw Table
J-11	1	300	°	1.38	312.61	300.3	3.60	WELD	NO	NO	0.27	No evaluation for 50.61a required

Table 6-6 Comparison of Flaws to the Flaw Tables in the Alternate PTS Rule for Plant J

STEP D: **Compare Flaws to 10 CFR 50.61a Flaw Tables**

Table 2 Comparison = Weld Flaws

Bin No.	Minimum TWE (inches)	Maximum TWE (inches)	(Allowable) Max. # of Flaws per 1,000 inches	(Cumulative) # of Flaws Detected	# of Flaws / L x 1,000	Acceptable?	Flaws
1	0	0.075	No limit	0	0.00	YES	
2	0.075	0.475	166.70	2	1.20	YES	J-9-1, J-9-2
3	0.125	0.475	90.80	2	1.20	YES	J-9-1, J-9-2
4	0.175	0.475	22.82	2	1.20	YES	J-9-1, J-9-2
5	0.225	0.475	8.66	2	1.20	YES	J-9-1, J-9-2
6	0.275	0.475	4.01	2	1.20	YES	J-9-1, J-9-2
7	0.325	0.475	3.01	1	0.60	YES	J-9-1
8	0.375	0.475	1.49	0	0.00	YES	
9	0.425	0.475	1.00	0	0.00	YES	
10	0.475	Infinite	0.00	0	0.00	YES	

Table 3 Comparison = Plate/Forging Flaws

Bin No.	Minimum TWE (inches)	Maximum TWE (inches)	(Allowable) Max. # of Flaws per 1,000 inches	(Cumulative) # of Flaws Detected	# of Flaws / A x 1,000	Acceptable?	Flaws
1	0	0.075	No limit	0	0.00	YES	
2	0.075	0.375	8.05	1	0.08	YES	J-7-1
3	0.125	0.375	3.15	1	0.08	YES	J-7-1
4	0.175	0.375	0.85	1	0.08	YES	J-7-1
5	0.225	0.375	0.29	0	0.00	YES	
6	0.275	0.375	0.08	0	0.00	YES	
7	0.325	0.375	0.01	0	0.00	YES	
8	0.375	Infinite	0.00	0	0.00	YES	

6.4 Guidance for Further Evaluation of Nondestructive Examination Data

This section provides guidance for further evaluation of NDE data (Steps G through I in Figure 6-1). Such guidance is based on Section II of 75 FR 13–29 [2], which states the following in regard to NDE-related uncertainties:

> The flaw sizes in Tables 2 and 3 represent actual flaw dimensions while the results from the ASME Code examinations are estimated dimensions. The available information indicates that, for most flaw sizes in Tables 2 and 3, qualified inspectors will oversize flaws. Comparing oversized flaws to the size and density distributions in Tables 2 and 3 is conservative and acceptable, but not necessary.
>
> As a result of stakeholder feedback received on the NRC solicitation for comments published in the August 2008 supplemental proposed rule, the final rule will permit licenses to adjust the flaw sizes estimated by inspectors qualified under the ASME Code, Section XI, Appendix VIII, Supplement 4 and Supplement 6.
>
> The NRC determined that, in addition to the NDE sizing uncertainties, licensees should be allowed to consider other NDE uncertainties, such as probability of detection and flaw density and location, because these uncertainties may affect the ability of a licensee to demonstrate compliance with the rule. As a result, the language in § 50.61a(e) will allow licensees to account for the effects of NDE-related uncertainties in meeting the flaw size and density requirements of Tables 2 and 3. The methodology to account for the effects of NDE-related uncertainties must be based on statistical data collected from ASME Code inspector qualification tests or any other tests that measure the difference between the actual flaw size and the size determined from the ultrasonic examination.

The sections below provide specific guidance on various elements of NDE data evaluation.

6.4.1 Guidance on the Elements and Nondestructive Examination Techniques Associated with ASME Code Examinations

The NRC developed the Alternate PTS Rule using a flaw density, spatial distribution, and size distribution determined from experimental data and from physical models and expert judgment. To implement the Alternate PTS Rule, actual flaw densities and distributions need to be estimated from the results of periodic ISI performed on RPV welds and adjacent base material. UT is the method used for these examinations. As discussed in Section 6.3, the licensee must acquire the data necessary to evaluate the Alternate PTS Rule using procedures, equipment, and personnel qualified under ASME Code, Section XI, Mandatory Appendix VIII, Supplements 4 and 6. Mandatory Appendix VIII provides requirements for demonstrating UT examination procedures, equipment, and personnel used to detect and size flaws. Supplement 4 specifies qualification requirements for examining the inner 15% of clad ferritic reactor vessels and may be applied to the inner 15% of unclad ferritic reactor vessels. Supplement 6 specifies qualification requirements for examining unclad ferritic components and the outer 85% of clad ferritic components.

Supplement 4 provides performance-demonstration rules intended to produce effective procedures, personnel, and equipment for detection and sizing of flaws typical of those that might form under service conditions. These rules result in targeting flaws that are primarily planar in orientation and emanate from the inside surface (clad-to-base-metal interface) of the RPV specimens that are used for the qualification process. The aspect ratio of flaws used for performance demonstration also closely follows the acceptance criteria of ASME Code, Section XI, Article IWB-3000. These flaws are the focus of the performance demonstration because they are of structural significance under standard operating conditions. Therefore, the objective of ASME Code, Section XI, Supplement 4, qualification is to demonstrate UT capabilities on planar flaws. Examinations using ASME Code, Section XI, Mandatory Appendix VIII, qualification may also detect larger fabrication flaws, which often occurs in practice because no known credible subcritical cracking mechanisms affect the RPV material for the current fleet of U.S. reactors.

The PFM analyses supporting the Alternate PTS Rule assumed all flaws were planar in nature. Because the empirical evidence on which the flaw distribution used in these analyses was based included both planar flaws and fabrication flaws [18], this assumption was considered conservative because it produced a higher density of planar flaws than typically found in nuclear RPVs. Fabrication flaws are considerably smaller than those within current Supplement 4 qualification specimens and are not typically connected to the clad-to-base-metal interface. Nevertheless, it is probable that parameters associated with qualified UT methods may be optimized to enhance the method’s capability to detect and size small fabrication flaws in the inner 1 inch of RPV base material. Therefore, licensees should consider enhancements to Mandatory Appendix VIII-qualified procedures to ensure accurate detection and sizing of the flaws inferred by the Alternate PTS Rule while maintaining the essential variables for which the procedure was qualified.

Within the context of a Mandatory Appendix VIII-qualified RPV examination, the licensee might be able to vary the elements and NDE techniques associated with the examination to provide better NDE data for comparison with the flaw limits in Tables 2 and 3 of the Alternate PTS Rule. Such elements and techniques may include, but are not limited to, the following:

- reduction of the scan index
- use of an ultrasonic straight-beam examination technique
- use of an enhanced recording criterion (lower threshold)

The NRC staff has been working with UT/NDE experts at PNNL to assess RPV examination and implementation of the Alternate PTS Rule. A technical letter report [23] addresses the assessment, including enhancements to procedures and examination techniques. Licensees that choose to apply the Alternate PTS Rule should consider the elements and techniques listed above when establishing the protocols and procedures for Mandatory Appendix VIII examinations to maximize the usefulness of the resulting NDE data and to provide reasonable assurance of the acceptability of the NDE data comparisons required by the Alternate PTS Rule.

6.4.2 Guidance on a Procedure To Adjust Nondestructive Examination Data and Comparison to Flaws Assumed in Probabilistic Fracture Mechanics Calculations

This section provides guidance on a mathematical procedure that licensees can use to adjust NDE data to account for flaw detection and sizing errors, as identified by Step G in Figure 6-1. This evaluation adjusts the as-found NDE data by taking into account flaw-sizing errors, POD uncertainties, and prior flaw distributions such as those used in the development of the Alternate PTS Rule (i.e., VFLAW [18]). The licensee may consider any or all of these uncertainties, depending on the level of detail needed for flaw assessment. After making such an adjustment, the licensee may again compare the adjusted NDE results with the flaw tables (Step H in Figure 6-1) because NDE techniques tend to oversize smaller flaws, thereby distributing detected flaws into larger bins where the allowed number of flaws is smaller. In such cases, adjustment for NDE flaw detection and sizing uncertainties may result in a less conservative distribution of flaw sizes and possibly result in a successful comparison of the adjusted NDE data to the flaw tables. The NRC staff would view a successful comparison of the revised NDE data to the flaw tables as providing reasonable assurance that the plant-specific flaw distribution is bounded by the flaw distribution used in the development of the Alternate PTS Rule, thus indicating that applying the alternate PTS screening criteria is appropriate (Step K in Figure 6-1).

Appendix C describes the development and application of a methodology for assessing uncertainties in NDE data, analyzing such data for the purpose of developing more realistic vessel-specific flaw depth and density distributions for comparison to the flaw tables, and performing a plant-specific PFM analysis (discussed in Section 6.2.2). The methodology considers POD, flaw-measurement error, and flaw-detection threshold in its application and uses Bayesian updating to combine the observed NDE data with the available flaw data and models used as part of the PTS reevaluation effort. Appendix C describes the Bayesian framework that this methodology uses, the application details of the NDE data uncertainties, (i.e., the POD and measurement/sizing error) and the Bayesian updating procedure. Appendix C demonstrates the application of the methodology using the ultrasonic NDE data obtained from a previous ISI examination of the Beaver Valley, Unit 2, RPV and a MATLAB software routine that uses the Bayesian equations developed in Appendix C. Appendix C also includes the MATLAB software listing.

As an example of this procedure, assume that Plant J performs an initial NDE assessment using the guidance of Section 6.3 with the results shown in Table 6-7. These results indicate that Plant J fails the flaw table check in the Alternate PTS Rule because it violated the flaw acceptance limit for Flaw Bin No. 2 (i.e., 170.10 actual flaws per 1,000 inches of weld versus 166.70 allowed flaws per 1,000 inches of weld). Therefore, Step D in Figure 6-1 yields a “FAIL” decision, thereby necessitating the evaluations associated with Step G in Figure 6-1. As a result, the licensee could choose to apply procedures similar to those described in Appendix C.

A key input for this procedure is a POD and associated flaw-sizing error data appropriate to the methods and techniques used to examine the RPV. EPRI has previously developed example PODs and flaw-sizing error data based on Performance Demonstration Initiative (PDI) qualification data [25]. Similar information should be obtained for the examination technique being applied and technically justified for use as a part of implementing the procedures described in Appendix C.

Table 6-7 Example for Plant J after Applying an Initial Alternate PTS Rule Flaw Table Check Using the Procedure in Section 6.3

Flaw Bin No.	Flaw Depth (inches)	Observed (Detected) Number of Flaws from NDE ISI	10 CFR 50.61a Flaw Limits (number of flaws per 1,000 inches of weld)	Acceptable? (Is the number of flaws less than the limit?)
1	0.000 < a ≤ 0.075	234.45	No limit	Yes
2	0.075 < a ≤ 0.475	170.10	166.70	No
3	0.125 < a ≤ 0.475	11.23	90.80	Yes
4	0.175 < a ≤ 0.475	0.90	22.82	Yes
5	0.225 < a ≤ 0.475	0.05	8.66	Yes
6	0.275 < a ≤ 0.475	0.01	4.01	Yes
7	0.325 < a ≤ 0.475	0.00	3.01	Yes
8	0.375 < a ≤ 0.475	0.00	1.49	Yes
9	0.425 < a ≤ 0.475	0.00	1.00	Yes

6.4.3 Guidance on the Application of Nondestructive Examination Uncertainties

Appendix D discusses the results of sensitivity analyses that apply the Bayesian updating methodology in Appendix C to systematically assess the effect of NDE uncertainties such as the POD and measurement (sizing) error on the estimated flaw populations. The sensitivity analyses were performed for a base case and 12 sensitivity cases that investigated variations in observed NDE data and application of prior PDFs, POD, and flaw-sizing error.

As a part of the sensitivity studies, lower NDE detection limits of 0.04 inch and 0.075 inch were also evaluated and found to have no significant effect on the observed data.

The results obtained from the 12 sensitivity cases consistently show that a small (i.e., 10%) overpopulation of flaws in Bins 2 and 3 of the Alternate PTS Rule flaw tables, as might be expected from actual plant inspections because of oversizing of small flaws, would be shifted to Flaw Bin Nos. 1 and 2 after accounting for the measurement error in the Bayesian update. When the POD was also considered, the effects of small flaws that might be missed by NDE methods were clearly seen in Flaw Bin Nos. 1 and 2, with an additional number of flaws in the posterior estimates as compared to the observed flaws. However, the results are sensitive to the POD used, especially the portion of the POD for smaller flaw sizes. Therefore, if a licensee uses a POD, this use must be sufficiently justified.

The effects of the choice of prior distributions of flaw density and flaw depth were significant. When no prior information was used to describe the flaw density and flaw depth distributions, the POD and measurement error were very sensitive and significantly amplified the number of flaws that resulted in Flaw Bin Nos. 1 and 2. However, when prior PDFs were used, existence of the prior PDFs significantly moderated the posterior PDFs, and the POD and measurement errors played less significant roles.

The results of the sensitivity analysis documented in Appendix D reveal the following:

- Neglecting consideration of prior PDFs in the evaluation provides a conservative assessment.

- Neglecting consideration of flaw-sizing error in the evaluation provides a conservative assessment.

- The POD significantly affects the evaluation, and it should be included for cases in which PDFs are not considered. For the evaluation of PDFs, the effect of the POD is relatively small and may be neglected.

- Consideration of flaw-sizing error, POD, or prior PDFs (identified as “NDE uncertainties” in the Alternate PTS Rule) using methods similar to those shown in Appendix C is successful in removing conservatisms that may unnecessarily prevent a licensee from passing the flaw tables in the Alternate PTS Rule.

7 GUIDANCE RELATED TO ALTERNATE SCREENING CRITERIA ON EMBRITTLEMENT

The regulation at 10 CFR 50.61a(c)(3) states the following (note that the **highlighting** is, as explained below, added for emphasis; the **highlighting** does not appear in the CFR):

> Each licensee shall compare the projected RT_{MAX-X} values for plates, forgings, axial welds, and circumferential welds to the PTS screening criteria in Table 1 of this section, for the purpose of evaluating a reactor vessel's susceptibility to fracture due to a PTS event. **If any of the projected RT_{MAX-X} values are greater than the PTS screening criteria in Table 1** of this section, then **the licensee may propose** the compensatory actions or **plant-specific analyses** as required in paragraphs (d)(3) through (d)(7) of this section, as applicable, to justify operation beyond the PTS screening criteria in Table 1 of this section.

This section describes one method by which licensees can perform the plant-specific analyses indicated by the **highlighted text**. This method is acceptable to the staff as long as the licensee satisfies all other requirements of 10 CFR 50.61a concerning flaw evaluations, flaw assessment, statistical evaluation of surveillance data, and plant corrective actions.

The RT_{MAX-X} screening criteria in Table 1 of 10 CFR 50.61a were established in NUREG-1874 based on a TWCF of $1x10^{-6}$ per reactor year. As described in NUREG-1874, the RT_{MAX-X} screening criteria are based on the results of PFM analyses; they account for the combined TWCF contributions from various flaw populations in the RPV. Some simplifications of the PFM data underlying these screening criteria were necessary to permit their expression in a tabular form. As an example, the TWCF attributable to circumferentially oriented flaws that occur in circumferential welds was held below $1x10^{-8}$ per reactor year rather than $1x10^{-6}$ per reactor year. This simplification was made for expedience and was not intended to address a safety concern. Therefore, the licensee can use the following procedure, which eliminates similar simplifying assumptions, to demonstrate compliance with the RT_{MAX-X} screening criteria in 10 CFR 50.61a, Table 1. Section 3.5.1 of NUREG-1874 describes this procedure as follows:

(1) Determine RT_{MAX-X} for all axial welds (RT_{MAX-AW}), plates (RT_{MAX-PL}), circumferential welds (RT_{MAX-CW}), and forgings (RT_{MAX-FO}) (as applicable) in the RPV beltline region according to the requirements of 10 CFR 50.61a. These RT_{MAX-X} values must be expressed in units of Rankine (R) (degrees F plus 459.69).

(2) Use the RT_{MAX-X} values from Step 1 to estimate the 95th percentile TWCF contribution from each component in the beltline using the following formulas:

$$TWCF_{95-AW} = \exp\{5.5198 \cdot \ln(RT_{MAX-AW} - 616) - 40.542\} \cdot \beta \quad (7\text{-}1)$$

$$TWCF_{95-PL} = \exp\{23.737 \cdot \ln(RT_{MAX-PL} - 300) - 162.38\} \cdot \beta \quad (7\text{-}2)$$

$$TWCF_{95-CW} = \exp\{9.1363 \cdot \ln(RT_{MAX-CW} - 616) - 65.066\} \cdot \beta \quad (7\text{-}3)$$

$$TWCF_{95-FO} = \exp\{23.737 \cdot \ln(RT_{MAX-FO} - 300) - 162.38\} \cdot \beta + \eta \cdot \{1.3 \times 10^{-137} \cdot 10^{0.185 \cdot RT_{MAX-FO}}\} \cdot \beta \quad (7\text{-}4)$$

where:

η = 0 if the forging is compliant with Regulatory Guide 1.43, "Control of Stainless Steel Weld Cladding of Low-Alloy Steel Components"; otherwise, η = 1.
β = 1 if $T_{WALL} \leq 9.5$ inches
$\beta = 1 + 8 \times (T_{WALL} - 9.5)$ if $9.5 < T_{WALL} < 11.5$ inches
β = 17 if $T_{WALL} \geq 11.5$ inches

(3) Estimate the total 95th percentile TWCF for the RPV using the following formulae (noting that, depending on the type of vessel in question, certain terms in the following formula will be zero):

$$TWCF_{95-TOTAL} = \begin{bmatrix} \alpha_{AW} \cdot TWCF_{95-AW} + \\ \alpha_{PL} \cdot TWCF_{95-PL} + \\ \alpha_{CW} \cdot TWCF_{95-CW} + \\ \alpha_{FO} \cdot TWCF_{95-FO} \end{bmatrix} \tag{7-5}$$

where:

α = 2.5 if $RT_{MAX-xx} \leq 625$ R
$\alpha = 2.5 - \frac{1.5}{250}\left(RT_{MAX-xx} - 625\right)$ if 625 R < RT_{MAX-xx} < 875 R
α = 1 if $RT_{MAX-xx} \geq 875$ R

(4) If the calculated $TWCF_{95-TOTAL}$ from Step 3 is less than 1×10^{-6} per reactor year, the requirements of Table 1 of 10 CFR 50.61a are considered to have been met.

8 SUMMARY

In early 2010, the NRC promulgated the Alternate PTS Rule in 10 CFR 50.61a, which amended existing regulations to provide alternate embrittlement requirements for protection against PTS events for PWR RPVs. These requirements are based on more comprehensive, accurate, and realistic analysis methods than those used to establish the screening criteria in 10 CFR 50.61. This action became desirable because the existing requirements, as contained in 10 CFR 50.61, are based on unnecessarily conservative assumptions. While still maintaining adequate safety margins, the Alternate PTS Rule reduces regulatory burden for those PWR licensees that expect to exceed the 10 CFR 50.61 embrittlement requirements before the expiration of their operating licenses. PWR licensees may choose to comply with the Alternate PTS Rule as a voluntary alternative to complying with the requirements in 10 CFR 50.61.

The Alternate PTS Rule provides revised PTS screening criteria in the form of embrittlement reference temperatures, RT_{MAX-X}, that characterize the RPV material's resistance to fracture initiating from flaws. Licensees may use the RT_{MAX-X} embrittlement screening criteria provided that they meet the following criteria:

(1) criteria related to the date of construction and design requirements

The Alternate PTS Rule applies to licensees whose construction permits were issued before February 3, 2010, and whose RPVs were designed and fabricated to the 1998 edition or an earlier edition of the ASME Code. The reason for this applicability restriction is that the structural and thermal-hydraulic analyses that established the basis for the Alternate PTS Rule's embrittlement screening criteria represented only plants constructed before this date. The licensee is responsible for demonstrating that the technical basis calculations developed in support of the Alternate PTS Rule adequately address the risk-significant factors that control PTS for any plant constructed after February 3, 2010. Chapter 4 of this document describes methods by which licensees can satisfy these criteria and identifies factors to be considered in such an evaluation.

(2) criteria related to plant-specific surveillance data

(3) The Alternate PTS Rule includes statistical tests that licensees must perform on RPV surveillance data to determine whether the surveillance data are sufficiently "close" to the predictions of an ETC to validate such predictions for use. Of particular interest from a regulatory perspective is the use of these statistical tests to determine whether plant-specific surveillance data deviate significantly from the predictions of the ETC in a manner that suggests that the ETC is very likely to underpredict plant-specific data trends. Chapter 5 of this document describes guidance by which licensees can assess the closeness of plant-specific data to the ETC using statistical tests, including the following:

- a detailed description of the mathematical procedures to use to assess compliance with the three statistical tests in the Alternate PTS Rule
- a list of factors to consider in diagnosing the reason why particular surveillance datasets may fail these statistical tests

- a description of certain situations in which routine adjustments of the ETC predictions can be made

(4) criteria related to ISI data and NDE requirements

(5) The Alternate PTS Rule describes a number of tests of and conditions on the collection and analysis of ISI data that should provide reasonable assurance that the distribution of flaws assumed to exist in the PFM calculations, which provide the basis for the RT_{MAX-X} screening criteria, provides an appropriate, or bounding, model of the population of flaws in the RPV of interest. Chapter 6 of this document includes guidance to help licensees satisfy these criteria. This document discusses the following guidance:

- guidance for plants with RPV flaws that fall outside the applicability of the flaw tables in the Alternate PTS Rule, including the following:

  – a mathematical procedure that can be used to preclude brittle fracture based on RT_{NDT} information

  – a mathematical procedure that can be used to combine the NDE data with the population of flaws assumed in the PFM calculations to estimate the total flaw distribution predicted to exist in the RPV and guidance on the use of this total flaw distribution as part of a PFM calculation using the FAVOR computer code

- guidance for initial evaluation of NDE data obtained from qualified ISI examinations

- guidance for further evaluation of NDE data obtained from qualified ISI examinations, as follows:

  – the elements and NDE techniques associated with the qualified ISI examinations performed in accordance with ASME Code, Section XI, Mandatory Appendix VIII, to assess compliance with the requirements of the Alternate PTS Rule

  – a mathematical procedure that can be used to adjust NDE data to account for flaw-detection and -sizing errors and comparison of the adjusted data to the population of flaws assumed in the PFM technical basis for the Alternate PTS Rule

(6) criteria related to alternate screening criteria on embrittlement

Guidance is provided by which licensees can estimate a plant-specific value of TWCF for cases that do not satisfy the RT_{MAX-X} screening criteria of the Alternate PTS Rule. Chapter 7 of this document describes these two sets of guidance to enable licensees to satisfy the embrittlement acceptability criteria.

This document provides guidance and the associated technical basis for methods by which licensees can satisfy the above criteria.

9 REFERENCES

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APPENDIX A DERIVATION OF THE STATISTICAL TEST FOR TYPE D DEVIATIONS

The value C_2 is defined so that the probability that all the normalized residuals are less than C_2 is 1 - α = 0.99, assuming that the embrittlement shift model is correct. Under this assumption, the normalized residuals all have a standard normal distribution with a mean of 0 and standard deviation of 1. The cumulative distribution function of the standard normal distribution, denoted by F, is then:

$$C_2 = F^{-1}\,(0.99)^{1/n} \qquad \text{A-1}$$

For any n and C_2 as determined above, define:

$$p = \text{Prob}\,\{C_1 < X \le C_2\} \qquad \text{A-2}$$

for any $C_1 < C_2$ and where X has a standard normal distribution, then:

$$1\text{-}p = \text{Prob}\,\{X \le C_1\} + \text{Prob}\,\{X > C_2\} \qquad \text{A-3}$$

However, the second term in (1-p) is negligible compared to the first term. In fact, from Table 5-4 in the main body of the text, $C_2 \ge 2.71$ for $n \ge 3$ and, therefore, Prob $\{X > C_2\} < 0.0034$ for $n \ge 3$. Thus, the following equation applies:

$$1\text{-}p \approx \text{Prob}\,\{X \le C_1\} \qquad \text{A-4}$$

The probability that the subject dataset does not show a Type D deviation can be expressed in terms of p. Because all of the n normalized residuals should be less than or equal to C_1 to pass the Outlier Test, the following may be written:

$$\text{Prob}\,\{x_{[1]} \le C_1\} = (1\text{-}p)^n \qquad \text{A-5}$$

In addition, the outlier test indicates that it is acceptable to have a single normalized residual between C_1 and C_2 while the other (n – 1) normalized residuals are all less than C_1. Therefore, the following equation applies:

$$\text{Prob}\,\{x_{[2]} < C_1 \le x_{[1]} \le C_2\} = np\,(1\text{-}p)^{n-1} \qquad \text{A-6}$$

Because A-5 and A-6 are mutually exclusive, the sum of their probabilities is the probability of a Type D deviation, or 1 - α = 0.99. This sum, denoted by G(p), is as follows:

$$G(p) = (1\text{-}p)^n + np\,(1\text{-}p)^{n-1} = (1\text{-}p)^{n-1}\,[1 + (n\text{-}1)p] \qquad \text{A-7}$$

By iteration, the value p_0 may be found that yields $G(p_0) = 0.99$. To calculate C_1 in Table 5-4, Prob $\{X \le C_1\}$ is set to $1\text{-}p_0$. The following equation then applies:

$$C_1 = F^{-1}\,(1\text{-}p_0) \qquad \text{A-8}$$

APPENDIX B REGULATORY ASSESSMENT OF STATISTICAL SURVEILANCE TESTS

Note that this appendix summarizes the evaluations provided for review only; they were performed to evaluate the proposed statistical surveillance tests. These calculations do not include an assessment of sister plant data, the licensee should not view them as a replacement of licensing-basis evaluations for each plant, and they do not represent the U.S. Nuclear Regulatory Commission's official position.

Table B-1 Type A Deviations (Mean Test)

General Information							Type A Deviation (Mean Test)		
Plant Name	**Unit**	**Reactor Type**	**Heat**	**Product Form**	**n**	**σ (ºF)**	**r_{mean} (ºF)**	**r_{max} (ºF)**	**Fails Test?**
Arkansas Nuclear	1	PWR	PAN101	P	6	21	-13	20	No
Arkansas Nuclear	1	PWR	WAN101	W	3	26	6	36	No
Arkansas Nuclear	2	PWR	PAN201	P	3	21	-3	29	No
Beaver Valley	1	PWR	PBV101	P	8	21	23.0	17.5	Yes
Beaver Valley	1	PWR	WBV101	W	4	26	-3	31	No
Beaver Valley	2	PWR	PBV201	P	6	19	-7	18	No
Beaver Valley	2	PWR	WBV201	W	3	26	-37	36	No
Braidwood	1	PWR	FBD101	F	6	19	-7	18	No
Braidwood	1	PWR	WBD101	W	3	19	3	25	No
Braidwood	2	PWR	FBD201	F	6	19	-9	18	No
Braidwood	2	PWR	WBD201	W	3	19	-8	25	No
Brunswick	1	BWR	PBR_01	P	5	21	31.3	22.1	Yes
Brunswick	1	BWR	WBR_01	W	3	26	35	36	No
Byron	1	PWR	FBY101	F	6	19	15	18	No
Byron	1	PWR	WBY101	W	3	19	0	25	No
Byron	2	PWR	FBY201	F	6	19	-5	18	No
Byron	2	PWR	WBY201	W	3	19	-1	25	No
Callaway		PWR	PCL101	P	8	19	-2	15	No
Callaway		PWR	WCL101	W	4	19	27.0	21.7	Yes
Calvert Cliffs	1	PWR	PCC103	P	3	21	-6	29	No
Calvert Cliffs	1	PWR	WCC101	W	3	26	-17	36	No

General Information							Type A Deviation (Mean Test)		
Plant Name	Unit	Reactor Type	Heat	Product Form	n	σ (ºF)	r_{mean} (ºF)	r_{max} (ºF)	Fails Test?
Calvert Cliffs	2	PWR	PCC202	P	3	21	-7	29	No
Catawba	1	PWR	FCB101	F	6	20	-16	19	No
Catawba	1	PWR	WCB101	W	3	19	-8	25	No
Catawba	2	PWR	PCB201	P	6	21	-1	20	No
Catawba	2	PWR	WCB201	W	3	19	1	25	No
Commanche Peak	1	PWR	PCP101	P	4	19	-5	22	No
Connecticut Yankee		ex-PWR	PCTY04	P	3	21	-4	29	No
Connecticut Yankee		ex-PWR	PCTY02	P	3	21	-13	29	No
Crystal River	3	PWR	PCR301	P	4	21	17	25	No
Crystal River	3	PWR	WCR301	W	4	26	12	31	No
Crystal River	3	PWR	WHSS66	W	4	26	-20	31	No
Crystal River	3	PWR	WHSSCR	W	3	26	-6	36	No
Crystal River & Surry	3 & 2	PWR	WHSS65	W	3	26	3	36	No
D.C. Cook	1	PWR	PCK101	P	8	21	-4	17	No
D.C. Cook	1	PWR	WCK101	W	3	26	-103	36	No
D.C. Cook	2	PWR	PCK201	P	8	21	24.6	17.5	Yes
D.C. Cook	2	PWR	WCK201	W	4	19	17	22	No
Davis Besse		PWR	FDB102	F	4	19	-7	22	No
Davis Besse		PWR	WDB101	W	5	26	1	28	No
Davis Besse		PWR	PRS101	P	3	21	-6	29	No
Davis Besse		PWR	WRS101	W	3	26	-14	36	No
Diablo Canyon	1	PWR	PDC103	P	3	21	-24	29	No
Diablo Canyon	1	PWR	WDC101	W	3	26	-2	36	No
Diablo Canyon	2	PWR	PDC201	P	8	21	-5	17	No
Diablo Canyon	2	PWR	WDC201	W	4	26	-3	31	No
Dresden	3	BWR	WDR302	W	3	26	-17	36	No
Dresden	2	BWR	PDR201	P	5	21	-32	22	No
Dresden	3	BWR	PDR301	P	6	21	-10	20	No
Dresden	3	BWR	WDR301	W	5	26	-5	28	No
Duane Arnold		BWR	PDAC01	P	3	21	10	29	No
Duane Arnold		BWR	WDAC01	W	3	19	-4	25	No

General Information							Type A Deviation (Mean Test)		
Plant Name	Unit	Reactor Type	Heat	Product Form	n	σ (°F)	r_{mean} (°F)	r_{max} (°F)	Fails Test?
Farley	1	PWR	PFA101	P	8	21	13	17	No
Farley	1	PWR	WFA101	W	4	26	-7	31	No
Farley	2	PWR	PFA201	P	8	21	15	17	No
Farley	2	PWR	WFA201	W	4	19	-51	22	No
FitzPatrick		BWR	PFTZ01	P	6	21	-11	20	No
Fort Calhoun		PWR	PFC101	P	5	21	-10	22	No
Fort Calhoun		PWR	WFC101	W	4	26	-1	31	No
Ginna		PWR	FGIN02	F	4	19	-18	22	No
Ginna		PWR	FGIN01	F	4	19	17	22	No
Ginna		PWR	WGIN01	W	4	26	13	31	No
H.B. Robinson	2	PWR	WHB201	W	3	26	6	36	No
Indian Point	2	PWR	PIP202	P	3	21	-1	29	No
Indian Point	2	PWR	PIP203	P	3	21	32.6	28.5	Yes
Indian Point	3	PWR	PIP304	P	5	21	13	22	No
Indian Point	3	PWR	WIP301	W	3	26	33	36	No
Kewaunee		PWR	FKWE02	F	4	19	-7	22	No
Kewaunee		PWR	FKWE01	F	4	19	-9	22	No
Kewaunee		PWR	WKWE01	W	4	26	16	31	No
Maine Yankee		ex-PWR	PMY_01	P	6	21	28.5	20.2	Yes
Maine Yankee		ex-PWR	SHSS01	SRM	17	21	1	12	No
Maine Yankee		ex-PWR	WMY_01	W	4	26	-8	31	No
McGuire	1	PWR	PMC101	P	8	21	13	17	No
McGuire	1	PWR	WMC101	W	4	26	-11	31	No
McGuire	2	PWR	FMC201	F	8	20	1	16	No
McGuire	2	PWR	WMC201	W	4	19	3	22	No
Millstone	1	ex-BWR	PML101	P	4	21	-6	25	No
Millstone	2	PWR	PML201	P	5	21	13	22	No
Millstone	2	PWR	WML201	W	3	26	-27	36	No
Nine Mile Point	1	BWR	PNM101	P	5	21	-10	22	No
North Anna	1	PWR	FNA101	F	6	20	-14	19	No
North Anna	1	PWR	WNA101	W	3	26	21	36	No

General Information							Type A Deviation (Mean Test)		
Plant Name	**Unit**	**Reactor Type**	**Heat**	**Product Form**	**n**	**σ (°F)**	**r_{mean} (°F)**	**r_{max} (°F)**	**Fails Test?**
North Anna	2	PWR	FNA201	F	6	20	-18	19	No
North Anna	2	PWR	WNA201	W	3	26	-23	36	No
Oconee	1	PWR	POC102	P	6	21	5	20	No
Oconee	1	PWR	SHSS02	SRM	64	21	-14	6	No
Oconee	1	PWR	WOC101	W	3	26	5	36	No
Oconee	2	PWR	FOC201	F	5	19	-3	19	No
Oconee	2	PWR	WOC201	W	3	26	-23	36	No
Oconee	3	PWR	FOC301	F	4	19	2	22	No
Oconee	3	PWR	FOC302	F	3	19	21	25	No
Oconee	3	PWR	WOC301	W	4	26	-28	31	No
Oyster Creek		BWR	PGG_01	P	4	19	2	22	No
Oyster Creek		BWR	PCPR02	P	4	21	-3	25	No
Oyster Creek		BWR	PEP2JP	P	5	19	-3	19	No
Oyster Creek		BWR	WGG_01	W	4	19	-8	22	No
Oyster Creek		BWR	WML101	W	6	26	-23	25	No
Oyster Creek		BWR	WQC102_1	W	4	26	26	31	No
Oyster Creek		BWR	WQC201_1	W	4	26	17	31	No
Oyster Creek		BWR	WRB_01	W	3	19	34.6	25.0	Yes
Palisades		PWR	PPAL01	P	7	21	-33	19	No
Palisades		PWR	WPAL01	W	4	26	-5	31	No
Point Beach	2	PWR	FPB202	F	4	20	19	23	No
Point Beach	1	PWR	PPB102	P	4	21	-28	25	No
Point Beach	1	PWR	PPB101	P	4	21	9	25	No
Point Beach	1	PWR	WPB101	W	4	26	-42	31	No
Point Beach	2	PWR	FPB201	F	4	19	16	22	No
Point Beach	2	PWR	WPB201	W	4	26	6	31	No
Prarie Island	1	PWR	FPI101	F	8	19	-2	15	No
Prarie Island	1	PWR	WPI101	W	4	26	-19	31	No
Prarie Island	2	PWR	FPI201	F	8	20	-4	16	No
Prarie Island	2	PWR	WPI201	W	4	26	-11	31	No
Quad Cities	1	BWR	PQC101	P	6	21	1	20	No

General Information							Type A Deviation (Mean Test)		
Plant Name	**Unit**	**Reactor Type**	**Heat**	**Product Form**	**n**	**σ (ºF)**	**r_{mean} (ºF)**	**r_{max} (ºF)**	**Fails Test?**
Quad Cities	1	BWR	WQC101	W	4	26	-16	31	No
Quad Cities	2	BWR	PQC201	P	4	21	-18	25	No
Quad Cities	2	BWR	WQC201	W	4	26	18	31	No
Saint Lucie	1	PWR	PSL101	P	5	21	-19	22	No
Saint Lucie	1	PWR	WSL101	W	3	26	-18	36	No
Saint Lucie	2	PWR	PSL201	P	3	21	14	29	No
Salem	1	PWR	PSA103	P	3	21	-30	29	No
Salem	1	PWR	PSA101	P	3	21	6	29	No
Salem	2	PWR	PSA201	P	8	21	10	17	No
Salem	2	PWR	WSA201	W	4	26	-18	31	No
San Onofre	2	PWR	PSO201	P	3	21	-7	29	No
San Onofre	3	PWR	PSO301	P	3	19	40.1	25.0	Yes
Seabrook	1	PWR	PSB101	P	4	19	19	22	No
Sequoyah	1	PWR	FSQ101	F	8	20	18.3	16.1	Yes
Sequoyah	1	PWR	WSQ101	W	4	26	32.4	30.8	Yes
Sequoyah	2	PWR	FSQ201	F	8	20	7	16	No
Sequoyah	2	PWR	WSQ201	W	4	26	23	31	No
South Texas	1	PWR	PST101	P	4	19	3	22	No
South Texas	2	PWR	PST201	P	4	19	4	22	No
Surry	1	PWR	PSU101	P	3	21	5	29	No
Surry	1	PWR	WSU101	W	3	26	43.5	35.5	Yes
Surry	2	PWR	PSU201	P	6	21	0	20	No
Surry	2	PWR	WSU201	W	3	26	-14	36	No
Three Mile Island	1	PWR	PTM101	P	3	21	-17	29	No
Trojan		ex-PWR	PTRO01	P	6	21	1	20	No
Trojan		ex-PWR	WTRO01	W	3	19	8	25	No
Turkey Point	3	PWR	FTP302	F	3	20	10	26	No
Turkey Point	3	PWR	SASTM	SRM	26	21	5	10	No
Turkey Point	3	PWR	WTP301	W	4	26	13	31	No
Virgil Summer	1	PWR	PVS101	P	8	21	-20	17	No
Virgil Summer	1	PWR	WVS101	W	4	19	0	22	No

General Information							Type A Deviation (Mean Test)		
Plant Name	Unit	Reactor Type	Heat	Product Form	n	σ (ºF)	r_{mean} (ºF)	r_{max} (ºF)	Fails Test?
Vogtle	1	PWR	PVO101	P	6	19	-1	18	No
Vogtle	1	PWR	WVO101	W	3	19	-4	25	No
Vogtle	2	PWR	PVO201	P	6	19	-14	18	No
Vogtle	2	PWR	WVO201	W	3	19	-13	25	No
Waterford	3	PWR	PWF301	P	3	19	-13	25	No
Watts Bar	1	PWR	FWB101	F	4	20	-6	23	No
Wolf Creek	1	PWR	PWC101	P	8	19	8	15	No
Wolf Creek	1	PWR	WWC101	W	4	19	17	22	No
Zion	1	ex-PWR	PZN101	P	8	21	-2	17	No
Zion	1	ex-PWR	WZN101	W	5	26	-6	28	No
Zion	2	ex-PWR	PZN201	P	6	21	3	20	No
Zion	2	ex-PWR	WZN201	W	3	26	3	36	No

Table B-2 Type B Deviations (Slope Test)

General Information							Type B Deviation (Slope Test)				
Plant Name	Unit	Reactor Type	Heat	Product Form	n	σ (°F)	m	se(m)	T_m	$T_{crit(\alpha)}$	Fails Test?
Arkansas Nuclear	1	PWR	PAN101	P	6	21	-26.06	10.09	-2.58	3.75	No
Arkansas Nuclear	1	PWR	WAN101	W	3	26	-37.69	19.02	-1.98	31.82	No
Arkansas Nuclear	2	PWR	PAN201	P	3	21	-5.72	16.85	-0.34	31.82	No
Beaver Valley	1	PWR	PBV101	P	8	21	-37.91	21.46	-1.77	3.14	No
Beaver Valley	1	PWR	WBV101	W	4	26	-56.91	15.54	-3.66	6.96	No
Beaver Valley	2	PWR	PBV201	P	6	19	4.78	6.63	0.72	3.75	No
Beaver Valley	2	PWR	WBV201	W	3	26	-50.14	20.08	-2.50	31.82	No
Braidwood	1	PWR	FBD101	F	6	19	26.30	21.44	1.23	3.75	No
Braidwood	1	PWR	WBD101	W	3	19	8.25	8.49	0.97	31.82	No
Braidwood	2	PWR	FBD201	F	6	19	14.24	22.91	0.62	3.75	No
Braidwood	2	PWR	WBD201	W	3	19	6.66	19.20	0.35	31.82	No
Brunswick	1	BWR	PBR_01	P	5	21	67.73	13.28	5.10	4.54	Yes
Brunswick	1	BWR	WBR_01	W	3	26	41.69	45.09	0.92	31.82	No
Byron	1	PWR	FBY101	F	6	19	7.34	15.79	0.46	3.75	No
Byron	1	PWR	WBY101	W	3	19	26.54	8.12	3.27	31.82	No
Byron	2	PWR	FBY201	F	6	19	0.03	19.60	0.00	3.75	No
Byron	2	PWR	WBY201	W	3	19	27.60	8.32	3.32	31.82	No
Callaway		PWR	PCL101	P	8	19	-8.04	14.97	-0.54	3.14	No
Callaway		PWR	WCL101	W	4	19	-41.68	12.80	-3.26	6.96	No
Calvert Cliffs	1	PWR	PCC103	P	3	21	13.74	2.75	4.99	31.82	No
Calvert Cliffs	1	PWR	WCC101	W	3	26	37.90	2.00	18.95	31.82	No
Calvert Cliffs	2	PWR	PCC202	P	3	21	11.27	12.00	0.94	31.82	No
Catawba	1	PWR	FCB101	F	6	20	24.31	20.63	1.18	3.75	No
Catawba	1	PWR	WCB101	W	3	19	7.91	2.47	3.20	31.82	No
Catawba	2	PWR	PCB201	P	6	21	0.93	10.27	0.09	3.75	No
Catawba	2	PWR	WCB201	W	3	19	91.48	9.59	9.54	31.82	No
Comanche Peak	1	PWR	PCP101	P	4	19	-19.21	15.89	-1.21	6.96	No
Connecticut Yankee		ex-PWR	PCTY04	P	3	21	-63.22	2.55	-24.79	31.82	No
Connecticut Yankee		ex-PWR	PCTY02	P	3	21	-47.44	1.52	-31.24	31.82	No
Crystal River	3	PWR	PCR301	P	4	21	22.02	11.98	1.84	6.96	No

General Information							Type B Deviation (Slope Test)				
Plant Name	Unit	Reactor Type	Heat	Product Form	n	σ (ºF)	m	se(m)	T_m	$T_{crit(\alpha)}$	Fails Test?
Crystal River	3	PWR	WCR301	W	4	26	46.92	13.65	3.44	6.96	No
Crystal River	3	PWR	WHSS66	W	4	26	-110.03	117.85	-0.93	6.96	No
Crystal River	3	PWR	WHSSCR	W	3	26	-116.65	31.01	-3.76	31.82	No
Crystal River & Surry	3 & 2	PWR	WHSS65	W	3	26	2.10	14.59	0.14	31.82	No
D.C. Cook	1	PWR	PCK101	P	8	21	-8.31	11.44	-0.73	3.14	No
D.C. Cook	1	PWR	WCK101	W	3	26	-27.17	98.72	-0.28	31.82	No
D.C. Cook	2	PWR	PCK201	P	8	21	1.58	17.98	0.09	3.14	No
D.C. Cook	2	PWR	WCK201	W	4	19	-14.88	17.64	-0.84	6.96	No
Davis Besse		PWR	FDB102	F	4	19	33.72	23.70	1.42	6.96	No
Davis Besse		PWR	WDB101	W	5	26	10.23	58.55	0.17	4.54	No
Davis Besse		PWR	PRS101	P	3	21	19.87	18.23	1.09	31.82	No
Davis Besse		PWR	WRS101	W	3	26	24.78	24.12	1.03	31.82	No
Diablo Canyon	1	PWR	PDC103	P	3	21	-2.29	33.31	-0.07	31.82	No
Diablo Canyon	1	PWR	WDC101	W	3	26	23.50	74.96	0.31	31.82	No
Diablo Canyon	2	PWR	PDC201	P	8	21	-1.49	7.64	-0.19	3.14	No
Diablo Canyon	2	PWR	WDC201	W	4	26	-34.17	7.34	-4.66	6.96	No
Dresden	3	BWR	WDR302	W	3	26	-25.60	231.23	-0.11	31.82	No
Dresden	2	BWR	PDR201	P	5	21	2.15	5.51	0.39	4.54	No
Dresden	3	BWR	PDR301	P	6	21	-2.52	4.90	-0.51	3.75	No
Dresden	3	BWR	WDR301	W	5	26	7.60	7.66	0.99	4.54	No
Duane Arnold		BWR	PDAC01	P	3	21	-2.02	13.71	-0.15	31.82	No
Duane Arnold		BWR	WDAC01	W	3	19	20.21	6.54	3.09	31.82	No
Farley	1	PWR	PFA101	P	8	21	21.46	8.51	2.52	3.14	No
Farley	1	PWR	WFA101	W	4	26	-27.48	10.40	-2.64	6.96	No
Farley	2	PWR	PFA201	P	8	21	20.33	15.54	1.31	3.14	No
Farley	2	PWR	WFA201	W	4	19	-25.24	19.69	-1.28	6.96	No
FitzPatrick		BWR	PFTZ01	P	6	21	8.83	10.75	0.82	3.75	No
Fort Calhoun		PWR	PFC101	P	5	21	-22.33	33.89	-0.66	4.54	No
Fort Calhoun		PWR	WFC101	W	4	26	-73.25	49.46	-1.48	6.96	No
Ginna		PWR	FGIN02	F	4	19	39.26	74.20	0.53	6.96	No
Ginna		PWR	FGIN01	F	4	19	-33.49	29.11	-1.15	6.96	No
Ginna		PWR	WGIN01	W	4	26	13.77	24.57	0.56	6.96	No

General Information							Type B Deviation (Slope Test)				
Plant Name	Unit	Reactor Type	Heat	Product Form	n	σ (ºF)	m	se(m)	T_m	$T_{crit(\alpha)}$	Fails Test?
H.B. Robinson	2	PWR	WHB201	W	3	26	7.86	33.97	0.23	31.82	No
Indian Point	2	PWR	PIP202	P	3	21	-59.41	46.88	-1.27	31.82	No
Indian Point	2	PWR	PIP203	P	3	21	-17.19	2.14	-8.05	31.82	No
Indian Point	3	PWR	PIP304	P	5	21	2.30	29.72	0.08	4.54	No
Indian Point	3	PWR	WIP301	W	3	26	-0.18	79.92	0.00	31.82	No
Kewaunee		PWR	FKWE02	F	4	19	5.09	6.32	0.81	6.96	No
Kewaunee		PWR	FKWE01	F	4	19	-3.54	28.08	-0.13	6.96	No
Kewaunee		PWR	WKWE01	W	4	26	-15.96	19.26	-0.83	6.96	No
Maine Yankee		ex-PWR	PMY_01	P	6	21	-6.49	15.82	-0.41	3.75	No
Maine Yankee		ex-PWR	SHSS01	SRM	17	21	-4.95	15.22	-0.33	2.60	No
Maine Yankee		ex-PWR	WMY_01	W	4	26	10.14	12.08	0.84	6.96	No
McGuire	1	PWR	PMC101	P	8	21	24.92	19.19	1.30	3.14	No
McGuire	1	PWR	WMC101	W	4	26	-43.26	13.24	-3.27	6.96	No
McGuire	2	PWR	FMC201	F	8	20	4.68	13.50	0.35	3.14	No
McGuire	2	PWR	WMC201	W	4	19	-34.72	13.01	-2.67	6.96	No
Millstone	1	ex-BWR	PML101	P	4	21	-46.63	28.45	-1.64	6.96	No
Millstone	2	PWR	PML201	P	5	21	23.17	31.56	0.73	4.54	No
Millstone	2	PWR	WML201	W	3	26	-56.09	3.80	-14.77	31.82	No
Nine Mile Point	1	BWR	PNM101	P	5	21	41.45	22.11	1.87	4.54	No
North Anna	1	PWR	FNA101	F	6	20	8.37	20.75	0.40	3.75	No
North Anna	1	PWR	WNA101	W	3	26	-40.22	70.03	-0.57	31.82	No
North Anna	2	PWR	FNA201	F	6	20	18.17	12.92	1.41	3.75	No
North Anna	2	PWR	WNA201	W	3	26	-5.18	23.10	-0.22	31.82	No
Oconee	1	PWR	POC102	P	6	21	-19.62	25.32	-0.77	3.75	No
Oconee	1	PWR	SHSS02	SRM	64	21	1.87	4.39	0.43	2.39	No
Oconee	1	PWR	WOC101	W	3	26	41.08	14.09	2.92	31.82	No
Oconee	2	PWR	FOC201	F	5	19	-15.62	13.86	-1.13	4.54	No
Oconee	2	PWR	WOC201	W	3	26	30.52	12.69	2.41	31.82	No
Oconee	3	PWR	FOC301	F	4	19	-2.79	5.78	-0.48	6.96	No
Oconee	3	PWR	FOC302	F	3	19	-21.76	32.80	-0.66	31.82	No
Oconee	3	PWR	WOC301	W	4	26	41.81	33.82	1.24	6.96	No
Oyster Creek		BWR	PGG_01	P	4	19	21.14	22.39	0.94	6.96	No

General Information							Type B Deviation (Slope Test)				
Plant Name	Unit	Reactor Type	Heat	Product Form	n	σ (ºF)	m	se(m)	T_m	$T_{crit(\alpha)}$	Fails Test?
Oyster Creek		BWR	PCPR02	P	4	21	-8.62	42.21	-0.20	6.96	No
Oyster Creek		BWR	PEP2JP	P	5	19	-32.14	8.29	-3.88	4.54	No
Oyster Creek		BWR	WGG_01	W	4	19	39.71	61.15	0.65	6.96	No
Oyster Creek		BWR	WML101	W	6	26	10.03	20.07	0.50	3.75	No
Oyster Creek		BWR	WQC102_1	W	4	26	6.48	11.60	0.56	6.96	No
Oyster Creek		BWR	WQC201_1	W	4	26	57.46	59.89	0.96	6.96	No
Oyster Creek		BWR	WRB_01	W	3	19	20.94	63.55	0.33	31.82	No
Palisades		PWR	PPAL01	P	7	21	-77.49	15.02	-5.16	3.36	No
Palisades		PWR	WPAL01	W	4	26	-42.23	5.32	-7.93	6.96	No
Point Beach	2	PWR	FPB202	F	4	20	41.30	12.36	3.34	6.96	No
Point Beach	1	PWR	PPB102	P	4	21	-76.91	8.77	-8.77	6.96	No
Point Beach	1	PWR	PPB101	P	4	21	-55.54	23.06	-2.41	6.96	No
Point Beach	1	PWR	WPB101	W	4	26	-12.46	53.53	-0.23	6.96	No
Point Beach	2	PWR	FPB201	F	4	19	-0.70	8.03	-0.09	6.96	No
Point Beach	2	PWR	WPB201	W	4	26	38.35	27.60	1.39	6.96	No
Prarie Island	1	PWR	FPI101	F	8	19	-0.54	17.08	-0.03	3.14	No
Prarie Island	1	PWR	WPI101	W	4	26	57.84	38.91	1.49	6.96	No
Prarie Island	2	PWR	FPI201	F	8	20	8.36	9.37	0.89	3.14	No
Prarie Island	2	PWR	WPI201	W	4	26	-40.19	12.22	-3.29	6.96	No
Quad Cities	1	BWR	PQC101	P	6	21	7.70	2.14	3.59	3.75	No
Quad Cities	1	BWR	WQC101	W	4	26	10.12	7.81	1.30	6.96	No
Quad Cities	2	BWR	PQC201	P	4	21	-10.04	3.17	-3.17	6.96	No
Quad Cities	2	BWR	WQC201	W	4	26	-3.89	4.21	-0.92	6.96	No
Saint Lucie	1	PWR	PSL101	P	5	21	-5.59	16.17	-0.35	4.54	No
Saint Lucie	1	PWR	WSL101	W	3	26	-46.07	12.84	-3.59	31.82	No
Saint Lucie	2	PWR	PSL201	P	3	21	49.57	1.95	25.45	31.82	No
Salem	1	PWR	PSA103	P	3	21	-6.76	19.49	-0.35	31.82	No
Salem	1	PWR	PSA101	P	3	21	5.06	24.98	0.20	31.82	No
Salem	2	PWR	PSA201	P	8	21	-3.87	21.39	-0.18	3.14	No
Salem	2	PWR	WSA201	W	4	26	-45.51	9.34	-4.87	6.96	No
San Onofre	2	PWR	PSO201	P	3	21	11.38	26.39	0.43	31.82	No
San Onofre	3	PWR	PSO301	P	3	19	15.75	21.22	0.74	31.82	No

General Information							Type B Deviation (Slope Test)				
Plant Name	Unit	Reactor Type	Heat	Product Form	n	σ (ºF)	m	se(m)	T_m	$T_{crit(\alpha)}$	Fails Test?
Seabrook	1	PWR	PSB101	P	4	19	-6.15	14.03	-0.44	6.96	No
Sequoyah	1	PWR	FSQ101	F	8	20	31.83	17.01	1.87	3.14	No
Sequoyah	1	PWR	WSQ101	W	4	26	-8.36	4.54	-1.84	6.96	No
Sequoyah	2	PWR	FSQ201	F	8	20	12.09	14.40	0.84	3.14	No
Sequoyah	2	PWR	WSQ201	W	4	26	-71.71	89.12	-0.80	6.96	No
South Texas	1	PWR	PST101	P	4	19	-9.15	21.18	-0.43	6.96	No
South Texas	2	PWR	PST201	P	4	19	16.33	4.60	3.55	6.96	No
Surry	1	PWR	PSU101	P	3	21	10.46	20.36	0.51	31.82	No
Surry	1	PWR	WSU101	W	3	26	9.51	7.62	1.25	31.82	No
Surry	2	PWR	PSU201	P	6	21	-2.98	13.63	-0.22	3.75	No
Surry	2	PWR	WSU201	W	3	26	7.37	24.69	0.30	31.82	No
Three Mile Island	1	PWR	PTM101	P	3	21	-41.07	2.89	-14.23	31.82	No
Trojan		ex-PWR	PTRO01	P	6	21	-2.31	12.00	-0.19	3.75	No
Trojan		ex-PWR	WTRO01	W	3	19	-14.97	10.82	-1.38	31.82	No
Turkey Point	3	PWR	FTP302	F	3	20	52.36	70.45	0.74	31.82	No
Turkey Point	3	PWR	SASTM	SRM	26	21	10.59	8.87	1.19	2.49	No
Turkey Point	3	PWR	WTP301	W	4	26	15.55	35.61	0.44	6.96	No
Virgil Summer	1	PWR	PVS101	P	8	21	-12.14	16.33	-0.74	3.14	No
Virgil Summer	1	PWR	WVS101	W	4	19	-20.29	23.75	-0.85	6.96	No
Vogtle	1	PWR	PVO101	P	6	19	20.85	19.05	1.09	3.75	No
Vogtle	1	PWR	WVO101	W	3	19	-41.81	19.81	-2.11	31.82	No
Vogtle	2	PWR	PVO201	P	6	19	15.57	10.12	1.54	3.75	No
Vogtle	2	PWR	WVO201	W	3	19	25.29	19.30	1.31	31.82	No
Waterford	3	PWR	PWF301	P	3	19	-87.52	64.25	-1.36	31.82	No
Watts Bar	1	PWR	FWB101	F	4	20	41.28	90.57	0.46	6.96	No
Wolf Creek	1	PWR	PWC101	P	8	19	-8.38	9.54	-0.88	3.14	No
Wolf Creek	1	PWR	WWC101	W	4	19	4.70	8.95	0.53	6.96	No
Zion	1	ex-PWR	PZN101	P	8	21	14.89	14.97	0.99	3.14	No
Zion	1	ex-PWR	WZN101	W	5	26	43.23	8.52	5.07	4.54	Yes
Zion	2	ex-PWR	PZN201	P	6	21	19.41	15.57	1.25	3.75	No
Zion	2	ex-PWR	WZN201	W	3	26	17.59	31.94	0.55	31.82	No

Table B-3 Type D Deviations (utlier Test)

General Information							Type D Deviation (Outlier Test)				
Plant Name	Unit	Reactor Type	Heat	Product Form	n	σ (°F)	$r_{i(max1)}$	$r_{i(max2)}$	C_1	C_2	Fails Test?
Arkansas Nuclear	1	PWR	PAN101	P	6	21	0.98	-0.13	1.93	2.93	No
Arkansas Nuclear	1	PWR	WAN101	W	3	26	1.47	0.03	1.55	2.71	No
Arkansas Nuclear	2	PWR	PAN201	P	3	21	0.36	-0.32	1.55	2.71	No
Beaver Valley	1	PWR	PBV101	P	8	21	2.52	2.26	2.05	3.02	Yes
Beaver Valley	1	PWR	WBV101	W	4	26	0.83	0.14	1.73	2.81	No
Beaver Valley	2	PWR	PBV201	P	6	19	-0.04	-0.06	1.93	2.93	No
Beaver Valley	2	PWR	WBV201	W	3	26	-0.61	-1.39	1.55	2.71	No
Braidwood	1	PWR	FBD101	F	6	19	0.41	0.23	1.93	2.93	No
Braidwood	1	PWR	WBD101	W	3	19	0.42	0.03	1.55	2.71	No
Braidwood	2	PWR	FBD201	F	6	19	0.85	0.41	1.93	2.93	No
Braidwood	2	PWR	WBD201	W	3	19	0.04	-0.59	1.55	2.71	No
Brunswick	1	BWR	PBR_01	P	5	21	4.09	2.99	1.84	2.88	Yes
Brunswick	1	BWR	WBR_01	W	3	26	2.56	1.53	1.55	2.71	No
Byron	1	PWR	FBY101	F	6	19	1.67	1.58	1.93	2.93	No
Byron	1	PWR	WBY101	W	3	19	0.38	0.37	1.55	2.71	No
Byron	2	PWR	FBY201	F	6	19	0.46	0.36	1.93	2.93	No
Byron	2	PWR	WBY201	W	3	19	0.59	-0.10	1.55	2.71	No
Callaway		PWR	PCL101	P	8	19	1.06	0.70	2.05	3.02	No
Callaway		PWR	WCL101	W	4	19	3.03	0.98	1.73	2.81	Yes
Calvert Cliffs	1	PWR	PCC103	P	3	21	-0.10	-0.19	1.55	2.71	No
Calvert Cliffs	1	PWR	WCC101	W	3	26	-0.14	-0.71	1.55	2.71	No
Calvert Cliffs	2	PWR	PCC202	P	3	21	-0.14	-0.38	1.55	2.71	No
Catawba	1	PWR	FCB101	F	6	20	0.14	0.05	1.93	2.93	No
Catawba	1	PWR	WCB101	W	3	19	-0.27	-0.46	1.55	2.71	No
Catawba	2	PWR	PCB201	P	6	21	0.30	0.26	1.93	2.93	No
Catawba	2	PWR	WCB201	W	3	19	1.75	0.74	1.55	2.71	No
Comanche Peak	1	PWR	PCP101	P	4	19	0.38	-0.15	1.73	2.81	No
Connecticut Yankee		ex-PWR	PCTY04	P	3	21	1.02	-0.60	1.55	2.71	No
Connecticut Yankee		ex-PWR	PCTY02	P	3	21	0.17	-0.45	1.55	2.71	No
Crystal River	3	PWR	PCR301	P	4	21	1.46	1.03	1.73	2.81	No

General Information							Type D Deviation (Outlier Test)				
Plant Name	Unit	Reactor Type	Heat	Product Form	n	σ (ºF)	$r_{i(max1)}$	$r_{i(max2)}$	C_1	C_2	Fails Test?
Crystal River	3	PWR	WCR301	W	4	26	1.12	1.00	1.73	2.81	No
Crystal River	3	PWR	WHSS66	W	4	26	0.71	-0.78	1.73	2.81	No
Crystal River	3	PWR	WHSSCR	W	3	26	0.77	0.06	1.55	2.71	No
Crystal River & Surry	3 & 2	PWR	WHSS65	W	3	26	0.23	0.18	1.55	2.71	No
D.C. Cook	1	PWR	PCK101	P	8	21	0.57	0.28	2.05	3.02	No
D.C. Cook	1	PWR	WCK101	W	3	26	-2.30	-3.73	1.55	2.71	No
D.C. Cook	2	PWR	PCK201	P	8	21	2.27	1.68	2.05	3.02	No
D.C. Cook	2	PWR	WCK201	W	4	19	1.47	1.28	1.73	2.81	No
Davis Besse		PWR	FDB102	F	4	19	0.98	-0.60	1.73	2.81	No
Davis Besse		PWR	WDB101	W	5	26	2.01	0.32	1.84	2.88	No
Davis Besse		PWR	PRS101	P	3	21	-0.05	-0.12	1.55	2.71	No
Davis Besse		PWR	WRS101	W	3	26	-0.26	-0.36	1.55	2.71	No
Diablo Canyon	1	PWR	PDC103	P	3	21	-0.53	-1.24	1.55	2.71	No
Diablo Canyon	1	PWR	WDC101	W	3	26	1.14	-0.69	1.55	2.71	No
Diablo Canyon	2	PWR	PDC201	P	8	21	0.21	-0.04	2.05	3.02	No
Diablo Canyon	2	PWR	WDC201	W	4	26	0.54	-0.15	1.73	2.81	No
Dresden	3	BWR	WDR302	W	3	26	0.74	-1.02	1.55	2.71	No
Dresden	2	BWR	PDR201	P	5	21	-0.23	-1.56	1.84	2.88	No
Dresden	3	BWR	PDR301	P	6	21	0.49	-0.20	1.93	2.93	No
Dresden	3	BWR	WDR301	W	5	26	1.01	0.43	1.84	2.88	No
Duane Arnold		BWR	PDAC01	P	3	21	0.66	0.39	1.55	2.71	No
Duane Arnold		BWR	WDAC01	W	3	19	0.14	-0.32	1.55	2.71	No
Farley	1	PWR	PFA101	P	8	21	1.39	1.20	2.05	3.02	No
Farley	1	PWR	WFA101	W	4	26	0.38	-0.46	1.73	2.81	No
Farley	2	PWR	PFA201	P	8	21	1.92	1.22	2.05	3.02	No
Farley	2	PWR	WFA201	W	4	19	-2.12	-2.13	1.73	2.81	No
FitzPatrick		BWR	PFTZ01	P	6	21	-0.03	-0.16	1.93	2.93	No
Fort Calhoun		PWR	PFC101	P	5	21	0.03	-0.11	1.84	2.88	No
Fort Calhoun		PWR	WFC101	W	4	26	0.59	0.32	1.73	2.81	No
Ginna		PWR	FGIN02	F	4	19	1.35	-0.34	1.73	2.81	No
Ginna		PWR	FGIN01	F	4	19	2.19	1.10	1.73	2.81	No
Ginna		PWR	WGIN01	W	4	26	1.17	0.58	1.73	2.81	No

General Information							Type D Deviation (Outlier Test)				
Plant Name	Unit	Reactor Type	Heat	Product Form	n	σ (°F)	$r_{i(max1)}$	$r_{i(max2)}$	C_1	C_2	Fails Test?
H.B. Robinson	2	PWR	WHB201	W	3	26	0.96	0.05	1.55	2.71	No
Indian Point	2	PWR	PIP202	P	3	21	1.26	-0.57	1.55	2.71	No
Indian Point	2	PWR	PIP203	P	3	21	1.81	1.53	1.55	2.71	No
Indian Point	3	PWR	PIP304	P	5	21	1.41	1.11	1.84	2.88	No
Indian Point	3	PWR	WIP301	W	3	26	1.90	1.54	1.55	2.71	No
Kewaunee		PWR	FKWE02	F	4	19	-0.08	-0.43	1.73	2.81	No
Kewaunee		PWR	FKWE01	F	4	19	-0.04	-0.05	1.73	2.81	No
Kewaunee		PWR	WKWE01	W	4	26	1.10	0.74	1.73	2.81	No
Maine Yankee		ex-PWR	PMY_01	P	6	21	2.36	1.58	1.93	2.93	No
Maine Yankee		ex-PWR	SHSS01	SRM	17	21	1.48	0.96	2.37	3.24	No
Maine Yankee		ex-PWR	WMY_01	W	4	26	0.05	-0.12	1.73	2.81	No
McGuire	1	PWR	PMC101	P	8	21	1.98	1.16	2.05	3.02	No
McGuire	1	PWR	WMC101	W	4	26	0.54	-0.68	1.73	2.81	No
McGuire	2	PWR	FMC201	F	8	20	1.52	0.13	2.05	3.02	No
McGuire	2	PWR	WMC201	W	4	19	1.32	0.14	1.73	2.81	No
Millstone	1	ex-BWR	PML101	P	4	21	0.43	0.18	1.73	2.81	No
Millstone	2	PWR	PML201	P	5	21	1.94	1.09	1.84	2.88	No
Millstone	2	PWR	WML201	W	3	26	-0.27	-1.13	1.55	2.71	No
Nine Mile Point	1	BWR	PNM101	P	5	21	0.05	-0.24	1.84	2.88	No
North Anna	1	PWR	FNA101	F	6	20	0.88	-0.65	1.93	2.93	No
North Anna	1	PWR	WNA101	W	3	26	2.07	0.94	1.55	2.71	No
North Anna	2	PWR	FNA201	F	6	20	-0.12	-0.17	1.93	2.93	No
North Anna	2	PWR	WNA201	W	3	26	-0.59	-0.63	1.55	2.71	No
Oconee	1	PWR	POC102	P	6	21	1.53	1.41	1.93	2.93	No
Oconee	1	PWR	SHSS02	SRM	64	21	1.47	1.40	2.83	3.62	No
Oconee	1	PWR	WOC101	W	3	26	0.87	0.31	1.55	2.71	No
Oconee	2	PWR	FOC201	F	5	19	0.94	0.00	1.84	2.88	No
Oconee	2	PWR	WOC201	W	3	26	-0.09	-1.17	1.55	2.71	No
Oconee	3	PWR	FOC301	F	4	19	0.37	0.16	1.73	2.81	No
Oconee	3	PWR	FOC302	F	3	19	2.53	0.98	1.55	2.71	No
Oconee	3	PWR	WOC301	W	4	26	0.89	-1.03	1.73	2.81	No
Oyster Creek		BWR	PGG_01	P	4	19	0.23	-0.05	1.73	2.81	No

General Information							Type D Deviation (Outlier Test)				
Plant Name	Unit	Reactor Type	Heat	Product Form	n	σ (ºF)	$r_{i(max1)}$	$r_{i(max2)}$	C_1	C_2	Fails Test?
Oyster Creek		BWR	PCPR02	P	4	21	0.48	-0.17	1.73	2.81	No
Oyster Creek		BWR	PEP2JP	P	5	19	0.86	0.12	1.84	2.88	No
Oyster Creek		BWR	WGG_01	W	4	19	0.62	-0.32	1.73	2.81	No
Oyster Creek		BWR	WML101	W	6	26	0.07	-0.70	1.93	2.93	No
Oyster Creek		BWR	WQC102_1	W	4	26	1.14	1.02	1.73	2.81	No
Oyster Creek		BWR	WQC201_1	W	4	26	1.16	1.03	1.73	2.81	No
Oyster Creek		BWR	WRB_01	W	3	19	2.27	1.87	1.55	2.71	Yes
Palisades		PWR	PPAL01	P	7	21	0.11	-0.48	2	2.98	No
Palisades		PWR	WPAL01	W	4	26	0.21	0.07	1.73	2.81	No
Point Beach	2	PWR	FPB202	F	4	20	1.64	1.35	1.73	2.81	No
Point Beach	1	PWR	PPB102	P	4	21	-0.37	-0.52	1.73	2.81	No
Point Beach	1	PWR	PPB101	P	4	21	1.08	1.03	1.73	2.81	No
Point Beach	1	PWR	WPB101	W	4	26	-0.46	-1.58	1.73	2.81	No
Point Beach	2	PWR	FPB201	F	4	19	1.06	0.94	1.73	2.81	No
Point Beach	2	PWR	WPB201	W	4	26	0.00	0.00	1.73	2.81	No
Prarie Island	1	PWR	FPI101	F	8	19	0.77	0.77	2.05	3.02	No
Prarie Island	1	PWR	WPI101	W	4	26	0.89	-0.43	1.73	2.81	No
Prarie Island	2	PWR	FPI201	F	8	20	0.56	0.11	2.05	3.02	No
Prarie Island	2	PWR	WPI201	W	4	26	0.57	-0.47	1.73	2.81	No
Quad Cities	1	BWR	PQC101	P	6	21	0.74	0.60	1.93	2.93	No
Quad Cities	1	BWR	WQC101	W	4	26	0.63	-0.63	1.73	2.81	No
Quad Cities	2	BWR	PQC201	P	4	21	-0.11	-0.38	1.73	2.81	No
Quad Cities	2	BWR	WQC201	W	4	26	1.07	0.81	1.73	2.81	No
Saint Lucie	1	PWR	PSL101	P	5	21	-0.55	-0.72	1.84	2.88	No
Saint Lucie	1	PWR	WSL101	W	3	26	-0.28	-0.68	1.55	2.71	No
Saint Lucie	2	PWR	PSL201	P	3	21	2.02	-0.01	1.55	2.71	No
Salem	1	PWR	PSA103	P	3	21	-1.09	-1.33	1.55	2.71	No
Salem	1	PWR	PSA101	P	3	21	0.91	0.01	1.55	2.71	No
Salem	2	PWR	PSA201	P	8	21	1.58	1.20	2.05	3.02	No
Salem	2	PWR	WSA201	W	4	26	-0.12	-0.24	1.73	2.81	No
San Onofre	2	PWR	PSO201	P	3	21	0.02	-0.10	1.55	2.71	No
San Onofre	3	PWR	PSO301	P	3	19	2.43	2.34	1.55	2.71	Yes

General Information							Type D Deviation (Outlier Test)				
Plant Name	Unit	Reactor Type	Heat	Product Form	n	σ (°F)	$r_{i(max1)}$	$r_{i(max2)}$	C_1	C_2	Fails Test?
Seabrook	1	PWR	PSB101	P	4	19	1.39	1.19	1.73	2.81	No
Sequoyah	1	PWR	FSQ101	F	8	20	2.37	1.73	2.05	3.02	No
Sequoyah	1	PWR	WSQ101	W	4	26	1.39	1.31	1.73	2.81	No
Sequoyah	2	PWR	FSQ201	F	8	20	1.57	1.36	2.05	3.02	No
Sequoyah	2	PWR	WSQ201	W	4	26	3.62	1.44	1.73	2.81	Yes
South Texas	1	PWR	PST101	P	4	19	0.71	0.59	1.73	2.81	No
South Texas	2	PWR	PST201	P	4	19	0.67	0.39	1.73	2.81	No
Surry	1	PWR	PSU101	P	3	21	0.80	0.02	1.55	2.71	No
Surry	1	PWR	WSU101	W	3	26	1.88	1.58	1.55	2.71	Yes
Surry	2	PWR	PSU201	P	6	21	0.55	0.47	1.93	2.93	No
Surry	2	PWR	WSU201	W	3	26	0.00	-0.58	1.55	2.71	No
Three Mile Island	1	PWR	PTM101	P	3	21	0.38	-1.29	1.55	2.71	No
Trojan		ex-PWR	PTRO01	P	6	21	0.74	0.14	1.93	2.93	No
Trojan		ex-PWR	WTRO01	W	3	19	0.77	0.55	1.55	2.71	No
Turkey Point	3	PWR	FTP302	F	3	20	1.05	0.67	1.55	2.71	No
Turkey Point	3	PWR	SASTM	SRM	26	21	1.98	1.94	2.53	3.36	No
Turkey Point	3	PWR	WTP301	W	4	26	1.30	0.36	1.73	2.81	No
Virgil Summer	1	PWR	PVS101	P	8	21	0.12	-0.15	2.05	3.02	No
Virgil Summer	1	PWR	WVS101	W	4	19	0.95	0.16	1.73	2.81	No
Vogtle	1	PWR	PVO101	P	6	19	0.70	0.56	1.93	2.93	No
Vogtle	1	PWR	WVO101	W	3	19	0.67	-0.02	1.55	2.71	No
Vogtle	2	PWR	PVO201	P	6	19	-0.17	-0.23	1.93	2.93	No
Vogtle	2	PWR	WVO201	W	3	19	-0.17	-0.49	1.55	2.71	No
Waterford	3	PWR	PWF301	P	3	19	0.53	-0.87	1.55	2.71	No
Watts Bar	1	PWR	FWB101	F	4	20	0.94	0.85	1.73	2.81	No
Wolf Creek	1	PWR	PWC101	P	8	19	1.10	0.88	2.05	3.02	No
Wolf Creek	1	PWR	WWC101	W	4	19	1.20	1.20	1.73	2.81	No
Zion	1	ex-PWR	PZN101	P	8	21	0.43	0.33	2.05	3.02	No
Zion	1	ex-PWR	WZN101	W	5	26	0.31	0.02	1.84	2.88	No
Zion	2	ex-PWR	PZN201	P	6	21	1.20	0.27	1.93	2.93	No
Zion	2	ex-PWR	WZN201	W	3	26	0.66	0.04	1.55	2.71	No

APPENDIX C FLAW DEPTH AND DENSITY DISTRIBUTIONS CONSIDERING PROBABILITY OF DETECTION AND BIAS IN NDE DATA WITH APPLICATIONS

Prepared for the U.S. Nuclear Regulatory Commission under Subcontract 4000099247 with UT-Battelle, LLC (Oak Ridge National Laboratory)

Mohammad Modarres
University of Maryland

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ABBREVIATIONS

PDF	Probability Density Function
CDF	Cumulative Density Function
ISI	In Service Inspection
NDE	Nondestructive Evaluation
POD	Probability of Detection
PTS	Pressurized Thermal Shock
RPV	Reactor Pressure Vessel
SAW	Submerged Arc Weld
SMAW	Shielded Metal Arc Weld
UT	Ultrasonic Test

SYMBOLS AND EXPRESSIONS

a	True flaw depth (inches)
A	Random variable representing flaw depth
	Logarithm of signal response amplitude in flaw detection NDE
a*	NDE measured (or observed) flaw depth (inches)
ath	Threshold flaw depth for detection below which flaw detection is beyond the capability of the NDE technology used
D	The event that a flaw is detected
	The event that a flaw is not detected
EM	Model error of the NDE measurement error, represented by a normal distribution with mean of zero and known standard deviation
fa(a* Mε|Φ)	PDF of the true flaw depth, given the vector of PDF parameters represented in terms of observed flaw depth a* but corrected for the measurement error Mε
	Conditional PDF of large flaw depth
	Conditional PDF of small flaw depth
f(.), g(.), h(.), l(.), m(.), x(.), g'(.). k(.), γ(.)	PDF functions of model parameters, flaw depth, or flaw density
g(Mε)	PDF of the measurement error (in terms of a*)
L(a|Φ)	Likelihood of true flaw depth given the vector of parameters Φ
L(Data|θ)	Likelihood of observed NDE data conditioned on (given) the unknown parameter θ
	Likelihood of observing n* flaws given there are a total of nj true flaws
Mε	NDE measurement error (combined random and systematic errors)
m*i	Number of flaw depths observed (reported in NDE) in the interval i
n	Number of flaw depth intervals (reported in NDE)
n*	Number of exact flaw depths observed (reported in NDE)

	Combination of n* observed flaws out of total flaws nj (observed or detected, and unobserved or not detected flaws)
N	Mean of the PDF of the number of flaws in volume v
N(0;σ)	Normal PDF with mean zero and standard deviation of σ
POD(a)	Probability of detection of a flaw of depth a
POD(a* Mε)	POD of true flaw depth represented in terms of observed flaw depth a* by correcting for the measurement error Mε
Pr(.)	Probability
Pr(D)	POD independent of flaw depth
	Probability of no detection regardless of size
	Probability of total flaws nj conditioned on observing n* flaws in NDE
Pr(Φ, ttr)	POD independent of flaw size (i.e., Pr(D))
ttr	Transition flaw depth which separates large flaw depth from small flaw depth
v	Volume of inspected weld
βi	Parameter i of the POD model
Δ	Weld bead thickness
ε	Random error of the model
λ	Flaw depth intensity parameter (inch 1) of the exponential distribution representing flaw depth distribution, also flaw intensity (flaws/ft3) representing Poisson flaw density distribution:
π0(θ)	Prior PDF of an unknown parameter θ
π1(θ|Data)	Posterior PDF of an unknown parameter θ given observed NDE data
Φ	Vector of parameters of the flaw depth PDF
θ	An unknown parameter of a model
Θ	Vector of parameters of the POD model
ρ	Poisson distribution parameter representing the volumetric intensity of flaws (flaws per unit volume)
σPOD(a)	Standard deviation of PDF of the POD model error vs. flaw depth
γ(.|α1, α2)	Gamma PDF with parameters α1 and α2

C.1 Introduction and Background

In 2010, the NRC amended its regulations to provide alternative screening methods for protection against Pressurized Thermal Shock (PTS) events that could affect the Reactor Pressure Vessels (RPVs) of the operating Pressurized-Water Reactors (PWRs). The new rule, 10 CFR 50.61a [C-1], provides a means for determining whether the flaws found through In-Service Inspection (ISI) of a particular RPV are consistent with the assumptions regarding the number and size of flaws used in the PTS analyses that provided the technical basis for the new rule. To address this requirement, 10 CFR 50.61a includes two tables (one table for weld material and one table for plate/forging material) that express the maximum flaw density and flaw depths that are allowed in the beltline of an RPV.

The new rule relies on flaw characteristics (flaw depth and density) that were simulated and used by the probabilistic fracture mechanics computer code FAVOR [C-2] to develop the 10 CFR 50.61a flaw tables. These flaw characteristics were proposed by Simonen et al. in NUREG/CR-6817 [C-3] and are used by the VFLAW code to generate the input flaws for FAVOR. The data include distribution functions that represent the initial fabrication flaws in some RPVs. The FAVOR computer code fully incorporates these distributions by sampling from each using Monte Carlo techniques.

The flaw distributions reported in NUREG/CR-6817 are based on information obtained from destructive and very precise techniques used to experimentally detect and size the flaws. These tables have been viewed as the permissible limit for distribution of the “true” flaw depths and flaw densities. These depth and densities may be contrasted with those “observed” in an ISI using Non-Destructive Evaluation (NDE) techniques such as the Ultrasonic Test (UT). The NDE results used to assess compliance with the 10 CFR 50.61a tables would be more representative of the specific vessel inspected than the flaw distributions in NUREG/CR-6817 and could be used to support development of vessel-specific flaw-size and -density distributions. However, the NDE results are influenced by detection limits, detection errors, and sizing and measurement errors. Development of the vessel-specific distribution of the true flaw density and depth should account for such uncertainties.

This report describes the development and application of a methodology to account for uncertainties in NDE data and to analyze such data for the purpose of developing more realistic vessel-specific flaw-depth and -density distributions for comparison to the 10 CFR 50.61a screening tables, as well as for use as an input to FAVOR analysis. The methodology considers detection probability, flaw-measurement error, and flaw-detection threshold in its application. Application of the methodology is demonstrated using the ultrasonic NDE data obtained from an ISI of the Beaver Valley 2 RPV.

Flaw distributions developed and reported in NUREG/CR-6817 are based on destructive evaluation of two cancelled RPVs supplemented by expert judgment data. In contrast, the vessel-specific inspection data come from NDE inspections using, for example, UT methods. The variability in both the characteristics of the data (size, range, and number of flaws measured) and the UT system performance (probability of detection and measurement/sizing errors) highlighted a need for analyzing the inspection results on a vessel-specific or data-set-specific basis. For this purpose, traditional methods were inadequate, and therefore a new methodology that could accept a very small number of flaws (typical of vessel-specific NDE results), including inspection-system flaw-detection reliability, flaw-sizing accuracy (measurement error), and flaw-detection threshold, was developed.

The methodology is demonstrated here through an application using the UT data reported for the Beaver Valley 2 RPV [C-13]. The objective was to provide a probabilistic description (in terms of the probability density function) of the actual flaw depth and flaw density of the welds based on the detected flaws from NDE examinations of this RPV using UT. Because the NDE data are uncertain and contain measurement errors, data developed as part of the PTS study (the so-called VFLAW data) were specialized to the Beaver Valley 2 RPV and used as the prior flaw information. Combination of the prior information and the NDE results of the Beaver Valley 2 RPV led to the development of the posterior flaw information, which represents the distribution of the true flaw depth and flaw density of the Beaver Valley 2 RPV welds. See Figure C-1 for an illustration of the Bayesian updating process. It is important to note that the VFLAW data, while representing generic values of flaw characteristics (based on expert judgment and on the PVRUF and Shoreham RPVs), may be specialized to a specific RPV, for example by using RPV-specific weld length, bead thickness, geometry and other weld characteristics of (in this case) Beaver Valley 2. Therefore, the specialized VFLAW data would be the most representative information that can be used to describe prior flaw-depth and flaw-density distributions and characteristics. If other prior information is available, such information may also be used instead of or in addition to the specialized VFLAW data.

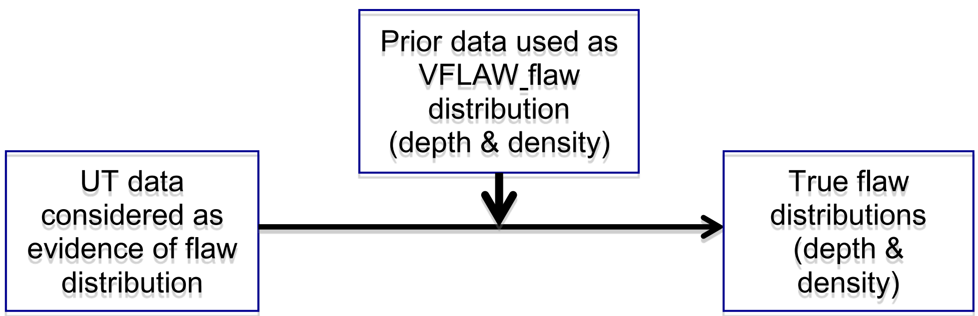

Figure C-1 A simple description of the Bayesian updating process.

In the remainder of this report, the methodology is described first, followed by the application to the Beaver Valley 2 ISI data. The results are used to compare the Beaver Valley 2 RPV to the 10 CFR 50.61a screening tables. As such, the VFLAW-based flaw models are updated to more realistically represent this RPV.

C.2 Probabilistic Approach to Combine Uncertain NDE Flaw Data with Prior Flaw Distributions

In this section, a Bayesian updating methodology is proposed to combine the observed NDE data with the available flaw data and models used as part of the PTS re evaluation effort. First, the Bayesian framework in general will be discussed, followed by the NDE data uncertainties (i.e., probability of detection and measurement/sizing error), and finally the developed Bayesian updating procedure will be discussed.

C.2.1 The Bayesian Framework

Suppose that background (prior) information is available about a model (e.g., the probability density functions representing flaw depth and flaw density). If new evidence becomes available, for example vessel specific NDE data, it is possible to update the prior information (e.g., distribution models) in light of the new NDE based evidence. The process of updating prior distribution models may be formally done through Bayesian inference. Bayesian inference is conceptually simple and logically consistent. It provides a powerful approach to combine observed or measured data with background (prior) information.

In Bayesian inference, the state of knowledge (uncertainty) of a random variable of unknown value that is of interest is quantified by assigning a probability distribution or Probability Density Function (PDF) to its possible values. Bayesian inference provides the mathematical formalism by which this uncertainty can be updated in light of any new evidence.

In the framework of the Bayesian approach, the parameters of the model of interest (e.g., the intensity parameter, λ, of an exponential distribution representing flaw depth) are treated as random variables, the true values of which are unknown. Thus, a PDF can be assigned to represent the parameter values. In practice, however, some prior information about the parameters may be known, including any prior data and subjective judgments regarding the parameter values that may be available. For example, the intensity parameter, λ, of an exponential distribution representing the variable flaw depth (e.g., in inch 1) may be known from related observations and data of similar vessels. If new NDE observations provide limited but more specific data about a particular RPV, it is possible to update any prior PDF of the flaw depth intensity parameter by combining the NDE data with the prior PDF. In this case, the prior knowledge is combined with the specific NDE data to build a posterior PDF that is more representative of the true intensity parameter and thus the true flaw depth distribution that accounts for the uncertainties in the observed NDE data.

Let θ be a parameter of interest (for example the flaw intensity parameter). Assume that θ is a continuous random variable, such that the prior and posterior PDFs of θ are likewise continuous. Also, let L(Data|θ) express how likely is it to observe the data (e.g., the NDE data measured) in light of given values of parameter θ. Certain values of θ show that the data observed are more likely to support the PDF whose parameter is θ. Then, according to Bayesian inference [C 4], the posterior PDF that represents a properly weighted combination of the prior PDF and the likelihood of the parameter θ will be:

$$\pi_1(\theta|\mathrm{Data}) = \frac{\pi_0(\theta)L(\mathrm{Data}|\theta)}{\int_\theta \pi_0(\theta)L(\mathrm{Data}|\theta)d\theta} \qquad \text{Eqn. (C-1)}$$

The posterior PDF, $\pi_1(\theta|\text{Data})$, represents the updated prior PDF of θ, $\pi_0(\theta)$, in light of the observed data (shown by its likelihood function L(Data|θ)). The denominator of Eqn. (C-1) is called the marginal density of the data or the normalization constant. The most difficult part of a Bayesian analysis, besides describing the likelihood function, is the computational challenge of determining the normalizing constant that often requires multidimensional numerical integration. The prior PDF $\pi_0(\theta)$ reveals knowledge of parameter θ before data are used. The posterior PDF $\pi_1(\theta|\text{Data})$ is called posterior because it reflects the PDF of θ after the data are used.

Certain prior PDFs are called "conjugate" [C-4]. This is the class of prior PDFs that yields the same functional form for the posterior distribution. For example, if flaw-depth distribution is represented by an exponential distribution, a gamma PDF representing the intensity parameter, λ, of the exponential distribution is a conjugate distribution. This means that when updated by new NDE flaw data, the posterior PDF of λ will also be a gamma distribution. Hamada et al. [C-5] present a comprehensive overview of the mathematical steps for updating the conjugate distributions used in the Bayesian analyses. In simple problems, the conjugate distribution makes posterior PDF calculations simple because it eliminates the complex, computationally challenging integrations in Eqn. (C-1).

For example, consider NDE flaw observations (data). In this case, the likelihood of all such data, given a parameter θ of the flaw-depth PDF L(Data| θ), would be expressed as the probability of the intersections of the individual flaw measurements; that is, the probability of an event consisting of *flaw-measurement-1* $\cap$ *flaw-measurement-2* $\cap$ *flaw-measurement-3* $\cap$ *...* . The likelihood, therefore, would be the product of the probability of observing each flaw depth, a_i, as shown by Eqn. (C-2). The likelihood function is independent of the order of each data point and is given by:

$$L(\text{Data} \mid \theta) = c\prod_i L_i(a_i \mid \theta) \qquad \text{Eqn. (C-2)}$$

where c is a combinatorial constant that quantifies the number of combinations in which the observed NDE data points, a_i, could have occurred. The constant c cancels from the numerator and denominator of Eqn. (C-1), and therefore is usually not included in the expressions of the likelihood function. Table C-1 summarizes the likelihood functions for different types of flaw data observations, if the PDF of the variable of interest (flaw depth in this case) is described by f(a|θ) with the corresponding Cumulative Density Function (CDF) of $F(a \mid \theta) = \int_0^a f(x \mid \theta)dx$.

Table C-1 Summary of Likelihood Functions

Type of Observation	Likelihood Function	Example Description
Exact Flaw Depth	$f(a_i|\theta)$	Exact flaw depth a_i is reported
Right Censored Flaw	$1-F(a_R|\theta)$	Flaw depth exceeds a_R
Left Censored Flaw	$F(a_L|\theta)$	Flaw depth is less than a_L
Interval Censored	$F(a_R|\theta) - F(a_L|\theta)$	Flaw depth is between a_L and a_R

Left Truncated	$f(a_i\|\theta) / [1-F(a_C\|\theta)]$	Flaw depth is a_i where flaw observations are not possible below a_C

C.2.2 Probability of Detection and Measurement Error

Interpretation of NDE data requires an understanding of the associated uncertainties. For example, one inspector may miss a specific flaw found by another. For this reason, the reliability of an inspection is customarily expressed in terms of the Probability of Detection (POD) of a given flaw size and expressed by curves of POD vs. flaw size. Determining detailed POD curves can also be difficult. Flaw detection depends on several factors and it can be difficult to produce statistical data to estimate the POD considering variations in material types, inspection methods, skill levels, equipment imprecision, and other factors.

Additionally, sizing or measurement errors occur and measurement model uncertainties exist. The measurement errors are generally composed of some combination of stochastic (random) errors and systematic errors. Random errors are intrinsic to any measurement and are caused by instrumentation imprecision and variability, among other sources. Systematic errors are biases in NDE measurement resulting in the mean of many separate measurements differing consistently and appreciably from the true value of the measured flaw. Biases or systematic errors are often significant contributors to flaw data uncertainties. For example, in UT application to RPVs, there is a general trend toward overestimating the size of small flaws while underestimating the size of larger flaws [C-6].

C.2.2.1 Probability of Detection

Formally, the POD can be defined as the probability that the NDE system detects a flaw of specific depth a, if it exists, and is denoted by POD(a) [C-6]. POD is generally modeled as a function of through-wall extent of the flaw. The POD also depends on other factors such as material test equipment, measurement method, and geometry. For example, POD generated for a particular material thickness might not be true for the same material with a different thickness. The POD should also consider appropriate adjustments for shallow surface flaws adjacent to the clad.

Consider a binary random variable D indicating a flaw detected (or $\overline{D}$ indicating a flaw not detected). Probability of detection of a flaw of depth a_i is:

$$\mathrm{POD}(a_i) = \Pr(D \mid a = a_i) \qquad \text{Eqn. (C-3)}$$

The data from which POD(a) functions are generated can be categorized into two types: hit/miss and signal-response amplitude. The hit/miss data type shows whether a flaw is detected or not. This type of data is subjective in nature depending on the operator experience. In this method, the smallest and largest flaw sizes detected should be identified. Any size below the smallest size is never detected, whereas a size above the largest size is always detected. The POD is then calculated as the ratio of the number of successful detections over the total number of inspections performed for a particular flaw size and is called the averaged POD.

Different forms of POD curves have been used in the literature (see References [C-7], [C-8], and [C-9]). The logistic POD model for hit/miss data is a common model and is represented as:

$$POD(a \mid \beta_1, \beta_2, a_{th}) = \begin{cases} logistics(a \mid \beta_1, \beta_2, a_{th}) & for \ \ a > a_{th} \\ 0 & otherwise \end{cases} \qquad \text{Eqn. (C-4)}$$

where a is the flaw depth and N(0;σ(a)) is the random error represented by a normal distribution with a constant standard deviation σ or a deviation which may be a function of flaw depth (that is, σ(a)). The random error accounts for the POD model error. Model parameters β_1 and β_2 may be uncertain (epistemic) and would be represented by the bivariate PDF k(Θ), where Θ is the vector of the parameters, $\Theta = \{\beta_1, \beta_2\}$. The PDF function m(σ(a)) may also be used to express any epistemic uncertainties by treating σ(a) as a random variable. The parameter a_{th} in Eqn. (C-4) represents the threshold (the flaw size below which detection is not possible).

The other type of POD data represents measurements of the amplitude of signal response recorded by the NDE system, such as in a UT system. For signal-response data, much more information is supplied in the signal for further analyses than is in the hit/miss data. In the signal-response approach, the most important parameters are the inspection threshold (noise level) and the decision threshold. All responses less than the inspection threshold are ignored.

In the signal-response approach, it is generally assumed that the logarithm of the signal-response amplitude, $\hat{a}$, is linearly correlated to the logarithm of the flaw depth, a, as shown in Eqn. (C-5):

$$\log(\hat{a}) = \beta_3 + \beta_4 \log(a) + \varepsilon \qquad \text{Eqn. (C-5)}$$

where ε is the random error and β_3 and β_4 are the regression parameters. The random error can be assumed to have a normal distribution with mean zero and a constant or variable standard deviation. Based on this assumption, it can be shown that the POD curve can be modeled using a lognormal CDF. The corresponding POD is shown as:

$$POD(a) = Pr(\hat{a} > \hat{a}_{th}) = Pr(\log(\hat{a}) > \log(\hat{a}_{th})) \qquad \text{Eqn. (C-6)}$$

where a_{th} is the decision (detection) threshold signal. The decision threshold is chosen to be a bit higher than the inspection threshold in order to minimize the probability of a false call (for cases in which the decision threshold is not intentionally chosen to allow a certain probability of a false call) in the POD estimates. The â vs. a data can also be converted into hit/miss data by using the decision threshold, and an averaged POD can be determined.

C.2.2.2 Measurement (Sizing) Error

Measurement results are always associated with errors of varying magnitudes. Measurement error is defined as the difference between the measured and the true flaw depth. Measurement error is defined by Eqn. (C-7), where M_ε is the measurement error, a^* is the measured value of flaw depth, and a is the true value of flaw depth:

$$M_\varepsilon = a^* - a \qquad \text{Eqn. (C-7)}$$

The measurement error has two components: systematic error (bias) and random error. Random error may be represented by a normal distribution with zero mean and constant standard deviation. Systematic error in most cases is a major contribution to flaw measurements and cannot be ignored. In its simplest form, the measurement error can be represented by a linear function of true size as shown in Eqn. (C-8), where m is the slope and c is the intercept of the line representing measurement error, M_ε, versus true flaw depth, a. If available, PDFs of m and c can be expressed to represent the epistemic uncertainty in these parameters. Also, M_ε, may be represented as a linear function of measured flaw depth a^* because all data available are in terms of a^*.

$$
\begin{aligned}
&M_\varepsilon = ma + c + E_M \\
&\text{where, } a = \text{true flaw depth and } E_M = N_M(0, \sigma_M), \\
&\text{or based on Eqn. (7):} \\
&M_\varepsilon = m(a^* - M_\varepsilon) + c + E_M; \text{ or} \\
&M_\varepsilon = \frac{m}{m+1} a^* + \frac{c}{m+1} + \frac{E_M}{m+1} = m'a^* + c' + E'_M \\
&\text{where, } a^* = \text{measured depth, } m' = \text{slope, } c' = \text{intercept,} \\
&\text{and } E'_M = N_M(0, \sigma'_M) \text{ of } M_\varepsilon \text{ vs. } a^*
\end{aligned}
\qquad \text{Eqn. (C-8)}
$$

The aleatory random measurement error E'_M is shown by the normal distribution $N_M(0; \sigma'_M)$ in Eqn. (C-8). As such, the total measurement error may be represented as the normal distribution $g(M_\varepsilon) = N(m'a^*+c'; \sigma'_M)$. Figure C-2 shows a conceptual example of the measurement error as a function of true flaw size (one can also show M_ε vs. a*). According to Eqn. (C-7), the relationship between the true flaw depth, a, and measured depth, a^*, is $a = a^* - M_\varepsilon$.

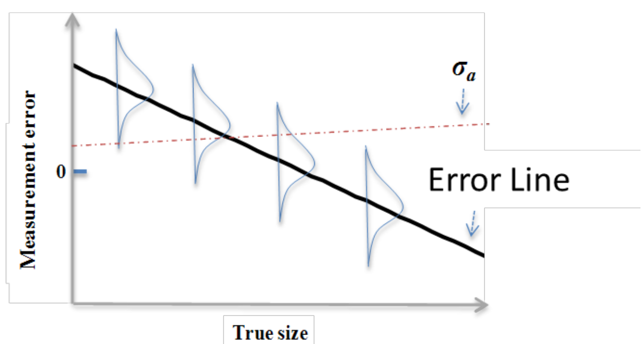

Figure C-2 Measurement error distribution

If the measurement error's given flaw depth, a, is M_ε, E_M describes the PDF of random or stochastic error. Clearly, Figure C-2 depicts a case in which the standard deviation of the PDF of E_M is not constant; rather, it is a monotonically increasing line.

C.2.3 The Methodology for Updating the NDE Data

This section discusses the details of the Bayesian updating approach, which combines UT data (including their uncertainties) with the prior PDF models of flaw depth and density (used in VFLAW to generated FAVOR input) to arrive at posterior distributions of flaw characteristics

C.2.3.1 Updating Flaw Depth Distribution Models

The ultimate objective of this analysis is to describe PDFs of the flaw depth and density considering UT measurement of flaws (which contain modeling uncertainty and stochastic variability in form of the POD and measurement error). We start with the Bayesian estimation of the (large and small) flaw depths, followed by the same estimation for flaw density.

In the Bayesian framework described by Eqn. (C-1), prior information on the flaw depth PDF (for example, data and expert elicitation described in NUREG/CR-6817) may be combined with the uncertain measurement data from NDE to assess a posterior distribution of the flaw depths. Consider the PDF of the flaw depth, a, as $f(a \mid \Phi)$, where Φ is a vector of all the PDF parameters.

The data reported in NUREG/CR-6817 show that the small and large flaw depths are represented using different distributions. For example, the models proposed and used in VFLAW rely on the exponential distribution for large flaw depths but use the multinomial distribution to model small flaw depths. The flaw depth that separates the two distributions is defined as the transition flaw depth. Therefore, a given PDF may only be true up to a limit from which it transitions to another distribution. For the transition flaw depth t_{tr}, the PDF that describes the flaw depth should be conditioned on exceeding or falling below the transition limit. Therefore:

$$f_l(a \mid \Phi, a \geq t_{tr}) = \frac{f(a \mid \Phi)}{\Pr(a \geq t_{tr})}$$
$$f_s(a \mid \Phi, a < t_{tr}) = \frac{f(a \mid \Phi)}{\Pr(a < t_{tr})}$$

Eqn. (C-9)

In VFLAW, for example, t_{tr} for the weld regions was selected as the flaw depth of about the bead thickness, Δ, of the corresponding weld. Further, in VFLAW the flaw depth is normalized to the dimensionless random variable a/Δ instead of to a. The approach discussed herein applies to PDFs of both a and a/Δ, but the respective equations of the approach are only shown in terms of the PDF similar to Eqn. (C-9).

Consider the PDF of NDE measurement error M_ε (represented by Eqn. (C-8)) of a measured flaw depth a^* with stochastic random variable *E*. The flaw-depth distribution corrected for the measurement error, M_ε, by assuming that true flaw depth, a, may be represented by correcting the measured depth a^* using the relationship $a = a^* - M_\varepsilon$ [C-10]. As stated earlier in Eqn. (C-8), the PDF of M_ε will be $g(M_\varepsilon) = N(m'a^* + c'; \sigma'_M)$. If there are epistemic uncertainties about parameters m' and c', they may be represented by the bivariate PDF x(Ω), where Ω is the vector of the parameters m' and c'. The expected distribution of measurement error would be:

$$g'(M_\varepsilon) = \int_\Omega g(M_\varepsilon) x(\Omega) d\Omega$$

Eqn. (C-10)

While the measurement-error-corrected PDF adjusts the flaw depths to true values, the flaws missed, as characterized by the POD, should also be accounted for. That is, for every measured flaw a^*, a corresponding probability (including uncertainties) that additional flaw(s) may be missed should be accounted for.

If the POD is represented as a mathematical function of the flaw size, a, the vector of parameters Θ of the POD function may be associated with a known multivariate PDF k(Θ) in order to account for the uncertainties. It is also possible to add a stochastic model error term, represented by a normal distribution with the mean zero and the standard deviation $\sigma_{POD}(a)$. For simplicity, it is also possible to assume that the error term is absorbed in the PDF of the POD model parameters (i.e., k(Θ)). The marginal POD independent of the random variables Θ and $\sigma_{POD}(a)$ would be:

$$POD(a) = \iint_{\sigma_{POD},\Theta} POD(a \mid \Theta, \sigma_{POD}(a)) k(\Theta) m(\sigma_{POD}(a)) d\Theta d\sigma_{POD} \qquad \text{Eqn. (C-11)}$$

Marginal POD, independent of flaw depth conditional on Φ (see Eqn. (C-9)) and t_{tr}, is then expressed as:

$$\begin{aligned} Pr_s(D) &= POD(\Phi, a < t_{tr}) = \int_0^{t_{tr}} POD(a) f_s(a \mid \Phi, a < t_{tr}) da \\ Pr_l(D) &= POD(\Phi, a \geq t_{tr}) = \int_{t_{tr}}^{\infty} POD(a) f_l(a \mid \Phi, a \geq t_{tr}) da \end{aligned} \qquad \text{Eqn. (C-12)}$$

where Pr(D) expresses the probability that a small or large flaw is detected regardless of size, which in general is a function of Φ and t_{tr}; that is, POD(Φ, t_{tr}). The probability of not detecting a flaw would be $Pr(\overline{D}) = 1 - Pr(D)$.$\overline{Pr(\overline{D})\text{=1-Pr(D)}}$. Let the random variable A represent the true flaw depth. Then, according to the Bayesian formulation by Celeux et al. [C-11], the probability that a detected flaw has a depth in the vicinity of a, inside an interval Δa, may be expressed as:

$$\begin{aligned} Pr(a < A < a + \Delta a \mid D) &= \frac{Pr[a < A < a + \Delta a \cap D]}{Pr(D)} \\ &= \frac{Pr(a < A < a + \Delta a) \cdot Pr(D \mid a < A < a + \Delta a)}{Pr(D)} \end{aligned} \qquad \text{Eqn. (C-13)}$$

where D is the event that a flaw is detected. The limit of Eqn. (C-13) as the flaw depth interval Δa approaches zero may be found after dividing Eqn. (C-13) by Δa. The left term limit represents the likelihood that a detected flaw will have the depth a. Further, by rearranging the right side, the PDF of flaw depth independent of detection and POD, given a flaw of depth a, may be found:

$$\begin{aligned} &\lim_{\Delta a \to 0} \frac{Pr(a < A < a + \Delta a \mid D)}{\Delta a} = L(a \mid D) = \lim_{\Delta a \to 0} \frac{Pr(a < A < a + \Delta a).Pr(D \mid a < A < a + \Delta a)}{Pr(D)\Delta a} = \\ &\underbrace{\lim_{\Delta a \to 0} \frac{Pr(a < A < a + \Delta a)}{\Delta a}}_{f(a|\Phi, t_{tr})} . \underbrace{\lim_{\Delta a \to 0} Pr(D \mid a < A < a + \Delta a)}_{POD(a)} . \frac{1}{Pr(D)} \end{aligned} \qquad \text{Eqn. (C-14)}$$

Using Eqn. (C-14), the corresponding likelihood that a detected flaw is of depth a may be expressed as:

$$L(a \mid \Phi) = \frac{f(a \mid \Phi, t_{tr}).POD(a)}{POD(\Phi, t_{tr})} \qquad \text{Eqn. (C-15)}$$

Eqn. (C-15) forms the basis for development of the likelihood function, which would be necessary in the Bayesian framework (as discussed in Section C.2.1) to estimate the posterior PDF of flaw depth given the observed NDE flaw data and the prior information about the characteristics of flaw PDF.

C.2.3.1.1 Likelihood Function of Exact Flaw-Depth Measurements

Suppose that the NDE reports exact flaw depths. Based on Eqn. (C-2), the likelihood function of n^* flaws of known depth (containing measurement errors) $a_1^*, a_2^*, a_3^*, \ldots$ would be $L(\text{Data} \mid \Phi) = \prod_{n^*} L(a^* \mid \Phi)$. It is important to correct for POD and the measurement error and parameter uncertainties according to Eqn. (C-10) and to represent flaw depths in terms of the measured value using Eqn. (C-7) so that $a^* = M_\varepsilon + a$ [2]. Therefore, using Eqn. (C-15), the likelihood of exact flaw measurements reported may be expressed as [C-10]:

$$L(\text{All exact measured data} \mid \Phi, t_{tr}) = \frac{1}{\left[POD(\Phi, t_{tr})\right]^{n^*}} \prod_{i=1}^{n^*} \int_{M_\varepsilon} POD(a_i^* - M_\varepsilon) f((a_i^* - M_\varepsilon) \mid \Phi, t_{tr}) g'(M_\varepsilon) dM_\varepsilon \qquad \text{Eqn. (C-16)}$$

Because NDE data are measured and have associated measurement error and other uncertainties, but the POD and measurement error discussed earlier are modeled to be relevant to the true flaw depth, a, in Eqn. (C-16) the true flaw depth is replaced with its equivalent (a^*-M_ε). The expectation of the numerator of Eqn. (C-15), independent of the measurement error, is found by multiplying the term $f(a \mid \Phi, t_{tr}).POD(a)$ by the expected PDF of the measurement error, $g'(M_\varepsilon)$, and integrating this over all values of the measurement error.

C.2.3.1.2 Likelihood Function of Interval Flaw-Depth Measurements

If in addition to or instead of the exact flaw-depth data, interval data are reported (such as the number of flaws observed less than a given depth or between an upper and lower limit), the likelihood of m_i^* flaws reported in the interval i, corrected for the measurement error but independent of the error, would be [C-12]:

$$L(\text{Interval consisting of } m_i^* \text{ measured flaw depths} \mid \Phi, t_{tr}) = \left[\frac{1}{POD(\Phi, t_{tr})} \int_{a_{i-1}^*}^{a_i^*} \int_{M_\varepsilon} POD(a^* - M_\varepsilon) f((a^* - M_\varepsilon) \mid \Phi) g'(M_\varepsilon) dM_\varepsilon \, da^* \right]^{m_i^*}$$

Eqn. (C-17)

[2] Note that if X and Y are two continuous random variables with probability density functions f(x) and g(y), the random variable Z = X + Y will have a probability density function h(Z) such that:

$$h(z) = \int_{-\infty}^{\infty} f(z - y) g(y) dy$$

If n such flaw-depth intervals were reported, the corresponding likelihood function using Eqn. (C-17) would be:

$$L(n\,\text{intervals of measured depths}\,|\Phi,t_{tr}) = \prod_{i=1}^{n}\left[\frac{1}{POD(\Phi,t_{tr})}\int_{a_{i-1}^*}^{a_i^*}\int_{M_\varepsilon} POD(a^* - M_\varepsilon)\,f((a^* - M_\varepsilon)\,|\,\Phi)\,g'(M_\varepsilon)\,dM_\varepsilon\,da^*\right]^{m_i^*}$$

Eqn. (C-18)

If exact and interval NDE data are both reported, the likelihood function would be a multiple of Eqn. (C-16) and Eqn. (C-18). That is:

$$L(\text{Mix Measured Flaw Depths}\,|\,\Phi, t_{tr}) =$$
$$L(n\,\text{Interval Measured Flaw Depths}\,|\,\Phi, t_{tr}) \times L(n^*\,\text{Exact Measured Flaw Depths}\,|\,\Phi, t_{tr})$$

If in addition to or instead of the exact flaw-depth data, interval data are reported (such as the number of flaws observed less than a given depth or between an upper and lower limit), the likelihood of m_i^* flaws reported in the interval i, corrected for the measurement error but independent of the error, would be [C-12]:

If n such flaw-depth intervals were reported, the corresponding likelihood function using Eqn. (C-17) would be:

If exact and interval NDE data are both reported, the likelihood function would be a multiple of Eqn. (C-16) and Eqn. (C-18). That is:

$$L(\text{Mix Measured Flaw Depths}\,|\,\Phi, t_{tr}) =$$
$$L(n\,\text{Interval Measured Flaw Depths}\,|\,\Phi, t_{tr}) \times L(n^*\,\text{Exact Measured Flaw Depths}\,|\,\Phi, t_{tr})$$

C.2.3.1.3 Bayesian Updating of Parameters of the Flaw Depth Distribution

Regardless of the form of the data (exact flaw-depth and/or interval data), the Bayesian inference of the vector of parameters Φ of the flaw-depth PDF would be obtained (according to Eqn. (C-1)) from $\pi_1(\Phi\,|\,\text{Data}, t_{tr}) \propto L(\text{Data}\,|\,\Phi, t_{tr})\pi_0(\Phi)$, where $\pi_1(\Phi\,|\,\text{Data})$ is the posterior multivariate PDF of vector Φ, and $\pi_0(\Phi)$ is the prior multivariate PDF of Φ.

Determination of the posterior $\pi_1(\Phi\,|\,\text{Data})$ requires complex integrations. Further, integration of the denominator of the Bayesian inference in Eqn. (C-1) also requires multi-dimensional integration that in most cases can only be performed numerically.

It is also critically important to note that Eqn. (C-9) through Eqn. (C-20) are all in terms of the actual flaw depth, a, measured in English or metric units. As stated before, it is also possible to express the equations in terms of the normalized flaw depth, a/Δ, instead. This is simply done by replacing flaw depth, a, with a/Δ in all PDFs, measurement error, and POD equations. Clearly the parameters of the equations should be adjusted accordingly.

C.2.3.2 Updating the Flaw Density Model

If flaws are detected with a probability given by Eqn. (C-11) and Eqn. (C-12) as $Pr(D) = POD(\Phi, t_{tr})$ (or not detected with a probability of $Pr(\bar{D}) = 1 - Pr(D)$), the probability that a specific total number of flaws n* observed in a given volume v out of the true number of flaws n_j follows the binomial distribution (see References [C-11] and [C-12]):

$$L(n^* \mid n_j) = \binom{n_j}{n^*} \left[\Pr(D)\right]^{n^*} \left[1 - \Pr(D)\right]^{n_j - n^*}$$

or Eqn. (C-19)

$$L(n^* \mid n_j) = \binom{n_j}{n^*} \left[POD(\Phi, t_{tr})\right]^{n^*} \left[1 - POD(\Phi, t_{tr})\right]^{n_j - n^*}$$

where $\binom{n_j}{n^*} = \frac{n_j!}{n^*!(n_j - n^*)!}$. The best estimate of the true number of flaws would be to assume that n^* represents the mean of Eqn. (C-19). Accordingly, the mean estimate of the true number of flaws, N, would be found from:

$$N = \frac{n^*}{POD(\Phi, t_{tr})} \qquad \text{Eqn. (C-20)}$$

A more formal way to estimate the number (and thus density) of flaws would be to use the Bayesian updating of n_j, which allows the estimation of the posterior distribution of n_j to describe the true number of flaws:

$$\Pr(n_j \mid n^*) = \frac{L(n^* \mid n_j)\Pr(n_j)}{\sum_{n_j} L(n^* \mid n_j)\Pr(n_j)} \qquad \text{Eqn. (C-21)}$$

Using Eqn. (C-19) (representing the likelihood of observing n^* flaws out of the unknown n_j flaws) and a Poisson prior flaw density model, the posterior probability distribution of the number of flaws would be obtained from:

$$\Pr(n_j \mid n^*) = \frac{\binom{n_j}{n^*}\left[POD(\Phi, t_{tr})\right]^{n^*}\left[1 - POD(\Phi, t_{tr})\right]^{n_j - n^*}\left[\frac{e^{-\rho v}(\rho v)^{n_j}}{n_j!}\right]}{\sum_{n_j = n^*}^{\infty}\binom{n_j}{n^*}\left[POD(\Phi, t_{tr})\right]^{n^*}\left[1 - POD(\Phi, t_{tr})\right]^{n_j - n^*}\left[\frac{e^{-\rho v}(\rho v)^{n_j}}{n_j!}\right]} \qquad \text{Eqn. (C-22)}$$

where ρ is the volumetric flaw intensity and ρv is the expected number of true flaws in the inspected volume v. If the mean number of flaws from Eqn. (C-20) is large, the computer rounding issues associated with Eqn. (C-22) may be avoided by performing the analysis for a smaller volume (for example, 1/100th of the inspected volume) and later prorating n_j accordingly. An alternative approach that is approximate, but simpler than Eqn. (C-19) through Eqn. (C-22), would be to update the parameter ρ itself based on the mean number of flaws. For example, if the volume of the UT inspection is v, the volumetric flaw intensity ρ of the flaws associated with the mean estimated N true flaws from Eqn. (C-20) in this volume would be $\rho = \frac{N}{v}$. Assuming that the mean occurrence intensity of flaws remains constant over the volume of inspection, the

Poisson distribution may be used to represent the likelihood of N flaws in volume v, given the volumetric flaw intensity ρ as shown by Eqn. (C-23):

$$L(N\,|\,\rho) = e^{-(\rho v)}\frac{(\rho v)^N}{N!} \qquad \text{Eqn. (C-23)}$$

where v is the inspection volume and ρ is the flaw intensity (flaws per unit volume) associated with the mean estimated number of flaws N.

If prior information about the flaw intensity, ρ, were available, it would be desirable to update the flaw intensity by using such prior information. For example, assume that the prior volumetric flaw intensity is described by the PDF, $\pi_0(\rho)$. Then, the posterior PDF, $\pi_1(\rho|N)$, can be estimated using the likelihood function in Eqn. (C-23) from:

$$\begin{aligned}&\pi_1(\rho\,|\,N) \propto L(N\,|\,\rho)\pi_0(\rho)\\ &\text{where}\, L(N\,|\,\rho) = \prod_j L(N\,|\,\rho_j)\end{aligned} \qquad \text{Eqn. (C-24)}$$

If the prior PDF of the flaw intensity is expressed by the gamma distribution with parameters $\boldsymbol{\alpha_1}$ **and** $\boldsymbol{\alpha_2}$, as $\gamma_0(\rho) = \text{gamma}(\rho\,|\alpha_1,\alpha_2) = \frac{\alpha_1^{\alpha_2}\rho^{\alpha_2-1}}{\Gamma(\alpha_2)}e^{-\alpha_1\rho}$, the posterior PDF is a conjugate distribution described by $\gamma_1(\rho) = \text{gamma}(\rho\,|\,v+\alpha_1, n_j+\alpha_2)$. The alternative form of the gamma distribution used by the MATLAB tool (to be used later in the following example) uses parameter β instead of parameter α_1, so that $\text{gamma}(\rho\,|\beta = \frac{1}{\alpha_1},\alpha_2)$.

C.3 Application Example

As part of a cooperative effort between the Electric Power Research Institute (EPRI) and the NRC to provide guidance on evaluation of PTS, NDE analyses were performed for a PWR RPV (Beaver Valley 2). In this section, the Beaver Valley 2 NDE data will be described first. Next, the VFLAW data described in NUREG/CR-6817 will be used as prior information, followed by the application of the Bayesian updating procedure discussed in Section C.2 to determine flaw-depth and flaw-density distributions specific to Beaver Valley 2. The resulting posterior distribution of the parameters of the flaw depth and flaw density, as described in Section C.2, will be derived and discussed. The results of flaw-depth and flaw-density PDFs will be used to compare against the 10 CFR 50.61a flaw tables, and to update the distribution models in VFLAW into new flaw distributions that are representative of the Beaver Valley 2 RPV.

C.3.1 Description of the NDE Data Used as Evidence to Build the Likelihood Function

The EPRI report by Spanner [C-13] provides UT-based measured flaw data near the inner surface (~2.5 inches) of the Beaver Valley 2 RPV, including small flaw sizes. These data, while subject to POD and measurement error, provide a more vessel-specific perspective of the distribution of flaws for Beaver Valley 2 than does the VFLAW distributions used in FAVOR.

The observed Beaver Valley 2 NDE data (with detection and sizing uncertainty) are mostly in the form of interval-censored data as summarized below [C-13]:

1. 19 weld flaws were detected by the UT NDE of Beaver Valley 2 in the first inch (the inspection volume specified in Supplement 4 to Mandatory Appendix VIII to Section XI of the ASME Code) of the RPV (~0.616 ft^3), all having a flaw depth less than 0.125".
2. 103 weld flaws were detected and reported by the UT NDE of Beaver Valley 2 in the first 3/8t (2.953") (the inspection volume specified in Supplement 6 to Mandatory Appendix VIII to Section XI of the ASME Code) of the RPV were reported, all with flaw depths less than 0.125", except for one flaw that measured 0.260".

The lower limit of the detected flaw intervals described above is not stated in [C-13], but is certainly not zero. Two possible subjective lower limits were assumed, and later the sensitivities of the final (posterior) flaw-distribution results to these two choices were assessed. The two lower limits are 0.04" and 0.075".

The NDE data described above provide an incomplete depiction of the true flaws in the Beaver Valley 2 RPV because they contain uncertainties associated with the UT technology used to detect and size flaws. The associated weld bead thicknesses are not reported. However, the weld region of the observed flaws and flaw length is reported. Such results should be corrected for detection and sizing capability, particularly for the small flaws.

The Beaver Valley 2 RPV weld map is shown in Figure C-3 [C-14]. In the absence of the Beaver Valley 2 average weld bead thickness as the point of transition between large and small depths, it is assumed that all flaws reported are Submerged Arc Welds (SAWs), which form over 90% of welds in the VFLAW data, with the bead thickness of $\Delta = t_{tr} = 0.26"$. Using the Beaver Valley 2 RPV information shown in Figure C-3, the following weld characteristics were computed and used to specialize the VFLAW data to represent the prior distributions of flaw depth and density for Beaver Valley 2 RPV:

Total Weld Length = 816.18"
Total Weld Volume[3] = 4.975 ft^3
Total Weld Fusion Area = 92 ft^2
Weld Volume of 1" = 0.616 ft^3
Weld Volume of 3/8t = 1.865 ft^3

[3] The total volume of reactor vessel weld area according to the weld dimensions shown in Figure C-3 = [1.375 × 99.45 × 2 × (86.531 - 78.656)] + [2 × 1.375 × 61.68 × (86.531 - 78.656)] + [1.25 × 3.14 × 2 × 86.531 × (86.5312 - 78.6562)] = 8,595.29 in^3 = 4.974 ft^3.

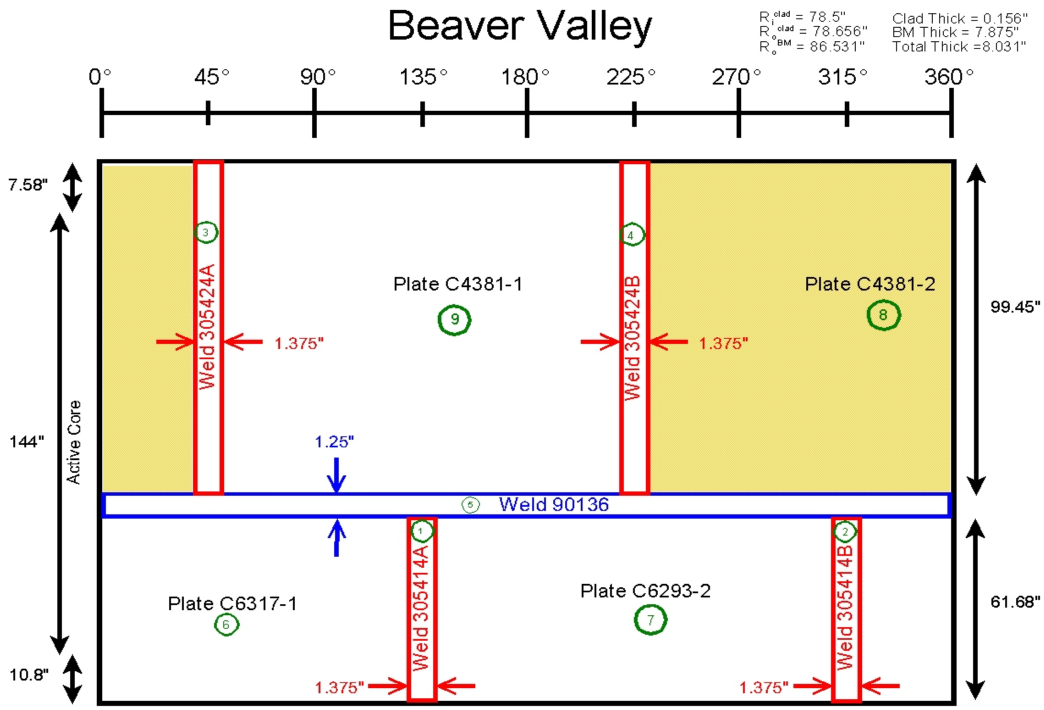

Figure C-3 Beaver Valley 2 weld map [C 14]

C.3.2 Description of Flaw-Depth and –Density Information Used in VFLAW as Prior PDFs in this Example

Smaller flaws neighboring the inner surface of the RPV that would be subjected to high thermal stresses during PTS events are dominant contributors to the risk of vessel failure posed by PTS. During the PTS re-evaluation effort in the late 1990s and early 2000s, the Marshall distribution was updated using the results of destructive tests of the Pressure Vessel Research User Facility (PVRUF) and Shoreham RPVs [C-2]. These analyses assumed that the flaws were near the inner surface of the RPV and included very small flaws of less than 0.125 inches (3 mm) in through-wall extent. The purpose of the re-evaluation was to provide an up-to-date estimate of the distribution of weld flaw density and sizes using modern NDE methods of analysis. These distributions represent the flaw-depth and flaw-density models in VFLAW [C-3].

Because we need prior distributions in the Bayesian inference described earlier, the VFLAW distributions many be specialized to Beaver Valley 2. This is done by using the corresponding bead thickness and other vessel characteristics for Beaver Valley 2 to determine the prior distributions of the flaw depth and flaw density from VFLAW distributions. The prior distributions fill the gaps in the limited inspected data and uncertainties associated with the NDE results.

Analysis of flaws should consider different vessel regions and welding types. Welding types include the Submerged Arc Weld (SAW), Shielded Metal Arc Weld (SMAW), and repair weld. Depending on the known details of fabrication, NUREG/CR-6817 estimated flaw distributions for each weld type used in a particular region of the vessel. Measured flaw data showed vessel-to-vessel variability in both flaw density and depth. To supplement the limited data from the PVRUF and Shoreham flaw measurements, NUREG/CR-6817 used expert elicitation.

Distribution functions to characterize the number and sizes of flaws in the various regions of the RPVs were then developed based on the measured data and insights from an expert elicitation exercise and used in VFLAW.

The prior distributions used in this example updated the PVRUF flaw models described in NUREG/CR-6817 and used in VFLAW, including the hyper-distributions that address the uncertainties associated with the parameters for the distribution functions describing flaw depth and flaw density. For example, the exponential distribution was used to represent the variability of large flaw depths. However, the parameter λ of the exponential distribution (i.e., assuming $f(a) = \lambda e^{-\lambda a}$, where a is the flaw depth) was in turn considered to be a random variable and described by the gamma distribution. The gamma distribution itself has two parameters, α_1 and α_2, that are given as constants in NUREG/CR-6817. These parameters were updated in this example based on the observed data from Beaver Valley 2. The values of the hyper-distributions used in VFLAW are shown in Table C-2. Note that the flaw-depth data in Table C-2 are in meters, whereas this example calculation is based on inches. The relationship between the flaw-depth and flaw-density PDFs and the corresponding hyper-PDFs of their parameters are illustrated in Figure C-4.

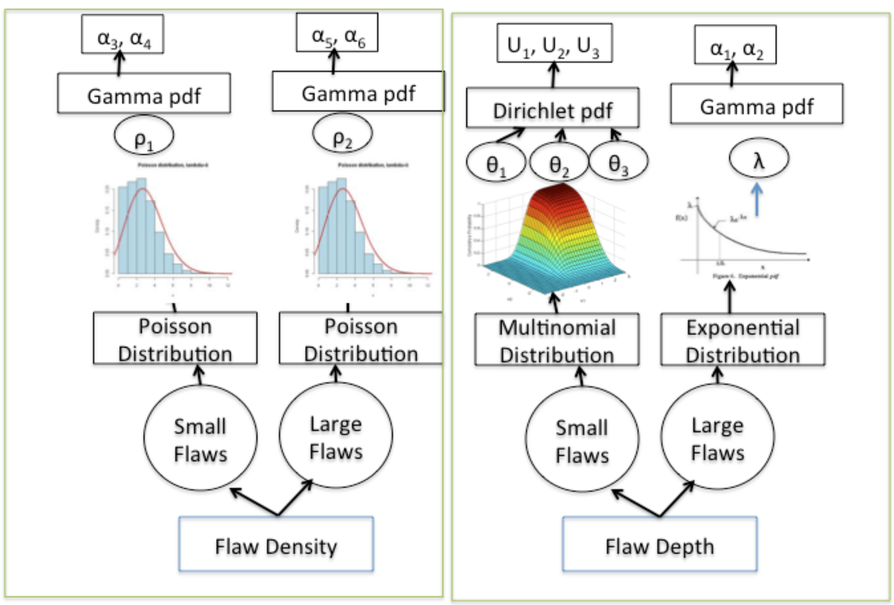

Figure C-4 Flaw depth and flaw density distributions used in VFLAW and their corresponding parameter hyper PDFs

Table C-2 Flaw-Depth (a) and Flaw-Density (b) Distributions and Hyper-PDF Parameters Used in VFLAW for PVRUF

(a) Flaw-depth characteristics (in meters) based on data from PVRUF RPV

Case	Flaw Size Category	Welding Process	Random Variable Representing Flaw Depth	PDF of Flaw Depth	Parameters of PDF	Distribution Describing Uncertainty of Parameters of PDF	Parameters of Uncertainty Distribution
1	Small ($a \le \Delta$)	SAW	a/Δ	Multinomial	P_1, P_2, P_3	Dirichlet	$U_1 = 34$ $U_2 = 8$ $U_3 = 1$
2	Small ($a \le \Delta$)	SMAW	a/Δ	Multinomial	P_1, P_2, P_3	Dirichlet	$U_1 = 34$ $U_2 = 8$ $U_3 = 1$
3	Small ($a \le \Delta$)	Repair Weld	a/Δ	Multinomial	P_1, P_2, P_3	Dirichlet	$U_1 = 34$ $U_2 = 8$ $U_3 = 1$
4	Large ($a > \Delta$)	SAW	a/Δ	Exponential	λ	Gamma	$\alpha_1 = 21.68$ $\alpha_2 = 52$
5	Large ($a > \Delta$)	SMAW	a/Δ	Exponential	λ	Gamma	$\alpha_1 = 21.68$ $\alpha_2 = 52$
6	Large ($a > \Delta$)	Repair Weld	a/Δ	Exponential	λ	Gamma	$\alpha_1 = 17.58$ $\alpha_2 = 13$

(b) Flaw-density characteristics based on data from PVRUF RPV

Case	Flaw Size Category	Welding Process	Random Variable Representing Flaw Depth	PDF of Flaw Depth	Parameters of PDF	Distribution Describing Uncertainty of Parameters of PDF	Parameters of Uncertainty Distribution
1	Small ($a \le \Delta$)	SAW	Flaws per cubic meter	Poisson	λ	Gamma	$\alpha_3 = 0.180$ $\alpha_4 = 1419$
2	Small ($a \le \Delta$)	SMAW	Flaws per cubic meter	Poisson	λ	Gamma	$\alpha_3 = 0.014$ $\alpha_4 = 197$
3	Small ($a \le \Delta$)	Repair Weld	Flaws per cubic meter	Poisson	λ	Gamma	$\alpha_3 = 0.00123$ $\alpha_4 = 12$
4	Large ($a > \Delta$)	SAW	Flaws per cubic meter	Poisson	λ	Gamma	$\alpha_3 = 0.180$ $\alpha_4 = 4$
5	Large ($a > \Delta$)	SMAW	Flaws per cubic meter	Poisson	λ	Gamma	$\alpha_3 = 0.014$ $\alpha_4 = 4$
6	Large ($a > \Delta$)	Repair Weld	Flaws per cubic meter	Poisson	λ	Gamma	$\alpha_3 = 0.00123$ $\alpha_4 = 7$

C.3.3 Detection and Sizing Error Models

Analysis of UT-detected performance data reported by EPRI [C-6] was used to identify a POD function for the purpose of this example. Currently, EPRI is updating these performance data and will supply more appropriate POD models for future consideration; the POD and flaw-sizing error functions used here are therefore intended only to illustrate this numerical method. The threshold limit of this POD function (Eqn. (C-4)) was taken as 0.00 and the epistemic uncertainties associated with the parameters of the model were not considered in this example. Accordingly, the following mean POD function based on Eqn. (C-4) was used[4]:

$$POD(a) = 1 - \frac{1}{1 + e^{63.2100(a - 0.1124)}} \qquad \text{Eqn. (C-25)}$$

where a is the true, unbiased flaw size. Figure C-5 shows a plot of this POD function.

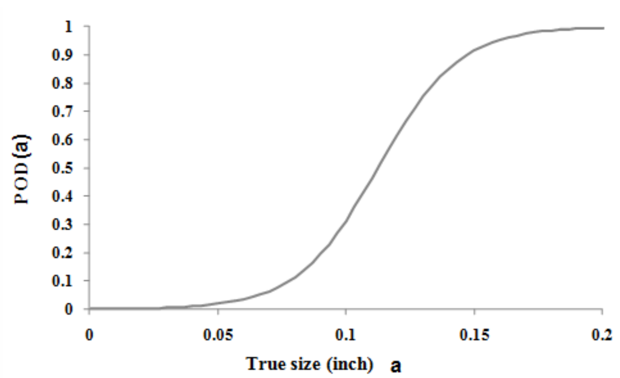

Figure C-5 POD vs. flaw depth

The measurement error was assumed, based on some examples and measurement errors reported in EPRI report [C-6]. The measurement error is a linear function that oversizes small flaws and undersizes large flaws. Figure C-6 depicts a plot of the measurement-error model used in this example. The model itself can be described as a line with a slope of -0.1905 and an intercept of 0.0476, with the variability resulting from the model error described by a normal distribution. That is, $M_\varepsilon = -0.1905a^* + 0.0476 + N(0, 0.0298)$, where N(0, 0.0298) is a normal distribution with a mean of zero and a constant standard deviation of 0.0298. Note that in this example we are not accounting for the epistemic uncertainties of the measurement-error model. However, such uncertainties should be considered when new measurement-error models are developed. Equally, as described by Eqn. (C-10), it is possible to represent the above line by the normal PDF: $g'(M_\varepsilon) = 13.41e^{-564.55(M_\varepsilon + 0.1905a^* - 0.0476)^2}$.

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[4] The model error associated with the logistic distribution was not considered.

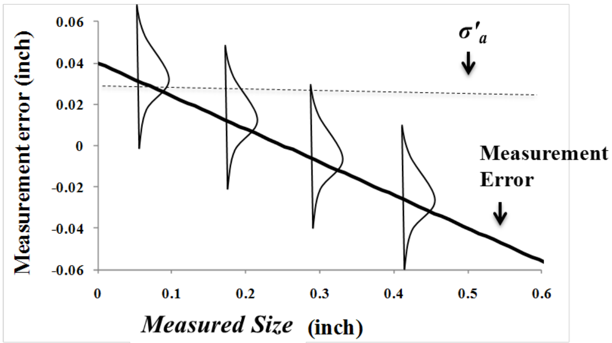


Figure C-6 Measurement error vs. flaw depth

C.3.4 Bayesian Updating of the Parameters of the Flaw-Depth Distributions

In this section, the process of updating the prior data specialized to Beaver Valley 2 with the observed NDE data using Bayesian inference will be discussed. Figure C-7 describes the main elements of the updating process. The observed UT-based flaw data discussed in Section C.3.1 is corrected for POD and measurement error. The POD and measurement error models were discussed in Section C.3.3. In the remainder of this section, development of the likelihood functions for the two sets of observed flaw data (one for the first one inch and another for the 3/8t of the inner RPV welds) will be discussed first. Then the Bayesian inference that combines the observed data with the prior data will be considered. The analysis will be performed for each of the NDE observed data sets to determine different conclusions.

1. The observed data for the first 3/8t of the RPV welds were used to update the prior models shown in Table C-2 in order to specialize them for the Beaver Valley 2 RPV. The updated values can be used for PTS calculations specific to the Beaver Valley 2 RPV using VFLAW and FAVOR.

2. The observed data for the first inch of the vessel were used to estimate the true number of flaws in the flaw-depth ranges of the 10 CFR 50.61a tables. This information is used to assess how the estimated number of flaws of a given size in Beaver Valley 2 (estimated based on inspection data, VFLAW distributions, and Bayesian inference) compares to the number and size of flaws permitted by the 10 CFR 50.61a tables.

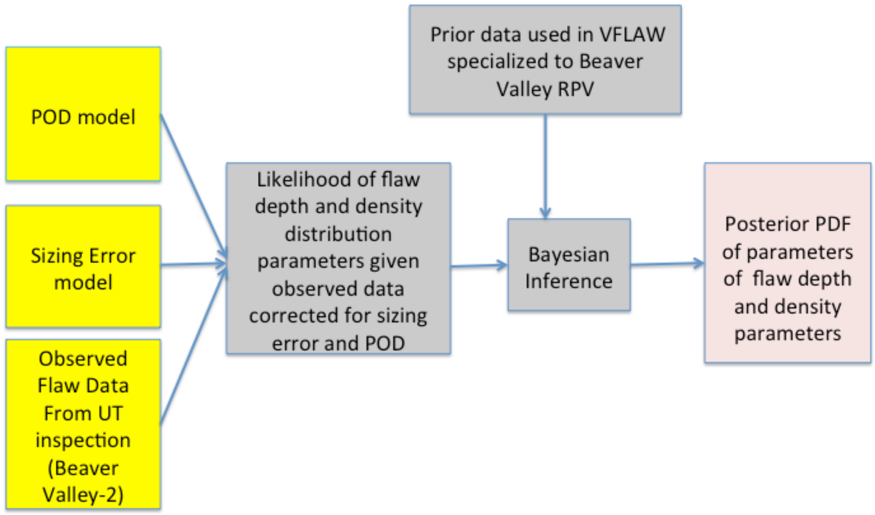


Figure C-7 Bayesian Updating Elements of the Beaver Valley 2 Example

C.3.4.1 Bayesian Updating of the Parameters of Large-Flaw Depth Distribution Based on the 3/8t UT Inspection Data

According to the prior data used by VFLAW as described in Section C.3.3, small-to-large flaw-size transition occurs at flaw depths exceeding the SAW weld bead thickness. According to Table C-2, large flaws will follow an exponential distribution, conditional on exceeding the transition flaw depth. Thus, the distribution of large-flaw depths corrected for the bias would be:

$$f(a \mid \lambda_l, a > t_{tr}) = \frac{f(a \mid \lambda_l)}{\Pr(a > t_{tr})} = \lambda_l e^{-\lambda_l (a - t_{tr})} = \lambda_1 e^{-\lambda_l (a^* - M_\varepsilon - t_{tr})} \qquad \text{Eqn. (C-26)}$$

where λ_l is the large-flaw depth intensity (per inch) and a_{tr} is the transition flaw depth (assumed to be 0.26"). To build the likelihood function, the flaws should be represented in terms of the measured flaw depths. Because the NDE data reported only one exact flaw depth ($n^* = 1$, $a_1^* = 0.26$) in the large-flaw region (exceeding the transition t_{tr}) for Beaver Valley 2, the likelihood function based on Eqn. (C-16) would be:

$$L(a^*_{data} \mid \lambda_l) = \frac{1}{[POD(\lambda_l)]^1} \prod_{i=1}^{1} \int_{-1}^{1} \left[1 - \frac{1}{1 + e^{63.2100(a_i^* - M_\varepsilon - 0.1124)}}\right] \left[\lambda_l \, e^{-\lambda_l \left(a_i^* - M_\varepsilon - 0.26\right)}\right] \left(13.41 e^{-564.55(M_\varepsilon + 0.1905 a_i^* - 0.0476)^2}\right) dM_\varepsilon$$

Eqn. (C-27)

where $POD(\lambda_l) = \int_{0.26}^{\infty} POD(a) \lambda_l e^{-\lambda_l (a-0.26)} da$ would be near 1 in this case because the POD(a) reaches unity when the flaw depth exceeds 0.2 inch in Eqn. (C-25). Note that, for simplicity, the random variable M_ε is integrated over the range of -1 to 1 because these are the extreme ranges of the measurement error. The next step is finding the posterior distribution of λ_l based on Eqn. (C-1). That is:

$$\pi_1(\lambda_l \mid a^*_{data}) = \frac{L(a^*_{data} \mid \lambda_l)\pi_0(\lambda_l)}{\int_{\lambda_l} L(a^*_{data} \mid \lambda_l)\pi_0(\lambda_l)\, d\lambda_l} \qquad \text{Eqn. (C-28)}$$

Using Eqn. (C-27) as the likelihood, the Bayesian updating with the gamma PDF as the prior hyper-PDF for λ_l, $\pi_0(\lambda_l) = gamma(\lambda_l \mid \alpha_1 = 1.2, \alpha_2 = 4)$ (or the alternative form $\pi_0(\lambda_l) = gamma(\lambda_l \mid \beta = 0.8333, \alpha_2 = 4)$), from the VFLAW (SAW) information specialized to Beaver Valley 2 by using the bead thickness of 0.26" and converted to per unit inch (using the SAW data listed in Table 6.6 of NUREG/CR-6817[5]), the posterior distribution of λ_l is calculated and fitted into another gamma distribution. The posterior gamma PDF representing the Beaver Valley 2 RPV would be $\pi_1(\lambda_l) = gamma(\lambda_l \mid \alpha_1 = 1.186, \alpha_2 = 5)$ and plotted and compared to the prior PDF in Figure C-8 (see Appendix C-1). The gamma distributions used to describe flaw-depth intensity and flaw density in Table C-2 are normalized based on the bead thickness. As evident from Table C-2, VFLAW uses normalized flaw-depth distributions (i.e., based on a/Δ instead of a). Assuming a bead thickness of 0.26", the normalized gamma prior and posterior PDFs for large-flaw-depth intensity for Beaver Valley 2 would be $\pi_0(\lambda_l) = gamma(\lambda_l \mid \alpha_1 = 4.615, \alpha_2 = 4)$ and $\pi_1(\lambda_l) = gamma(\lambda_l \mid \alpha_1 = 4.563, \alpha_2 = 5)$. Note that Figure C-8 is not the normalized version. The normalized posterior would be the new hyper-distribution that reflects the measured data and can be used in the VFLAW and FAVOR runs for Beaver Valley 2 RPV.

From Figure C-8, it is evident that the prior and posterior values are very similar, because only one flaw depth data point is reported and used, so the posterior relies primarily on the prior information. The impact will, however, affect the density PDF more strongly.

[5] Note that to specialize VFLAW flaw-depth distributions for Beaver Valley 2, only PVRUF large-flaw depths reported for SAW in Table 6.6 of the NUREG/CR-6817 were used instead of the distributions summarized in Table 1-2 of this report.

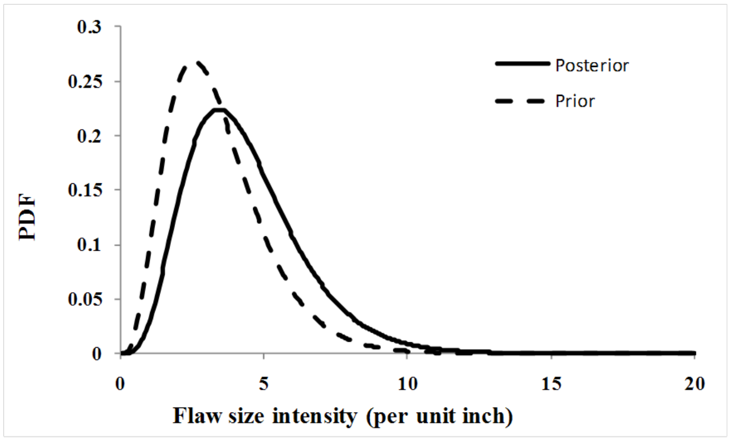


Figure C-8 Prior and posterior distributions of the flaw-depth intensity of parameter λ_l

C.3.4.2 Bayesian Updating of the Parameters of Small Flaw Depth Distribution Based on the 3/8t UT Inspection Data

Flaw depths smaller than the bead thickness for PVRUF (from Table 6.4 in NUREG/CR-6817) were analyzed and appeared to best fit an exponential PDF. That is:

$$f(a \mid \lambda_s) = \frac{\lambda_s e^{-\lambda_s a}}{1 - e^{-0.26\lambda_s}}, \lambda_s > 0, \; a > 0 \qquad \text{Eqn. (C-29)}$$

where λ_s is the flaw depth (per inch) for small flaws. The hyper-distribution of λ_s was also estimated as the gamma distribution $\pi_0(\lambda_s) = gamma(\lambda_s \mid \alpha_1 = 2.854, \alpha_2 = 39)$ that was used as the prior PDF for Beaver Valley 2.

The procedure from this point on is the same as that for the large flaws with the exception that the NDE data for small flaws were given in the form of a single flaw depth interval, as discussed in Section C.3.1. Accordingly, with m = 1 and using Eqn. (C-17), the likelihood function for the evidence consisting of 103 detected (observed) flaws, all with a depth of less than 0.125" but larger than 0.04" (or 0.075" as sensitivity value), will be:

$$L(\text{Data} \mid \lambda_s) = \left[\frac{1}{POD(\lambda_s)} \int_{0.075 or 0.04}^{0.125} \int_{-1}^{1} \left[1 - \frac{1}{1 + e^{63.2100(a^* - M_\varepsilon - 0.1124)}} \right] \left(\frac{\lambda_s e^{-\lambda_s (a^* - M_\varepsilon)}}{1 - e^{-0.26\lambda_s}} \right) \left(13.41 e^{-564.55(M_\varepsilon + 0.1905 a^* - 0.0476)^2} \right) dM_\varepsilon da^* \right]^{10}$$

Eqn. (C-30)

The Bayesian updating for small flaws is the same as Eqn. (C-28) and the likelihood given by Eqn. (C-30) results in the posterior distributions of λ_s as shown in Figure C-9 (see Appendix C-1). Also, a plot of the POD(λ_s) as expressed by equation:

$$POD(\lambda_s) = \int_{0}^{0.26} \left(1 - \frac{1}{1 + e^{63.2100(a - 0.1124)}} \right) \frac{\lambda_s e^{-\lambda_s a}}{\left(1 - e^{-0.26\lambda_s a}\right)} da \qquad \text{Eqn. (C-31)}$$

is shown in Figure C-10. Clearly, because small flaws are associated with small POD and considerable measurement error, the impact of these would be significant in the posterior results shown in Figure C-9. The posterior can be expressed as the gamma PDF $\pi_1(\lambda_s) = gamma(\lambda_s \mid \alpha_1 = 1.614, \alpha_2 = 60)$. The normalized versions of the prior and posterior can be expressed by dividing α_1 by the bead thickness of 0.26". Note that Figure C-9 does not show the normalized versions of the prior and posterior distributions.

The VFLAW data for small flaw depths uses the multinomial distribution, whose parameters are described by the Dirichlet PDF. Accordingly, it is possible to find the equivalent Dirichlet PDFs that best describe the posterior PDF of λ_s expressed in form of the gamma distribution.

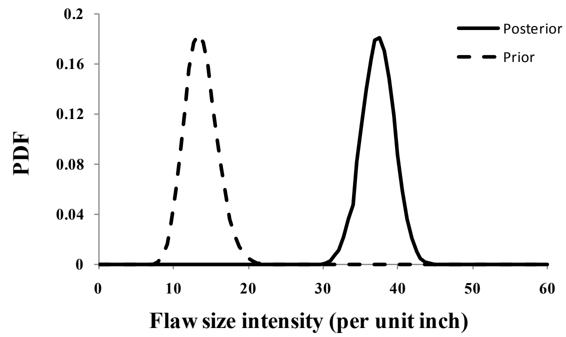


Figure C-9 Bayesian prior and posterior PDFs of λs (per unit inch)

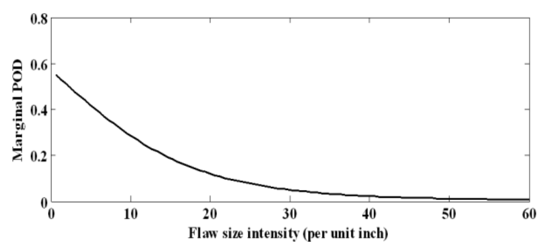


Figure C-10 Marginal POD independent of small flaw depth

To update the Dirichlet hyper-distribution that represents uncertainties in the parameters of the multinomial distribution representing small-flaw-depth PDF used in VFLAW, the posterior PDF of λ_s shown in Figure C-9 is used to calculate the number of flaws in each of the ranges (0" to 0.072", 0.072" to 0.126", and 0.126" to 0.170") used by the multinomial distribution in VFLAW. Because the Dirichlet distribution is a conjugate distribution, the posterior number of flaws is found (see Section C.3.4.3.2 for estimating the number of posterior flaws) by adding the posterior mean number of flaws in each flaw-depth bin (see Table C-3). When added to the prior number of flaws (see Appendix A of NUREG/CR-6817 for the procedure), the updated Dirichlet values are viewed as being more representative of the distributions of true flaws in the Beaver Valley 2 RPV and are summarized in Table C-3.

Table C-3 Updated VFLAW Distribution for Small Flaws

Flaw-Depth Bins (in)	Normalized Flaw-Depth Bins (per NUREG/ CR-6817) per Unit of Bead Thickness	Prior U (see Table C-2)	Prior Multinomial Parameter	Posterior U	Updated Mean of Multinomial Parameter
a_1 (0 to 0.072)	0.25 (0.0 to 0.4)	$U_1 = 34$	$P_1 = 0.7907$	$U'_1 = 479.75$	$P'_1 = 0.9639$
a_2 (0.072 to 0.126)	0.55 (0.4 to 0.7)	$U_2 = 8$	$P_2 = 0.1860$	$U'_2 = 9.71$	$P'_2 = 0.0332$
a_3 (0.126 to 0.17)	0.85 (0.7 to 0.1)	$U_3 = 1$	$P_3 = 0.0233$	$U'_3 = 5.354$	$P'_3 = 0.0029$

A critical observation from this example is that the posterior results of the flaw-depth distribution in general and small depth distribution in particular are most sensitive to the POD model and measurement error model and their associated uncertainties. The lower tail of the POD model, in the ranges of small flaw depths (<0.1-in.), expects small probabilities of detection. When a flaw of small depth is reported, because of the corresponding small POD, it increases the likelihood that there are several flaws not detected for the one detected. This will substantially affect the results.

Appendix C-1 describes the MATLAB routine used to solve the integrals in Eqn. (C-29) through Eqn. (C-31) to estimate the posterior PDF of small flaws.

C.3.4.3 Results of Updating Parameters of Flaw Density Distribution Based on the 3/8t UT Inspection Data

In Section C.2.3.2, two methods were presented to update the flaw densities. One was based on a binomial likelihood function (Eqn. (C-19)) and one used the Poisson density and took advantage of the conjugate properties of the prior gamma PDF used as the prior distribution of the intensity, ρ, of the Poisson distribution (Eqn. (C-23)). The later method is used to update the flaw densities for this example. This method is based on the mean values only and is simpler than the former.

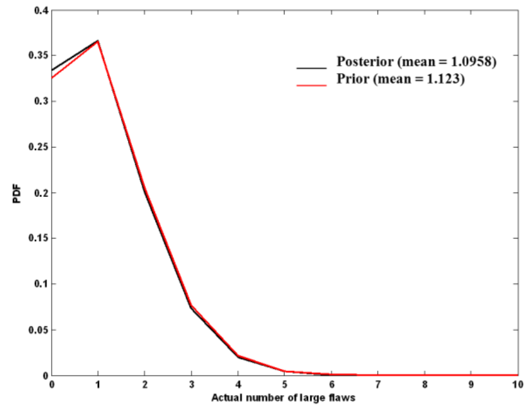
C.3.4.3.1 Posterior Density of Large Flaws

The number of large flaws (size > 0.26 inch), given the single UT-detected flaw, yields the posterior flaw depth intensity, λ_l, which was shown in Figure C-8. The marginal POD independent of the flaw size was almost 1 (for any value of posterior λ_l). Accordingly, using Eqn. (C-20), the number of flaws based on the posterior estimates of flaw depth would be 1.

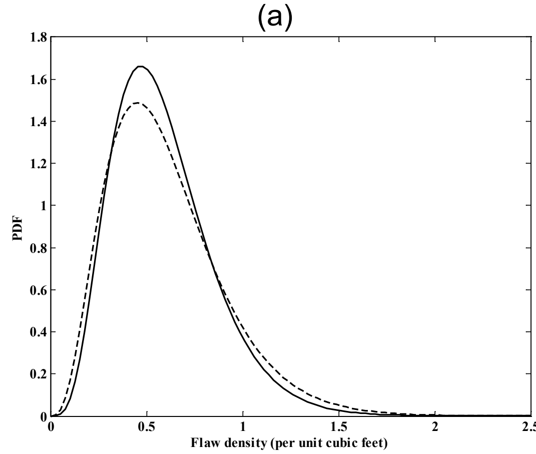
Using the conjugate features of the prior gamma distribution for $\rho_{l,}$ the posterior distribution (see Appendix A of NUREG/CR-6817) will be:

$$\pi_1(\rho_l \mid n_l) = gamma(\rho_l \mid \alpha_1 = 6.6467 + V, \alpha_2 = 4 + n_l) = gamma(\rho_l \mid \alpha_1 = 8.5119, \alpha_2 = 5)\ \text{flaws/ ft}^3 \qquad \text{Eqn. (C-32)}$$

Figure C-11 compares prior and posterior distributions of the number of flaws and flaw intensity of large flaws for Beaver Valley 2 in a volume of 1.8652 ft^3. Note that VFLAW values are in cubic meter. The equivalent prior and posterior distributions in cubic meter are summarized in Table C-4.



(a)



(b)

Figure C-11 Prior and posterior flaw density (a) and intensity (b) for large size flaw

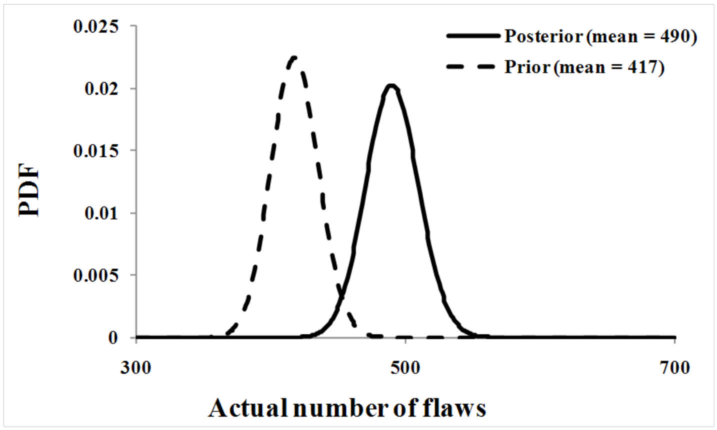
C.3.4.3.2 Posterior Density of Small Flaws

Similar to the large flaw density, the prior gamma distribution representing the flaw density per unit volume, ρ_s, used in the VFLAW was updated based on the 103 UT-detected small flaws in the interval of 0.04" to 0.125". This would yield the posterior flaw depth intensity, λ_s, as was shown in Figure C-9. The mean value of the flaw depth intensity (i.e., λ_s = 37.16) estimated by the posterior shown in Figure C-9 yields a marginal probability of detection independent of flaw depth of, POD(λ_s) = 0.0274.

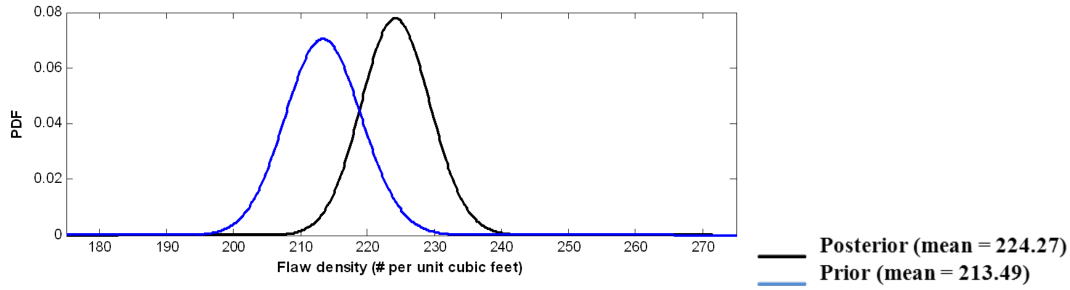
The likelihood of observing ns small flaws would be expressed as:

$$\pi_1(\rho_s \mid n_s) = gamma(\rho_s \mid \alpha_{1,s}^{pos} = 6.6467 + V, \alpha_{2,s}^{pos} = 1419 + n_s)$$
$$= gamma(\rho_s \mid \alpha_{1,s}^{pos} = 8.5119, \alpha_{2,s}^{pos} = 1909)$$
$$\pi_0(\rho_s) = gamma(\rho_s \mid \alpha_{1,s} = 6.6467, \alpha_{2,s} = 1419)\text{flaws}/\text{ft}^3$$
$$(\text{Table 6.2 SAW} - \text{PVRUF NUREG/CR-6817}) \qquad \text{Eqn. (C-33)}$$

Figure C-12 compares prior and posterior distributions of the number of flaws and volumetric flaw intensity of small flaws.



(a)



(b)

Figure C-12 Prior and posterior flaw density (a) and intensity (b) for small size flaws

Because the posterior flaw density distributions shown in Figure C-11 and Figure C-12 are based on the mean values of λ for both large and small flaws, a Monte Carlo simulation was used to select random realizations of λ from the posterior PDFs of λ for large and small flaws to develop the corresponding posterior flaw density PDFs. Figure C-13 shows the results of the spread of the number of the flaws of various depths for the Beaver Valley 2 RPV, including the epistemic uncertainties shown in the form of box plots.

Similar to the flaw-depth distribution, the posterior distribution of flaw density will be dominated by the POD and measurement error models and their uncertainties. Specifically, when a large number of small flaws are reported during the NDE inspection, the corresponding low POD value increases the number of expected undetected flaws.

Based on the results of this section, Table C-4 summarizes the posterior results to be used for Beaver Valley 2 VFLAW and FAVOR runs. The posterior results have been changed to metric units in this table, because VFLAW uses metric values.

Table C-4 Summary of the Posterior Parameter PDFs of Flaw Depth and Flaw Density to be used in VFLAW and FAVOR Runs for Beaver Valley 2

Case	Flaw Size Category	Welding Process	Random Variable Representing Flaw Depth	PDF of Flaw Depth	Parameters of PDF	Distribution Describing Uncertainty of Parameters of PDF	Original VFLAW Parameters of Uncertainty Distribution (Flaw Depth parameters are specialized to Beaver Valley 2	Posterior Parameters of Uncertainty Distribution Based on Beaver Valley 2 Specialized Prior and NDE Data
1	Small ($a \leq \Delta$)	SAW	Flaws per cubic meter	Poisson	ρ	Gamma	$\alpha_3 = 0.180$ $\alpha_4 = 1419$	$\alpha'_3 = 0.230$ $\alpha'_4 = 1909$
2	Large ($a > \Delta$)	SAW	Flaws per cubic meter	Poisson	ρ	Gamma	$\alpha_3 = 0.180$ $\alpha_4 = 4$	$\alpha'_3 = 0.230$ $\alpha'_4 = 5$
3	Small ($a \leq \Delta$)	SAW	a/Δ	Multinomial	P_1, P_2, P_3	Dirichlet	$U_1 = 34$ $U_2 = 8$ $U_3 = 1$	$U'_1 = 513.75$ $U'_2 = 17.71$ $U'_3 = 1.54$
4	Large ($a > \Delta$)	SAW	a/Δ	Exponential	λ	Gamma	$\alpha_1 = 4.615$[6] $\alpha_2 = 4$	$\alpha'_1 = 4.563$ $\alpha'_2 = 5$

[6] VFLAW combined all SAW and SMAW flaw data to arrive at the gamma distribution with $\alpha_1 = 21.68$ $\alpha_2 = 52$. As described in Section C.3.4.1, this example used only PVRUF SAW data for large flaw depths to build the specialized Beaver Valley prior PDF.

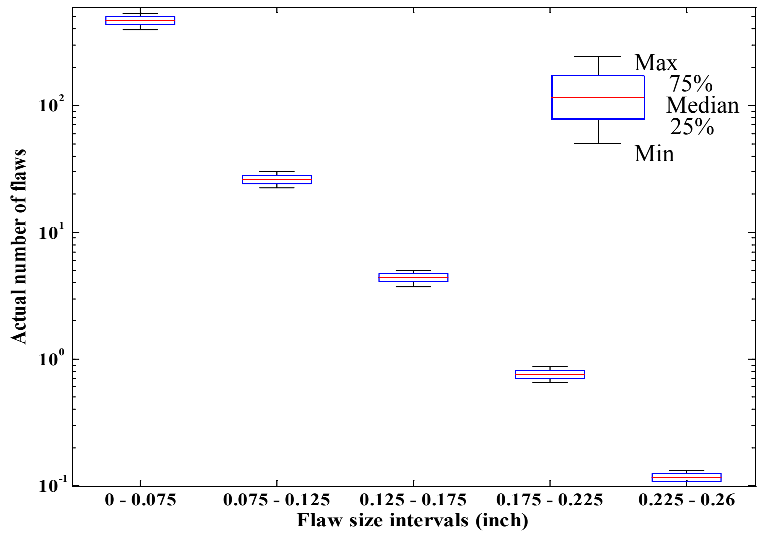


Figure C-13 Posterior number of flaws in the 3/8t region in various flaw size intervals including epistemic uncertainties

C.3.4.3.3 Sensitivity of the Flaw Density Results to a Lower Bound of 0.075" for the Interval Data Observed in the 3/8t Region

Estimations of the posterior PDFs presented in Sections C.3.4.3.1 and C.3.4.3.2 have been made by assuming that the observed interval of small flaws was 0.075" to 0.125". To assess the sensitivity of this assumption, it is assumed that the detection up to 0.075" is possible and all data would be between 0.075" and 0.125". Repeating the calculations in Section C.3.4 (including subsections) yields the posterior flaw depth and density PDFs that are very similar. Therefore, it was concluded that the results are relatively insensitive to choice for the lower bound of the data. More discussions of this topic are presented in Section C.3.5.

C.3.5 Updating the 10 CFR 50.61a Tables

The NDE data from the inspection volume specified in Supplement 4 to Mandatory Appendix VIII to Section XI of the ASME Code (the first one-inch of the weld) is used as the evidence for the Bayesian updating procedure described in the previous sections to obtain the flaw depth and density characteristics for Beaver Valley 2. The posterior characteristics are used to develop the corresponding 10 CFR50.61a flaw tables (consisting of only 19 UT-detected flaws in the interval 0.04" to 0.125"). The procedure is the same as the one used to update the UT data observed in the 3/8t region as discussed in Section C.3.4.

If the posterior distributions of the flaw density are used to estimate the mean number of flaws in the ranges of flaw sizes described in the 10 CFR 50.61a flaw tables, the results should be prorated to the number of flaws per 1,000" of weld. Because Beaver Valley 2 has a total weld length of 816.18", the prorated mean number of flaws was calculated and compared with the allowable number of flaws per length of weld, as shown in Table C-5. If the lower limit of the observed data interval is changed from 0.04" to 0.075" to line up with the smallest bin size in the 10 CFR 50.61a flaw tables, the results summarized in Table C-5 are calculated. In this case, the results of the mean number of flaws were also not too sensitive to the choice of the lower limit of the interval of NDE data.

To assess the epistemic uncertainties in the POD and measurement error uncertainties, again for the case of the Supplement 4 inspection volume (the first one inch), a Monte Carlo simulation was used to select random realizations of λ from the posterior PDFs of λ for both large and small flaws to develop the corresponding posterior flaw density PDFs. Repeating this process will result in the epistemic uncertainty for each flaw depth interval used in Table C-4. Figure C-14 shows the results of the number of the flaws of various depth intervals, by employing box and whisker plots. Epistemic uncertainties are larger (than those shown in Figure C-13), because of the smaller evidence, because there were only 19 observed flaws in the Supplement 4 inspection volume.

Table C-5 Alternate PTS Rule Flaw Table Assessment using Mean Number-of-Flaws by Size Interval for Beaver Valley 2 (Assuming a Lower Limit of 0.04" for Observed Data Interval)

Flaw Depth (inch)	Observed (Detected) Number of Flaws (Biased)	Posterior Mean Number of Flaws (Unbiased and Corrected for POD)	Rule's Limits per 1,000" of Weld
0.000 < a ≤ 0.075	19	124.98	No limit
0.075 < a ≤ 0.475		38.21	166.70
0.125 < a ≤ 0.475	0	14.13	90.80
0.175 < a ≤ 0.475	0	4.86	22.82
0.225 < a ≤ 0.475	0	1.30	8.66
0.275 < a ≤ 0.475	0	0.21	4.01
0.325 < a ≤ 0.475	0	0.13	3.01
0.375 < a ≤ 0.475	0	0.09	1.49
0.425 < a ≤ 0.475	0	0.04	1.00

Table C-6 Alternate PTS Rule Flaw Table Assessment using Mean Number-of-Flaws by Size Interval for Beaver Valley 2 (Assuming a Lower Limit of 0.075" for Observed Data Interval)

Flaw Depth (inch)	Observed (Detected) Number of Flaws (Biased)	Posterior Mean Number of Flaws (Unbiased and Corrected for POD)	Rule's Limits per 1,000" of Weld
0.000 < a ≤ 0.075	0	122.89	No limit
0.075 < a ≤ 0.475	19	39.05	166.70
0.125 < a ≤ 0.475	0	14.69	90.80

0.175 < a ≤ 0.475	0	5.12	22.82
0.225 < a ≤ 0.475	0	1.38	8.66
0.275 < a ≤ 0.475	0	0.21	4.01
0.325 < a ≤ 0.475	0	0.13	3.01
0.375 < a ≤ 0.475	0	0.08	1.49
0.425 < a ≤ 0.475	0	0.04	1.00

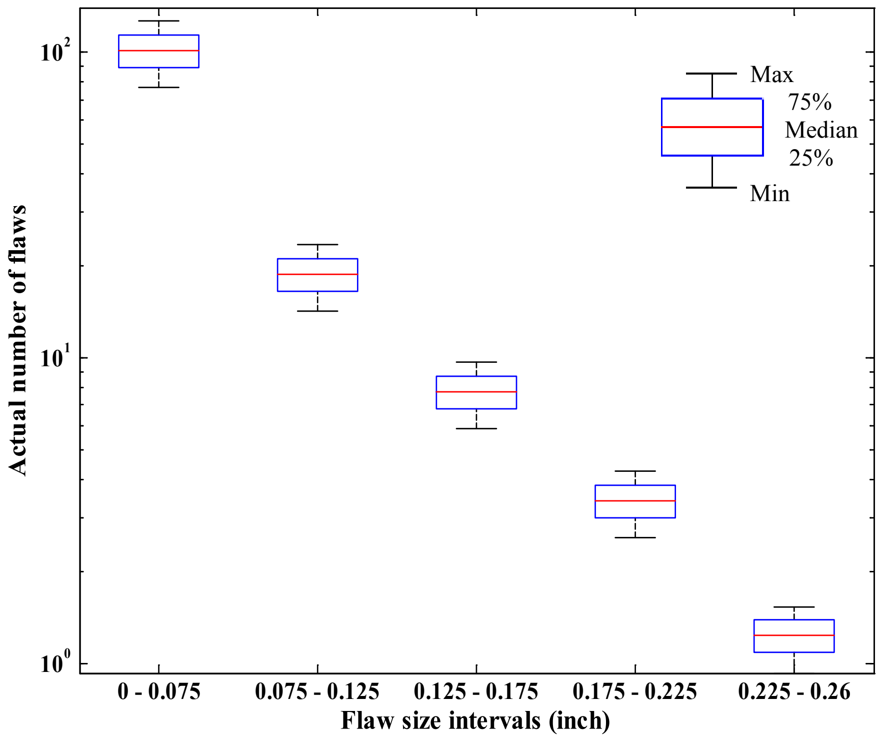


Figure C-14 Posterior number of flaws in the Supplement 4 inspection volume in various flaw size intervals including epistemic uncertainties

C.4 References

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[C-2] Williams, P.T., T.L. Dickson, and S. Yin, "Fracture Analysis of Vessels - Oak Ridge FAVOR, v09.1, Computer Code: Theory and Implementation of Algorithms, Methods, and Correlations," ORNL/TM-2010/5, January 2010, Oak Ridge National Laboratory, Oak Ridge, TN.

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[C-7] Georgiou, G.A., "Probability of Detection (PoD) Curves: Derivation, Applications and Limitations," Research Report 454, UK Health & Safety Executive, London, UK, 2006.

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[C-10] Chatterjee, K., and M. Modarres, "A Bayesian Probabilistic Approach to Improved Health Management of Steam Generator Tubes," published online by the Prognostics and Health Management Society, 2011, available at https://www.phmsociety.org/sites/phmsociety.org/files/phm_submission/2011/phmc_11_012.pdf (accessed July 21, 2014).

[C-11] Celeux, G., et al., "Using Markov Chain Monte Carlo Methods to Solve Full Bayesian Modeling of PWR Vessel Flaw Distributions," *Reliability Engineering and System Safety*, 66(3):243–252, December 1999.

[C-12] Chatterjee, K., and M. Modarres, "A Probabilistic Approach for Estimating Defect Size and Density Considering Detection Uncertainties and Measurement Errors," *Journal of Risk and Reliability*, 227(1):28–40, February 2013.

[C-13] Spanner, J., "Materials Reliability Program: Reanalysis of Reactor Vessel Examination Data from the 1996 Beaver Valley 2 Vessel Examination (MRP-207), RPV Flaw Distribution," EPRI Report 1014548, November 2006, Electric Power Research Institute, Palo Alto, CA.

[C-14] NRC, "Probabilistic Fracture Mechanics - Models, Parameters, and Uncertainty Treatment Used in FAVOR Version 04.1," NUREG-1807, June 2007, ADAMS Accession No. ML072010411.

Appendix C-1: Sample MATLAB Routine

```
clear
%%*********************************************************************
%%This MATLAB routine estimates posterior values of parameters of flaw-
%%depth distributions for small and large flaws in RPVs using NDE data,
%%accounting for measurement error, POD, and epistemic uncertainties. The
%%routine solves Equations 16, 17 and 18. The specific data used in this
%%routine are related to the POD of Eqn. 25 and the measurement error
%%discussed in Section C.3.3 The NDE data of Beaver Valley 2 are used. It
%%also shows the solution to the likelihood functions of Eqn. 27 and Eqn. 30.
%%Finally the routine solves the Bayesian inferences in Eqn. 28 for both
%%small and large flaws.
%%*********************************************************************
% THIS ROUTINE IS FOR DEMONSTRATION OF ONE WAY TO SOLVE THE BAYESIAN
% INFERENCE METHODS DISCUSSED IN THIS REPORT. THE RESULTS MAY BE USED TO
% CROSS-CHECK THE RESULTS IF OTHER VALUES OR OTHER SOLUTION ROUTINES ARE
% USED. THE ROUTINE DOES NOT COVER ALL E ANALYSES PERFORMED AND DISCUSSED
% IN THIS REPORT. FOR EXAMPLE, THE ROUTINE TO ESTIMATE THE FLAW-DENSITY
% DISTRIBUTIONS HAS NOT BEEN PRESENTED (ONLY FLAW-DEPTH MODEL
% DISTRIBUTIONS HAVE BEEN PRESENTED).
%%*********************************************************************
%%LIMITATIONS
% 1. THIS ROUTINE ASSUMES THE SINGLE PARAMETER EXPONENTIAL DISTRIBUTION
% FOR MODELING DISTRIBUTION OF BOTH SMALL AND LARGE FLAW DEPTHS.
% 2. THE POSTERIOR FOR SMALL FLAWS WILL GO TO INFINITY IF THE RIGHT EXTREME
% OF THE LEFT-CENSORED NDE DATA OR LEFT EXTREME OF INTERVAL DATA FOR
% SMALL FLAWS IS EXTREMELY SMALL (THAT IS, LESS THAN 0.09 INCH).
% 3. THE POSTERIOR FOR SMALL FLAWS APPROACHES INFINITY FOR LARGE SIGMA;
% THAT IS, THE RANDOM ERROR FOR THE MEASUREMENT ERROR MODEL (WHEN SIGMA
% EXCEEDS 0.035").
%%*********************************************************************
%%ASSUMPTIONS
% 1. THIS ROUTINE ASSUMES LEFT-TRUNCATED SINGLE-PARAMETER EXPONENTIAL
% DISTRIBUTION FOR FLAW DEPTH FOR SMALL FLAWS.
% 2. THIS ROUTINE ASSUMES RIGHT-TRUNCATED SINGLE-PARAMETER EXPONENTIAL
% DISTRIBUTION FOR LARGE FLAWS.
% 3. THIS ROUTINE ASSUMES TWO-PARAMETER LOGISTIC DISTRIBUTION EQN. 4 WITH
% A POD THRESHOLD OF ZERO.
% 4. SIMILARLY TO EQN. 30, INTEGRAL RANGE FOR THE MEASUREMENT IS BETWEEN
% -1 AND 1, WHICH COVERS THE EXTREME RANGES OF THE BIAS AND RANDOM ERRORS.
%%*********************************************************************
%%NOMENCLATURE:
%m & c are parameters discussed in Eqn. 8; sigma is standard deviation of
%random error associated with the measurement error model of Eqn. 8.
%beta1 & beta2 are POD function parameters in Eqn. 4; ath is the detection
%threshold of Eqn. 4.
%atr is the transition flaw depth between small and large flaws discussed
%in Eqn. 9.
%lambda1 & lambda2 are flaw-depth distribution parameters (i.e., the flaw-
% depth intensity) for small and large defects respectively.
%n1 is the total number of censored NDE data for small flaws.
%are is the right extreme of left-censored or interval of small-flaw-
%depth NDE data.
%ale is the left extreme of interval of small-flaw-depth data; ale must
```

```
% be greater than the parameter c of the measurement error model.
%a1 is a set, representing values of exact small-flaw-depth NDE data
%reported.
%n2 is the number of exact small-flaw-depth NDE data reported
%n3 is the total number of exact large-flaw-depth NDE data reported
%n4 is the total number of interval or left-censored large-flaw-depth NDE
%data reported
%a2 is set, representing exact values of large-flaw-depth NDE data
%reported
%are_large is the right extreme of the left-censored or interval large-
%flaw-depth NDE data reported
%ale_large is the left extreme of interval data of large-flaw-depth NDE
%data reported
%%*********************************************************************
%%Measurement error parameters
m=0.84;c=0.04;sigma=0.0298;
%%*********************************************************************
%%POD parameters
ath=0;beta1=63.21;beta2=0.1124;
%%*********************************************************************
%%Transition point for large flaws
atr=0.26;
%%*********************************************************************
%%*********************************************************************
%%NDE data of small flaws
n1=103;are=0.125;ale=c;a1=[0.15];n2=0;
%%*********************************************************************
%%*********************************************************************
%%NDE data of large flaws
a2=[0.26];n3=length(a2);n4=0;ale_large=0.27;are_large=0.3;
%%*********************************************************************
%BAYESIAN INFERENCE FOR ESTIMATING POSTERIOR DISTRIBUTION OF THE PARAMETER
%LAMBDA (FLAW-DEPTH INTENSITY) OF THE SMALL-FLAW-DEPTH EXPONENTIAL PDF
lambda1=linspace(0,60,100);
Norm_const=0;
for i=2:length(lambda1)
Marginal_Pod=@(a)((1-(1+exp(-beta1*beta2))./(1+exp(beta1*(a-beta2-ath)))).*(l
ambda1(i).*exp(-lambda1(i).*a)./(1-exp(-lambda1(i).*atr))));
Likeli_int=@(Ea,a)((1-(1+exp(-beta1*beta2))./(1+exp(beta1*(a-Ea-beta2-ath))))
.*(lambda1(i).*exp(-lambda1(i).*(a-Ea))./(1-exp(-lambda1(i).*atr))).*((1/sqrt
(2*pi*sigma^2)).*exp(-(1/(2*sigma^2)).*((m*Ea+(1-m)*a-c)/m).^2)));
Likeli_exact=@(Ea)((1-(1+exp(-beta1*beta2))./(1+exp(beta1*(a1-Ea-beta2-ath)))
).*(lambda1(i).*exp(-lambda1(i).*(a1-Ea))./(1-exp(-lambda1(i).*atr))).*((1/sq
rt
(2*pi*sigma^2)).*exp(-(1/(2*sigma^2)).*((m*Ea+(1-m)*a1-c)/m).^2)));
Likelihood_exact(i)=((quad(Likeli_exact,-1,1))./(quad(Marginal_Pod,0,atr)))^n
2;
Likelihood_int(i)=((dblquad(Likeli_int,-1,1,ale,are))./(quad(Marginal_Pod,0,a
tr)))^n1;
Prior_small(i)=(gampdf(lambda1(i),39,.3504));
Numerator(i)=Likelihood_int(i).*Likelihood_exact(i).*Prior_small(i);
Norm_const=Norm_const+Numerator(i)*(lambda1(i)-lambda1(i-1));
end
Posterior_small=Numerator/Norm_const;
Mean_Posterior_Small_Flaw_Depth_Intensity=sum(lambda1.*Posterior_small)*0.606
1
Mean_Posterior_Small_Flaw_Depth=1/Mean_Posterior_Small_Flaw_Depth_Intensity
```

```
POD_of_Posterior_Mean_Small_Flaw_Depth=1-(1+exp(-beta1*beta2))./(1+exp(beta1*
(Mean_Posterior_Small_Flaw_Depth-beta2-ath)))
subplot(211)
plot(lambda1,Posterior_small,lambda1,Prior_small,'-.','LineWidth',2)
xlabel('Flaw Depth intensity (per unit
inch)','fontsize',12,'fontweight','b','FontName','Times New Roman')
ylabel('Relative Frequency','fontsize',12,'fontweight','b','FontName','Times
New Roman')
title('Posterior and prior flaw depth intensity for small
flaws','fontsize',14,'fontweight','b','FontName','Times New Roman')
h = legend('Posterior_small','Prior_small');
set(h,'Interpreter','none')
set(gca,'FontSize',12,'FontWeight','b','FontName','Times New Roman')
%%***************************************************************
%BAYESIAN INFERENCE FOR ESTIMATING POSTERIOR DISTRIBUTION OF THE PARAMETER
%LAMBDA (FLAW-DEPTH INTENSITY) OF THE LARGE-FLAW-DEPTH EXPONENTIAL PDF
lambda2=linspace(0,10,100);
Norm_const1=0;
for i=2:length(lambda2)
Marginal_Pod1=@(a)((1-(1+exp(-beta1*beta2))./(1+exp(beta1*(a-beta2-ath)))).*(
lambda2(i).*exp(-lambda2(i).*(a-atr))));
Likeli_exact1=@(Ea)((1-(1+exp(-beta1*beta2))./(1+exp(beta1*(a2-Ea-beta2-ath))
)).*(lambda2(i).*exp(-lambda2(i).*(a2-Ea-atr))).*((1/sqrt(2*pi*sigma^2)).*exp
(-(1/
(2*sigma^2)).*((m*Ea+(1-m)*a2-c)/m).^2)));
Likelihood_exact1(i)=((quad(Likeli_exact1,-1,1))./(quad(Marginal_Pod1,atr,10)
))^n3;
Likeli_int1=@(Ea,a)((1-(1+exp(-beta1*beta2))./(1+exp(beta1*(a-Ea-beta2-ath)))
).*(lambda2(i).*exp(-lambda2(i).*(a-Ea-atr))).*((1/sqrt(2*pi*sigma^2)).*exp(-
(1/
(2*sigma^2)).*((m*Ea+(1-m)*a-c)/m).^2)));
Likelihood_int1(i)=((dblquad(Likeli_int1,-1,1,ale_large,are_large))./(quad(Ma
rginal_Pod1,atr,10)))^n4;
Prior_large(i)=(gampdf(lambda2(i),4,0.8333));
Numerator1(i)=Likelihood_exact1(i).*Likelihood_int1(i).*Prior_large(i);
Norm_const1=Norm_const1+Numerator1(i)*(lambda2(i)-lambda2(i-1));
end
Posterior_large=Numerator1/Norm_const1;
Posterior_small=Numerator/Norm_const;
Mean_Posterior_Large_Flaw_Depth_Intensity=sum(lambda2.*Posterior_large)*0.101
0
Mean_Posterior_Large_Flaw_Depth=1/Mean_Posterior_Large_Flaw_Depth_Intensity
POD_of_Posterior_Mean_Large_Flaw_Depth=1-(1+exp(-beta1*beta2))./(1+exp(beta1*
(Mean_Posterior_Large_Flaw_Depth-beta2-ath)))
subplot(212)
f1=plot(lambda2,Posterior_large,lambda2,Prior_large,'-.','LineWidth',2)
xlabel('Flaw depth intensity (per unit
inch)','fontsize',12,'fontweight','b','FontName','Times New Roman')
ylabel('Relative Frequency','fontsize',12,'fontweight','b','FontName','Times
New Roman')
title('Posterior and prior flaw depth intensity for large
flaws','fontsize',14,'fontweight','b','FontName','Times New Roman')
h = legend('Posterior_large','Prior_large');
set(h,'Interpreter','none')
set(gca,'FontSize',12,'FontWeight','b','FontName','Times New Roman')
screen_size = get(0, 'ScreenSize');
f1 = figure(1);
```

```
set(f1, 'Position', [0 0 screen_size(3) screen_size(4) ] );
%%***********************************************************************
```

Output from the above routine is displayed in Figure C-14 (also shown in Figure C-8 and Figure C-9)

```
Mean_Posterior_Small_Flaw_Depth_Intensity =
37.8118
Mean_Posterior_Small_Flaw_Depth =
0.0264
POD_of_Posterior_Mean_Small_Flaw_Depth =
0.0035
Mean_Posterior_Large_Flaw_Depth_Intensity =
5.4042
Mean_Posterior_Large_Flaw_Depth =
0.1850
POD_of_Posterior_Mean_Large_Flaw_Depth =
0.9900
f1 =
230.0087
231.0082
Published with MATLAB® 7.12
```

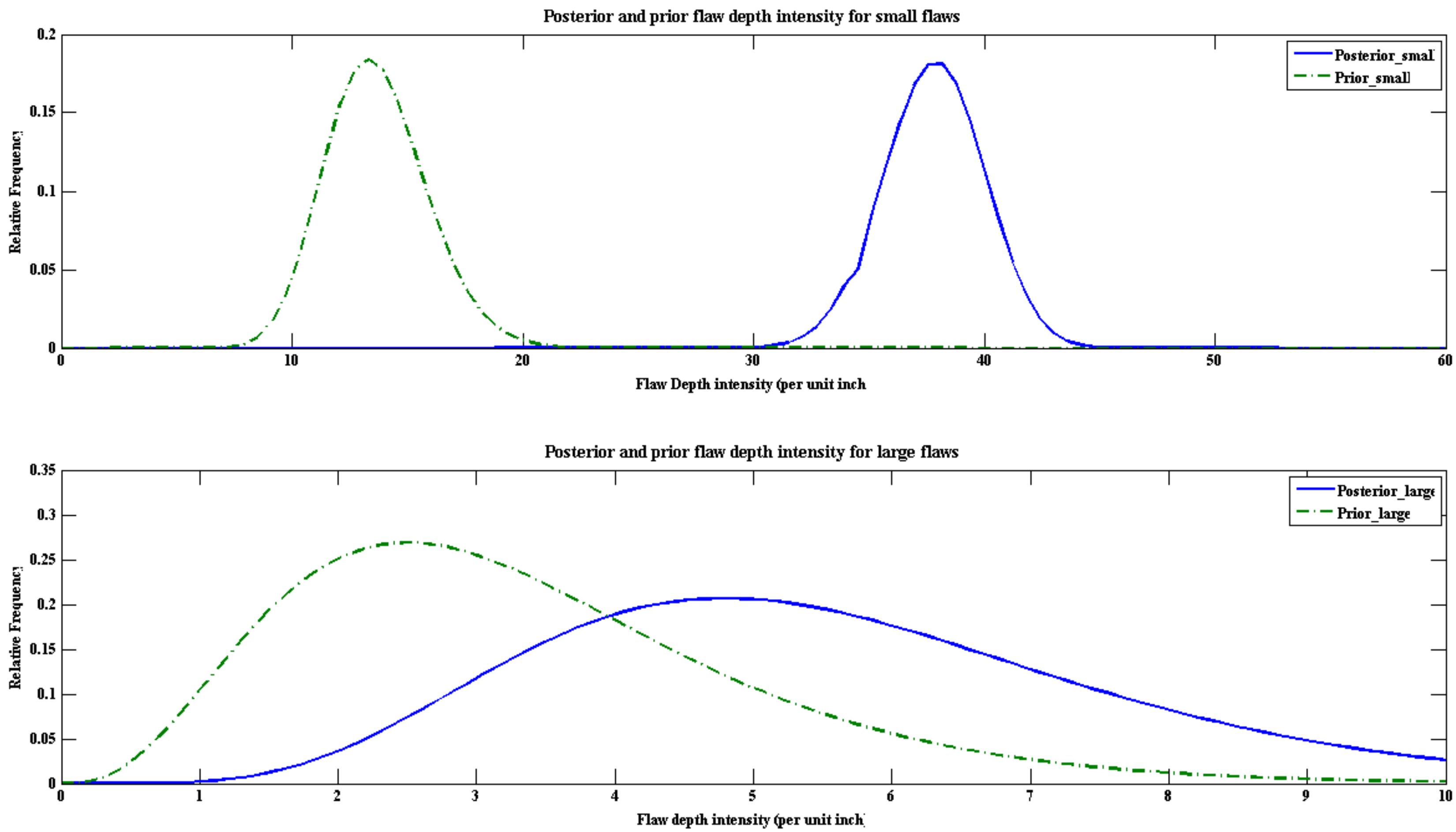

Figure C-15 MATLAB Routine Output

APPENDIX D SENSITIVITY STUDY RESULTS ON FLAW DISTRIBUTIONS CONSIDERING VFLAW DATA, POD, AND MEASUREMENT ERRORS IN NDE DATA

Prepared for the U.S. Nuclear Regulatory Commission under the Subcontract 4000111626 with UT Battelle, LLC (Oak Ridge National Laboratory)

Mohammad Modarres
University of Maryland

March 2012

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ABBREVIATIONS

PDF	Probability Density Function
NDE	Nondestructive Evaluation
POD	Probability of Detection
RPV	Reactor Pressure Vessel
SAW	Submerged Arc Weld
UT	Ultrasonic Test

SYMBOLS AND EXPRESSIONS

a	True flaw depth (inches)
a*	NDE measured (or observed) flaw depth (inches)
ath	Threshold flaw depth for detection, below which flaw detection is beyond the capability of the NDE technology used
D	The event that a flaw is detected
	The event that a flaw is not detected
EM	Model error of the NDE measurement error, represented by a normal distribution with a mean of zero and known standard deviation
L(a|Φ)	Likelihood of true flaw depth given the vector of parameters Φ
L(Data|θ)	Likelihood of observed NDE data conditioned on (given) the unknown parameter θ
	Likelihood of observing n* flaws given that there are a total of nj true flaws
Mε	NDE measurement error (combined random and systematic errors)
n	Number of flaw depth intervals (reported in NDE)
"n" ¯	Mean of the PDF of the number of flaws in volume v
n*	Number of exact flaw depths observed (reported in NDE)
	Combination of n* observed flaws out of total flaws nj (observed or detected, and unobserved or not detected flaws)
POD(a)	Probability of detection of a flaw of depth a
Pr(.)	Probability
Pr(D)	POD independent of flaw depth
	Probability of no detection regardless of size
	Probability of total flaws nj conditioned on observing n* flaws in NDE
βi	Parameter i of the POD model
Δ	Weld bead thickness
π0(θ)	Prior PDF of an unknown parameter θ
π1(θ|Data)	Posterior PDF of an unknown parameter given observed NDE data
Φ	Vector of parameters of the flaw depth PDF
θ	An unknown parameter of a model

D.1 Introduction

This report discusses the results of a sensitivity analysis by applying a Bayesian updating methodology described in Appendix C to account for probability of detection (POD) and measurement (sizing) error in the data for flaws detected through ultrasonic testing (UT). The methodology estimates vessel specific flaw depth and density distributions for comparison to the 10 CFR 50.61a screening tables and updates the VFLAW code's distributions for further analysis with the FAVOR code. The sensitivity analysis was performed using assumed nondestructive examination (NDE) flaw data. Existing VFLAW distributions for flaw depth and density, representing welds of the Pressure Vessel Research User Facility (PVRUF) vessel, were specialized to the Beaver Valley 2 reactor pressure vessel (RPV) welds and assumed to properly describe prior flaw depth and flaw density distributions and characteristics.

In the remainder of this Appendix, a very brief overview of the methodology is described first, followed by the results of the sensitivity analysis. The results are compared to the 10 CFR 50.61a screening tables and conclusions are summarized.

D.2 Overview of the Bayesian Approach to Update Flaw-Depth and Flaw-Density Distributions

Finding flaws using NDE requires characterization of associated uncertainties. The reliability of an inspection is customarily expressed in terms of the POD of a given flaw size and expressed by curves of POD vs. flaw size. Additionally, sizing or measurement errors occur and model uncertainties exist. Sizes of UT-detected small flaws in RPVs tend to be overestimated while the sizes of large flaws are underestimated [D-1].

POD is generally modeled as a function of true flaw depth. Different forms of POD curves have been used in the literature (see References [D-2], [D-3], and [D-4]. The logistic POD model for hit/miss data is a common model and is represented as:

$$POD(a \mid \beta_1, \beta_2, a_{th}) = \begin{Bmatrix} 1 - \dfrac{1 + e^{-\beta_1 \beta_2}}{1 + e^{\beta_1 (a - \beta_2 - a_{th})}} & \text{for } a > a_{th} \\ 0 & \text{otherwise} \end{Bmatrix} \quad \text{Eqn. (D-1)}$$

Measurement error is defined by Eqn. (D-2), where Mε is the measurement error, a* is the measured value of flaw depth, and a is the true value of flaw depth:

$$M_\varepsilon = a^* - a \quad \text{Eqn. (D-2)}$$

In its simplest form, Mε can be represented by a linear function of true size, as shown in Eqn. (D-1), where m is the slope and c is the intercept of the line representing measurement error versus true flaw depth:

$$\begin{aligned} &M_\varepsilon = ma + c + E_M \\ &\text{where, } a = \text{true flaw depth and } E_M = N_M(0, \sigma_M) \end{aligned} \quad \text{Eqn. (D-3)}$$

The likelihood of exact flaw measurements reported may be expressed as a function of POD and Mε (see Appendix C). If, in addition to or instead of the exact flaw depth data, intervals of flaw depths are reported (such as the number of flaws observed at less than a given depth or between an upper and lower limit), the likelihood may also be similarly expressed (see Appendix C).

Regardless of the form of the data (exact flaw depth and/or interval data), the Bayesian inference of the vector of parameters Φ of the flaw-depth probability density function (PDF) would be obtained from the Bayesian inference $\pi_1(\Phi \mid \text{Data}) \propto L(\text{Data} \mid \Phi)\pi_0(\Phi)$, where $\pi_1(\Phi \mid \text{Data})$ is the posterior multivariate PDF of vector Φ and $\pi_0(\Phi)$ is the prior multivariate PDF of Φ.

If flaws are detected with a probability Pr(D) (or not detected with a probability of $\Pr(\overline{D}) = 1 - \Pr(D)$), the probability that a specific total number of flaws n* observed in a given volume v out of the true number of flaws n_j follows the binomial distribution (see References [D-5] and [D-6]:

$$L(n^* \mid n_j) = \binom{n_j}{n^*}[\Pr(D)]^{n^*n}[1 - \Pr(D)]^{n_j - n^*} \qquad \text{Eqn. (D-4)}$$

Accordingly, the mean estimate of the true number of flaws $\bar{n}$ would be found from:

$$\bar{n} = \frac{n^*}{POD(D)} \qquad \text{Eqn. (D-5)}$$

The Bayesian updating of n_j, which allows the estimation of the posterior distribution of n_j to describe the true number of flaws, would be:

$$\Pr(n_j \mid n^*) = \frac{L(n^* \mid n_j)\Pr(n_j)}{\sum_{n_j} L(n^* \mid n_j)\Pr(n_j)} \qquad \text{Eqn. (D-6)}$$

where the prior $\Pr(n_j)$ may be expressed by a Poisson distribution with parameter ρ (defined in VFLAW).

D.3 Application to a Base Case Example

The EPRI report by Spanner [D-7] provides UT-based measured flaw data near the inner surface (~2.5 inches) of the Beaver Valley Unit 2 RPV, including small flaw sizes. These data, while subject to POD and measurement error, provide a more vessel-specific perspective of the distribution of flaws for weld metals in the Beaver Valley 2 RPV than do the VFLAW distributions used in FAVOR.

The observed Beaver Valley 2 NDE data (with detection and sizing uncertainty) are mostly in the form of interval data as summarized below [D-7]:

> *19 weld flaws were detected by the UT NDE of Beaver Valley 2 in the first inch (ASME Code, Section XI, Mandatory Appendix VIII, Supplement 4 inspection volume) of the*

RPV (these data are assumed normalized to 1,000" of weld length), all having a flaw depth less than 0.125". [7]

The lower limit of the detected flaw intervals described above was not stated in [D-7], but is not zero. Two possible subjective lower limits were assumed, and later the sensitivities of the final (posterior) flaw distributions to these two choices were assessed. The two lower limits selected were 0.04" and 0.075".

The associated weld bead thicknesses are not reported in [D-7]. However, the weld region of the observed flaws and flaw length is reported. Such results must be corrected for detection and sizing capability, particularly for the small flaws. The Beaver Valley 2 RPV weld map is shown in Figure D-1 [D-8]. In the absence of the Beaver Valley average weld bead thickness as the point of transition between large and small depths, it was assumed that all flaws reported are in submerged arc welds (SAWs), which form over 90% of welds in the VFLAW data, with the bead thickness of Δ = 0.26". Using the Beaver Valley 2 RPV information shown in Figure D-1, the VFLAW data were specialized to represent the prior distributions of flaw depth and density for Beaver Valley 2 RPV.

Total Weld Length = 816.18"
Total Weld Volume = 4.975 ft^3
Total Weld Fusion Area = 92 ft^2
Weld Volume of 1" = 0.616 ft^3
Weld Volume of 3/8t = 1.865 ft^3

[7] In Appendix C, the same analysis is performed, except that the analysis did not assume that the data were normalized to 1,000" of linear length of weld. Instead, it assumed that the data came from 816.18" of weld, which is the actual length of weld in the Beaver Valley 2 RPV.

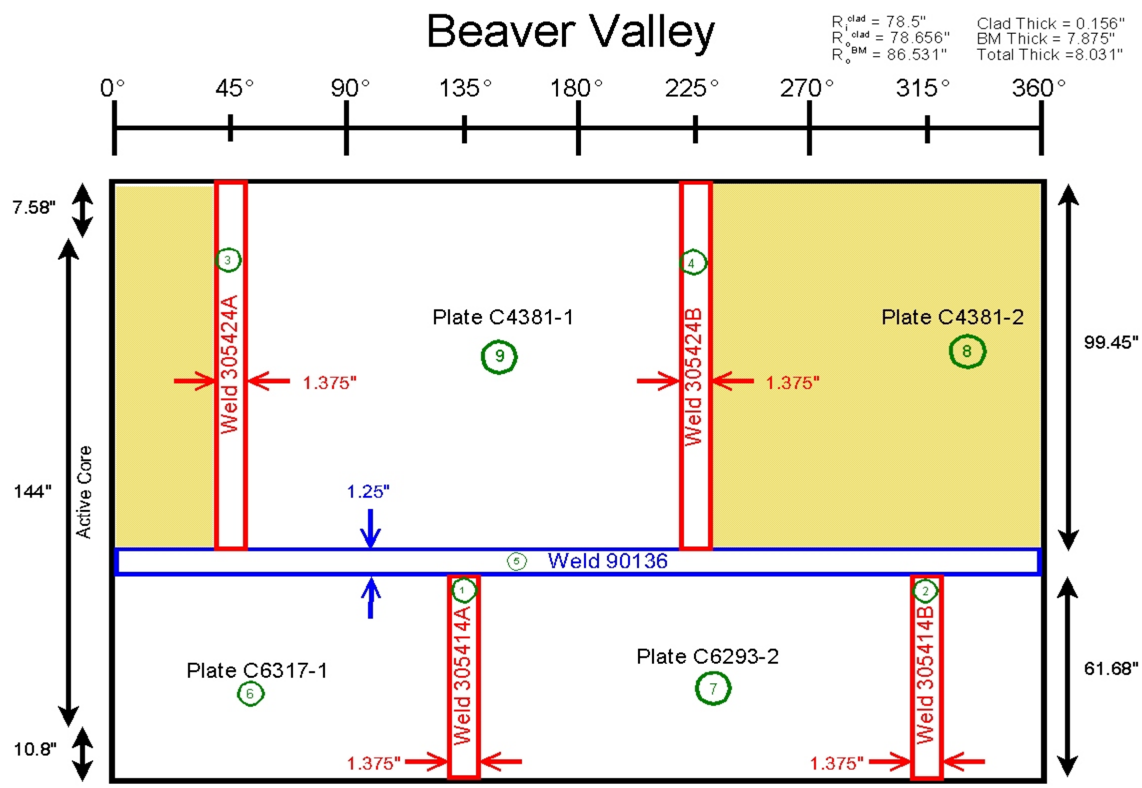

Figure D-1 Beaver Valley 2 Weld Map [D-8]

The relationship between the flaw depth and flaw density PDFs and the corresponding prior hyper-PDFs of their parameters are illustrated in Figure D-2.

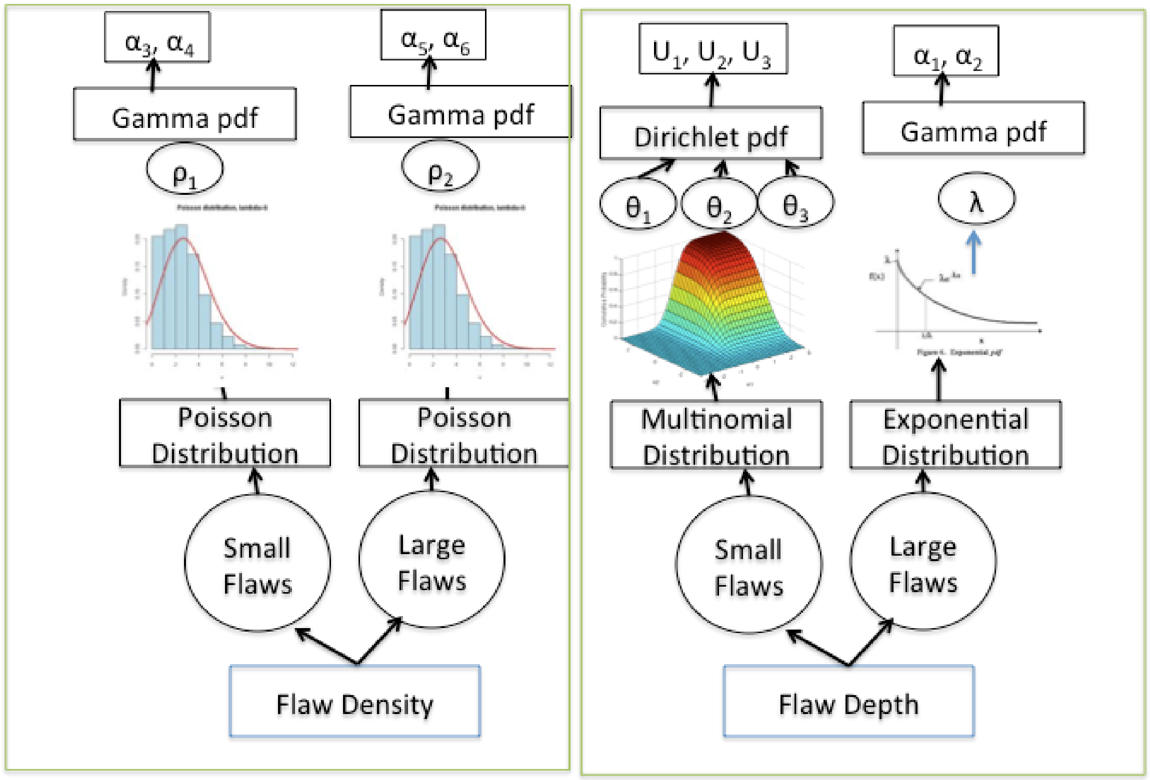

Figure D-2 Flaw-Depth and Flaw-Density Distributions Used in VFLAW and Their Corresponding Parameter Hyper-PDFs

Analysis of UT-detected performance data reported by the Electric Power Research Institute (EPRI) [D-7] was used to identify a POD function for the purpose of this example. The threshold limit of this POD function was taken as 0.00, and the epistemic uncertainties associated with the parameters of the model were not considered in this study. Accordingly, the following mean POD function was used:

$$POD(a) = 1 - \frac{1}{1 + e^{63.2100(a - 0.1124)}} \qquad \text{Eqn. (D-7)}$$

The measurement error was assumed based on some examples and measurement errors reported in Reference [D-7]. After combination of Eqn. (D-2) and Eqn. (D-3), the measurement error (a linear function that oversizes small flaws and undersizes large flaws) is:

$$M_{\varepsilon} = -0.1905a^{*} + 0.0476 + N(0, 0.0298) \qquad \text{Eqn. (D-8)}$$

where N(0, 0.0298) is a normal distribution with a mean of zero and a constant standard deviation of 0.0298. The observed data for the first inch of the vessel were used to estimate the true number of flaws in the flaw-depth ranges of the Alternate PTS Rule flaw tables. This information was used to assess how the estimated number of flaws of a given size in Beaver Valley 2 (estimated based on inspection data, VFLAW distributions, and Bayesian inference) compares to the number and size of flaws permitted by the Alternate PTS Rule flaw tables. The posterior characteristics were used to develop the corresponding Alternate PTS Rule flaw tables.

If the lower limit of the observed data interval is changed from 0.04" to 0.075" to line up with the smallest bin size in the Alternate PTS Rule flaw tables, the results summarized in Table D-1 are calculated. In this case, the results of the mean number of flaws show no sensitivity to the choice of the lower limit of the interval of NDE data. Given this flaw observation, true estimated numbers of flaws in all bins were below the Alternate PTS Rule flaw limits.

Table D-1 Alternate PTS Rule Flaw Table Assessment Using Mean Number of Flaws by Size Interval for Beaver Valley 2 (assuming a Lower Limit of 0.04" vs. 0.075" for Observed Data Interval)

Bin No.	Flaw Depth (in)	Base Case 1		Base Case 2		Alternate PTS Rule Limit (per 1,000" of Weld)
		Observed (Detected) Number of Flaws (Biased with Lower Detection Limit of 0.04")	Posterior Mean Number of Flaws (Unbiased and Corrected for POD)	Observed (Detected) Number of Flaws (Biased with Lower Detection Limit of 0.075")	Posterior Mean Number of Flaws (Unbiased and Corrected for POD)	
1	0.000 < a ≤ 0.075	19	111.41	0	109.09	No limit
2	0.075 < a ≤ 0.475		25.73	19	27.02	166.70
3	0.125 < a ≤ 0.475	0	8.46	0	8.98	90.80
4	0.175 < a ≤ 0.475	0	2.98	0	2.88	22.82
5	0.225 < a ≤ 0.475	0	0.79	0	0.79	8.66
6	0.275 < a ≤ 0.475	0	0.29	0	0.29	4.01
7	0.325 < a ≤ 0.475	0	0.14	0	0.14	3.01
8	0.375 < a ≤ 0.475	0	0.09	0	0.09	1.49
9	0.425 < a ≤ 0.475	0	0.05	0	0.05	1.00

D.4 Application to Sensitivity Cases

In order to examine the effects of changes in the number of flaws observed through NDE, as well as the significance of the POD and the VFLAW prior distributions, twelve sensitivity cases were identified and examined. Methods and tools discussed in Sections D.2 and D.3 were used to carry out these sensitivity cases. The sensitivity cases examined were as follows:

1. No flaws detected, with consideration of the VFLAW prior distributions, POD, and measurement error.
2. 70% of the Alternate PTS Rule's allowed flaws in Bins 2 and 3 are detected, with consideration of the VFLAW prior distributions, POD, and measurement error.
3. 110% of the Alternate PTS Rule's allowed flaws in Bin 3 are detected, with consideration of the VFLAW prior distributions, POD, and measurement error.
4. No flaws detected, with no consideration of VFLAW priors (i.e., non-informative priors) and POD, but with consideration of flaw measurement error only (i.e., no POD or VFLAW prior).
5. 70% of the Alternate PTS Rule's allowed flaws in Bins 2 and 3 are detected, with no consideration of VFLAW priors and POD, but with consideration of flaw measurement error only.
6. 110% of the Alternate PTS Rule's allowed flaws in Bin 3 are detected, with no consideration of VFLAW priors and no consideration of POD, but with consideration of flaw measurement error only.
7. No flaws detected, no consideration of VFLAW priors, but with consideration of POD and flaw measurement error.
8. 70% of the Alternate PTS Rule's allowed flaws in Bins 2 and 3 are detected, with no consideration of VFLAW priors, but with consideration of POD and flaw measurement error.
9. 110% of the Alternate PTS Rule's allowed flaws in Bin 3 are detected, with no consideration of VFLAW priors, but with consideration of POD and flaw measurement error.
10. No flaws detected, no consideration of POD, but with consideration of VFLAW priors and flaw measurement error.
11. 70% of the Alternate PTS Rule's allowed flaws in Bins 2 and 3 are detected, with no consideration of POD, but with consideration of VFLAW priors and flaw measurement error.
12. 110% of the Alternate PTS Rule's allowed flaws in Bin 3 are detected, with no consideration of POD, but with consideration of VFLAW priors and flaw measurement error.

The results of the sensitivity studies are listed in Table D-2 through Table D-13.

Table D-2 Results of Sensitivity Case 1

Bin No.	Flaw Depth (in)	Base Case 1: Observed (Detected) No. of Flaws (Biased with Detection Limit of 0.04")	Base Case 1: Posterior Mean No. of Flaws (Unbiased and Corrected for POD)	Sensitivity Case 1: Assumed No. of Detected Flaws (with Bias)	Sensitivity Case 1: Posterior Mean No. of Flaws (Unbiased)	Alternate PTS Rule Limit (per 1,000" of Weld)
1	0.000 < a ≤ 0.075	19	111.41	0	80.13	No limit
2	0.075 < a ≤ 0.475		25.73	0	40.76	166.70
3	0.125 < a ≤ 0.475	0	8.46	0	18.79	90.80
4	0.175 < a ≤ 0.475	0	2.98	0	7.81	22.82
5	0.225 < a ≤ 0.475	0	0.79	0	2.71	8.66
6	0.275 < a ≤ 0.475	0	0.29	0	0.29	4.01
7	0.325 < a ≤ 0.475	0	0.14	0	0.14	3.01
8	0.375 < a ≤ 0.475	0	0.09	0	0.09	1.49
9	0.425 < a ≤ 0.475	0	0.05	0	0.05	1.00

Table D-3 Results of Sensitivity Case 2

Bin No.	Flaw Depth (in)	Base Case 1: Observed (Detected) No. of Flaws (Biased with Detection Limit of 0.04")	Base Case 1: Posterior Mean No. of Flaws (Unbiased and Corrected for POD)	Sensitivity Case 2: Assumed No. of Detected Flaws (with Bias)	Sensitivity Case 2: Posterior Mean No. of Flaws (Unbiased)	Alternate PTS Rule Limit (per 1,000" of Weld)
1	0.000 < a ≤ 0.075	19	111.41	0	306.12	No limit
2	0.075 < a ≤ 0.475		25.73	116.69	34.16	166.70
3	0.125 < a ≤ 0.475	0	8.46	63.56	7.71	90.80
4	0.175 < a ≤ 0.475	0	2.98	0	1.69	22.82
5	0.225 < a ≤ 0.475	0	0.79	0	0.44	8.66
6	0.275 < a ≤ 0.475	0	0.29	0	0.29	4.01
7	0.325 < a ≤ 0.475	0	0.14	0	0.14	3.01
8	0.375 < a ≤ 0.475	0	0.09	0	0.09	1.49
9	0.425 < a ≤ 0.475	0	0.05	0	0.04	1.00

Table D-4 Results of Sensitivity Case 3

Bin No.	Flaw Depth (in)	Base Case 1		Sensitivity Case 3		Alternate PTS Rule Limit (per 1,000" of Weld)
		Observed (Detected) No. of Flaws (Biased with Detection Limit of 0.04")	Posterior Mean No. of Flaws (Unbiased and Corrected for POD)	Assumed No. of Detected Flaws (with Bias)	Posterior Mean No. of Flaws (Unbiased)	
1	0.000 < a ≤ 0.075	19	111.41	0	155.03	No limit
2	0.075 < a ≤ 0.475		25.73	0	41.33	166.70
3	0.125 < a ≤ 0.475	0	8.46	99.88	15.21	90.80
4	0.175 < a ≤ 0.475	0	2.98	0	4.51	22.82
5	0.225 < a ≤ 0.475	0	0.79	0	1.21	8.66
6	0.275 < a ≤ 0.475	0	0.29	0	0.29	4.01
7	0.325 < a ≤ 0.475	0	0.14	0	0.14	3.01
8	0.375 < a ≤ 0.475	0	0.09	0	0.09	1.49
9	0.425 < a ≤ 0.475	0	0.05	0	0.05	1.00

Table D-5 Results of Sensitivity Case 4

Bin No.	Flaw Depth (in)	Base Case 1		Sensitivity Case 4		Alternate PTS Rule Limit (per 1,000" of Weld)
		Observed (Detected) No. of Flaws (Biased with Detection Limit of 0.04")	Posterior Mean No. of Flaws (Unbiased and Corrected for POD)	Assumed No. of Detected Flaws (with Bias)	Posterior Mean No. of Flaws (Unbiased)	
1	0.000 < a ≤ 0.075	19	111.41	0	0.00	No limit
2	0.075 < a ≤ 0.475		25.73	0	0.00	166.70
3	0.125 < a ≤ 0.475	0	8.46	0	0.00	90.80
4	0.175 < a ≤ 0.475	0	2.98	0	0.00	22.82
5	0.225 < a ≤ 0.475	0	0.79	0	0.00	8.66
6	0.275 < a ≤ 0.475	0	0.29	0	0.00	4.01
7	0.325 < a ≤ 0.475	0	0.14	0	0.00	3.01
8	0.375 < a ≤ 0.475	0	0.09	0	0.00	1.49
9	0.425 < a ≤ 0.475	0	0.05	0	0.00	1.00

Table D-6 Results of Sensitivity Case 5

Bin No.	Flaw Depth (in)	Base Case 1		Sensitivity Case 5		Alternate PTS Rule Limit (per 1,000" of Weld)
		Observed (Detected) No. of Flaws (Biased with Lower Detection Limit of 0.04")	Posterior Mean No. of Flaws (Unbiased and Corrected for POD)	Assumed No. of Detected Flaws (with Bias)	Posterior Mean No. of Flaws (Unbiased)	
1	0.000 < a ≤ 0.075	19	111.41	0	56.47	No limit
2	0.075 < a ≤ 0.475		25.73	116.69	60.22	166.70
3	0.125 < a ≤ 0.475	0	8.46	63.56	36.13	90.80
4	0.175 < a ≤ 0.475	0	2.98	0	18.67	22.82
5	0.225 < a ≤ 0.475	0	0.79	0	5.98	8.66
6	0.275 < a ≤ 0.475	0	0.29	0	0.00	4.01
7	0.325 < a ≤ 0.475	0	0.14	0	0.00	3.01
8	0.375 < a ≤ 0.475	0	0.09	0	0.00	1.49
9	0.425 < a ≤ 0.475	0	0.05	0	0.00	1.00

Table D-7 Results of Sensitivity Case 6

Bin No.	Flaw Depth (in)	Base Case 1		Sensitivity Case 6		Alternate PTS Rule Limit (per 1,000" of Weld)
		Observed (Detected) No. of Flaws (Biased with Detection Limit of 0.04")	Posterior Mean No. of Flaws (Unbiased and Corrected for POD)	Assumed No. of Detected Flaws (with Bias)	Posterior Mean No. of Flaws (Unbiased)	
1	0.000 < a ≤ 0.075	19	111.41	0	32.85	No limit
2	0.075 < a ≤ 0.475		25.73	0	67.03	166.70
3	0.125 < a ≤ 0.475	0	8.46	99.88	47.02	90.80
4	0.175 < a ≤ 0.475	0	2.98	0	27.19	22.82
5	0.225 < a ≤ 0.475	0	0.79	0	11.17	8.66
6	0.275 < a ≤ 0.475	0	0.29	0	0.00	4.01
7	0.325 < a ≤ 0.475	0	0.14	0	0.00	3.01
8	0.375 < a ≤ 0.475	0	0.09	0	0.00	1.49
9	0.425 < a ≤ 0.475	0	0.05	0	0.00	1.00

Table D-8 Results of Sensitivity Case 7

Bin No.	Flaw Depth (in)	Base Case 1		Sensitivity Case 7		Alternate PTS Rule Limit (per 1,000" of Weld)
		Observed (Detected) No. of Flaws (Biased with Detection Limit of 0.04")	Posterior Mean No. of Flaws (Unbiased and Corrected for POD)	Assumed No. of Detected Flaws (with Bias)	Posterior Mean No. of Flaws (Unbiased)	
1	0.000 < a ≤ 0.075	19	111.41	0	0.00	No limit
2	0.075 < a ≤ 0.475		25.73	0	0.00	166.70
3	0.125 < a ≤ 0.475	0	8.46	0	0.00	90.80
4	0.175 < a ≤ 0.475	0	2.98	0	0.00	22.82
5	0.225 < a ≤ 0.475	0	0.79	0	0.00	8.66
6	0.275 < a ≤ 0.475	0	0.29	0	0.00	4.01
7	0.325 < a ≤ 0.475	0	0.14	0	0.00	3.01
8	0.375 < a ≤ 0.475	0	0.09	0	0.00	1.49
9	0.425 < a ≤ 0.475	0	0.05	0	0.00	1.00

Table D-9 Results of Sensitivity Case 8

Bin No.	Flaw Depth (in)	Base Case 1		Sensitivity Case 8		Alternate PTS Rule Limit (per 1,000" of Weld)
		Observed (Detected) No. of Flaws (Biased with Detection Limit of 0.04")	Posterior Mean No. of Flaws (Unbiased and Corrected for POD)	Assumed No. of Detected Flaws (with Bias)	Posterior Mean No. of Flaws (Unbiased)	
1	0.000 < a ≤ 0.075	19	111.41	0	5131.91	No limit
2	0.075 < a ≤ 0.475		25.73	116.69	263.80	166.70
3	0.125 < a ≤ 0.475	0	8.46	63.56	35.54	90.80
4	0.175 < a ≤ 0.475	0	2.98	0	4.88	22.82
5	0.225 < a ≤ 0.475	0	0.79	0	0.39	8.66
6	0.275 < a ≤ 0.475	0	0.29	0	0.00	4.01
7	0.325 < a ≤ 0.475	0	0.14	0	0.00	3.01
8	0.375 < a ≤ 0.475	0	0.09	0	0.00	1.49
9	0.425 < a ≤ 0.475	0	0.05	0	0.00	1.00

Table D-10 Results of Sensitivity Case 9

Bin No.	Flaw Depth (in)	Base Case 1		Sensitivity Case 9		Alternate PTS Rule Limit (per 1,000" of Weld)
		Observed (Detected) No. of Flaws (Biased with Detection Limit of 0.04")	Posterior Mean No. of Flaws (Unbiased and Corrected for POD)	Assumed No. of Detected Flaws (with Bias)	Posterior Mean No. of Flaws (Unbiased)	
1	0.000 < a ≤ 0.075	19	111.41	0	1233.10	No limit
2	0.075 < a ≤ 0.475		25.73	0	202.01	166.70
3	0.125 < a ≤ 0.475	0	8.46	99.88	54.12	90.80
4	0.175 < a ≤ 0.475	0	2.98	0	13.13	22.82
5	0.225 < a ≤ 0.475	0	0.79	0	1.95	8.66
6	0.275 < a ≤ 0.475	0	0.29	0	0.00	4.01
7	0.325 < a ≤ 0.475	0	0.14	0	0.00	3.01
8	0.375 < a ≤ 0.475	0	0.09	0	0.00	1.49
9	0.425 < a ≤ 0.475	0	0.05	0	0.00	1.00

Table D-11 Results of Sensitivity Case 10

Bin No.	Flaw Depth (in)	Base Case 1		Sensitivity Case 10		Alternate PTS Rule Limit (per 1,000" of Weld)
		Observed (Detected) No. of Flaws (Biased with Detection Limit of 0.04")	Posterior Mean No. of Flaws (Unbiased and Corrected for POD)	Assumed No. of Detected Flaws (with Bias)	Posterior Mean No. of Flaws (Unbiased)	
1	0.000 < a ≤ 0.075	19	111.41	0	79.14	No limit
2	0.075 < a ≤ 0.475		25.73	0	41.18	166.70
3	0.125 < a ≤ 0.475	0	8.46	0	19.09	90.80
4	0.175 < a ≤ 0.475	0	2.98	0	7.93	22.82
5	0.225 < a ≤ 0.475	0	0.79	0	2.42	8.66
6	0.275 < a ≤ 0.475	0	0.29	0	0.29	4.01
7	0.325 < a ≤ 0.475	0	0.14	0	0.14	3.01
8	0.375 < a ≤ 0.475	0	0.09	0	0.09	1.49
9	0.425 < a ≤ 0.475	0	0.05	0	0.05	1.00

Table D-12 Results of Sensitivity Case 11

Bin No.	Flaw Depth (in)	Base Case 1		Sensitivity Case 11		Alternate PTS Rule Limit (per 1,000" of Weld)
		Observed (Detected) No. of Flaws (Biased with Detection Limit of 0.04")	Posterior Mean No. of Flaws (Unbiased and Corrected for POD)	Assumed No. of Detected Flaws (with Bias)	Posterior Mean No. of Flaws (Unbiased)	
1	0.000 < a ≤ 0.075	19	111.41	0	73.49	No limit
2	0.075 < a ≤ 0.475		25.73	116.69	57.04	166.70
3	0.125 < a ≤ 0.475	0	8.46	63.56	31.09	90.80
4	0.175 < a ≤ 0.475	0	2.98	0	14.66	22.82
5	0.225 < a ≤ 0.475	0	0.79	0	4.81	8.66
6	0.275 < a ≤ 0.475	0	0.29	0	0.29	4.01
7	0.325 < a ≤ 0.475	0	0.14	0	0.14	3.01
8	0.375 < a ≤ 0.475	0	0.09	0	0.09	1.49
9	0.425 < a ≤ 0.475	0	0.05	0	0.05	1.00

Table D-13 Results of Sensitivity Case 12

Bin No.	Flaw Depth (in)	Base Case 1		Sensitivity Case 12		Alternate PTS Rule Limit (per 1,000" of Weld)
		Observed (Detected) No. of Flaws (Biased with Detection Limit of 0.04")	Posterior Mean No. of Flaws (Unbiased and Corrected for POD)	Assumed No. of Detected Flaws (with Bias)	Posterior Mean No. of Flaws (Unbiased)	
1	0.000 < a ≤ 0.075	19	111.41	0	63.04	No limit
2	0.075 < a ≤ 0.475		25.73	0	66.84	166.70
3	0.125 < a ≤ 0.475	0	8.46	99.88	39.42	90.80
4	0.175 < a ≤ 0.475	0	2.98	0	20.55	22.82
5	0.225 < a ≤ 0.475	0	0.79	0	7.21	8.66
6	0.275 < a ≤ 0.475	0	0.29	0	0.29	4.01
7	0.325 < a ≤ 0.475	0	0.14	0	0.14	3.01
8	0.375 < a ≤ 0.475	0	0.09	0	0.09	1.49
9	0.425 < a ≤ 0.475	0	0.05	0	0.05	1.00

D.5 Discussion and Summary

In this study, analysis of a base case of UT detected weld flaw data involving measurement (sizing) error for Beaver Valley 2 was performed. The base case was evaluated for interval flaw depths detected in the inspection volume specified in Supplement 4 to Mandatory Appendix VIII to Section XI of the ASME Code. Detected flaw depth intervals were analyzed assuming lower UT detection limits of 0.04" and 0.075". Subsequently, twelve sensitivity cases were assessed based on variations in the assumed detected flaw depth data (in the form of intervals), choices of considering VFLAW flaw depth and flaw densities as prior information (as opposed to no prior information), and choices of considering the POD (as opposed to perfect detection; i.e., no POD) were evaluated and compared to the base case as well as the Alternate PTS Rule flaw table limits. No sensitivities to the choice of the lower UT detection limit on the observed data were found.

The results obtained from the twelve sensitivity cases were consistent and showed that small overpopulations of flaws in Bins 2 and 3 of the Alternate PTS Rule flaw tables resulting from possible oversizing of small flaws would be shifted to Bins 1 and 2 after accounting for the measurement error in the Bayesian inference. When POD is considered, the effect of the missed small flaws was clearly seen in Bins 1 and 2 with an additional number of flaws in the posterior estimates as compared to the observed flaws.

The effects of the consideration and choice of the prior distributions of flaw density and depth were significant. When no prior information was used to describe the flaw density and flaw depth distributions, POD and measurement error were also sensitive and significantly amplified the number of flaws in Bins 1 and 2. However, when prior VFLAW PDFs were used, the posteriors were significantly moderated by the existence of the prior PDFs, and the POD and measurement errors played less significant roles.

If the approach documented in this appendix is used to reassess actual NDE flaws, it would be advisable to use informative or semi informative prior estimates of the flaw depth and density distributions.

D.6 References

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10. SUPPLEMENTARY NOTES

11. ABSTRACT (200 words or less)

During plant operation, the of reactor pressure vessel (RPVs) is exposed to neutron radiation, resulting in embrittlement of the vessel steel in the area of the RPV adjacent to the core. If an embrittled RPV had a flaw of critical size and if certain severe system transients occurred, the flaw could rapidly propagate through the vessel that could challenge the integrity of the RPV. The severe transients of concern, known as pressurized thermal shock (PTS), are characterized by a rapid cooling of the internal RPV surface in combination with repressurization of the RPV. Advances in understanding material behavior, the ability to realistically model plant systems and operational characteristics, and the ability to better evaluate PTS transients to estimate loads on vessel walls led the U.S. Nuclear Regulatory Commission (NRC) to develop a risk informed revision of the existing PTS Rule in Title 10 of the Code of Federal Regulations (10 CFR) 50.61a, "Alternate Fracture Toughness Requirements for Protection against Pressurized Thermal Shock Events." This report explains the basis for the requirements that establish the entry conditions to permit the use of 10 CFR 50.61a and describes methods that licensees can use to meet the requirements of 10 CFR 50.61a.

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