



NuScale Standard Plant Design Certification Application

Initial Test Program and Inspections, Tests, Analyses, and Acceptance Criteria

PART 2 - TIER 2

Revision 0 December 2016

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CHAPTER 14 INITIAL TEST PROGRAM AND INSPECTIONS, TESTS, ANALYSES, AND ACCEPTANCE CRITERIA

14.0 Verification Programs

Verification programs include the initial test programs for the NuScale Power, LLC (NuScale) Power Plant. The initial test programs are comprised of preoperational tests, initial fuel loading, initial criticality, low-power tests, and power-ascension tests. The verification programs ensure that the as-built facility configuration and operation comply with the approved plant design and applicable regulations.

The verification programs also include Inspections, Tests, Analyses, and Acceptance Criteria (ITAAC). The methodology associated with developing ITAAC is described in Section 14.3. The ITAAC are presented in Tier 1.

The initial test program addresses structures, systems, and components and design features for both the nuclear portion of the facility and the balance-of-plant. The initial test program contains information that:

- addresses the major phases of the test program including preoperational tests, initial fuel loading, initial criticality, low-power tests, and power-ascension tests, including scope and general plans for demonstrating that due consideration has been given to matters that normally require advance planning.
- demonstrates that an adequate number of qualified personnel support the program.
- demonstrates the adequacy of administrative controls to govern the conduct of the program.
- allows plant staff the ability to train using the plant's operating procedures.
- demonstrates and verifies the adequacy of plant operating and emergency procedures to the extent practicable during the period of the initial test program.
- allows for the verification of functional requirements.
- demonstrates sequence of testing such that the safety of the plant does not depend on untested structures, systems, and components.

Tier 2 14.0-1 Revision 0

14.1 Specific Information to be Addressed for the Initial Plant Test Program

The initial test program establishes procedures and controls used to conduct and evaluate the results of tests as described in Section 14.2 and to satisfy the relevant requirements of the following regulations:

- 10 CFR 30.53, as it relates to testing radiation detection equipment and monitoring instruments
- 10 CFR 50.34(b)(6)(iii), as it relates to providing information associated with preoperational testing and initial operations
- Section XI of Appendix B to 10 CFR Part 50, as it relates to test programs to demonstrate that systems, structures, and components will perform satisfactorily
- Option A or Option B of Appendix J of 10 CFR Part 50, as it relates to preoperational leakage rate testing
- 10 CFR 52.79 as it pertains to preoperational testing and initial operations
- Subpart A, Subpart B, and Subpart C of 10 CFR Part 52 as they relate to the Inspections, Tests, Analyses, and Acceptance Criteria that the applicant must submit

Tier 2 14.1-1 Revision 0

14.2 Initial Plant Test Program

14.2.1 Summary of Initial Test Program and Objectives

The Initial Test Program (ITP) consists of a series of preoperational and startup tests. Preoperational testing is conducted following completion of construction testing but prior to fuel load. Completion of preoperational testing is necessary to ensure the overall plant is ready for fuel loading and startup testing of a NuScale Power Module (NPM).

Startup tests of an NPM are performed following the completion of preoperational testing. Startup testing includes the following:

- initial fuel loading and pre-critical testing
- initial criticality testing
- low-power testing
- power-ascension testing

Startup testing is performed to confirm the design bases of the NPM and to demonstrate, to the extent practical, that the NPM will operate in accordance with its design and is capable of responding to anticipated transients and postulated accidents as described in Section 15.0.

The objectives of the ITP are to

- provide assurance that structures, systems, and components (SSC) operate in accordance with their design.
- provide assurance that construction and installation of equipment in the facility has been completed in accordance with the design. Verification of design requirements is also performed as part of construction testing phase of the ITP.
- demonstrate to the extent practical the validity of analytical models used to predict
 plant responses to anticipated transients and postulated accidents, and to
 demonstrate to the extent practical the correctness and conservatism of assumptions
 used in those models.
- familiarize the plant's operating and technical staff with the operation of the facility.
- perform testing to the extent practical using the plant conditions that simulate the
 actual operating, abnormal operating occurrences, and emergency conditions to
 which the SSC may be subjected.
- verify to the extent practical by trial use that the facility operating procedures, surveillance procedures and emergency procedures are adequate.
- verify that interfaces and system and component interactions are in accordance with the design.
- complete and document the ITP testing required to satisfy preoperational and startup testing requirements and Inspections, Tests, Analyses, and Acceptance Criteria (ITAAC) testing requirements.

Tier 2 14.2-1 Revision 0

Preoperational and startup testing is performed on those SSC that are:

- relied upon for safe shutdown and cooldown of the NPM under normal conditions and for maintaining a safe condition for an extended shutdown period.
- relied upon for safe shutdown and cooldown of the NPM under transient and postulated accident conditions and for maintaining a safe condition for an extended shutdown period following such conditions.
- relied upon for establishing conformance with safety limits or limiting conditions for operation that are included in the technical specifications (TS).
- assumed to function or for which credit is taken in the accident analysis as described in Chapter 15.
- used to process, store, control, or limit the release of radioactive materials.
- relied upon to maintain their structural integrity during normal operation, anticipated transients, simulated test parameters, and design basis event conditions to avoid damage to safety-related SSC.
- identified as risk-significant in the probabilistic risk assessment.

The ITP is implemented consistent with the requirements of Section XI of 10 CFR 50 Appendix B. Implementation of the ITP ensures that the testing required to demonstrate that SSC perform satisfactorily in service, are identified and performed in accordance with written test procedures that incorporate the requirements and acceptance limits in the applicable design documents.

Leakage rate testing of the NPM and related systems and components penetrating the containment pressure boundary is described in Section 6.2. Leakage rate testing test abstracts are presented in Section 14.2.12.

The methodology associated with the development of the ITAAC necessary to demonstrate that the facility has been constructed and will be operated in conformity with the final safety analysis report and the applicable Nuclear Regulatory Commission (NRC) regulations is presented in Section 14.3.

NuScale Power Plant compliance with the proposed technical resolution of unresolved safety issues and medium- and high-priority generic safety issues that are identified in NUREG-0933 are addressed in Section 1.9.3. Operating experience insights are addressed in Section 1.9.4 and Section 14.2.8. Compliance with technically relevant portions of the Three Mile Island requirements are addressed in Section 1.9.5.

14.2.1.1 Construction and Installation

The objective of construction and installation tests are to verify that on a system basis that the system is constructed and installed in accordance with design requirements. Construction tests include but are not limited to:

- initial instrument calibration
- flushing
- cleaning

- hydrostatic pressure tests
- wiring
- continuity and separation checks
- functional tests of components

14.2.1.2 Preoperational Test Phase Objectives

Preoperational tests are performed to demonstrate that SSC operate in accordance with design requirements so that initial fuel loading, initial criticality, and subsequent power operation can be safely undertaken. The objectives of the preoperational test phase are to

- demonstrate that SSC will perform their functions in accordance with their design during the preoperational test phase.
- verify and demonstrate expected operation following a loss of power sources and in degraded modes for which the systems are designed to remain operational.
- test the backup power supply system (BPSS) to ensure that backup sources of alternating current (AC) electrical power are available when the normal AC power sources are not available.
- verify and demonstrate the operational readiness of valves and dynamic restraints before relying on those components to perform their safety functions.
- perform inspections or testing for flow-induced vibration loads on components that must maintain their structural integrity.
- obtain baseline test and operating data on equipment and systems for future reference.
- operate equipment for a sufficient period of time to achieve normal equilibrium conditions (e.g., temperatures and pressures) so that design, manufacturing, and installation defects can be detected and corrected.
- ensure to the extent practical plant systems operate properly on an integrated basis.
- evaluate normal, abnormal, and emergency operating procedures to the extent practical.
- demonstrate equipment performance.
- test, as appropriate, manual operation and automatic operation of systems and their components.
- test the proper functioning of controls, permissives, interlocks, and equipment protective devices for which malfunction or premature actuation may shut down or defeat the operation of systems or equipment.
- provide the plant operating staff with the opportunity to obtain practical experience in the operation and maintenance of equipment and systems including instrument calibrations and functional tests of components.
- demonstrate equipment performance is satisfactory to proceed to initial fuel loading and initial criticality.

Tier 2 14.2-3 Revision 0

Test abstracts associated with preoperational testing are included in Section 14.2.12.

14.2.1.3 Startup Test Phase Objectives

14.2.1.3.1 Initial Fuel Loading and Pre-Critical Tests

This phase of testing is performed in order to ensure that initial fuel loading of an NPM can be accomplished in an orderly and safe manner. A description of the fuel loading process is presented Section 14.2.10.2. The objectives of the initial fuel loading and pre-critical tests are to:

- conduct initial fuel loading cautiously to preclude inadvertent criticality. Establish and follow specific safety measures, such as:
 - ensuring that the applicable TS requirements and other prerequisites have been satisfied
 - continuous monitoring of the neutron flux throughout core loading so that changes in the multiplication factor are observed
 - verifying that the fuel and control components have been properly installed
- establish that the required SDM exists, without achieving criticality
- establish the functionality of plant systems and components, including reactivity control systems and other systems and components necessary to ensure the safety of plant personnel and the public in the event of errors or malfunctions
- confirm the proper operation of plant systems and design features that could not be completely tested during preoperational testing
- confirm interdependent effects among the safety features of the design are acceptable

14.2.1.3.2 Initial Criticality

The objectives associated with the initial criticality phase of the startup testing program are to achieve initial criticality in a safe and controlled manner. In order to meet this objective the following are performed:

- The initial approach to criticality is performed in a deliberate and orderly manner using the same rod withdrawal sequences and patterns that will be used during subsequent startups.
- The neutron flux levels are continuously monitored and periodically evaluated. A neutron count rate of at least 1/2 counts per second should register on the startup channels before startup begins, and the signal to noise ratio should be known to be greater than 2.
- The systems required for startup or protection of the plant, including the reactor protection system and engineered safety features (ESFs), are operable and in a state of readiness.

Tier 2 14.2-4 Revision 0

- The control rod or poison removal sequence is accomplished using approved plant procedures.
- The reactor achieves initial criticality by boron dilution. Control rods are withdrawn before dilution begins.
- The control rod insertion limits defined in the technical specifications are observed and followed.
- Criticality predictions for boron concentration and control rod positions are provided.
- The reactivity addition sequence is prescribed, and plant procedures require a cautious approach to achieving criticality to prevent passing through criticality in a period shorter than approximately 30 seconds (<1 decade per minute).

A description of the process followed to achieve initial criticality is provided in Section 14.2.10.3.

14.2.1.3.3 Low - Power Testing

Following criticality, low-power testing is performed. The objectives associated with performing low-power testing are to

- confirm the design and validate analytical models.
- verify the correctness of assumptions used in the safety analyses.
- confirm the functionality of plant systems and design features that could not be completely tested during the preoperational test phase because of the lack of an adequate heat source for the reactor coolant and main steam systems.

14.2.1.3.4 Power-Ascension Testing

Following low-power testing, power-ascension testing is performed. Power-ascension testing is performed to bring the reactor to full power with testing at power levels of approximately 25 percent, 50 percent, 75 percent, and 100 percent. The objectives associated with performing power-ascension testing are to

- achieve reactor full power in a safe and controlled manner.
- demonstrate that the plant operates in accordance with its design bases during normal steady-state conditions and, to the extent practical, during and following anticipated transients.
- validate models used to predict plant response.
- demonstrate the ability of major or principal plant control systems to automatically control process variables within design limits.
- demonstrate that the facility's integrated dynamic response is in accordance with design for plant events such as reactor scram, turbine trip, and loss of feedwater heaters or pumps.

Tier 2 14.2-5 Revision 0

14.2.2 Organization and Staffing

COL Item 14.2-1: A COL applicant that references the NuScale Power Plant design certification will describe the site-specific organizations that manage, supervise, or execute the Initial Test Program, including the associated training requirements.

14.2.3 Test Procedures

14.2.3.1 Initial Test Program Procedures

Test procedures are developed and reviewed by individuals with the appropriate technical background and expertise. Once the test procedures have been developed they are reviewed by plant management personnel who upon acceptance designate the procedures as final.

Input from the principal design organization is utilized to establish the test objectives and acceptance criteria for the system. Operating experience, as discussed in Section 14.2.8 is used in the development of test procedures.

Test procedure testing and acceptance criteria are founded upon the information contained in design specifications, design documents, the Final Safety Analysis Report, and regulatory documents. A test procedure is prepared for each specific system test to be performed during the test program.

Preoperational and startup testing procedures include checklists and signature blocks to control the sequence and performance of testing. The administrative controls associated with test procedure development address the following:

- test procedure format
- application, to the extent practical, of normal plant operating procedures, emergency operating procedures, and surveillance procedures in support of test procedure development
- test procedure review and approval
- test procedure change and revision

The content of each test procedure addresses

- objectives.
- detailed step-by-step procedures specifying how testing is to be performed.
- special precautions.
- test instrumentation.
- test equipment calibration.
- initial test conditions, including provisions to perform testing under environmental conditions as close as practical to those the equipment will experience in both normal and accident situations.
- methods to direct and control test performance.

Tier 2 14.2-6 Revision 0

- acceptance criteria by which testing is evaluated. Acceptance criteria account for measurement errors and uncertainties associated with normal operation as well as operation during transients and accidents. Acceptance criteria are biased conservatively. In some cases the acceptance criteria is qualitative. Where applicable, quantitative values, with appropriate tolerances, are used as acceptance criteria.
- test prerequisites including as necessary prerequisite statements to ensure that nonstandard arrangements are restored to their normal status after the test is completed (for example, electric jumper cable use does not invalidate electrical separation; jumper cables are removed following testing; valve configurations, and instrument settings are returned to their normal orientations and settings).
- identification of the data to be collected and the method of documentation.
- actions to take if unanticipated errors or malfunctions occur while testing.
- remedial actions to take if acceptance criteria are not satisfied.
- actions to take if an unexpected or unanalyzed condition occurs.

14.2.3.2 Graded Approach to Testing

The ITP allows for the application of a graded approach to testing. The graded approach to testing is founded in the requirements of General Design Criterion 1, "Quality Standards and Records," of Appendix A to 10 CFR Part 50 that requires, in part, that SSC important to safety shall be tested to quality standards commensurate with the importance of the safety functions to be performed. Criterion XI of Appendix B to 10 CFR Part 50 also includes a graded approach for important to safety SSC in the Quality Assurance Program. The administrative requirements that govern the conduct of the test program (e.g., test program objectives, organizational elements, personnel qualifications, evaluation and approval of test results, and test records retention) contain provisions that allow for testing of SSC in a manner commensurate with the safety significance of the SSC within its scope. This provides a systematic approach to the "defense-in-depth" concept. This concept dictates that the plant be designed, constructed, and tested to (1) provide for safe normal operation, (2) ensure that, in the event of errors, malfunctions, and off-normal conditions, the reactor protection systems and other design features will mitigate the event or limit its consequences to defined and acceptable levels, and (3) ensure that adequate safety margin exists for events of extremely low probability or arbitrarily postulated hypothetical events without substantial reduction in the safety margin for the protection of public health and safety.

Application of the graded approach to testing provides reasonable assurance that the SSC being tested will perform satisfactorily while accomplishing the testing in a cost-effective manner. The administrative requirements that govern the conduct of the test program allow for the preparation of documentation (such as procedures and records) associated with testing to be prepared commensurate with the importance to safety of the SSC being tested.

During the SSC classification process, the subject matter expert identified all functions of the system. Each of these functions was compared to safety functional requirements

and regulatory functional requirements to establish a functional hierarchy. This hierarchy established a supporting to supported relationship between the systems and tied it to a set of plant functions as described in Section 17.4 to identify a classification for the functions. The functions were categorized as A1 (safety-related, risk-significant), A2 (safety-related, not risk-significant), B1 (nonsafety-related, risk-significant), or B2 (nonsafety-related, not risk-significant). This safety significance evaluation was the basis for the graded approach in the ITP.

The hierarchy in the NuScale approach to preoperational testing is:

- Testing of active, safety-related system functions (A1 or A2 functions)
- Testing of active, non-safety-related functions which require ITAAC verification (B1 and B2)
- Testing of active non-safety-related functions which do not require ITAAC verification (B1 and B2)

The preoperational test abstracts contained in Table 14.2-1 through Table 14.2-69 provide a definition of the test scope for each system by listing the associated active system functions and their safety categorization. The test abstract also provides system functions tested by another test abstract, thereby providing an "inventory" of all testable system functions.

Table 17.4-1 contains a list of all A1 and B1 system functions. All active, safety-related A1 functions are tested by the safety-related module protection system (MPS) logic testing found in Table 14.2-63. The remaining safety-related functions categorized as A2 are also tested by the MPS test abstract. The NuScale graded approach provides for testing of A2 functions to the same rigor as A1 functions.

As indicated by Table 14.2-63, all active, safety-related functions are one of the following types:

- provides safety-related instrument information signals to MPS
- removes electrical power to the control rod drive
- removes electrical power to the pressurizer heaters
- removes electrical power to the trip solenoids of safety-related valves
- closes safety-related valves

The MPS test abstract also describes testing of the following safety-related design features:

- MPS response to loss of electrical power
- MPS operating bypasses and permissives
- Safety-related containment isolation valve response time
- MPS safety-related sensor response time

Table 14.3-1 and Table 14.3-2 identify all ITAAC by its unique ITAAC number. The tables provide a discussion of the ITAAC, including a reference to a verifying preoperational

test abstract, if required. This results in a cross-reference between Tier 1 ITAAC and the associated Tier 2 test abstract. Table 14.3-1 or Table 14.3-2 is annotated with the unique ITAAC number entered in the acceptance criteria column of the associated test abstract.

Table 14.2-63 identifies that the acceptance criteria of the all MPS test abstracts which test a safety-related function have an associated ITAAC.

Preoperational testing of non-safety-related systems is necessary to verify ITAAC for the following design features. The acceptance criteria of the associated test abstract acceptance criteria are annotated with the ITAAC number.

- Radiation isolation
- Battery room ventilation for hydrogen control
- Control room building and reactor building differential pressure
- Control room envelope design features
- Post-accident monitoring (PAM) signals
- Turbine trip
- Fire protection pump flow
- Plant lighting illumination in the main control room, remote shutdown, and for post-fire shutdown
- Important Human Actions for CFD addition of water to containment
- Important Human Actions for CVC addition of water to the reactor coolant system

Credit is taken for the logic testing performed for the nonsafety-related module control system (MCS) described in Section 7.04.5, and the nonsafety-related plant control system (PCS) described in Section 7.04.6. Therefore, if the component is controlled by MCS or PCS, the component-level logic testing in the preoperational test is limited to the testing of component-level design features described below (if the design feature is applicable to the system) unless the preoperational test verifies an ITAAC. The component tests are standardized to provide the same level of test detail across all systems. This graded approach does not affect system-level tests which require integrated system operation. The standardized component tests are:

- Remote operation of equipment.
- Manual control of variable-speed pump or fan.
- Automatic start of standby pump or fan.
- Automatic operation of pump recirculation valve.
- Pump start does not create a water hammer.
- Remote operation of valve or damper.
- Valve or damper fails to its safe position on loss of air.
- Valve or damper fails to its safe position on loss of electrical power to its solenoid.
- Damper or fan responds to fire or smoke alarm.

- Equipment response to automatic signals to protect plant equipment.
- Automatic operation of tank or basin level control valve.
- Local grab sample can be obtained from a system grab sample device.
- Automatic bus transfer via bus tie breaker.
- System instrument calibration.
- Each instrument is monitored in the MCR and the remote shutdown station (RSS), if the signal is designed to be displayed in the RSS. (Test not required if the instrument calibration verified the MCR and RSS display.)
- Equipment protection logic

14.2.3.3 Testing of First-of-a-Kind Design Features

First-of-a-kind (FOAK) tests are new, unique, or special tests used to verify design features that are being reviewed for the first time by the NRC. The NuScale Power Plant contains design features which are new and unique and have not been tested previously; therefore, testing of these design features is treated as FOAK. For the FOAK tests, the testing frequency is specified in the test abstract. The NuScale comprehensive vibration assessment program is a FOAK program. The program is implemented consistent with the requirements of the NuScale "Comprehensive Vibration Assessment Program (CVAP) Technical Report", TR-0716-50439. The CVAP is addressed in Design Control Document (DCD) Section 3.9.2. Table 14.2-108: Reactor Module Vibration Test #108 contains a startup test to support the CVAP.

14.2.4 Conduct of the Test Program

The ITP activities are controlled by administrative procedures contained within the Startup Administrative Manual.

COL Item 14.2-2: A COL applicant that references the NuScale Power Plant design certification is responsible for the development of the Startup Administration Manual that will contain the administrative procedures and requirements that control the activities associated with the Initial Test Program. The COL applicant will provide a milestone for completing the Startup Administrative Manual and making it available for NRC inspection.

Administrative controls are established to ensure that the designated construction-related inspections and tests are completed prior to initiating preoperational testing. In addition controls are established to ensure completion of preoperational testing prior to initiating startup testing. Administrative controls address adherence to approved test procedures during the conduct of the test program and the methods for effecting changes to approved test procedures.

The controls used to ensure that test prerequisites associated with each major phase of testing, as well as individual system or component testing are met, include requirements for performing inspections and checks, identification of test personnel, completing data forms or check sheets, and identification of dates of completion.

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The controls provided to implement plant modification and repairs ensure that the required modifications and repairs are made. Retesting is conducted following modifications or repairs. Reviews of proposed facility modifications by designated design organizations is conducted prior to performing the modification or repair.

Controls are established to ensure that retesting that is required for modifications or maintenance remains in compliance with ITAAC commitments.

The documentation associated with the conduct of the test plan is captured and auditable.

14.2.5 Review, Evaluation, and Approval of Test Results

Administrative procedures control the review and approval of preoperational and startup test results for each phase of the test program. This includes approval of test data for each major test phase before proceeding to the next test phase as well as approval of test data at each power test plateau (during the power-ascension phase) before increasing the power level. Test exceptions or results that do not meet acceptance criteria are identified to the responsible design organization as well as plant operations and plant technical staff and corrective actions and retests, as required, are performed.

These administrative procedures address the following:

- notification of responsible design organizations when test acceptance criteria are not met
- methods and schedules for approval of test data for each major phase
- methods used for initial review of individual parts of multiple tests
- technical evaluation of test results by qualified personnel and approval of such results by personnel in designated management positions
- provisions to allow design organizations to participate in the resolution of designrelated problems that result in, or contribute to, a failure to meet test acceptance criteria
- provisions to retain test reports, including test procedures and results, as part of the plant historical records

14.2.6 Test Records

Initial test program reports, test procedures and results are retained as part of the plant's historical record in accordance with 10 CFR 50.36, "Technical Specification," 10 CFR 50.71, "Maintenance of Records, Making of Reports," and 10 CFR 50, Appendix B, Criterion XVII, "Quality Assurance Records." The test reports include test results associated with the testing of SSCs identified in the ITP. A summary of the startup testing is included in a startup report. This summary includes the following information:

- description of the method and objectives for each test
- comparison of applicable test data with the related acceptance criteria, including the systems' responses to major plant transients (such as reactor scram and turbine trip)

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- design and construction related deficiencies discovered during testing, and system modifications, the corrective actions required to correct those deficiencies, and the schedule for implementing the identified modifications and corrective actions
- justification for acceptance of systems or components that are not in conformance with design predictions or performance requirements
- conclusions about system or component adequacy
- identity of test observers and recorders
- type of observation
- identifying numbers of test or measuring equipment
- results of tests

14.2.7 Test Programs Conformance with Regulatory Guides

The ITP conforms to Regulatory Guide (RG) 1.68, Revision 4 except for aspects that address specific SSC design features not in the design.

The following list of regulatory guides provides information used to supplement the information, recommendations, and guidance presented in RG 1.68 Rev 4 relative to testing of SSC:

- RG 1.20 Comprehensive Vibration Assessment Program for Reactor Internals During Preoperational and Initial Startup Testing, Rev. 3
- RG 1.29 Seismic Design Classification for Nuclear Power Plants, Rev. 5
- RG 1.45 Guidance on Monitoring and Responding to Reactor Coolant System Leakage, Rev. 1
- RG 1.68.1 Initial Test Program of Condensate and Feedwater Systems for Light-Water Reactors, Rev. 2
- RG 1.68.2 Initial Startup Test Program to Demonstrate Remote Shutdown Capability for Water- Cooled Nuclear Power Plants, Rev 2
- RG 1.68.3 Preoperational Testing of Instrument and Control Air Systems, Rev.1
- RG 1.69 Concrete Radiation Shields and Generic Shield Testing for Nuclear Power Plants, Rev. 1
- RG 1.79 Preoperational Testing of Emergency Core Cooling Systems for Pressurized Water Reactors, Rev. 2
- RG 1.118 Periodic Testing of Electric Power and Protection Systems, Rev. 3
- RG 1.128 Installation Design and Installation of Vented Lead-Acid Storage Batteries for Nuclear Power Plants Rev. 2
- RG 1.140 Design, Inspection, and Testing Criteria for Air Filtration and Adsorption Units of Normal Atmosphere Cleanup Systems in Light-Water- Cooled Nuclear Power Plants, Rev. 2
- RG 1.155 Station Blackout, Rev.1

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 RG 8.38 - Control of Access to High and Very High Radiation Areas of Nuclear Power Plants, Rev. 1

14.2.8 Utilization of Reactor Operating and Testing Experience in Test Program Development

The operational experience gained from pressurized-water and other reactor designs is factored into the design and testing.

Operations and technical staff review the following documents for information that can be included in the ITP:

- NRC licensee event reports
- NRC generic communications (i.e., inspection and enforcement bulletins, circulars, generic letters, administrative letters, information notices, and regulatory issue summaries)
- Institute of Nuclear Power Operations issuances

The administrative procedures control the review of reactor operating experience and its incorporation in the ITP.

14.2.9 Trial Use of Plant Operating Procedures, Emergency Procedures, and Surveillance Procedures

Plant emergency, operating, and surveillance test procedures are, to the extent practical, developed, trial tested, and corrected during the ITP before fuel load to establish their adequacy. Trial testing of procedures is accomplished by having plant operators trained to these procedures to the extent practicable during the ITP. Following completion of trial testing these procedures are used as part of the ITP.

Additionally, emergency, operating, and surveillance test procedures are incorporated into the plant reference simulator, which meets the requirements of 10 CFR 55.46(c), and are trial tested as part of the operator training program.

The administrative procedures control the trial use of approved plant operating procedures, emergency operating procedures, and surveillance procedures.

14.2.10 Initial Fuel Loading, and Initial Criticality

Approved startup tests are used to control startup testing for initial fuel loading, pre-critical tests, initial criticality, low-power tests, and power-ascension tests in a controlled, deliberate, and safe manner. Technical specification compliance is met prior to initiation of startup testing. Startup test procedures are prepared based upon test abstracts provided in Section 14.2.12.

Startup tests procedures contain general provisions, precautions, prerequisites, and measures consistent with the requirements of RG 1.68 Rev. 4.

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14.2.10.1 Initial Fuel Loading and Pre-Criticality Testing

As part of the startup test program, initial fuel loading and pre-criticality testing are performed by first implementing the prerequisite and precautionary measures that are contained in test procedures and identified below:

- technical specification compliance is met
- successful completion of all ITAAC
- actions to be taken in the event of unanticipated errors or malfunctions are clearly identified
- completion of a review of preoperational test results (the Startup Administrative Manual contains administrative procedures to control the verification process for successful completion of preoperational tests required for fuel load)
- review and status of design changes
- review of retests that were performed due to preoperational test deficiencies
- review of test exceptions

14.2.10.2 Initial Fuel Loading

Initial fuel loading is conducted to preclude inadvertent criticality. Specific safety measures are followed including (1) ensuring that the applicable TS are met, (2) performing continuous monitoring of the neutron flux throughout core loading so that changes in the multiplication factor are observed, (3) establishing requirements for periodic data taking, and (4) independently verifying that the fuel and control components have been properly installed.

Predictions of core reactivity are prepared in advance of the initial fuel loading to aid in evaluating the measured responses to specified loading increments. Comparative data on neutron detector responses from previous loadings of essentially identical core designs may be used in lieu of these predictions. Criteria and requirements for actions to be taken if the measured results deviate from expected values are established prior to the initial fuel loading. In addition, prior to initial fuel loading the required shutdown margin (SDM) is confirmed.

To provide further assurance of safe loading, requirements for the functionality of plant systems and components are established, including reactivity control systems and other systems and components necessary to ensure the safety of plant personnel and the public in the event of errors or malfunctions. The initial core loading is directly supervised by a senior licensed operator having no other concurrent duties, and the loading operation is conducted in strict accordance with detailed approved procedures.

14.2.10.3 Initial Criticality Testing

Control rods are withdrawn in the normal sequence to a configuration that does not violate the zero power rod insertion limits. Initial criticality is then achieved in a deliberate, orderly, and controlled fashion using boron dilution. Core neutron flux is

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continuously monitored during the approach to critical. Changes in reactivity are continuously monitored, and inverse multiplication plots are maintained and interpreted.

The following conditions exist prior to initial criticality:

- A minimum crew is required to support initial criticality, including a senior reactor operator with no other concurrent duties who is in charge of the operation.
- Critical rod position and boron concentration predictions are identified so that anomalies can be noted and evaluated.
- Systems needed for startup are aligned and in proper operation.
- Emergency systems are operable and in readiness.
- TS compliance is met.
- Nuclear instruments are calibrated.
- Neutron count rate of at least 1/2 counts per second registers on startup channels before the startup begins.
- Signal to noise ratio is greater than two.
- Conservative startup rate limit (greater than approximately a 30-second period) is established.
- High flux scram trips are set at their lowest value.
- Implementation of the radiation monitoring program as it pertains to operation of radiation barriers, airborne radiation monitors, air sampling, as well as performance of baseline surveys before pulling control rods for the approach to critical.

14.2.10.4 Low-Power Testing

Following initial criticality, low-power tests (at less than 5 percent power) are conducted to (1) confirm the design and, to the extent practical, validate the analytical models, and verify the correctness or conservatism of assumptions used in the safety analyses for the facility, and (2) confirm the functionality of plant systems and design features that could not be completely tested during the preoperational test phase because of the lack of an adequate heat source for the reactor coolant and main steam systems.

Low-power testing is performed in a controlled manner in accordance with written procedures. The minimum crew required to support low-power testing is available in addition to a senior reactor operator with no other concurrent duties who is in charge of low-power testing operations. Low-power testing procedures include instructions and precautions necessary for conducting tests such as adherence to TS requirements, testing sequence, measurement to be taken and test conditions as well as actions to be taken in the event of unanticipated errors or malfunctions. These procedures provide direction for restoration to normal following the test.

Refer to Section 14.2.12 for a list of low-power tests.

COL Item 14.2-3: A COL applicant that references the NuScale Power Plant design certification will identify the specific operator training to be conducted during low-power testing related to the resolution of TMI Action Plan Item I.G.1, as described in NUREG-0660, NUREG-0694, and NUREG-0737.

14.2.10.5 Power-Ascension Tests

Power-ascension testing is performed following the successful completion of low-power testing. Power-ascension testing is performed to bring the reactor to full power and while doing so performing major testing at power levels of approximately 25 percent, 50 percent, 75 percent, and 100 percent. The purpose of the testing is to demonstrate that the plant operates in accordance with its design bases during normal steady state conditions and, to the extent practicable, during and following anticipated transients as well as to demonstrate the validity of analytical models by comparing measured responses with predicted responses. Predicted responses are developed using real or expected values of attributes such as beginning of life core reactivity coefficients, flow rates, pressures, temperatures, and response times of equipment, as well as the actual status of the plant (not those values or plant conditions assumed for conservative evaluations of postulated accidents).

Tests and acceptance criteria are prescribed to demonstrate the ability of principal plant control systems to automatically control process variables within design limits. Such tests are expected to provide assurance that the facility's integrated dynamic response is in accordance with the design for plant events such as reactor scram, turbine trip, and loss of feedwater heaters or pumps. The testing performed is sufficiently comprehensive to establish that the facility can operate in the operating modes for which it has been designed. Testing is not conducted in operating modes or plant configurations that have not been analyzed or that fall outside the range of assumptions used in analyzing postulated accidents described in the Final Safety Analysis Report.

Power-ascension testing is performed in a controlled manner in accordance with written procedures. The minimum crew required to support power-ascension testing is available in addition to a senior reactor operator with no other concurrent duties who is in charge of power-ascension testing operations. Power-ascension testing procedures include instructions and precautions necessary for conducting tests such as adherence to TS requirements, testing sequence, measurement to be taken and test conditions as well as actions to be taken in the event of unanticipated errors or malfunctions. These procedures provide direction for restoration to normal following the test.

Refer to Section 14.2.12 for a list of power-ascension tests.

The completed power-ascension testing program is reviewed at each plateau. Test results are evaluated and the required approvals are received before ascending to the next power level or test condition.

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14.2.11 Test Program Schedule and Sequence

Testing schedules are developed taking into account development and approval of plant procedures for use as part of the ITP.

Testing schedules are developed so that SSC that are required to prevent or mitigate the consequences of postulated accidents are tested prior to fuel loading.

Approved test procedures are submitted to the NRC approximately 60 days before their intended use or at least 60 days prior to fuel loading for fuel loading and startup test procedures. The NRC is notified of test procedure changes prior to performance.

Test procedures are essentially identical for each NPM. SSC identification numbering is specific to each NPM.

For individual startup tests, test requirements are completed in accordance with plant TS requirements associated with SSC functionality before changing plant modes.

Testing required to be completed prior to fuel load that is intended to satisfy the requirements for completing ITAAC is identified and documented as such.

Vibration testing that is performed at the factory is performed in accordance to the requirements of the NuScale "Comprehensive Vibration Assessment Program" as described in the "Comprehensive Vibration Assessment Program (CVAP) Technical Report," TR-0716-50439. The technical report contains a schedule for the CVAP testing. Test results are verified following power-ascension testing. See Section 3.9.2 for information pertaining to the CVAP.

The sequential schedule for individual startup tests establishes, insofar as practicable, that test requirements are completed prior to exceeding 25 percent power for the plant SSC that are relied upon to prevent, limit, or mitigate the consequences of postulated accidents. The schedule establishes that, insofar as practicable, the sequencing of testing is accomplished as early in the test program as feasible and that the safety of the plant is not dependent on the performance of untested systems, components, or features. Startup test data is reviewed and approved prior to moving onto the next power plateau. Startup testing is discussed in Section 14.2.1.3.

The NuScale Power Plant is comprised of up to 12 NPMs. A schedule is developed for startup of each NPM. Preoperational and startup testing schedule considerations include:

- preoperational test schedule duration will be greatest for the first NPM because the first NPM will require testing of systems common to other NPMs
- preoperational and startup test schedule duration should decrease for each successive NPM due to increase in personnel experience and refinement of test procedures
- scheduling such that overlapping test program schedules will not result in significant divisions of responsibilities or dilute staff provided to implement the test program
- plant safety will not be dependent on the performance of untested SSC during the startup test program

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Refer to Section 21.3.3 for information pertaining to phased construction and testing activities due to addition of individual NPMs.

COL Item 14.2-4: A COL applicant that references the NuScale Power Plant design certification will provide a schedule for the Initial Test Program.

14.2.12 Individual Test Descriptions

Individual test abstracts are provided in Table 14.2-1 through Table 14.2-108. Table 14.2-109 provides a listing of the test abstracts. Each abstract identifies each test by title, identifies test objectives, prerequisites, test methods, and acceptance criteria. Detailed preoperational and startup test procedures are developed using these test abstracts.

The test abstracts identify pertinent precautions for individual tests, as necessary (e.g., minimum flow requirements or reactor power level that must be maintained).

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Table 14.2-1: Spent Fuel Pool Cooling System Test # 1

1 able 14.2	-1: Spent Fuel Pool Cooling Syste	em Test # 1
Preoperational test is required to be p	erformed once.	
	.2.1. SFPCS functions are not verified by	SFPCS tests. SFPCS functions verified
by another test is:		
System Function	System Function Categorization	Function Verified by Test #
The spent fuel pool cooling system (SFPCS) supports the pool cleanup system (PCUS) by providing fuel pool water for purification of the ultimate heat sink (UHS).	nonsafety-related	Test #2-1
Prerequisites		
<u> </u>	completed, with approved records and w	ithin all calibration due dates, for all
Test Objective	Test Method	Acceptance Criteria
 i. Verify each SFPCS remotely-operated valve can be operated remotely. ii. Verify each SFPCS air-operated valve 		MCR display and local, visual observation indicate each valve fully opens and fully closes. MCR display and local, visual
fails to its safe position on loss of air.	Isolate and vent air to the valve.	observation indicate each valve fails to its safe position.
iii. Verify each SFPCS air-operated valve fails to its safe position on loss of electrical power to its solenoid.	Place each valve in its non-safe position. Isolate electrical power to each air-operated valve.	MCR display and local, visual observation indicate each valve fails to its safe position.
iv. Verify each SFPCS pump can be started and stopped remotely.	Align the SFPCS to allow for pump operation. Stop and start each pump from the MCR.	MCR display and local, visual observation indicate each pump starts and stops.
v. Verify each SFPCS pump automatically stops to protect the pump.	Align the SFPCS to allow for pump operation. Place a pump in service. Initiate a simulated stop signal for the following system conditions. i. Low pump suction pressure ii. High pump discharge pressure.	MCR display and local, visual observation indicate each pump stops.
vi. Verify a local grab sample can be obtained from a SFPCS grab sample device.	Place the system in service to allow flow through the grab sampling device.	A local grab sample is successfully obtained.
vii. Verify each SFPCS instrument is monitored in the MCR and the remote shutdown station (RSS), if the signal is designed to be displayed in the RSS. (Test not required if the instrument	Initiate a single real or simulated instrument signal from each SFPCS transmitter.	 i. The instrument signal is displayed on an MCR workstation or recorded by the applicable control system historian. ii. The instrument signal is displayed on an RSS workstation or recorded
calibration verified the MCR and RSS display)		by the applicable control system historian if the instrument signal is designed to be displayed in the RSS. iii. The instrument signal is displayed on an MCR module-specific safety display instrument monitor or an MCR common safety display instrument monitor if the
		instrument signal is designed to be displayed on a safety display instrument monitor.

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Table 14.2-1: Spent Fuel Pool Cooling System Test # 1 (Continued)

System Level Tests	
None	

Table 14.2-2: Pool Cleanup System Test # 2

The PCUS is described in Section 9.1.3.2.3 and the functions verified by this test are:		
System Function	System Function Categorization	Function Verified by Test #
 The SFPCS supports the PCUS by providing spent fuel pool water for purification of the UHS. 	nonsafety-related	Test #2-1
 The reactor pool cooling system (RPCS) supports the PCUS by providing reactor pool water for purification of the UHS. 	nonsafety-related	Test #2-1

Prerequisites

- i. Verify an instrument calibration has been completed, with approved records and within all calibration due dates, for all instruments required to perform this test.
- ii. Verify a pump curve test has been completed and approved for the RPCS pumps.
- iii. Verify a pump curve test has been completed and approved for the SFPCS pumps.

Co	Component Level Tests			
Te	st Objective	Test Method	Acceptance Criteria	
i.	Verify each PCUS remotely-operated valve can be operated remotely.	Operate each valve from the MCR and local control panel (if design has local valve control)	MCR display and local, visual observation indicate each valve fully opens and fully closes.	
ii.	Verify each PCUS air-operated valve fails to its safe position on loss of air.	Place each valve in its non-safe position. Isolate and vent air to the valve.	MCR display and local, visual observation indicate each valve fails to its safe position.	
	Verify each PCUS air-operated valve fails to its safe position on loss of electrical power to its solenoid.	Place each valve in its non-safe position. Isolate electrical power to each air- operated valve.	MCR display and local, visual observation indicate each valve fails to its safe position.	
	Verify a local grab sample can be obtained from a PCUS grab sample device.	Place the system in service to allow flow through the grab sampling device.	A local grab sample is successfully obtained.	
v.	Verify each PCUS instrument is monitored in the MCR and the RSS, if the signal is designed to be displayed in the RSS.	Initiate a single real or simulated instrument signal from each PCUS transmitter.	 The instrument signal is displayed on an MCR workstation or recorded by the applicable control system historian. 	
	(Test not required if the instrument calibration verified the MCR and RSS display.)		ii. The instrument signal is displayed on an RSS workstation or recorded by the applicable control system historian if the instrument signal is designed to be displayed in the RSS.	
			iii. The instrument signal is displayed on an MCR module-specific safety display instrument monitor or an MCR common safety display instrument monitor if the instrument signal is designed to be displayed on a safety display instrument monitor.	

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Table 14.2-2: Pool Cleanup System Test # 2 (Continued)

System Level Test #2-1				
Test Objective	Test Method	Acceptance Criteria		
Verify the PCUS demineralizers are protected against high water temperature.	 Place the SFPCS in service to flow through a pool cleanup filter and a demineralizer and return flow to the spent fuel pool. 	i. a. The MCR indication for SFPCS pump flow satisfies the design flow rate specified in Table 9.1.3		
	AND Place the RPCS in service to flow through a different pool cleanup filter and demineralizer and return	b. The MCR indication for RPCS pump flow satisfies the design flow rate specified in Table 9.1.3		
	flow to the reactor pool. ii. Simulate a high water temperature upstream of one of the pool cleanup	ii. a. SFPCS flow and RPCS flow to th pool cleanup filters and demineralizers stop.		
	filters.	b. The SFPCS flow is bypassed to the spent fuel pool.		
		c. The RPCS cooling flow is bypassed to the reactor pool.		
		d. The MCR indication for SFPCS pump flow satisfies the design flow rate specified in Table 9.1.3		
		e. The MCR indication for RPCS pump flow satisfies the design flow rate specified in Table 9.1 1b		

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		2-3: Reactor Pool Cooling Systen	
Preoperational test is required to be performed once.			
	e RPCS is described in Section 9.1.3.2 rified by other tests are:	2.2. RPC system functions are not verifie	ed by RPCS tests. RPCS functions
Sy	stem Function	System Function Categorization	Function Verified by Test #
	e RPCS supports the PCUS by	nonsafety-related	PCU Test #2-1
	oviding reactor pool water for		
	rification of the UHS.		
	erequisites		
	rify an instrument calibration has been struments required to perform this test.	completed, with approved records and w	ithin all calibration due dates, for all
Со	mponent Level Tests		
Те	st Objective	Test Method	Acceptance Criteria
i.	Verify each RPCS remotely-operated valve can be operated remotely.	Operate each valve from the MCR and local control panel (if design has local valve control)	MCR display and local, visual observation indicate each valve fully opens and fully closes.
i.	Verify each RPCS air-operated valve fails to its safe position on loss of air.	Place each valve in its non-safe position. Isolate and vent air to the valve.	MCR display and local, visual observation indicate each valve fails to its safe position.
ii.	Verify each RPCS air-operated valve fails to its safe position on loss of	Place each valve in its non-safe position. Isolate electrical power to each air-	MCR display and local, visual observation indicate each valve fails to
	electrical power to its solenoid.	operated valve.	its safe position.
٧.	Verify each RPCS pump can be	Align the RPCS to allow for pump	MCR display and local, visual
	started and stopped remotely.	operation.	observation indicate each pump starts and stops.
_	V-::f DDCC	Stop and start each pump from the MCR.	· ·
/.	Verify each RPCS pump automatically stops to protect the pump.	Align the RPCS to allow for pump operation. Place a pump in service. Initiate a simulated stop signal for the	MCR display and local, visual observation indicate each pump stops
		following system conditions.	
		i. Low pump suction pressure.	
		ii. High pump discharge pressure.	
/i.	Verify a local grab sample can be	Place the system in service to allow flow	A local grab sample is successfully
	obtained from an RPCS grab sample	through the grab sampling device.	obtained.
	device indicated on the RPCS piping and instrumentation diagram.		
,ii	Verify each RPCS instrument is	Initiate a single real or simulated	i. The instrument signal is displayed
V 11.	monitored in the MCR and the RSS, if the signal is designed to be displayed in the RSS.	instrument signal from each RPCS transmitter.	on an MCR workstation or recorded by the applicable control system historian.
	(Test not required if the instrument calibration verified the MCR and RSS display)		ii. The instrument signal is displayed on an RSS workstation or recorded by the applicable control system historian if the instrument signal is designed to be displayed in the RS
			iii. The instrument signal is displayed on an MCR module-specific safety display instrument monitor or an MCR common safety display instrument monitor if the instrument signal is designed to be displayed on a safety display instrument monitor.

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instrument monitor.

Table 14.2-3: Reactor Pool Cooling System Test # 3 (Continued)

System Level Tests	
None	

Table 14.2-4: Pool Surge Control System Test #4

• • • •	The pool surge control system (PSCS) is described in Section 9.1.3.2.4 and the function verified by this test is:					
-	stem Function	System Function Categorization	Function Verified by Test #			
sur	e PSCS supports the UHS by providing rge control for UHS operations.	nonsafety-related	Test #4-1			
Pre	erequisites					
	rify an instrument calibration has been truments required to perform this test.	completed, with approved records and w	ithin all calibration due dates, for all			
Co	mponent Level Tests					
Te	st Objective	Test Method	Acceptance Criteria			
i.	Verify each PSCS remotely-operated valve can be operated remotely.	Operate each valve from the MCR and local control panel (if design has local valve control)	MCR display and local, visual observation indicate each valve fully opens and fully closes.			
ii.	Verify each PSCS air-operated valve fails to its safe position on loss of air.	Place each valve in its non-safe position. Isolate and vent air to the valve.	MCR display and local, visual observation indicate each valve fails to its safe position.			
	Verify each PSCS air-operated valve fails to its safe position on loss of electrical power to its solenoid.	Place each valve in its non-safe position. Isolate electrical power to each air- operated valve.	MCR display and local, visual observation indicate each valve fails to its safe position.			
iv.	Verify each PSCS pump can be started and stopped remotely.		MCR display and local, visual observation indicate each pump starts and stops.			
V.	Verify the PSCS automatically responds to mitigate a release of radioactivity.	Initiate a real or simulated high radiation signal in the PSCS tank vent line.	 i. The PSCS tank inlet isolation valve is closed. ii. The PSCS tank outlet isolation valve is closed. [ITAAC 03.09.10] 			
vi.	Verify a local grab sample can be obtained from a PSCS grab sample device indicated on the PSC piping and instrumentation diagram.	Place the system in service to allow flow through the grab sampling device.	A local grab sample is successfully obtained.			
vii.	Verify each PSC system instrument is monitored in the MCR and the RSS, if the signal is designed to be displayed in the RSS). (Test not required if the instrument calibration verified the MCR and RSS display.)	Initiate a single real or simulated instrument signal from each PSCS transmitter.	 i. The instrument signal is displayed on an MCR workstation or recorded by the applicable control system historian. ii. The instrument signal is displayed on an RSS workstation or recorded by the applicable control system historian if the instrument signal is designed to be displayed in the RSS iii. The instrument signal is displayed 			
			on an MCR module-specific safety display instrument monitor or an MCR common safety display instrument monitor if the instrument signal is designed to be displayed on a safety display instrument monitor.			

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Table 14.2-4: Pool Surge Control System Test #4 (Continued)

System Level Test #4-1					
Test Objective	Test Method	Acceptance Criteria			
	Align the PSCS for fill and drain of the dry dock. Fill the dry dock to a level that allows operation of the reactor inspection dry dock evacuation pump. i. Start a PSCS pump and simulate the following PSCS conditions: a. Dry dock low level b. PSC tank high level c. High dry dock level	 i. a. Pump is stopped and return line to pool surge control tank isolation valve is closed. b. Pump is stopped and return line to PSCS tank isolation valve is closed. c. PSCS tank main discharge line isolation valve is closed. 			

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Table 14.2-5: Ultimate Heat Sink Test # 5

There are no preoperational	tests for the UHS.					
The UHS is described in Section 9.2.5. The only active functions for the UHS are to provide PAM Type D instrument signals to the safety display and indication system (SDIS). Refer to Table 14.2-66: Safety Display and Indication test #66 for testing of PAM Type D displays.						
System Function	System Function Categorization	Function Verified by Test #				
None	N/A	N/A				
Prerequisites:	·	<u> </u>				
N/A						
Component Level Tests						
None						

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Table 14.2-6: Pool Leak Detection System Test # 6

There are no preoperational tests for the pool leakage detection system (PLDS).					
The PLDS is described in Section 9.1.3.2.5 Leakage from the UHS liner gravity drains to the radiation waste drain system (RWDS). Test #23-2 tests the MCR alarm when the RWDS sump fill rate exceeds the PLDS leakage rate setpoint.					
System Function	System Function				
None	N/A	N/A			
Prerequisites:					
N/A					
Component Level Tests					
None					

Table 14.2-7: Reactor Component Cooling Water System Test # 7

Preoperational test is required to be performed once for shared/common components, 6 times for the module-specific components on the 6A NPMs and once for shared/common components, 6 times for the module-specific components on the 6B NPMs.

The RCCWS is described in Section 9.2.2 and 11.5.2.2.12 and the function verified by this test is:

System Function	System Function Categorization	Function Verified by Test #
The reactor component cooling water	nonsafety-related	Test #7-1
system (RCCWS) supports the following		
systems by providing cooling water.		
 control rod drive system (CRDS) chemical and volume control system (CVCS) 		
containment evacuation system (CES)process sampling system (PSS)		

Prerequisites

- i. Verify an instrument calibration has been completed, with approved records and within all calibration due dates, for all instruments required to perform this test.
- ii. Verify an RCCWS flow balance has been performed.
- iii. Verify a pump curve test has been completed for the RCCWS pumps.

Component Level Tests

Te	st Objective	Test Method	Acceptance Criteria
i.	Verify each RCCWS remotely-	Operate each valve from the MCR and	MCR display and local, visual
	operated valve can be operated	local control panel (if design has local	observation indicate each valve fully
	remotely.	valve control)	opens and fully closes.
ii.	Verify each RCCWS air-operated valve	Place each valve in its non-safe position.	MCR display and local, visual
	fails to its safe position on loss of air.	Isolate and vent air to the valve.	observation indicate each valve fails to
			its safe position.
iii.	Verify each RCCWS air-operated valve	Place each valve in its non-safe position.	MCR display and local, visual
	fails to its safe position on loss of	Isolate electrical power to each air-	observation indicate each valve fails to
	electrical power to its solenoid.	operated valve.	its safe position.
iv.	Verify each RCCWS pump can be	Align the RCCWS to allow for pump	MCR display and local, visual
	started and stopped remotely.	operation.	observation indicate each pump starts
		Stop and start each pump from the MCR.	and stops.
			Audible and visible water hammer are
			not observed when the pump starts.
٧.	Verify the RCCWS standby pump	Align the RCCWS to allow for pump	MCR display and local, visual
	automatically starts to protect plant	operation. Place a pump in service.	observation indicate the standby pump
	equipment.	Initiate a simulated RCCWS pump low	starts.
		header pressure signal.	Audible and visible water hammer are
			not observed when the pump starts.
vi.	Verify RCCWS demineralized makeup		MCR display and local, visual
	water level control valve	high level signal.	observation indicate the following:
	automatically operates to maintain	ii. Initiate a simulated expansion tank	i. The demineralized makeup water
	RCCW expansion tank level.	low level signal.	level control valve is fully closed.
			ii. The demineralized makeup water
			level control valve is fully open.
vii.	Verify a local grab sample can be	Place the system in service to allow flow	A local grab sample is successfully
	obtained from an RCCWS grab	through the grab sampling device.	obtained.
	sample device.		

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Table 14.2-7: Reactor Component Cooling Water System Test # 7 (Continued)

·	Initiate a single real or simulated instrument signal from each RCCWS transmitter.	 i. The instrument signal is displayed on an MCR workstation or recorded by the applicable control system historian. ii. The instrument signal is displayed on an RSS workstation or recorded by the applicable control system historian if the instrument signal is designed to be displayed in the RSS. iii. The instrument signal is displayed on an MCR module-specific safety display instrument monitor or an MCR common safety display instrument monitor if the instrument signal is designed to be displayed on a safety display instrument monitor.
System Level Test #7-1		1
Test Objective	Test Method	Acceptance Criteria
Verify RCCWS cooling water flow rates satisfy design flow.	i. Align the 6A RCCWS to provide flow to all the Module 1 heat exchangers cooled by RCCWS listed below: Module 1 Heat Exchangers Control rod drive mechanism (CRDM) cooling coils CVCS non-regenerative heat exchanger CES vacuum pump CES condenser PSS analyzer cooler PSS temperature control unit ii. Repeat module 1 test for modules 2 through 6. iii. Align the 6B RCCWS to provide flow to all the Module 7 heat exchangers cooled by RCCWS listed below: Module 7 Heat Exchangers CRDM cooling coils CVCS non-regenerative heat exchanger CES vacuum pump CES condenser PSS analyzer cooler PSS analyzer cooler PSS temperature control unit iv. Repeat Module 7 test for modules 8	The RCCWS cooling flow to each heat exchanger under test meets the flow rate acceptance criteria contained in the RCCWS flow balance report.

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Table 14.2-8: Chilled Water System Test # 8

Preoperational test is required to be performed once.			
The chilled water system (CHWS) is described in Section 9.2.8 and the function verified by this test is:			
System Function System Function Categorization Function Verified b			
The CHWS supports the following	nonsafety-related	Test #8-1	
systems by providing cooling water:		Test #8-2	
 Reactor Building HVAC system (RBVS) normal control room HVAC system (CRVS) Radioactive Waste Building HVAC system (RWBVS) 			
 liquid radioactive waste system (LRWS) gaseous radioactive waste system (GRWS) 			

Prerequisites

- i. Verify an instrument calibration has been completed, with approved records and within all calibration due dates, for all instruments required to perform this test.
- ii. Verify a CHWS flow balance has been performed.
- iii. Verify a pump curve test has been completed for the CHWS pumps.

_	verify a partie test has been completed for the CHWS parties.			
Co	Component Level Tests			
Te	st Objective	Test Method	Acceptance Criteria	
i.	Verify each CHWS remotely-operated valve can be operated remotely.	Operate each valve from the MCR and local control panel (if design has local valve control)	MCR display and local, visual observation indicate each valve fully opens and fully closes.	
ii.	Verify each CHWS air-operated valve fails to its safe position on loss of air.	Place each valve in its non-safe position. Isolate and vent air to the valve.	MCR display and local, visual observation indicate each valve fails to its safe position.	
iii.	Verify each CHWS air-operated valve fails to its safe position on loss of electrical power to its solenoid.	Place each valve in its non-safe position. Isolate electrical power to each air- operated valve.	MCR display and local, visual observation indicate each valve fails to its safe position.	
iv.	Verify the speed of each CHWS variable-speed pump can be manually controlled.	Align the CHWS to provide a flow path to operate a selected pump. Vary the CHWS pump speed from minimum to maximum from the MCR.	MCR display indicates the speed of each obtains both minimum and maximum pump speeds. Audible and visible water hammer are not observed when the pump starts.	
v.	Verify automatic operation of CHWS pumps and CHWS chiller to protect plant equipment.	following system conditions.	MCR display and local, visual observation indicate the following: i. a. Operating pump stops b. Operating chiller stops ii. Operating chiller stops	

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Table 14.2-8: Chilled Water System Test # 8 (Continued)

monitored in the MCR and the RSS, if the signal is designed to be displayed in the RSS. (Test not required if the instrument calibration verified the MCR and RSS display)	Initiate a single real or simulated instrument signal from each CHWS transmitter.	 i. The instrument signal is displayed on an MCR workstation or recorded by the applicable control system historian. ii. The instrument signal is displayed on an RSS workstation or recorded by the applicable control system historian if the instrument signal is designed to be displayed in the RSS. iii. The instrument signal is displayed on an MCR module-specific safety display instrument monitor or an MCR common safety display instrument monitor if the instrument signal is designed to be displayed on a safety display instrument monitor.
System Level Test #8-1 Test Objective	Test Method	Acceptance Criteria
Verify CHWS cooling water flow rates satisfy design.		The CHWS cooling flow to each heat exchanger under test meets the minimum flow rate acceptance criteria contained in the CHWS flow balance report.
System Level Test #8-2 Test Objective	Test Method	Acceptance Criteria
	i. Align the CHWS to provide flow to the CRVS air handling units and the CRVS fan coil units cooled by the	The CRVS standby CHWS cooling flow to each heat exchanger meets the minimum flow rate acceptance criteria

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Table 14.2-9: Auxiliary Boiler System Test # 9

scribed in Section 10.4.10 and 11.5.2.	Preoperational test is required to be performed once. The auxiliary boiler system (ABS) is described in Section 10.4.10 and 11.5.2.2.14 and the functions verified by this test				
scribed in Section 10.4.10 and 11.5.2.2	2. 14 and the functions vermed by this te				
System Function Categorization	Function Verified by Test #				
sts are:					
nonsafety-related	CPS Test #30-1				
•	CAR Test #32-1				
nonsafety-related	CAR Test #32-1				
	TG Test #33-1				
	sts are: nonsafety-related nonsafety-related nonsafety-related nonsafety-related				

- Verify an instrument calibration has been completed, with approved records and within all calibration due dates, for all instruments required to perform this test.
- ii. Verify a pump curve test has been completed for the auxiliary boiler pumps.

Co	mponent Level Tests			
Test Objective		Test Method	Acceptance Criteria	
i.	Verify each auxiliary boiler remotely- operated valve can be operated remotely.	Operate each valve from the MCR and local control panel (if design has local valve control)	MCR display and local, visual observation indicate each valve fully opens and fully closes.	
ii.	Verify each auxiliary boiler air- operated valve fails to its safe position on loss of air.	Place each valve in its non-safe position. Isolate and vent air to the valve.	MCR display and local, visual observation indicate each valve fails to its safe position.	
iii.	Verify each auxiliary boiler air- operated valve fails to its safe position on loss of electrical power to its solenoid.	Place each valve in its non-safe position. Isolate electrical power to each air- operated valve.	MCR display and local, visual observation indicate each valve fails to its safe position.	
iv.	Verify each auxiliary boiler low pressure boiler feedwater pump can be started and stopped remotely.	Align the ABS to allow for pump operation. Stop and start each pump from the MCR.	MCR display and local, visual observation indicate each pump starts and stops. Audible and visible water hammer are not observed when the pump starts.	
V.	Verify the speed of each auxiliary boiler high pressure boiler feedwater pump can be manually controlled.	Align the ABS to provide a flow path to operate a selected AB variable-speed pump. Vary the auxiliary boiler pump speed from minimum to maximum speed from the MCR.	MCR display indicates the speed of each variable speed pump obtains both minimum and maximum pump speeds. Audible and visible water hammer are not observed when the pump starts.	
vi.	Verify the ABS automatically responds to mitigate a release of radioactivity.	Initiate a real or simulated high radiation signal for the auxiliary boiler flash tank vent.	MCR display verifies the following: i. auxiliary boiler flash tank vent isolation valve is closed. ii. auxiliary boiler high pressure steam supply isolation valves are closed. [ITAAC 03.09.08] (i.and ii.)	

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Table 14.2-9: Auxiliary Boiler System Test # 9 (Continued)

None			
Test Objective	•	Test Method	Acceptance Criteria
System Level			
Secretary Laval	T4		designed to be displayed in the RSS. iii. The instrument signal is displayed on an MCR module-specific safety display instrument monitor or an MCR common safety display instrument monitor if the instrument signal is designed to be displayed on a safety display instrument monitor.
	equired if the instrument verified the MCR and RSS		ii. The instrument signal is displayed on an RSS workstation or recorded by the applicable control system historian if the instrument signal is
monitored		Initiate a single real or simulated instrument signal from each ABS transmitter.	 The instrument signal is displayed on an MCR workstation or recorded by the applicable control system historian.
			valve is closed. [ITAAC 03.09.09]
	o mitigate a release of	Initiate a real or simulated high radiation signal for the auxiliary boiler high pressure to low pressure steam supply.	MCR display verifies the following: auxiliary boiler high pressure to low pressure steam supply pressure control

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Table 14.2-10: Circulating Water System Test # 10

This preoperational test is required to be performed once for each circulating water subsystem. The circulating water system (CWS) is described in Section 10.4.5 and the function verified by this test is:				
System Function	System Function Categorization	Function Verified by Test #		
The utility water system (UWS) supports the CWS by providing makeup water to maintain water level in the CWS cooling tower basins.	nonsafety-related	Component-Level Test vi.		
The CWS function verified by another t	test is:			
System Function	System Function Categorization	Function Verified by Test #		
The CWS supports the FWS by removing heat from the main condenser.	nonsafety-related	CAR Test #32-1		
Droroguisitos	•			

Prerequisites

Verify an instrument calibration has been completed, with approved records and within all calibration due dates, for all instruments required to perform this test.

Component Level Tests: NPM #1 (#7)

The minimum inventory of pumps, fans and valves tested for NPM #1 (#7) is that inventory required for 6A (6B) CWS operation to support operation of NPM #1 (#7). The testing will continue until all 6A (6B) CWS equipment is tested.

Te	st Objective	Test Method	Acceptance Criteria
i.	Verify each CWS remotely-operated	Operate each valve from the MCR and	MCR display and local, visual
	valve can be operated remotely.	local control panel (if design has local	observation indicate each valve fully
		valve control)	opens and fully closes.
ii.	Verify each CWS air-operated valve	Place each valve in its non-safe position.	MCR display and local, visual
	fails to its safe position on loss of air.	Isolate and vent air to the valve.	observation indicate each valve fails to
			its safe position.
iii.	Verify each CWS air-operated valve	Place each valve in its non-safe position.	MCR display and local, visual
	fails to its safe position on loss of	Isolate electrical power to each air-	observation indicate each valve fails to
	electrical power to its solenoid.	operated valve.	its safe position.
iv.	Verify each CWS cooling tower fan	Align the CWS to allow for cooling tower	MCR display and local, visual
	can be started and stopped remotely	fan operation.	observation indicate each cooling tower
		Stop and start each cooling tower fan	fan starts and stops.
		from the MCR.	
٧.	Verify each CWS pump can be started	Align the CWS to allow for pump	i. MCR display and local, visual
	and stopped remotely.	operation.	observation indicate each pump
		Stop and start each pump from the MCR.	starts and stops.
		· · ·	ii. Audible and visible water hammer
			are not observed when the pump
			starts.
			iii. CWS pump cavitation is not
			observed.
			iv. Cooling towers do not experience
			flow surge or overflow.
vi	Verify automatic operation of the	i. Initiate a cooling tower basin low	MCR displays and local, visual
۷۱.	CWS cooling tower basin level	level signal.	observation verifies the following:
	control valve to maintain CWS	ii. Initiate a cooling tower basin high	i. The cooling tower basin level
	cooling tower basin level.	level signal.	control valve is open.
	cooming tower busin level.	lever signal.	'
			ii. The cooling tower basin level
			control valve is closed.

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Table 14.2-10: Circulating Water System Test # 10 (Continued)

	1			
vii. Verify each CWS instrument is monitored in the MCR and the RSS, if	Initiate a single real or simulated instrument signal from each CWS	i.	The instrument signal is displayed on an MCR workstation or recorded	
the signal is designed to be displayed in the RSS.	_		by the applicable control system historian.	
(Test not required if the instrument calibration verified the MCR and RSS display.)		ii.	The instrument signal is displayed on an RSS workstation or recorded by the applicable control system historian if the instrument signal is designed to be displayed in the RSS.	
		iii.	The instrument signal is displayed on an MCR module-specific safety display instrument monitor or an MCR common safety display instrument monitor if the instrument signal is designed to be displayed on a safety display instrument monitor.	
System Level Tests				
None				

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Table 14.2-11: Site Cooling Water System Test # 11

Preoperational test is required to be performed for each NPM.				
The site cooling water system (SCWS) is described in Section 9.2.7 and 11.5.2.2.13 and the functions verified by t				
test are:				
System Function	System Function Categorization	Function Verified by Test #		
The SCWS supports the following systems by providing cooling water.	nonsafety-related	Test #11-1		
turbine generator system (TGS)RCCWS				
condenser air removal system (CARS)PSS				
• CHWS				
 instrument air system (IAS) 				
• SFPCS				
• RPCS				
 auxiliary boiler 				
The UWS supports the SCWS by providing makeup water to maintain water level in the SCWS cooling tower	nonsafety-related	Component-Level Test vii.		

Prerequisites

basins.

- Verify an instrument calibration has been completed, with approved records and within all calibration due dates, for all instruments required to perform this test.
- ii. Verify an SCWS flow balance has been performed and the system flow balance records have been approved.
- iii. Verify a pump curve test has been completed and approved for the SCWS pumps.

Component Level Tests Test Objective Test Method Acceptance Criteria Verify each SCWS remotely-operated Operate each valve from the MCR and MCR display and local, visual valve can be operated remotely. local control panel (if design has local observation indicate each valve fully valve control). opens and fully closes. Verify each SCWS air-operated valve Place each valve in its non-safe position. MCR display and local, visual fails to its safe position on loss of air. Isolate and vent air to the valve. observation indicate each valve fails to its safe position. iii. Verify each SCWS air-operated valve Place each valve in its non-safe position. MCR display and local, visual fails to its safe position on loss of solate electrical power to each airobservation indicate each valve fails to electrical power to its solenoid. operated valve. its safe position. iv. Verify each SCWS cooling tower fan Align the SCWS to allow for cooling MCR display and local, visual can be started and stopped remotely. tower fan operation. observation indicate each cooling tower fan starts and stops. Stop and start each cooling tower fan from the MCR. Verify each SCWS pump can be Align the SCWS to allow for pump MCR display and local, visual started and stopped remotely. operation. observation indicate each pump starts and stops. Stop and start each pump from the MCR. Audible and visible water hammer are not observed when the pump starts. vi. Verify the SCWS standby pump Align the SCWS to allow for pump MCR display and local, visual automatically starts to protect plant operation. Place a pump in service. observation indicate the standby pump equipment. Initiate a simulated start signal for the discharge valve opens to a throttled following system conditions. position, the pump starts, and then the discharge valve fully opens. Low pump header pressure signal. Audible and visible water hammer are ii. Low pump header flow signal. not observed when the pump starts.

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Table 14.2-11: Site Cooling Water System Test # 11 (Continued)

vii.	SCWS cooling tower basin level	 i. Initiate a simulated cooling tower basin low level signal. ii. Initiate a simulated cooling tower basin high level signal. 	MCR displays and local, visual observation verifies the following: i. The cooling tower basin level control valve is open. ii. The cooling tower basin level control valve is closed.
viii		Place the system in service to allow flow through the grab sampling device.	A local grab sample is successfully obtained.
ix.	Verify each SCWS instrument is monitored in the MCR and the RSS, if the signal is designed to be displayed in the RSS.	_	i. The instrument signal is displayed on an MCR workstation or recorded by the applicable control system historian.
	(Test not required if the instrument calibration verified the MCR and RSS display)		ii. The instrument signal is displayed on an RSS workstation or recorded by the applicable control system historian if the instrument signal is designed to be displayed in the RSS.
			iii. The instrument signal is displayed on an MCR module-specific safety display instrument monitor or an MCR common safety display instrument monitor if the instrument signal is designed to be displayed on a safety display instrument monitor.

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Table 14.2-11: Site Cooling Water System Test # 11 (Continued)

Method eactor Power Module 1 Test lign the SCWS to provide flow to all le Module 1 and common heat schangers cooled by SCWS listed elow: eactor Power Module 1 Heat schangers ARS heat exchanger GS cooler GS lube oil cooler	Acceptance Criteria The SCWS cooling flow to each heat exchanger under test meets the minimum flow rate acceptance criteria contained in the SCWS flow balance report.
lign the SCWS to provide flow to all the Module 1 and common heat techangers cooled by SCWS listed telow: teactor Power Module 1 Heat techangers ARS heat exchanger	exchanger under test meets the minimum flow rate acceptance criteria contained in the SCWS flow balance
schangers ARS heat exchanger GS cooler	
ASS DEHC cooler WS sample cooler SS sample cooler COMMON Heat Exchangers HWS chillers Strument air coolers SS chillers PCS heat exchangers PCS heat exchangers CCWS heat exchangers ux boiler blowdown coolers ne operation of two SCWS pumps nay be required to provide sufficient ow to meet acceptance criteria in ne SCWS flow balance report. PERCENT POWER MODULE 2-12 Test ne scope of each subsequent test ill include one or more additional codules. The scope will also include reviously tested modules to verify test the flow rate still meets the flow	
orrelation of the state of the	mmon Heat Exchangers WS chillers rument air coolers chillers CS heat exchangers CS heat exchangers CWS heat exchangers c boiler blowdown coolers c operation of two SCWS pumps be required to provide sufficient of to meet acceptance criteria in SCWS flow balance report. cactor Power Module 2-12 Test c scope of each subsequent test include one or more additional dules. The scope will also include

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Table 14.2-12: Potable Water System Test # 12

The potable water system (PWS) is described in Section 9.2.4. The PWS is a site-specific system, and the testing of the PWS is the responsibility of the COL applicant.

COL Item 14.2-5: A COL applicant that references the NuScale Power Plant design certification will provide a test abstract for the potable water system pre-operational testing.

•	, , ,	
System Function	System Function Categorization	Function Verified by Test #
As described in Section 9.2.4	nonsafety-related	Provided by COL applicant
Prerequisites		<u> </u>
Provided by COL applicant		
Component Level Tests		
Provided by COL applicant		
System Level Tests		
Provided by COL applicant		

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Table 14.2-13: Utility Water System Test # 13

Preo	Preoperational test is required to be performed once.			
The UWS is described in Section 9.2.9 and the functions verified by this test are:				
Syste	em Function	System Function Categorization	Function Verified by Test #	
W	The UWS supports the circulating water system by providing makeup water to maintain water level in the EW system cooling tower basins.	nonsafety-related	Reference 14.2-10 Component-Level Test vi.	
p w	The UWS supports the SCWS by broviding makeup water to maintain water level in the SCWS cooling ower basins.	nonsafety related	Reference 14.2-11 Component-Level Test vii.	

Prerequisites

- i. Verify an instrument calibration has been completed, with approved records and within all calibration due dates, for all instruments required to perform this test.
- ii. Verify a pump curve test has been completed for the UWS pumps.

Component Level Tests
Test Objective

Te	st Objective	Test Method	Acceptance Criteria
i.	Verify each UWS remotely-operated valve can be operated remotely.	Operate each valve from the MCR and local control panel (if design has local valve control).	MCR display and local, visual observation indicate each valve fully opens and fully closes.
	fails to its safe position on loss of air.	Isolate and vent air to the valve.	MCR display and local, visual observation indicate each valve fails to its safe position.
iii.	Verify each UWS air-operated valve fails to its safe position on loss of electrical power to its solenoid.	Place each valve in its non-safe position. Isolate electrical power to each air- operated valve.	MCR display and local, visual observation indicate each valve fails to its safe position.
iv.	Verify each UWS pump can be started and stopped remotely.	Align the UWS to allow for pump operation. Stop and start each pump from the MCR.	MCR display and local, visual observation indicate each pump starts and stops. Audible and visible water hammer are not observed when the pump starts.
v.	Verify UWS flow capability by automatic start of each UWS pump while in standby mode.	Align the UWS to allow for pump operation. Place a pump in service. Initiate a simulated pump discharge pressure lowl.	MCR display and local, visual observation indicate the standby pump starts. Audible and visible water hammer are not observed when the pump starts.
vi.	Verify demineralized water system (DWS) pumps automatically stops to protect plant equipment.	Align the DWS to allow for pump operation. Place a pump in service. Initiate a simulated DWS storage tank low level signal.	MCR display and local, visual observation indicate each pump stops.
vii.	Verify pump low flow protection	 i. Align the DWS to allow for DWS pump operation. Place a DWS pump in operation. Manually throttle a valve in the DWS pump flow path until the pump flow rate reaches the pump minimum flow setpoint. ii. Open the throttled valve. 	MCR displays and local, visual observation verifies the following: i. The pump minimum flow valve is open. ii. The pump minimum flow valve is closed.

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Table 14.2-13: Utility Water System Test # 13 (Continued)

	1			
viii. Verify each DWS instrument is	Initiate a single real or simulated	i.	The instrument signal is displayed	
monitored in the MCR and the RSS, if	_		on an MCR workstation or recorded	
the signal is designed to be displayed	transmitter.		by the applicable control system	
in the RSS.			historian.	
(Test not required if the instrument		ii.	The instrument signal is displayed	
calibration verified the MCR and RSS			on an RSS workstation or recorded	
display.)			by the applicable control system	
			historian if the instrument signal is	
			designed to be displayed in the RSS.	
		iii.		
			on an MCR module-specific safety	
			display instrument monitor or an	
			MCR common safety display	
			instrument monitor if the	
			instrument signal is designed to be	
			displayed on a safety display	
			instrument monitor.	
System Level Tests				
None				

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Table 14.2-14: Demineralized Water System Test # 14

Preoperational test is required to be performed once.			
The DWS is described in Section 9.2.3 and 11.5.2.2.16 and the function verified by this test is:			
System Function	System Function Categorization	Function Verified by Test #	
The DWS supports the following systems by providing cooling water.	nonsafety-related	component-level tests	
 CVCSm boron addition system (BAS) Liquid Radioactive Waste (LRW) SFPCS RCCWS Process Sampling System (PSS) FWS ABS CRVS CARS 			

Prerequisites

- i. Verify an instrument calibration has been completed, with approved records and within all calibration due dates, for all
 instruments required to perform this test.
- ii. Verify a pump curve test has been completed for the DWS pumps.

Component Level Tests

Te	st Objective	Test Method	Acceptance Criteria
i.	Verify each DWS remotely-operated valve can be operated remotely.	Operate each valve from the MCR and local control panel (if design has local valve control)	MCR display and local, visual observation indicate each valve fully opens and fully closes.
ii.	Verify each DWS air-operated valve fails to its safe position on loss of air.	Place each valve in its non-safe position. Isolate and vent air to the valve.	MCR display and local, visual observation indicate each valve fails to its safe position.
iii.	Verify each DWS air-operated valve fails to its safe position on loss of electrical power to its solenoid.	Place each valve in its non-safe position. Isolate electrical power to each air- operated valve.	MCR display and local, visual observation indicate each valve fails to its safe position.
iv.	Verify the DWS pump can be started and stopped remotely.	Align the DWS to allow for pump operation. Stop and start each pump from the MCR.	MCR display and local, visual observation indicate each pump starts and stops. Audible and visible water hammer are not observed when the pump starts.
V.	Verify DWS flow capability by automatic start of each DWS pump while in standby mode.	Align the DWS to allow for pump operation. Place a pump in service. Initiate a simulated low pump header pressure low signal.	MCR display and local, visual observation indicate the standby pump starts. Audible and visible water hammer are not observed when the pump starts.
vi.	Verify DWS pumps automatically stops to protect plant equipment.	Align the DWS to allow for pump operation. Place a pump in service. Initiate a simulated DWS storage tank low level signal.	MCR display and local, visual observation indicate each pump stops.
vii.	Verify pump low flow protection	 i. Align the DWS to allow for DWS pump operation. Place a DWS pump in operation. Manually throttle a valve in the DWS pump flow path until the pump flow rate reaches the pump minimum flow setpoint. ii. Open the throttled valve. 	MCR displays and local, visual observation verifies the following: i. The pump minimum flow valve is open. ii. The pump minimum flow valve is closed.

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Table 14.2-14: Demineralized Water System Test # 14 (Continued)

viii. Verify each DWS instrument is	Initiate a single real or simulated	i.	The instrument signal is displayed	
monitored in the MCR and the RSS, if	instrument signal from each DWS		on an MCR workstation or recorded	
the signal is designed to be displayed	transmitter.		by the applicable control system	
in the RSS.			historian.	
(Test not required if the instrument		ii.	The instrument signal is displayed	
calibration verified the MCR and RSS			on an RSS workstation or recorded	
display.)			by the applicable control system	
			historian if the instrument signal is	
			designed to be displayed in the RSS.	
		iii.	The instrument signal is displayed	
			on an MCR module-specific safety	
			display instrument monitor or an	
			MCR common safety display	
			instrument monitor if the	
			instrument signal is designed to be	
			displayed on a safety display	
			instrument monitor.	
System Level Tests				
None				

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None

Table 14.2-15: Nitrogen Distribution System Test # 15

	eoperational test is required to be pe				
Th	The nitrogen distribution system (NDS) is described in Section 9.3.1 and the functions verified by this test are:				
Sy	stem Function	System Function Categorization	Function Verified by Test #		
fur	s no specific system function, all nctionality is supported through pported systems testing.	N/A	N/A		
Pr	erequisites		1		
ins	truments required to perform this test.	completed, with approved records and w	ithin all calibration due dates, for all		
	mponent Level Tests				
Te	st Objective	Test Method	Acceptance Criteria		
i.	Verify each NDS remotely-operated valve can be operated remotely.	Operate each valve from the MCR and local control panel (if design has local valve control)	MCR display and local, visual observation indicate each valve fully opens and fully closes.		
ii.	Verify each NDS air-operated valve fails to its safe position on loss of air.	Place each valve in its non-safe position. Isolate and vent air to the valve.	MCR display and local, visual observation indicate each valve fails to its safe position.		
iii.	Verify each NDS air-operated valve fails to its safe position on loss of electrical power to its solenoid.	Place each valve in its non-safe position. Isolate electrical power to each air- operated valve.	MCR display and local, visual observation indicate each valve fails to its safe position.		
iv.	Verify the NDS high pressure isolation valve closes to protect equipment.	Initiate a simulated signal for the following system conditions. i. High flow to high pressure header ii. High pressure on high pressure header	MCR display and local, visual observation indicate the nitrogen supply to the high pressure header valuis closed.		
v.	Verify a local grab sample can be obtained from a NDS grab sample device indicated on the NDS piping and instrumentation diagram.	Place the system in service to allow flow through the grab sampling device.	A local grab sample is successfully obtained.		
vi.	the signal is designed to be displayed in the RSS. (Test not required if the instrument	Initiate a single real or simulated instrument signal from each NDS transmitter.	 The instrument signal is displayed on an MCR workstation or recorded by the applicable control system historian. The instrument signal is displayed 		
	calibration verified the MCR and RSS display.)		on an RSS workstation or recorded by the applicable control system historian if the instrument signal is designed to be displayed in the RS		
			iii. The instrument signal is displayed on an MCR module-specific safety display instrument monitor or an MCR common safety display instrument monitor if the instrument signal is designed to be		
			displayed on a safety display instrument monitor.		

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Table 14.2-16: Service Air System Test # 16

The service air system (SAS) is describ	ed in Section 9.3.1 and the functions ver	ified by this test are:
System Function	System Function Categorization	Function Verified by Test #
Has no specific system function, all	N/A	N/A
functionality is supported through		
supported systems testing.		
Prerequisites	•	
Verify an instrument calibration has bee	n completed, with approved records and w	ithin all calibration due dates, for all
instruments required to perform this tes	t.	
Component Level Tests		
Test Objective	Test Method	Acceptance Criteria
 Verify each SAS remotely-operated valve can be operated remotely. 	Operate each valve from the MCR and local control panel (if design has local valve control)	MCR display and local, visual observation indicate each valve fully opens and fully closes.
 Verify each SAS air-operated valve fails to its safe position on loss of air. 	Place each valve in its non-safe position. Isolate and vent air to the valve.	MCR display and local, visual observation indicate each valve fails to its safe position.
 Verify each SAS air-operated valve fails to its safe position on loss of electrical power to its solenoid. 	Place each valve in its non-safe position. Isolate electrical power to each air- operated valve.	MCR display and local, visual observation indicate each valve fails to its safe position.
iv. Verify the instrument air to service ai isolation valve closes to protect equipment.	r Initiate a simulated signal for the following system conditions. i. IAS header low pressure ii. SAS high flow iii. SAS low pressure iv. SAS filter high differential pressure	MCR display and local, visual observation indicate the instrument air to service air isolation valve closes.
v. Verify each SAS instrument is monitored in the MCR and the RSS, i the signal is designed to be displayed in the RSS. (Test not required if the instrument calibration verified the MCR and RSS display)	transmitter.	 i. The instrument signal is displayed on an MCR workstation or recorded by the applicable control system historian. ii. The instrument signal is displayed on an RSS workstation or recorded by the applicable control system historian if the instrument signal is designed to be displayed in the RSS iii. The instrument signal is displayed on an MCR module-specific safety display instrument monitor or an MCR common safety display instrument monitor if the instrument signal is designed to be displayed on a safety display instrument monitor.

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Table 14.2-17: Instrument Air System Test # 17

The IAS is described in Section 9.3.1 and the functions verified by this test are:		
System Function	System Function Categorization	Function Verified by Test #
Has no specific system function, all	N/A	N/A
functionality is supported through		
supported systems testing.		

Prerequisites

Verify an instrument calibration has been completed, with approved records and within all calibration due dates, for all instruments required to perform this test. Verify performance testing of air compressor skids have been completed by the manufacturer or a site acceptance test has been completed in accordance with manufacturer instructions.

ma	manufacturer or a site acceptance test has been completed in accordance with manufacturer instructions.				
Co	Component Level Tests: First NPM				
Test Objective		Test Method	Acceptance Criteria		
i.	Verify each IAS remotely-operated valve can be operated remotely.	Operate each valve from the MCR and local control panel (if design has local valve control).	MCR display and local, visual observation indicate each valve fully opens and fully closes.		
ii.	Verify each IAS air-operated valve fails to its safe position on loss of air.	Place each valve in its non-safe position. Isolate and vent air to the valve.	MCR display and local, visual observation indicate each valve fails to its safe position.		
iii.	Verify each IAS air-operated valve fails to its safe position on loss of electrical power to its solenoid.	Place each valve in its non-safe position. Isolate electrical power to each air- operated valve.	MCR display and local, visual observation indicate each valve fails to its safe position.		
iv.	Verify the speed of each IAS variable- speed compressor can be manually controlled.	Align the system to provide a flow path to operate a selected compressor. Vary the compressor speed from minimum to maximum from the MCR.	MCR display indicate the speed of each compressor obtains both minimum and maximum pump speeds.		
v.	Verify each IAS standby compressor automatically starts to protect plant equipment.	I = -	MCR display and local, visual observation indicate the following standby compressor starts.		
vi.	Verify each IAS operating compressor automatically stops to protect the compressor.	Align the IAS to allow for compressor operation. Place a compressor in service. Initiate a simulated signal for the following system conditions. i. Pre-filter high differential pressure protection ii. Post-filter high differential pressure protection iii. High dew point protection	MCR display and local, visual observation indicate the operating compressor stops.		

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Table 14.2-17: Instrument Air System Test # 17 (Continued)

the signal is designed to be displayed	Initiate a single real or simulated instrument signal from each IAS transmitter.	i. The instrument signal is displayed on an MCR workstation or recorded by the applicable control system
in the RSS.		historian.
(Test not required if the instrument calibration verified the MCR and RSS display.)		ii. The instrument signal is displayed on an RSS workstation or recorded by the applicable control system historian if the instrument signal is designed to be displayed in the RSS.
		iii. The instrument signal is displayed on an MCR module-specific safety display instrument monitor or an
		MCR common safety display
		instrument monitor if the
		instrument signal is designed to be
		displayed on a safety display instrument monitor.
Component Level Tests: NPMs 2-12		instrument monitor.
Test Objective	Test Method	Acceptance Criteria
i. Verify each IAS remotely-operated	Operate each valve from the MCR and	MCR display and local, visual
valve can be operated remotely.	local control panel (if design has local valve control)	observation indicate each valve fully opens and fully closes.
ii. Verify each IAS air-operated valve	Place each valve in its non-safe position.	MCR display and local, visual
fails to its safe position on loss of air.	Isolate and vent air to the valve.	observation indicate each valve fails to its safe position.
iii. Verify each IAS air-operated valve	Place each valve in its non-safe position.	MCR display and local, visual
fails to its safe position on loss of	Isolate electrical power to each air-	observation indicate each valve fails to
electrical power to its solenoid.	operated valve.	its safe position.
System Level Tests		
None		

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Table 14.2-18: Control Room Habitability System Test # 18

	Preoperational test is required to be performed once.				
	The control room habitability system (CRHS) is described in Section 6.4 and the functions verified by this test are:				
	stem Function	System Function Categorization	Function Verified by Test #		
1.	The CRHS supports the Control	nonsafety-related	Test #18-1		
	Building (CRB) by providing clean		Test #18-2		
	breathing air to the control room				
	envelope (CRE) and maintaining a				
	positive control room pressure				
	during high radiation or loss of offsite				
	power conditions.				
2.	The CRHS supports the CRB by	nonsafety-related	Test #18-1		
	providing high pressure, clean		Test #18-2		
	breathing air in air bottles for use.				
3.	The CRVS supports the CRB by	nonsafety-related	Test #18-1		
	providing isolation of the CRE from				
	the surrounding areas and outside				
	environment via isolation dampers.				
4.	The plant protection system (PPS)	nonsafety-related	Test #18-1		
	supports the CRHS by providing				
	actuation and control signals.				
5.	The CRVS supports the CRB by	nonsafety-related	Test #18-1		
	providing isolation of the CRE from	-			
	the surrounding areas and outside				
	environment via isolation dampers.				
6.	The CRVS supports the PPS by	nonsafety-related	Test #18-1		
	providing instrument information	,			
	signals relating to isolation of the CRE				
	and activation of the CRH system.				
7.	The CRVS supports the CRB by	nonsafety-related	Test #18-1		
	isolating the CRVS outside air intake				
	when radiation is detected				
	downstream of the charcoal filtration				
	unit.				

Prerequisites

- i. Verify an instrument calibration has been completed, with approved records and within all calibration due dates, for all
 instruments required to perform this test.
- ii. Verify a CRHS air balance has been performed and the CRHS air balance records have been approved. [This prerequisite is not required for component-level tests.]
- iii. Verify CRHS air bottlers are pressurized to their design working pressure. [This prerequisite is not required for component-level tests.]

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Table 14.2-18: Control Room Habitability System Test # 18 (Continued)

Component Level Tests		
	Test Method	Acceptance Criteria
i. Verify each CRHS remotely-operated valve can be operated remotely.	Place the CRHS air bottles in service. Place CRVS in service to supply air to the CRE. Operate each valve from the MCR.	i. MCR workstation display, safety display instrument display and local, visual observation indicate each valve fully opens and fully closes under preoperational temperature, differential pressure, and flow conditions. [ITAAC 03.01.02]
valve fails to its safe position on loss of electrical power to its solenoid.	Place the CRHS air bottles in service. Place CRVS in service to supply air to the CRE. i. Place each valve in its non-safe position. Isolate electrical power to its solenoid.	i. MCR display, safety display instrument display and local, visual observation indicate each valve fails open under preoperational temperature, differential pressure, and flow conditions. [ITAAC 03.01.03]
monitored in the MCR and the RSS, if	Initiate a single real or simulated instrument signal from each CRHS transmitter.	 i. The instrument signal is displayed on an MCR workstation or recorded by the applicable control system historian. ii. The instrument signal is displayed on an RSS workstation or recorded by the applicable control system historian if the instrument signal is designed to be displayed in the RSS. iii. The instrument signal is displayed on an MCR module-specific safety display instrument monitor or an MCR common safety display instrument monitor if the instrument signal is designed to be displayed on a safety display instrument monitor.
System Level Test #18-1	L	
·	Test Method	Acceptance Criteria
Verify the CRHS and the CRVS automatically respond to provide breathable air to the CRE under accident conditions.	Place the CRVS in automatic operation. Place the CRHS air bottles in service. Place CRVS in service to supply air to the CRE. Initiate each of the following real or simulated CRHS actuation signals: High radiation signal downstream of the CRVS filter unit Loss of AC power.	MCR workstation display and local, visual observation indicate the following: i. The CRVS outside air damper closes. ii. The CRVS filter unit fan stops. iii. The CRVS control room envelope isolation dampers close. iv. The CRHS air supply isolation valves open. v. CRHS pressure relief isolation valves open. vi. CRVS air handling unit stops. vii. CRE general exhaust fan stops. viii. CRVS battery room exhaust fan stops. [ITAAC 03.09.02] (items i through v)

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Table 14.2-18: Control Room Habitability System Test # 18 (Continued)

System Level Test #18-2			
Test Objective	Test Method	Acceptance Criteria	
have sufficient volume to provide 72 hours of breathable air through both the main and backup supply flow path to the CRE described in Section 6.4.2.1.	 i. Align air bottles for testing. Assume 25% of the bottles are unavailable and use 1/6 of the remaining bottles to simulate a test conduct of 72 hours (12 hours/72 hours). Initiate a real or simulated CRHS actuation signal to isolate the CRE. Conduct a CRE test for 12 hours. ii. At the end of 12 hours isolate the main supply flow path and align the manual backup flow path to the CRE. Align air bottles for testing. Assume 25% of the bottles are unavailable and use the remaining bottles. 	 i. a. The CRE described in Section 6.4.2.1 maintains a positive pressure relative to the adjacent areas as specified in Table 6.4-1 as indicated by the CRE differential pressure transmitters. [ITAAC 03.01.05] b. The CRHS minimum flow rate for the main flow path is maintained as specified in Table 6.4-1 for the duration of the test. c. The CRHS flow rate for the manual backup flow path is maintained as specified in Table 6.4-1. 	
System Level Test #18-3			
Test Objective	Test Method	Acceptance Criteria	
The air exfiltration from the CRE does not			
exceed the air exfiltration flow rate	at 1/8 in. wg. of positive pressure with	does not exceed the unfiltered	
identified in the CRHS exfiltration/	respect to surrounding areas by	inleakage flow rate identified in Table	
infiltration analysis.	performing tracer gas testing in accordance with ASTM E741.	6.4-1. [ITAAC 03.01.01]	

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Table 14.2-19: Normal Control Room HVAC System Test # 19

The	Preoperational test is required to be performed once. The CRVS is described in Sections 6.4.3.2, 9.4.1, and 11.5.2.2.1, and the functions verified by this test are:				
	stem Function	System Function Categorization	Function Verified by Test #		
-	The CRVS supports the CRB by	nonsafety-related	Test #19-1		
	providing cooling, heating and	,	Test #19-2		
	humidity control to maintain a				
	suitable environment for the safety				
	and comfort of plant personnel.				
2.	The CRVS supports the systems	nonsafety-related	Test #19-1		
	located in the CRB by providing	_	Test #19-2		
	cooling, heating and humidity				
	control to maintain a suitable				
	environment for the operation of				
	system components.				
<u> </u>	The CRVS supports the CRB by	nonsafety-related	Test #19-1		
	maintaining the CRB at a positive		1 22		
	pressure with respect to adjacent				
	areas during normal operation.				
4	The CRVS supports the CRB by	nonsafety-related	Test #19-3		
••	maintaining the CRB at a positive	inonsarcty related			
	ambient pressure relative to the				
	Reactor Building (RXB) and the				
	outside atmosphere to control the				
	ingress of potentially airborne				
	radioactivity from the RXB or the				
	outside atmosphere to the CRB.				
5	The PPS supports the CRVS by	nonsafety-related	Test #19-3		
	providing actuation and control				
	signals to the outside air isolation				
	dampers.				
<u> </u>	The CRVS supports the CRB by	nonsafety-related	Test #19-4		
٠.	protecting personnel from exposure				
	to radiation during a design basis				
	accident, when power is available, by				
	removing radioactive contamination				
	from outside air via charcoal				
	filtration, as required by radiation				
	dose analyses.				
Γh	e CRVS functions verified by other te	sts are:	1		
	-	nonsafety-related	Test #18-1		
	CRVS outside air intake when		330		
	liation is detected downstream of the				
	arcoal filtration unit.				
	CRVS supports the CRB by providing	nonsafety-related	Test #18-1		
	lation of the CRE from the surrounding	inonsarcty related	1.550 110 1		
	as and outside environment via				
	lation dampers.				
	CRVS supports the PPS by providing	nonsafety-related	Test #18-1		
Ih4	- city o supports the FF oby providing	inormaticity related	1030 110 1		
ins	trument information signals relating solation of the CRE and activation of				

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Table 14.2-19: Normal Control Room HVAC System Test # 19 (Continued)

Prerequisites

- i. Verify an instrument calibration has been completed, with approved records and within all calibration due dates, for all instruments required to perform this test.
- ii. Verify a CRVS air balance has been performed and the CRVS air balance records have been approved. [This prerequisite is not required for component-level tests.]
- iii. Verify CRVS high-efficiency particulate air (HEPA) and charcoal adsorbers have been installed and tested and the test records have been approved. [This prerequisite is not required for component-level tests.]
- iv. Verify CRVS control room isolation dampers have been leak tested and the test records have been approved. [This prerequisite is not required for component-level tests.]

_	prerequisite is not required for component-level tests.] Component Level Tests			
Te	st Objective	Test Method	Acceptance Criteria	
i.	Verify each CRVS remotely-operated damper can be operated remotely.	Operate each damper from the MCR and local control panel (if design has local damper control).	MCR display and local, visual observation indicate each damper fully opens and fully closes.	
	Verify each CRVS air-operated damper fails to its safe position on loss of air. Verify each CRVS air-operated damper fails to its safe position on loss of electrical power to its solenoid.	Place each damper in its non-safe position. Isolate and vent air to the damper. Place each damper in its non-safe position. Isolate electrical power to its solenoid.	MCR display and local, visual observation indicate each damper fails to its safe position. MCR display and local, visual observation indicate each damper fails to its safe position.	
	Verify CRVS dampers automatically close on associated smoke or fire signals.	Open each damper actuated by a smoke or fire signal. Initiate an alarm signal for each damper.	MCR display and local, visual observation indicate each damper closes.	
	Verify each required CRVS fan stops on actuation of its associated fire or smoke alarm.	Initiate an alarm signal for each fan.	MCR display and local, visual observation indicate each fan stops.	
	Verify each CRVS pressurization fan starts automatically on the actuation of its associated fire or smoke alarm.	Initiate an alarm signal for each fan.	MCR display and local, visual observation indicate each pressurization fan starts.	
	Verify the fan speed of each CRVS variable-speed fan can be manually controlled.	Vary the speed of each fan from the MCR and local control panel (if design has local fan control).	MCR display indicates the speed of each fan varies from minimum to maximum speed.	
viii	. Verify the standby CRVS main supply air handling unit (AHU) starts automatically on the stop of the operating CRVS main supply AHU.	Place an AHU in service. Place the standby AHU in automatic control. Stop the operating AHU.	MCR display and local, visual observation indicate the standby AHU starts.	
ix.		Place an FCU in service. Place the standby FCU in automatic control. Stop the operating FCU.	MCR display and local, visual observation indicate the standby FCU starts.	
	safe position on loss of air.	Place each damper in its non-safe position. Isolate and vent air to the damper.	Each CRVS control room envelope isolation damper fails to its closed position on loss of air under preoperational temperature, differential pressure, and flow conditions while the CRV system is supplying flow to the CRE. [ITAAC 03.02.01]	
xi.	Verify each CRVS control room envelope isolation damper fails to its safe position on loss of electrical power to its solenoid.	Place each damper in its non-safe position. Isolate electrical power to its solenoid.	Each CRVS control room envelope isolation damper fails to its closed position on loss of electrical power under preoperational temperature, differential pressure, and flow conditions while the CRVS is supplying flow to the CRE. [ITAAC 03.02.01]	

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Table 14.2-19: Normal Control Room HVAC System Test # 19 (Continued)

monitored in the MCR and the RSS, if the signal is designed to be displayed in the RSS. (Test not required if the instrument calibration verified the MCR and RSS display) Test Method			
the signal is designed to be displayed in the RSS. (Test not required if the instrument calibration verified the MCR and RSS display) The instrument signal is displayed on an RSS workstation or recorded by the applicable control system historian. The instrument signal is designed to be displayed on an RSS workstation or recorded by the applicable control system historian if the instrument signal is designed to be displayed on an MCR mordule-specific safety display instrument monitor or an MCR common safety display instrument monitor. Test Objective Verify CRB design temperatures and humidity conditions during normal operation. Verify The CRVS maintains a positive pressure in the CRB pressure relative the outside environment while the CRVS is operating in normal alignment. Verify the CRVS maintains the air flow to the battery rooms to maintain hydrogen concentration to less than 19% by volume. Test Objective Test Objective Verify CRB design temperatures and humidity conditions of the CRP pressure relative to the outside environment while the CRVS in automatic operation. The temperature and humidity monitored by the MCR are maintained at design temperature and humidity conditions while concentration to less than 19% by volume. Test Objective Test Objective Test Method Test Method Acceptance Criteria The temperature and humidity of rooms and areas monitored by the MCR are maintained at design temperature and humidity conditions while cooling to the CRV main supply AHU. Blace the CRVS in automatic operation. In the temperature and humidity of rooms and areas monitored by the MCR astrument and humidity conditions while cooling to the CRV main supply AHU. Blace the CRVS in automatic operation. In the temperature and humidity of rooms and areas monitored by the MCR astrument and humidity conditions	xii. Verify each CRVS instrument is	Initiate a single real or simulated	, ,
in the RSS. (Test not required if the instrument calibration verified the MCR and RSS display) In the control system calibration verified the MCR and RSS display) In the instrument signal is displayed on an RSS workstation or recorded by the applicable control system historian if the instrument signal is designed to be displayed in the RSS. Iii. The instrument signal is designed to be displayed in the RSS. Iii. The instrument signal is designed to be displayed in the RSS. Iii. The instrument signal is designed to be displayed on a safety display instrument monitor or a MCR common safety display instrument monitor. In the instrument signal is designed to be displayed on a safety display instrument monitor. In the instrument signal is designed to be displayed on a safety display instrument monitor. In the instrument monitor. In the instrument signal is designed to be displayed on a safety display instrument monitor. In the instrument signal is designed to be displayed on a safety display instrument monitor. In the instrument signal is designed to be displayed on a safety display instrument monitor. In the instrument signal is designed to be displayed on a safety display instrument monitor. In the instrument signal is designed to be displayed on a safety display instrument monitor. In the instrument signal is designed to be displayed on a safety display instrument monitor. In the instrument signal is designed to be displayed on a safety display instrument monitor. In the instrument monitor and MCR common safety display instrument monitor. In the instrument monitor and MCR common safety display instrument monitor. In the temperature and humidity of rooms and areas monitored by the MCR satisfy the design temperature and humidity monitored by the MCR satisfy the design temperature and humidity monitored by the MCR satisfy the design temperature and humidity monitored by the MCR satisfy the design temperature and humidity monitored by the MCR satisfy the design temperature and humidity monitored by t		_	
(Test not required if the instrument calibration verified the MCR and RSS display) Iii. The instrument signal is displayed on an RSS workstation or recorded by the applicable control system historian if the instrument signal is designed to be displayed on an MCR module-specific safed by the applicable control system historian if the instrument signal is designed to be displayed on an MCR module-specific safed displayed on an MCR common safety display instrument monitor or an MCR common safety display instrument monitor or an MCR common safety display instrument monitor of the instrument signal is designed to be displayed on an MCR common safety display instrument monitor or an MCR commo		transmitter.	
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and humidity conditions while cooling to the CRV main supply AHU is supplied by the CHWS standby chiller. System Level Test #19-3 Test Objective Verify the CRVS isolates makeup air when smoke or toxic gas is detected in the makeup air ductwork. Test Method Place the CRVS in automatic operation. i. Initiate a real or simulated high radiation signal for the makeup air ductwork upstream of the CRVS filter requirements contained in Table 9.4.1-2. Contained in Table 9.4.1-2. Outside air damper is closed to isolate makeup air.		1 1 1	
cooling to the CRV main supply AHU is supplied by the CHWS standby chiller. System Level Test #19-3 Test Objective Verify the CRVS isolates makeup air when smoke or toxic gas is detected in the makeup air ductwork. Initiate a real or simulated high radiation signal for the makeup air ductwork upstream of the CRVS filter Test Method Place the CRVS in automatic operation. i. Initiate a real or simulated high makeup air ductwork upstream of the CRVS filter		indee the city's in automatic operation.	requirements contained in Table 9.4.1-2.
is supplied by the CHWS standby chiller. System Level Test #19-3 Test Objective Verify the CRVS isolates makeup air when smoke or toxic gas is detected in the makeup air ductwork. Initiate a real or simulated high radiation signal for the makeup air ductwork upstream of the CRVS filter Test Method Place the CRVS in automatic operation. i. Initiate a real or simulated high makeup air. ductwork upstream of the CRVS filter			
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Test Objective Verify the CRVS isolates makeup air when smoke or toxic gas is detected in the makeup air ductwork. Test Method Place the CRVS in automatic operation. i. Initiate a real or simulated high radiation signal for the makeup air ductwork upstream of the CRVS filter Acceptance Criteria Outside air damper is closed to isolate makeup air.			
Verify the CRVS isolates makeup air when smoke or toxic gas is detected in the makeup air ductwork. Place the CRVS in automatic operation. i. Initiate a real or simulated high radiation signal for the makeup air ductwork upstream of the CRVS filter	System Level Test #19-3		
i. Initiate a real or simulated high makeup air. makeup air ductwork. i. Initiate a real or simulated high radiation signal for the makeup air ductwork upstream of the CRVS filter	Test Objective		_
radiation signal for the makeup air ductwork upstream of the CRVS filter		-	
ductwork upstream of the CRVS filter			makeup air.
·	makeup air ductwork.		
unit.		-	
		unit.	

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Table 14.2-19: Normal Control Room HVAC System Test # 19 (Continued)

ystem Level Test #19-4		
Test Objective	Test Method	Acceptance Criteria
to mitigate the consequences of high radiation in the outside air.		 i. Outside air is diverted through the CRVS filter unit by closing the CRVS filter unit bypass dampers and opening the CRVS filter unit isolation dampers. ii. The CRVS filter unit fan starts. [ITAAC 03.09.01] (items i. and ii.)

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Table 14.2-20: Reactor Building HVAC System Test # 20

Preoperational test is required to be performed once.		
The RBVS is described in Section 9.4.2	and the functions verified by this test	are:
System Function	System Function Categorization	Function Verified by Test #
I. The RBVS supports the RXB by providing cooling, heating and humidity control to maintain a suitable environment for the safety and comfort of plant personnel.	nonsafety-related	Test #20-1 Test #20-2
2. The RBVS supports the systems located in the RXB by providing cooling, heating and humidity control to maintain a suitable environment for the operation of system components.	nonsafety-related	Test #20-1 Test #20-2
3. The RBVS supports the RXB by maintaining the RXB at a negative ambient pressure relative to the outside atmosphere to control the movement of potentially airborne radioactivity from the RXB to the environment.	nonsafety-related	Test #20-1 Test #20-3

Prerequisites

- i. Verify an instrument calibration has been completed, with approved records and within all calibration due dates, for all instruments required to perform this test.
- ii. Verify an RBVS air balance has been performed and the RBV system air balance records have been approved. [This prerequisite is not required for component-level tests.]
- iii. RBVS high-efficiency particulate air and charcoal adsorbers have been installed and tested. [This prerequisite is not required for component-level tests.]

	required for component-level tests.]			
Co	Component Level Tests			
Tes	st Objective	Test Method	Acceptance Criteria	
i.	Verify each RBVS remotely-operated damper can be operated remotely.	Operate each damper from the MCR and local control panel (if design has local damper control).	MCR display and local, visual observation indicate each damper fully opens and fully closes.	
ii.	Verify each RBVS air-operated damper fails to its safe position on loss of air.	Place each damper in its non-safe position. Isolate and vent air to the damper.	MCR display and local, visual observation indicate each damper fails to its safe position.	
iii.	Verify each RBVS air-operated damper fails to its safe position on loss of electrical power to its solenoid.	Place each damper in its non-safe position. Isolate electrical power to its solenoid.	MCR display and local, visual observation indicate each damper fails to its safe position.	
iv.	Verify RBVS dampers automatically close on associated smoke or fire signals.	Open each damper actuated by a smoke or fire signal. Initiate an alarm signal for each damper.	MCR display and local, visual observation indicate each damper closes.	
V.	Verify each required RBVS fan stops on actuation of its associated fire or smoke alarm.	Initiate an alarm signal for each fan.	MCR display and local, visual observation indicate each fan stops.	
vi.	Verify each RBVS pressurization fan starts automatically on the actuation of its associated fire or smoke alarm.	Initiate an alarm signal for each fan.	MCR display and local, visual observation indicate each RWBVS pressurization fan starts.	
vii.	Verify the fan speed of each RBVS variable-speed fan can be manually controlled.	Vary the speed of each fan from the MCR and local control panel (if design has local fan control).	MCR display indicates the speed of each fan varies from minimum to maximum speed.	

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Table 14.2-20: Reactor Building HVAC System Test # 20 (Continued)

viii	. Verify each standby RBVS air	Place an AHU in service. Place the	MCR display and local, visual
	handling unit starts automatically on	standby AHU in automatic control. Stop	observation indicate the standby AHU
	the stop of the operating RBVS air	the operating AHU.	starts.
	handling unit.		
ix.	Verify each standby RBVS fan coil unit	Place an FCU in service. Place the standby	MCR display and local, visual
	starts automatically on the stop of	FCU in automatic control. Stop the	observation indicate the standby FCU
	the operating RBVS fan coil unit.	operating FCU.	starts.
x.	Verify each RBV system instrument is monitored in the MCR and the RSS, if the signal is designed to be displayed in the RSS.	_	 The instrument signal is displayed on an MCR workstation or recorded by the applicable control system historian.
	(Test not required if the instrument calibration verified the MCR and RSS display)		 The instrument signal is displayed on an RSS workstation or recorded by the applicable control system historian if the instrument signal is designed to be displayed in the RSS.
			iii. The instrument signal is displayed on an MCR module-specific safety display instrument monitor or an MCR common safety display instrument monitor if the instrument signal is designed to be displayed on a safety display instrument monitor.
xi.	Verify each RBVS remotely-operated	Operate each damper from the MCR and	MCR display and local, visual
	damper can be operated remotely.	local control panel (if design has local	observation indicate each damper fully
		damper control)	opens and fully closes.

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Table 14.2-20: Reactor Building HVAC System Test # 20 (Continued)

Sy	stem Level Test #20-1		
Te	st Objective	Test Method	Acceptance Criteria
i. ii.	Verify RXB design temperatures and humidity monitored by the MCR are maintained at design temperature and humidity conditions during normal operation.	Place the RBVS supply, general area exhaust and spent fuel pool exhaust in automatic operation. Place the RWBVS in automatic operation. i. Record the RXB temperatures and humidity indications monitored by the MCR. ii. Measure the RXB pressure relative the outside environment. iii. Measure the RWB pressure relative the outside environment. iv. Measure the air flow rate to the battery rooms.	 i. The temperature and humidity of rooms and areas monitored by the MCR satisfy the design temperature and humidity requirements contained in Table 9.4.2-2. ii. MCR display indicates the RBVS maintains a negative pressure in the RXB relative to the outside environment while operating in the normal operating alignment. [ITAAC 03.03.01] iii. MCR display indicates the RBVS maintains a negative pressure in the RWB relative to the outside environment while operating in the normal operating alignment. [ITAAC 03.03.02] iiii. Measured flow to the battery rooms is equal to or greater than the flow specified by the air flow balance.
			[ITAAC 03.03.03]
Sy	stem Level Test #20-2	1	1
Te	st Objective	Test Method	Acceptance Criteria
i.	Verify design temperatures of the following rooms can be controlled using AHUs with installed direct expansion coils. a. RSS b. module protection system (MPS) equipment rooms c. battery rooms d. battery charger rooms	Place the RBVS air handling units with installed direct expansion coils in automatic operation.	i. The temperature and humidity of rooms and areas monitored by the MCR satisfy the design temperature and humidity requirements contained in Table 9.4.2-2.

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Table 14.2-20: Reactor Building HVAC System Test # 20 (Continued)

System Level Test #20-3		
Test Objective	Test Method	Acceptance Criteria
 i. Verify RBVS automatic alignment on a simulated spent fuel pool hi-hi radiation level. ii. Verify The RBVS maintains a negative pressure in the RXB relative to the outside environment while the RBVS is operating in accident alignment. iii. Verify The RWBVS maintains a negative pressure in the RWB relative to the outside environment while the RBVS is operating in accident alignment. 	Place the RBVS supply in automatic operation. Place the RWBVS supply system in automatic operation. Simulate a Hi-Hi radiation signal in the	 i. The RBVS general area exhaust isolation damper for the spent fuel pool and dry dock area is closed to isolate the spent fuel pool area exhaust flow from the RBVS general exhaust. ii. The RBVS diverts spent fuel pool exhaust flow to charcoal adsorbers and additional HEPAs in the spent fuel pool charcoal filter units. iii. Flow from the RBVS supply fans is reduced to maintain the design negative pressure in the RXB and RWB relative to the outside environment while the RBVS is operating in the off- normal alignment. [ITAAC 03.09.03] (items i thru iii)

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Table 14.2-21: Radioactive Waste Building HVAC System Test # 21

Preoperational test is required to be performed once.				
System Function	The RWBVS is described in Section 9.4.3 and the functions verified by this test are: System Function Function Verified by Test #			
 The RWBVS supports the RWB by providing cooling, heating and humidity control to maintain a suitable environment for the safety and comfort of plant personnel. 	nonsafety-related	Test #21-1		
 The RWBVS supports the systems located in the RWB by providing cooling, heating and humidity control to maintain a suitable environment for the operation of system components. 	nonsafety-related	Test #21-1		
 The RWBVS supports the RWB by maintaining the RWB at a negative ambient pressure relative to the outside atmosphere to control the movement of potentially airborne radioactivity from the RWB to the environment. 	nonsafety-related	Test #21-1 (normal RBVS exhaust alignment) Test #20-3 (off-normal RBVS exhaust alignment)		

Prerequisites

- i. Verify an instrument calibration has been completed, with approved records and within all calibration due dates, for all instruments required to perform this test.
- ii. Verify an RWBVS air balance has been performed and the RWBVS air balance records have been approved. [This prerequisite is not required for component-level tests.]

Component Level Tests

Tes	t Objective	Test Method	Acceptance Criteria
i.	Verify each RWBVS remotely- operated damper can be operated remotely.	Operate each damper from the MCR and local control panel (if design has local damper control).	MCR display and local, visual observation indicate each damper fully opens and fully closes.
ii.	. '	Place each damper in its non-safe position. Isolate and vent air to the damper.	MCR display and local, visual observation indicate each damper fails to its safe position.
iii.		Place each damper in its non-safe position. Isolate electrical power to its solenoid.	MCR display and local, visual observation indicate each damper fails to its safe position.
iv.	Verify RWBVS dampers automatically close on associated smoke or fire signals.	Open each damper actuated by a smoke or fire signal. Initiate an alarm signal for each damper.	MCR display and local, visual observation indicate each damper closes.
v.	Verify each required RWBVS fan stops on actuation of its associated fire or smoke alarm.	Initiate an alarm signal for each fan.	MCR display and local, visual observation indicate each fan stops.
vi.	Verify each RWBVS pressurization fan starts automatically on the actuation of its associated fire or smoke alarm.	Initiate an alarm signal for each fan.	MCR display and local, visual observation indicate each pressurization fan starts.
vii.	Verify the fan speed of each RWBVS variable-speed fan can be manually controlled.	Vary the speed of each fan from the MCR and local control panel (if design has local fan control).	MCR display indicates the speed of each fan varies from minimum to maximum speed.

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Table 14.2-21: Radioactive Waste Building HVAC System Test # 21 (Continued)

	A C C C C C C C C C C C C C C C C C C C	DI ALIII: : DI (!	MCD II II I I I
VIII	,	Place an AHU in service. Place the	MCR display and local, visual
	supply AHU starts automatically on	standby AHU in automatic control. Stop	observation indicate the standby AHU
	the stop of the operating RWBVS	the operating recirculation AHU.	starts.
	main supply AHU.		
ix.	Verify each standby RWBVS FCU		MCR display and local, visual
	starts automatically on the stop of	FCU in automatic control. Stop the	observation indicate the standby FCU
	the operating RWBVS fan coil unit.	operating FCU.	starts.
x.	Verify each RWBVS instrument is	Initiate a single real or simulated	i. The instrument signal is displayed
		instrument signal from each RWBVS	on an MCR workstation or recorded
	the signal is designed to be displayed	transmitter.	by the applicable control system
	in the RSS.		historian.
	(Test not required if the instrument		ii. The instrument signal is displayed
	calibration verified the MCR and RSS		on an RSS workstation or recorded
	display)		by the applicable control system
			historian if the instrument signal is
			designed to be displayed in the RSS.
			iii. The instrument signal is displayed
			on an MCR module-specific SDIS
			monitor or an MCR common SDIS
			monitor if the instrument signal is
			designed to be displayed on a SDIS
			monitor.
Sys	tem Level Test #21-1		
Tes	t Objective	Test Method	Acceptance Criteria
i.	Verify the RWB design temperatures	Place the RWBVS in automatic operation.	i. The temperature and humidity of
	and humidity monitored by the MCR	Place the RXB ventilation system in	rooms and areas monitored by the
	are maintained at design	automatic operation.	MCR satisfy the design temperature
	temperature and humidity		and humidity requirements
	conditions during normal operation.		contained in Table 9.4.1-2.
ii.	Verify the RWBVS maintains a		ii. MCR display indicates the RWBVS
	negative pressure in the RWB relative		maintains a negative pressure in the
	to the outside environment while the		RWB relative to the outside
	RWBVS is operating in normal		environment while operating in the
	alignment.		normal operating alignment.
Ц	<u> </u>	<u>l</u>	

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Table 14.2-22: Turbine Building Ventilation Test # 22

Pre	Preoperational test is required to be performed once.		
The Turbine Building HVAC system (TBVS) is described in Section 9.4.4 and the function verified by this test is:			
_	stem Function		Function Verified by Test #
the pro	e TBVS supports the systems located in Turbine Generator Building (TGB) by oviding cooling, heating and humidity ntrol to maintain a suitable	non-safety related	Test #22-1
en coi	vironment for the operation of system mponents.		
Ve ins	erequisites rify an instrument calibration has been truments required to perform this test. mponent Level Tests	completed, with approved records and wi	thin all calibration due dates, for all
	st Objective	Test Method	Acceptance Criteria
i.	Verify each TBVS remotely-operated damper can be operated remotely.	Operate each damper from the MCR and local control panel (if design has local damper control).	MCR display and local, visual observation indicate each damper fully opens and fully closes.
	Verify TBVS dampers automatically close on associated smoke or fire signals.	or fire signal. Initiate an alarm signal for each damper.	MCR display and local, visual observation indicate each damper closes.
iii.	Verify each required TBVS fan stops on actuation of its associated fire or smoke alarm.	Initiate an alarm signal for each fan.	MCR display and local, visual observation indicate each fan stops.
iv.	Verify the fan speed of each TBVS variable-speed fan can be manually controlled.	Vary the speed of each fan from the MCR and local control panel (if design has local fan control).	MCR display indicates the speed of each fan varies from minimum to maximum speed.
v.		Initiate a single real or simulated instrument signal from each TBVS transmitter.	 i. The instrument signal is displayed on an MCR workstation or recorded by the applicable control system historian. ii. The instrument signal is displayed on an RSS workstation or recorded by the applicable control system historian if the instrument signal is designed to be displayed in the RSS. iii. The instrument signal is displayed on an MCR module-specific safety display instrument monitor or an MCR common safety display instrument monitor if the instrument signal is designed to be displayed on a safety display instrument monitor.

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Table 14.2-22: Turbine Building Ventilation Test # 22 (Continued)

system (BPDS) instrument is	Initiate a single real or simulated instrument signal from each BPDS transmitter.	 i. The instrument signal is displayed on an MCR workstation or recorded by the applicable control system historian. ii. The instrument signal is displayed on an RSS workstation or recorded by the applicable control system historian if the instrument signal is designed to be displayed in the RSS. iii. The instrument signal is displayed on an MCR module-specific safety display instrument monitor or an MCR common safety display instrument monitor if the instrument signal is designed to be displayed on a safety display instrument monitor.
System Level Test #22-1		
Test Objective	Test Method	Acceptance Criteria
battery charger room design	Place the turbine bypass system battery and battery charger room ventilation units in automatic operation.	The temperature and humidity of Turbine Building battery and battery charger rooms satisfy the temperature and humidity requirements.

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Table 14.2-23: Radioactive Waste Drain System Test # 23

Preoperational test is required to be performed once.				
The RWDS is described in Section 9.3.3 and the functions verified by this test are:				
Sy	stem Function	System Function Categorization	Function Verified by Test #	
1.	The RWDS supports the RWB by collecting radioactive waste in drain sumps and tanks and transfers it to the LRWS for processing.	nonsafety-related	Test #23-1	
2.	The RWDS supports the RXB by collecting radioactive waste in drain sumps and tanks and transfers it to the LRWS for processing.	nonsafety-related	Test #23-1	
	The RWDS supports the ANB by collecting radioactive waste in drain sumps and tanks and transfers it to the LRWS for processing.	nonsafety-related	Test #23-1	
4.	The RWDS supports the UHS by providing detection and monitoring of leakage through the UHS liner and the dry dock liner.	nonsafety-related	Test #23-2	
5.	The LRWS supports the RWDS by receiving and processing the effluent from the RWB radioactive waste drain sumps.	nonsafety-related	Test #23-1	
6.	The LRWS supports the RWDS by receiving and processing the effluent from the RXB radioactive waste drain sumps.	nonsafety-related	Test #23-1	
	The LRWS supports the RWDS by receiving and processing the effluent from the ANB radioactive waste drain sumps.	nonsafety-related	Test #23-1	

Prerequisites

Verify an instrument calibration has been completed, with approved records and within all calibration due dates, for all instruments required to perform this test.

Component Level Tests

Te	st Objective	Test Method	Acceptance Criteria
i.	valve can be operated remotely.	Operate each valve from the MCR and local control panel (if design has local valve control).	MCR display and local, visual observation indicate each valve fully opens and fully closes.
ii.		Place each valve in its non-safe position. Isolate and vent air to the valve.	MCR display and local, visual observation indicate each valve fails to its safe position.
iii.	Verify each RWDS air-operated valve fails to its safe position on loss of electrical power to its solenoid.	Place each valve in its non-safe position. Isolate electrical power to each air- operated valve.	MCR display and local, visual observation indicate each valve fails to its safe position.
iv.	Verify each RWDS pump can be started and stopped remotely.	Align the RWDS to allow for pump operation. Stop and start each pump from the MCR.	MCR display and local, visual observation indicate each pump starts and stops.
v.	, .	Place the system in service to allow flow through the grab sampling device.	A local grab sample is successfully obtained.

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Table 14.2-23: Radioactive Waste Drain System Test # 23 (Continued)

vi. Verify each RWDS instrument is monitored in the MCR and the RSS, if the signal is designed to be displayed in the RSS. (Test not required if the instrument calibration verified the MCR and RSS display).	Initiate a single real or simulated instrument signal from each RWDS transmitter.	 i. The instrument signal is displayed on an MCR workstation or recorded by the applicable control system historian. ii. The instrument signal is displayed on an RSS workstation or recorded by the applicable control system historian if the instrument signal is designed to be displayed in the RSS. iii. The instrument signal is displayed on an MCR module-specific safety display instrument monitor or an MCR common safety display instrument monitor if the instrument signal is designed to be displayed on a safety display instrument monitor.
System Level Test #23-1	<u> </u>	matument monitor.
Test Objective	Test Method	Acceptance Criteria
Verify RWDS pumps start and stop automatically and transfer liquid waste to its design location.	Align each RWDS sump or tank to allow water in a selected sump or tank to be pumped to its design location in the LRWS (as indicated by the RWDS piping and instrumentation diagrams). i. Fill the selected sump or tank until a HI water level is obtained to start the first (primary) pump. ii. Continue filling the sump or tank until a HI-HI level starts the second (alternate) pump. iii. Stop filling the sump or tank to allow the primary and alternate pumps to stop on low level. iv. Refill the sump or tank until the alternate pump starts on HI level.	 MCR displays and local, visual observation verifies the following: i. The first pump starts on HI level and transfers water to its design location in the LRWS. ii. The second (alternate) pump starts on HI-HI level. iii. Both primary and alternate pumps stop on LO level. iv. The alternate pump starts on HI level.
System Level Test #23-2		
Test Objective Verify each RWDS equipment drain sump	Test Method Fill the selected sump at a rate that	Acceptance Criteria PCS data indicates the sump fill rate
	exceeds the PLDS leakage rate setpoint.	alarmed at the PLDS leakage rate setpoint.

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Table 14.2-24: Balance-of-Plant Drains Test # 24

Table 14.2-24: Balance-of-Plant Drains Test # 24					
Preoperational test is required to be performed to support sequence of construction turnover of the BPD system. BPD system is described in Section 9.3.3 and 11.5.2.2.15 and the functions verified by this test are:					
System Function	,				
1. The BPDS supports the condensate polisher demineralizers, the three cooling tower chemical addition systems, and the DWS reverse osmosis units by providing a means to collect and transfer chemical wastes to either the LRWS or to the UWS.	nonsafety-related	Test #24-1			
 The BPDS supports the two TGBs, the two diesel generators, the auxiliary boiler, the combustion turbine, the Central Utility Building, and the diesel driven firewater pump by providing a means to collect, treat, and transfer the waste water to the either the LRWS or to the UWS. 	nonsafety-related	Test #24-1			
 The BPDS supports the CRB floor drains by providing a means to collect, treat, and transfer the waste water to the UWS. 	nonsafety-related	Test #24-1			
Prerequisites		-			
	completed, with approved records and w	ithin all calibration due dates, for all			
instruments required to perform this test					
Component Level Tests	T				
Test Objective	Test Method	Acceptance Criteria			
i. Verify each BPDS remotely-operated valve can be operated remotely.	Operate each valve from the MCR and local control panel (if design has local valve control).	MCR display and local, visual observation indicate each valve fully opens and fully closes.			
ii. Verify each BPDS air-operated valve fails to its safe position on loss of air.	Place each valve in its non-safe position. Isolate and vent air to the valve.	MCR display and local, visual observation indicate each valve fails to its safe position.			
iii. Verify each BPDS air-operated valve	Place each valve in its non-safe position.	MCR display and local, visual			

1.6	or opjective	i est Method	Acceptance criteria
i.	Verify each BPDS remotely-operated valve can be operated remotely.	Operate each valve from the MCR and local control panel (if design has local valve control).	MCR display and local, visual observation indicate each valve fully opens and fully closes.
ii.	Verify each BPDS air-operated valve fails to its safe position on loss of air.	Place each valve in its non-safe position. Isolate and vent air to the valve.	MCR display and local, visual observation indicate each valve fails to its safe position.
iii.	Verify each BPDS air-operated valve fails to its safe position on loss of electrical power to its solenoid.	Place each valve in its non-safe position. Isolate electrical power to each air- operated valve.	MCR display and local, visual observation indicate each valve fails to its safe position.
iv.	Verify each BPDS pump can be started and stopped remotely.	Align the BPDS to allow for pump operation. Stop and start each pump from the MCR.	MCR display and local, visual observation indicate each pump starts and stops.
V.	Verify the pump speed of each BPDS variable-speed pump can be manually controlled.	Vary the speed of each pump from the MCR and local control panel (if design has local pump control).	MCR display indicates the speed of each pump varies from minimum to maximum speed.

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Table 14.2-24: Balance-of-Plant Drains Test # 24 (Continued)

	Initiate a single real or simulated instrument signal from each BPDS transmitter.	 i. The instrument signal is displayed on an MCR workstation or recorded by the applicable control system historian. ii. The instrument signal is displayed on an RSS workstation or recorded by the applicable control system historian if the instrument signal is designed to be displayed in the RSS. iii. The instrument signal is displayed on an MCR module-specific safety display instrument monitor or an MCR common safety display instrument monitor if the instrument signal is designed to be displayed on a safety display instrument monitor.
System Level Test #24-1		
Test Objective	Test Method	Acceptance Criteria
Verify BPDS automatically controlled pumps start and stop automatically and transfer liquid waste to its design location.	Align each BPDS sump or tank to allow water in a selected sump or tank to be pumped to its design location. i. Fill the selected sump or tank until a HI water level is obtained to start the first (primary) pump. ii. Continue filling the sump or tank until a HI-HI level starts the second (alternate) pump. iii. Stop filling the sump or tank to allow the primary and alternate pumps to stop on low level. iv. Refill the sump or tank until the alternate pump starts on HI level.	 MCR displays and local, visual observation verifies the following: i. The first pump starts on HI level and transfers water to its design location in the LRW system. ii. The second (alternate) pump starts on HI-HI level. iii. Both primary and alternate pumps stop on LO level. iv. The alternate pump starts on HI level.
System Level Test #24-2		
Test Objective	Test Method	Acceptance Criteria
Verify the BPDS automatically responds to mitigate a release of radioactivity.	Place a north chemical waste water sump pump in operation. Initiate a real or simulated high radiation signal on the 6A CPS regeneration skid waste effluent.	sump pump stops.

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Table 14.2-24: Balance-of-Plant Drains Test # 24 (Continued)

System Level Test #24-3		
Test Objective	Test Method	Acceptance Criteria
Verify the BPDS automatically responds	Place a south chemical waste water	i. The pump stops.
to mitigate a release of radioactivity.	sump pump in operation. Initiate a real or simulated high radiation signal on the 6B CPS regeneration skid waste effluent.	
		iii. South chemical waste collection sump to LRW high conductivity waste tank isolation valve is closed.
		[ITAAC 03.18.02]
		(i through iii)
System Level Test #24-4		
Test Objective	Test Method	Acceptance Criteria
Verify the BPDS automatically responds to mitigate a release of radioactivity.	Place a north waste water sump pump in operation. Initiate a real or simulated high radiation signal in the BPDS north	stops.
	TGB floor drains.	ii. North waste water sump discharge to BPDS collection tank isolation valve is closed.
		iii. North waste water sump discharge to LRW high conductivity waste tank isolation valve is closed.
		[ITAAC 03.17.03]
		(i thorugh iii)
System Level Test #24-5		(r thoragin iii)
Test Objective	Test Method	Acceptance Criteria
Verify the BPDS automatically responds	Place a south waste water sump pump in	i. The south waste water sump pump
to mitigate a release of radioactivity.	operation. Initiate a real or simulated	stops.
	high radiation signal in the BPDS south TGB floor drains.	ii. South waste water sump discharge to BPDS collection tank isolation valve is closed.
		iii. South waste water sump discharge to LRW high conductivity waste tank isolation valve is closed.
		[ITAAC 03.18.03]
		(i through iii)
System Level Test #24-6		<u>, </u>
Test Objective	Test Method	Acceptance Criteria
Verify the BPDS automatically responds	Place a north waste water sump pump in	-
to mitigate a release of radioactivity.	operation. Initiate a real or simulated	sump pump stops.
	high radiation signal in the BPDS auxiliary blowdown cooler condensate.	ii. North chemical waste collection sump to BPDS collection tank isolation valve is closed.
		iii. North chemical waste collection sump to LRW high conductivity waste tank isolation valve is closed.
		[ITAAC 03.17.04] (i through iii)

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Table 14.2-25: Fire Protection System Test # 25

Preoperational test is required to be performed once.			
The fire protection system (FPS) is described in Section 9.5.1 and the functions verified by this test are:			
System Function	System Function Categorization	Function Verified by Test #	
 The FPS supports the following buildings and systems by providing fire prevention, detection, and suppression. RXB TGB RWB Security Buildings ANB Diesel Generator Building Administration and Training Building Warehouse Building Fire Water Building Switchyard system (SWYD) Transformers Site plant cooling structures Central Utility Building CRB MPS 13.8 KV and SWYD system (EHVS) Medium voltage AC electrical distribution system (EMVS) Low voltage AC electrical distribution system (ELVS) RWBVS CRVS RBVS 	nonsafety-related	Component-level tests	
2. The FPS supports the CRB by providing audible and visual alarms	nonsafety-related	Component-level test vii	
to alert operators in the MCR.			

Prerequisites

- Verify an instrument calibration has been completed, with approved records and within all calibration due dates, for all
 instruments required to perform this test.
- ii. Verify an FPS flow balance has been performed.
- iii. Verify a pump curve test has been completed for the fire protection pumps.

Component Level Tests

Te	st Objective	Test Method	Acceptance Criteria
i.	, , ,		MCR display and local, visual observation indicate each valve fully
			opens and fully closes.
ii.	fails to its safe position on loss of air.	Isolate and vent air to the valve.	MCR display and local, visual observation indicate each valve fails to its safe position.
iii.	fails to its safe position on loss of	Isolate electrical power to each air-	MCR display and local, visual observation indicate each valve fails to its safe position.

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Table 14.2-25: Fire Protection System Test # 25 (Continued)

iv. Verify	each FPS pump can be started	Align the FPS to allow for pump	i. MCR display and local, visual
	topped remotely	operation.	observation indicate each pump
	,	i.Start each pump from the MCR and	starts.
		locally.	Audible and visible water hammer
		ii.Stop each pump locally.	are not observed when the pump
			starts.
			ii. MCR display and local, visual
			observation indicate each pump
Varifi	variable and matter of FDC	: Aliana tha FDC and place the FDC	stops.
v. verify	automatic operation of FPS	i. Align the FPS and place the FPS pumps in automatic operation to	Any MCR display or the local, visual observation indicate the following:
Pump	J3.	pressurize the system.	i. The jockey pump maintains the FPS
		ii. Stop the jockey pump and simulate a	header at or greater than 10 psig
		low FPS header pressure to start the	above the pressure setting for the
		electric fire pump.	automatic start of the electric fire
		iii. Stop the electric fire pump and	pump.
		simulate a low FPS header pressure	ii. The electric fire pump starts.
		to start the diesel fire pump.	iii. The diesel pump starts.
		Partially close each FPS manual valve	An alarm is received in the MCR when
switch	h alarms when partially closed.	with a tamper switch to its alarm position	each valve is partially closed.
		(approximately 20 per cent of its total	
vii Vori£.	vasch smaka and fire datastar	travel distance).	The MCR receives an alarm and
	each smoke and fire detector des audible and visual alarms	Isolate the water supply to each preaction or deluge sprinkler before	ine MCR receives an alarm and indication from each smoke and fire
	nnunciation in the MCR.	perming this test to prevent wetting	detector.
		equipment.	
		Simulate a smoke or fire signal to each	
		detector.	
	fire pump flow meets its fire	Align the FPS for pump operation	i. The electric fire pump meets its
prote	ction volumetric flow rate.	through the recirculation line.	design volumetric flow rate.
		i. Start the electric fire pump.	[ITAAC 03.07.02]
		ii. Start the diesel fire pump.	
			ii. The diesel fire pump meets its
			design volumetric flow rate.
	LEDGI		[ITAAC 03.07.02]
		Initiate a single real or simulated instrument signal from each FPS	 The instrument signal is displayed on an MCR workstation or recorded
	gnal is designed to be displayed	1	by the applicable control system
in the		cransmicci.	historian.
	not required if the instrument		ii. The instrument signal is displayed
	ration verified the MCR and RSS		on an RSS workstation or recorded
displa	ay.)		by the applicable control system
			historian if the instrument signal is
			designed to be displayed in the RSS.
			iii. The instrument signal is displayed
			on an MCR module-specific safety display instrument monitor or an
			MCR common safety display
			instrument monitor if the
			instrument signal is designed to be
			displayed on a safety display
			instrument monitor.
_	evel Tests		
None			

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Table 14.2-26: Fire Detection Test # 26

Preoperational test is required to be performed once				
The fire detection system (FDS) is described in Section 9.5.1 and the functions verified by this test are:				
System Function	em Function System Function Categorization Function Verified by Test #			
As described in Test Abstract Table 14.2-	nonsafety-related	As described in Test Abstract Table 14.2-		
25		25		
Prerequisites				
As described in Test Abstract Table 14.2-25				
Component Level Tests				
As described in Test Abstract Table 14.2-25				
System Level Tests				
As described in Test Abstract Table 14.2-25				

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None

Table 14.2-27: Main Steam Test # 27

Table 14.2-27: Main Steam Test # 27			
Preoperational test is required to be performed for each NPM. The MSS is described in Section 10.3. MS functions are not verified by this test. The MSS functions verified by other			
tests are:	is functions are not vermed by this test	. The M33 functions verified by other	
System Function	System Function Categorization	Function Verified by Test #	
The MSS supports the SG by delivering steam to the main condenser.	nonsafety-related	TG Test #33-2	
The MSS supports the TGS by providing steam to the TGS.	nonsafety-related	TG Test #33-2	
Prerequisites			
Prerequisites associated with MSS testing Test #" heading.	are identified in the referenced test abstra	act cited under the "Function Verified by	
Component Level Tests			
Test Objective	Test Method	Acceptance Criteria	
i. Verify each MSS remotely-operated valve can be operated remotely.	Operate each valve from the MCR and local control panel (if design has local valve control)	MCR display and local, visual observation indicate each valve fully opens and fully closes.	
ii. Verify each MSS air-operated valve fails to its safe position on loss of air.	Place each valve in its non-safe position. Isolate and vent air to the valve.	MCR display and local, visual observation indicate each valve fails to its safe position.	
iii. Verify each MSS air-operated valve fails to its safe position on loss of electrical power to its solenoid.	Place each valve in its non-safe position. Isolate electrical power to each air- operated valve.	MCR display and local, visual observation indicate each valve fails to its safe position.	
iv. Verify automatic operation of MSS extraction steam to protect the main turbine.	Initiate a simulated signal for the following system conditions. i. feedwater heater high level ii. turbine trip	Any remote display or local verification indicates the following: i. extraction steam block valve closes ii. extraction steam non-return check valve closes	
v. Verify each MSS instrument is monitored in the MCR and the RSS, if the signal is designed to be displayed in the RSS. (Test not required if the instrument calibration verified the MCR and RSS display.)	Initiate a single real or simulated instrument signal from each MSS transmitter.	 i. The instrument signal is displayed on an MCR workstation or recorded by the applicable control system historian. ii. The instrument signal is displayed on an RSS workstation or recorded by the applicable control system historian if the instrument signal is designed to be displayed in the RSS. iii. The instrument signal is displayed on an MCR module-specific safety display instrument monitor or an MCR common safety display instrument monitor if the instrument signal is designed to be displayed on a safety display 	
ystem Level Tests		MCR o instru instru	

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Table 14.2-28: Feedwater System Test # 28

Preoperational test is required to be performed for each NPM. The FWS is described in Section 10.4.7; Section 9.2.6 (condensate storage tank); Section 10.4.1 (condenser); FWS functions are not verified by FWS tests. FWS functions verified by other tests are:			
 The FWS supports the MSS by accepting effluent from main steam drains and steam traps into the main condenser. 	nonsafety-related	TG Test #33-2	
The FWS supports the CPS by providing water for CPS rinse and CPS resin transfer.	nonsafety-related	CPS Test #30-1	
 The FWS supports the turbine generator by condensing the gland seal steam in the gland exhaust condenser. 	nonsafety-related	CAR Test #32-1	
 The FWS supports the CARS by accepting water drawn from the exhaust of the vacuum pump. 	nonsafety-related	CAR Test #32-1	
 The FWS supports the TG by cooling superheated steam in the gland steam desuperheater prior to the steam entering the gland seals. 	nonsafety-related	TG Test #33-1	
The FWS supports the containment system (CNTS) by supplying feedwater to the SGs.	nonsafety-related	TG Test #33-1	
7. The FWS supports the turbine generator by cooling superheated turbine bypass steam in the turbine bypass desuperheater prior to the steam entering the main condenser.	nonsafety-related	TG Test #33-1	
 The FWS supports the turbine generator by accepting turbine bypass steam into the main condenser. 	nonsafety-related	TG Test #33-1	
 The FWS supports the turbine generator by accepting exhaust steam from the turbine into the main condenser. 		TG Test #33-2	
The FWS supports the CNTS by providing secondary isolation of the feedwater lines.	nonsafety-related	MPS Test #63-5	
11. The FWS supports the decay heat removal system (DHRS) by providing secondary isolation of the feedwater lines, ensuring required boundary conditions for DHRS operation. Prerequisites	nonsafety-related	MPS Test #63-5	

Prerequisites

Prerequisites associated with FWS testing are identified in the referenced test abstract cited under the "Function Verified by Test #" heading.

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Table 14.2-28: Feedwater System Test # 28 (Continued)

	mponent Level Tests		
Tes	st Objective	Test Method	Acceptance Criteria
i.	Verify each FWS remotely-operated valve can be operated remotely.	Operate each valve from the MCR and local control panel (if design has local valve control).	MCR display and local, visual observation indicate each valve fully opens and fully closes.
ii.	Verify each FWS air-operated valve fails to its safe position on loss of air.	Place each valve in its non-safe position. Isolate and vent air to the valve.	MCR display and local, visual observation indicate each valve fails to its safe position.
	Verify each FWS air-operated valve fails to its safe position on loss of electrical power to its solenoid.	Place each valve in its non-safe position. Isolate electrical power to each air- operated valve.	MCR display and local, visual observation indicate each valve fails to its safe position.
iv.	Verify each FWS condensate pump can be started and stopped remotely.	Align the FWS to allow for pump operation. Stop and start each pump from the MCR.	MCR display and local, visual observation indicate each pump starts and stops. Audible and visible water hammer are not observed when the pump starts.
v.	Verify the pump speed of each FWS variable-speed pump can be manually controlled.	Align the FWS to provide a flow path to operate a selected FW variable-speed pump. Vary the FWS pump speed from minimum to maximum speed from the MCR.	MCR display indicates the speed of each variable speed pump obtains both minimum and maximum pump speeds. Audible and visible water hammer are not observed when the pump starts.
vi.	Verify the condensate standby pump automatically starts to protect plant equipment.	Align the FWS to allow for pump operation. Place a pump in service. Initiate a simulated low pump header pressure low signal.	MCR display and local, visual observation indicate the standby pump starts. Audible and visible water hammer are not observed when the pump starts.
vii.	Verify the feedwater standby pump automatically starts to protect plant equipment.	Align the FWS to allow for pump operation. Place a pump in service. Initiate a simulated low pump header pressure low signal.	MCR display and local, visual observation indicate the standby pump starts. Audible and visible water hammer are not observed when the pump starts.
viii.	Verify CPS bypass to protect plant equipment.	Align the FWS to provide a flow path through the condensate polishers. Initiate a simulated CPS bypass signal.	MCR display and local, visual observation indicate the CPS bypass valve is open.
	Verify condensate pump low flow protection and short cycle automatic operation.	 i. Align the FWS for automatic short cycle cleanup. Place a condensate pump in operation. ii. Manually throttle a valve in the pump flow path until the flow rate reaches the pump minimum flow setpoint. iii. Open the throttled valve. 	MCR displays and local, visual observation verifies the following: i. The short cycle flow is automatically maintained by the short cycle cleanup flow control valve. ii. The condensate pump minimum flow valve is open. iii. The condensate pump minimum flow valve is closed.
x.	Verify feedwater pump low flow protection.	 i. Align the FWS for automatic long cycle cleanup. Place a condensate pump in operation. ii. Manually throttle a valve in the pump flow path until the flow rate reaches the feedwater pump minimum flow setpoint. iii. Open the throttled valve. 	MCR displays and local, visual observation verifies the following: i. The long cycle flow is automatically maintained by the long cycle cleanup flow control valve. ii. The feedwater pump minimum flow valve is open. iii. The feedwater pump minimum flow valve is closed.

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Table 14.2-28: Feedwater System Test # 28 (Continued)

xi.	, , ,	Place the system in service to allow flow through the grab sampling device.	A local grab sample is successfully obtained.
xii.	Verify each FWS instrument is monitored in the MCR and the RSS, if the signal is designed to be displayed in the RSS.	1	i. The instrument signal is displayed on an MCR workstation or recorded by the applicable control system historian.
	(Test not required if the instrument calibration verified the MCR and RSS display.)		ii. The instrument signal is displayed on an RSS workstation or recorded by the applicable control system historian if the instrument signal is designed to be displayed in the RSS.
			iii. The instrument signal is displayed on an MCR module-specific safety display instrument monitor or an MCR common safety display instrument monitor if the instrument signal is designed to be displayed on a safety display instrument monitor.
Sys	stem Level Tests		
No	None		

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None

Table 14.2-29: Feedwater Treatment Test # 29

Preoperational test is required to be performed for the 6A NPMs and for the 6B NPMs.					
Th	The feedwater treatment system (FWTS) is described in Section 10.4.11 and the function verified by this test is:				
	stem Function	System Function Categorization	Function Verified by Test #		
cor	e FWTS supports the FWS by ntrolling and maintaining feedwater emistry within specification.	nonsafety-related	Component-level tests		
Pre	erequisites	,			
Vei	ify an instrument calibration has been	completed, with approved records and w	ithin all calibration due dates, for all		
	truments required to perform this test.		·		
	mponent Level Tests				
		Test Method	Acceptance Criteria		
i.	-	Operate each valve from the MCR and	MCR display and local, visual		
	valve can be operated remotely.	local control panel (if design has local valve control).	observation indicate each valve fully opens and fully closes.		
ii.	Verify each FWTS air-operated valve fails to its safe position on loss of air.	Place each valve in its non-safe position. Isolate and vent air to the valve.	MCR display and local, visual observation indicate each valve fails to its safe position.		
iii.	Verify each FWTS air-operated valve fails to its safe position on loss of electrical power to its solenoid.	Place each valve in its non-safe position. Isolate electrical power to each air- operated valve.	MCR display and local, visual observation indicate each valve fails to its safe position.		
iv.	Verify each FWTS pump can be started and stopped remotely and locally (if designed).	Align the FWTS to allow for pump operation. Stop and start each remotely-controlled pump from the MCR. Stop and start each locally-controlled pump locally.	MCR display and local, visual observation indicate each pump starts and stops.		
v.	Verify the speed of each FWTS variable-speed pump can be manually controlled.	Vary the speed of each pump from the MCR and local control panel (if design has local pump control).	MCR display indicates pump speed varies from minimum to maximum speed.		
vi.		Initiate a single real or simulated instrument signal from each FWTS transmitter.	 i. The instrument signal is displayed on an MCR workstation or recorded by the applicable control system historian. ii. The instrument signal is displayed on an RSS workstation or recorded by the applicable control system historian if the instrument signal is designed to be displayed in the RSS iii. The instrument signal is displayed on an MCR module-specific safety display instrument monitor or an 		
Sve	stem Level Tests		MCR common safety display instrument monitor if the instrument signal is designed to be displayed on a safety display instrument monitor.		

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Table 14.2-30: Condensate Polisher Resin Regeneration System Test # 30

Preoperational test is required to be	performed once.			
The CPS is described in Section 10.4.6. The CPS and other system functions verified by this test are:				
System Function	System Function Categorization	Function Verified by Test #		
The CPS supports the FWS by providing purification of the feedwater to maintain feedwater chemistry within specification.	nonsafety-related	Test #30-1		
The FWS supports the CPS by providing water for CPS rinse and CPS resin transfer.	nonsafety-related	Test #30-1		
 The ABS supports the CPS by supplying steam for resin regeneration. 	nonsafety-related	Test #30-1		

Prerequisites:

Verify an instrument calibration has been completed, with approved records and within all calibration due dates, for all instruments required to perform this test.

	instruments required to perform this test.				
Co	Component Level Tests				
Test Objective		Test Method	Acceptance Criteria		
i.	Verify each CPS remotely-operated valve can be operated remotely.	Operate each valve from the MCR and local control panel (if design has local valve control).	MCR display and local, visual observation indicate each valve fully opens and fully closes.		
ii.	Verify each CPS air-operated valve fails to its safe position on loss of air.	Place each valve in its non-safe position. Isolate and vent air to the valve.	MCR display and local, visual observation indicate each valve fails to its safe position.		
iii.	Verify each CPS air-operated valve fails to its safe position on loss of electrical power to its solenoid.	Place each valve in its non-safe position. Isolate electrical power to each air- operated valve.	MCR display and local, visual observation indicate each valve fails to its safe position.		
iv.	Verify each CPS pump can be started and stopped remotely and locally (if designed).	Align the CPS to allow for pump operation. Stop and start each remotely-controlled pump from the MCR. Stop and start each locally-controlled	MCR display and local, visual observation indicate each pump starts and stops.		
		pump locally.			
v.	Verify the speed of each CPS variable- speed pump can be manually controlled.	Vary the speed of each pump from the MCR and local control panel (if design has local pump control)	MCR display indicates pump speed varies from minimum to maximum speed.		
vi.	Verify a local grab sample can be obtained from a CPS grab sample device.	Place the system in service to allow flow through the grab sampling device.	A local grab sample is successfully obtained.		

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Table 14.2-30: Condensate Polisher Resin Regeneration System Test # 30 (Continued)

vii. Verify each CPS instrument is monitored in the MCR and the RSS, if the signal is designed to be displayed in the RSS.	Initiate a single real or simulated instrument signal from each CPS transmitter.	i. The instrument signal is displayed on an MCR workstation or recorded by the applicable control system historian.
(Test not required if the instrument calibration verified the MCR and RSS display.)		ii. The instrument signal is displayed on an RSS workstation or recorded by the applicable control system historian if the instrument signal is designed to be displayed in the RSS.
		iii. The instrument signal is displayed on an MCR module-specific safety display instrument monitor or an MCR common safety display instrument monitor if the instrument signal is designed to be displayed on a safety display instrument monitor.
System Level Test #30-1	,	,
Test Objective	Test Method	Acceptance Criteria
Verify the CPS automatically completes resin regeneration.	Align the FWS to support CPS resin regeneration.	i. The resin transferred to the regeneration skid.
	Align the ABS to support CPS resin regeneration.	ii. The CPS regeneration cycle completed successfully.
	 i. Automatically transfer the test resin bed from a condensate polisher to the CPS regeneration skid. 	iii. The resin transferred to a condensate polisher.
	ii. Initiate an automatic regeneration of the resin.	
	iii. Automatically transfer the test resin bed from the CPS regeneration skid to a condensate polisher.	

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Table 14.2-31: Heater Vents and Drains Test # 31

Preoperational test is required to be performed for each NPM.				
The heater vents and drains (HVD) system is described in Section 10.4.7. and the functions verified by this test are:				
•		System Function Categorization	Function Verified by Test #	
	The HVD system supports the FWS by venting the feedwater heaters.	·	Component level tests	
2.	The HVD system supports the FWS by controlling level in the shell sides feedwater heaters.	nonsafety-related	Component level tests	
Pre	erequisites			
	rify an instrument calibration has been struments required to perform this test.	completed, with approved records and w	ithin all calibration due dates, for all	
Co	mponent Level Tests			
Te	st Objective	Test Method	Acceptance Criteria	
i.	Verify each HVD remotely-operated valve can be operated remotely.	Operate each valve from the MCR and local control panel (if design has local valve control).	MCR display and local, visual observation indicate each valve fully opens and fully closes.	
ii.	Verify each HVD air-operated valve fails to its safe position on loss of air.	Place each valve in its non-safe position. Isolate and vent air to the valve.	MCR display and local, visual observation indicate each valve fails to its safe position.	
iii.	Verify each HVD air-operated valve fails to its safe position on loss of electrical power to its solenoid.	Place each valve in its non-safe position. Isolate electrical power to each air- operated valve.	MCR display and local, visual observation indicate each valve fails to its safe position.	
iv.	Verify automatic operation of HVD valves to protect the turbine on	Initiate a simulated turbine trip.	Any remote display or local verification indicates the following:	
	turbine trip.		 Low, intermediate and high pressure feedwater heater extraction steam supply valves are closed. 	
			ii. Low, intermediate and high pressure feedwater heater air assisted check valves are closed.	
			iii. Low, intermediate and high pressure feedwater heater extraction steam dump valves are open.	
v.	Verify automatic operation of HVD valves to protect turbine on high	Initiate a simulated signal for the following system conditions.	Any remote display or local verification indicates the following:	
	feedwater heater level.	 i. Low pressure feedwater heater high level. ii. Intermediate pressure feedwater heater high level. iii. High pressure feedwater heater high level 	 i. Low pressure feedwater heater extraction steam supply valve and low pressure feedwater heater extraction steam dump valve are open. ii. Intermediate pressure feedwater heater extraction steam supply valve and intermediate pressure feedwater heater extraction steam dump valve are open. iii. High pressure feedwater heater extraction steam supply valve and high pressure feedwater heater extraction steam supply valve and high pressure feedwater heater extraction steam dump valve are 	

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open.

Table 14.2-31: Heater Vents and Drains Test # 31 (Continued)

vi. Verify each HVD system instrument is monitored in the MCR and the RSS, if the signal is designed to be displayed in the RSS.	instrument signal from each HVD system	i.	The instrument signal is displayed on n MCR workstation or recorded by the applicable control system historian.
(Test not required if the instrument calibration verified the MCR and RSS display.)		ii.	The instrument signal is displayed on an RSS workstation or recorded by the applicable control system historian if the instrument signal is designed to be displayed in the RSS.
		iii.	The instrument signal is displayed on an MCR module-specific safety display instrument monitor or an MCR common safety display instrument monitor if the instrument signal is designed to be displayed on a safety display instrument monitor.
System Level Tests			
None			

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Table 14.2-32: Condenser Air Removal System Test # 32

Preoperational test is required to be po	erformed for each NPM.			
The condenser air removal system (CARS) is described in Section 10.4.2 and the functions verified by this test are:				
System Function	System Function Categorization	Function Verified by Test #		
 The CARS supports the condensate and FWS by removing air and non- condensable gases from the main condenser. 	nonsafety-related	Test #32-1		
The circulating water system (CWS) supports the FWS by removing heat from the main condenser.	nonsafety related	Test #32-1		
 The ABS supports the turbine generator by supplying gland seal steam. 	nonsafety-related	Test #32-1		
The FWS supports the CARS by accepting water drawn from the exhaust of the vacuum pump.	nonsafety-related	Test #32-1		
 The FWS supports the turbine generator by condensing the gland seal steam in the gland exhaust condenser. 	nonsafety-related	Test #32-1		
The auxiliary boiler supports the FWS by supplying steam to the condenser for sparging when necessary.		Test #32-1		
Prerequisites		•		
Verify an instrument calibration has been instruments required to perform this test		d within all calibration due dates, for all		
Component Level Tests	-			

instruments required to perform this test.				
Co	mponent Level Tests			
Tes	st Objective	Test Method	Acceptance Criteria	
i.	Verify each CARS remotely-operated valve can be operated remotely.	Operate each valve from the MCR and local control panel (if design has local valve control).	MCR display and local, visual observation indicate each valve fully opens and fully closes.	
ii.	Verify each CARS air-operated valve fails to its safe position on loss of air.	Place each valve in its non-safe position. Isolate and vent air to the valve.	MCR display and local, visual observation indicate each valve fails to its safe position.	
iii.	Verify each CARS air-operated valve fails to its safe position on loss of electrical power to its solenoid.	Place each valve in its non-safe position. Isolate electrical power to each air- operated valve.	MCR display and local, visual observation indicate each valve fails to its safe position.	
iv.	Verify each CARS pump can be started and stopped remotely.	Align the CARS to allow for pump operation. Stop and start each pump from the MCR.	MCR display and local, visual observation indicate each pump starts and stops. Audible and visible water hammer are not observed when the pump starts.	
V.	Verify CARS valves automatically operate to maintain CARS seal water separator tank level.	Initiate a simulated signal for the following system conditions. i. CARS seal water separator tank high level. ii. CARS seal water separator tank low level.	Any remote display or local verification indicates the following: i. CARS seal water separator tank makeup valve is closed and drain valve is open. ii. The CARS seal water separator makeup valve is open and drain valve is closed.	

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Table 14.2-32: Condenser Air Removal System Test # 32 (Continued)

the signal is designed to be displayed in the RSS. (Test not required if the instrument calibration verified the MCR and RSS display.)	Align the CARS to allow for pump operation. Place a pump in service. Initiate a simulated main condenser high pressure. Initiate a single real or simulated instrument signal from each CARS transmitter.	MCR display and local, visual observation indicate the standby pump starts. Audible and visible water hammer are not observed when the pump starts. i. The instrument signal is displayed on an MCR workstation or recorded by the applicable control system historian. ii. The instrument signal is displayed on an RSS workstation or recorded by the applicable control system historian if the instrument signal is designed to be displayed in the RSS. iii. The instrument signal is displayed on an MCR module-specific safety display instrument monitor or an MCR common safety display instrument monitor if the instrument signal is designed to be displayed on a safety display instrument monitor.
System Level Test #32-1 Test Objective	Test Method	Accontance Cuitoria
Verify the CARS can maintain main condenser vacuum pressure.	Place the ABS in automatic control to supply gland seal steam. Place the FWS in automatic control to condense the gland seal steam in the gland exhaust condenser. Place the CWS in automatic control to provide cooling to the main condenser. i. Place the CARS in service to establish vacuum in the main condenser. ii. Open the feedwater sparge isolation valves to provide steam sparging to the main condenser.	 i. a. The auxiliary boiler gland seal steam prevents air leakage into and out of the turbine to maintain main condenser design vacuum pressure. b. The CWS provides cooling to maintain main condenser design vacuum pressure. c. The FWS cools superheated steam in the gland steam desuperheater to design setpoint. d. The CARS removes noncondenser design vacuum pressure. ii. The ABS is capable of providing sparging steam to the main condenser.

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Table 14.2-33: Turbine Generator Test # 33

	Preoperational test is required to be performed for each NPM.				
Th	The TGS is described in Sections 10.2, 10.4.3, and 10.4.4. The TGS and other functions verified by this test are:				
Sy	stem Function	System Function Categorization	Function Verified by Test #		
1.	The TGS supports the MSS by providing steam bypass from the MSS to the main condenser.	nonsafety-related	Test #33-1		
2.	The MHS supports the CVCS by adding heat to primary coolant.	non-safety related	Test #33-1		
3.	The CVCS supports the reactor coolant system (RCS) by heating primary coolant.	nonsafety-related	Test #33-1		
	The ABS supports the module heatup system (MHS) by supplying steam for heating reactor coolant at startup and shutdown.	nonsafety-related	Test #33-1		
5.	The FWS supports the CNTS by supplying feedwater to the SGs.	nonsafety-related	Test #33-1		
6.	The FWS supports the TGS by cooling superheated turbine bypass steam in the turbine bypass desuperheater prior to the steam entering the main condenser.	nonsafety-related	Test #33-1		
7.	The FWS supports the TGS by accepting turbine bypass steam into the main condenser.	nonsafety-related	Test #33-1		
	The FWS supports the TGS by cooling superheated steam in the gland steam desuperheater prior to the steam entering the gland seals.	nonsafety-related	Test #33-1		
	The FWS supports the TGS by accepting exhaust steam from the turbine into the main condenser.	nonsafety-related	Test #33-2		
10.	The MSS supports the TGS by providing steam to the TGS.	nonsafety-related	Test #33-2		

Prerequisites

i. Verify an instrument calibration has been completed, with approved records and within all calibration due dates, for all instruments required to perform this test.

The following prerequisites are not required for component testing:

- ii. Verify Test #32-1 has been completed to verify the CARS can maintain main condenser vacuum pressure (reference test 14.2-32).
- iii. The SG feedwater flush is complete.
- iv. The CARS is automatically maintaining main condenser vacuum.
- v. Initial RCS temperature must be approximately 200°F to allow for hot functional testing to obtain data at an RCS temperature of 200°F and above.
- vi. The NPM and supporting systems are aligned to increase RCS temperature and pressure.

Component Level Tests				
Test Objective		Test Method	Acceptance Criteria	
i.	Verify each TGS remotely-operated	Operate each valve from the MCR and	MCR display and local, visual	
	valve can be operated remotely.	local control panel (if design has local	observation indicate each valve fully	
		valve control).	opens and fully closes.	

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Table 14.2-33: Turbine Generator Test # 33 (Continued)

ii.	Verify each TGS air-operated valve	Place each valve in its non-safe position.	MCR display and local, visual
	· · · · · · · · · · · · · · · · · · ·	Isolate and vent air to the valve.	observation indicate each valve fails to
	·		its safe position.
iii.	Verify each TGS air-operated valve	Place each valve in its non-safe position.	MCR display and local, visual
	fails to its safe position on loss of	Isolate electrical power to each air-	observation indicate each valve fails to
	electrical power to its solenoid.	operated valve.	its safe position.
iv.		Align the TGS to allow for main lube oil,	MCR display and local, visual
	started and stopped remotely.	auxiliary lube oil, and emergency pump	observation indicate each pump starts
		operation.	and stops.
		Stop and start each pump from the MCR.	
٧.	Verify the TGS exhaust hood is	Initiate a simulated high exhaust hood	Any remote display or the local, visual
	protected against high temperature.	temperature.	observation indicates the exhaust hood
			spray valve is open.
vi.		Align the TGS to allow for main lube oil	MCR display and local, visual
	capability by automatic start of the	and auxiliary lube oil pump operation.	observation indicate the auxiliary oil
	auxiliary lube oil pump.	Place the TGS main oil pump in normal	pump starts.
		service. Place the auxiliary oil pump in	Audible and visible water hammer are
		standby.	not observed when the pump starts.
		Simulate a TGS low main oil pump	
		discharge pressure.	
vii.	Verify TGS lubricating oil flow	Align the TGS to allow for auxiliary lube	MCR displays and local, visual
	capability by automatic start of the	oil pump and emergency lube oil pump	observation indicate the TGS emergency
	emergency direct current (DC) lube	operation. Place the turbine generator	oil pump starts.
	oil pump.	auxiliary oil pump in normal service.	Audible and visible water hammer are
			not observed when the pump starts.
		pump low discharge pressure or simulate	
		a loss of ac power to start the TGS	
viii	Verify the turbine stop valve and	emergency oil pump. i. Simulate an overspeed trip signal	i. The turbine stop valve and turbine
VIII.	turbine control valves close on	from the turbine overspeed	control valves close.
	turbine overspeed.	emergency trip system.	
	tarbine overspeed.	ii. Simulate an overspeed trip signal	[ITAAC 02.04.02]
		from the governor overspeed	
		detection circuit.	ii. The turbine stop valve and turbine
		detection enedit	control valves close.
			[ITAAC 02.04.02]
ix.	Verify each TGS instrument is	Initiate a single real or simulated	i. The instrument signal is displayed
	monitored in the MCR and the RSS, if		on an MCR workstation or recorded
	the signal is designed to be displayed	transmitter.	by the applicable control system
	in the RSS.		historian.
	(Test not required if the instrument		ii. The instrument signal is displayed
	calibration verified the MCR and RSS		on an RSS workstation or recorded
	display).		by the applicable control system
			historian if the instrument signal is designed to be displayed in the RSS.
			1
			iii. The instrument signal is displayed
			on an MCR module-specific safety
			display instrument monitor or an MCR common safety display
			instrument monitor if the
			instrument signal is designed to be
			displayed on a safety display
			instrument monitor.
<u> </u>			

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Table 14.2-33: Turbine Generator Test # 33 (Continued)

Sy	System Level Test #33-1				
Test Objective		Test Method		Acceptance Criteria	
i.	,	Align the plant to cool the RCS via the TGS bypass system. Warm main steam lines.	i.	CVCS supply remains in a sub- cooled state while heating the RCS using the module heatup system.	
ii.	the RCS to establish natural	Place the TGS steam bypass valve in automatic control. Place the feedwater regulating valve in steam generator inventory control.	ii. iii.	RCS temperature is sufficient to obtain criticality. RCS natural circulation flow is sufficient to obtain criticality.	
iii.	turbine bypass flow to the main condenser.	Place the MHS and the CVCS in automatic control to heat the RCS.	iv.	The TGS bypass flow is maintained at setpoint. The feedwater flow to the steam	
iv.	Verify the FWS automatically controls flow to the SGs to maintain SG inventory.	Place the ABS high-pressure system in automatic control to heat the MHS heat exchanger from RCS ambient temperature to the highest temperature		generator is maintained at setpoint. The cooled TGS bypass flow is maintained at setpoint.	
v.	Verify the FWS automatically cools the TGS bypass steam flow in the main steam desuperheater.	achievable by MHS heating.	vii.	A local grab sample is successfully obtained at RCS normal operating temperature and pressure.	
vi.	Verify a local grab sample can be obtained from an MHS system grab sample device.				

System Level Test #33-2

This test may be performed after the completion of Test 33-1 when the RCS is at normal operating pressure and the RCS has achieved the maximum temperature achievable by warming the RCS using MHS heating.

Test Objective	Test Method	Acceptance Criteria
Verify the maximum main turbine speed	Place the main turbine in service as	The maximum main turbine speed is
that can be obtained using the MHS to	follows:	obtained.
heat the RCS.	 Ensure the RCS is at RCS is at normal operating pressure and the RCS is at maximum temperature achievable by warming the RCS using MHS heating. 	
	ii. Place turbine on turning gear with seal steam in service.iii. Warm up turbine to required	
	temperature. iv. Increase main turbine speed.	
	iv. increase main turbine speed.	

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Table 14.2-34: Turbine Lube Oil System Test # 34

Pr	Preoperational test is required to be performed once for the 6A NPMs and once for and the 6B NPMs.			
The turbine lube oil storage (TLOS) system is described in Section 10.2.2.1.3 and the functions verified by this test are:				
System Function		System Function Categorization	Function Verified by Test #	
1.	The TLOS system supports the turbine generator by supplying lube oil storage for clean and dirty lube oil for protection of plant assets	nonsafety-related	Component-level tests	
2.	The TLOS system supports the turbine generator by receiving and purifying lube oil from the turbine generator lube oil reservoir for protection of plant assets.	non-safety related	Component-level tests	
3.	The TLOS system supports the turbine generator by providing clean lube oil makeup to the turbine generator lube oil reservoir.	nonsafety-related	Component-level tests	

Prerequisites

Verify an instrument calibration has been completed, with approved records and within all calibration due dates, for all instruments required to perform this test.

ins	instruments required to perform this test.				
Co	Component Level Tests				
Test Objective		Test Method	Acceptance Criteria		
i.	Verify each TLOS remotely-operated valve can be operated remotely.	Operate each valve from the MCR and local control panel (if design has local valve control).	MCR display and local, visual observation indicate each valve fully opens and fully closes.		
ii.	Verify each TLOS air-operated valve fails to its safe position on loss of air.	Place each valve in its non-safe position. Isolate and vent air to the valve.	MCR display and local, visual observation indicate each valve fails to its safe position.		
iii.	Verify each TLOS air-operated valve fails to its safe position on loss of electrical power to its solenoid.	Place each valve in its non-safe position. Isolate electrical power to each air- operated valve.	MCR display and local, visual observation indicate each valve fails to its safe position.		
iv.	Verify each TLOS pump can be started and stopped remotely and locally (if designed).	Align the TLOS system to allow for pump operation. Stop and start each remotely-controlled pump from the MCR. Stop and start each locally-controlled pump locally.	MCR display and local, visual observation indicate each pump starts and stops.		
V.	Verify the speed of each TLOS variable-speed pump can be manually controlled.	Vary the speed of each pump from the MCR and local control panel (if design has local pump control).	MCR display indicates pump speed varies from minimum to maximum speed.		

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Table 14.2-34: Turbine Lube Oil System Test # 34 (Continued)

,	Initiate a single real or simulated	i.	The instrument signal is displayed
if the signal is designed to be	instrument signal from each TLOS system transmitter.		on an MCR workstation or recorded by the applicable control system
displayed in the RSS.			historian.
(Test not required if the instrument calibration verified the MCR and RSS display).		ii.	The instrument signal is displayed on an RSS workstation or recorded by the applicable control system historian if the instrument signal is designed to be displayed in the RSS
		iii.	The instrument signal is displayed on an MCR module-specific safety display instrument monitor or an MCR common safety display instrument monitor if the instrument signal is designed to be displayed on a safety display instrument monitor.
System Level Tests		•	
None			

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Table 14.2-35: Liquid Radioactive Waste System Test # 35

The LRWS is described in Section 11.2 a	nd 11.5.2.1.5 and the functions verif	ied by this test are:
System Function	System Function Categorization	Function Verified by Test #
The LRWS supports the solid	nonsafety-related	Test #35-1
radioactive waste system (SRWS) by		Test #35-2
receiving and processing liquid		
radioactive waste from the SRWS		
dewatering skid.		
2. The LRWS supports the SFPCS by	nonsafety-related	Test #35-1
receiving contaminated pool water		Test #35-2
to aid in the removal of titrated water		
or boron. Treated liquid radwaste has		
the option to return to the pool as		
makeup.		
3. The LRWS supports the CVCS by	nonsafety-related	Test #35-1
receiving and processing primary		Test #35-2
coolant from CVCS letdown.		
4. The LRWS supports the RWDS by	nonsafety-related	Test #35-1
receiving and processing the effluent		Test #35-2
from the RWB radioactive waste drain		
sumps.		
5. The LRWS supports the RWDS by	nonsafety-related	Test #35-1
receiving and processing the effluent		Test #35-2
from the RXB radioactive waste drain		
sumps.		
6. The LRWS supports the RWDS by	nonsafety-related	Test #35-1
receiving and processing the effluent		Test #35-2
from the ANB radioactive waste drain		
sumps.		
The LRWS functions verified by other to	ests are:	
System Function	System Function Categorization	Function Verified by Test #
The LRWS supports the CVCS by	nonsafety-related	Test #38-1
receiving and processing primary		
coolant from CVCS letdown.		
The LRWS supports the RWDS by	nonsafety-related	Test #23-1
receiving and processing the effluent		
from theRWB radioactive waste drain		
sumps.		
The LRWS supports the RWDS by	nonsafety-related	Test #23-1
receiving and processing the effluent		
from theRXB radioactive waste drain		
sumps.		
The LRWS supports the RWDS by	nonsafety-related	Test #23-1
receiving and processing the effluent		
from the ANB radioactive waste drain		
sumps.		
Dropoguicitos		<u> </u>

Prerequisites

Verify an instrument calibration has been completed, with approved records and within all calibration due dates, for all instruments required to perform this test.

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Table 14.2-35: Liquid Radioactive Waste System Test # 35 (Continued)

Co	Component Level Tests			
Te	st Objective	Test Method	Acceptance Criteria	
i.	Verify each LRWS remotely-operated valve can be operated remotely.	Operate each valve from the MCR and local control panel (if design has local valve control)	MCR display and local, visual observation indicate each valve fully opens and fully closes.	
	fails to its safe position on loss of air.	Place each valve in its non-safe position. Isolate and vent air to the valve.	MCR display and local, visual observation indicate each valve fails to its safe position.	
	Verify each LRWS air-operated valve fails to its safe position on loss of electrical power to its solenoid. Verify each LRWS pump can be started and stopped remotely.	Place each valve in its non-safe position. Isolate electrical power to each air- operated valve. Align the LRWS to allow for pump operation. Stop and start each pump from the MCR.	MCR display and local, visual observation indicate each valve fails to its safe position. MCR display and local, visual observation indicate each pump starts and stops. Audible and visible water hammer are	
v.	Verify the speed of each LRWS variable-speed pump can be manually controlled.	Align the LRWS to provide a flow path to operate a selected pump. Vary the LRWS pump speed from minimum to maximum from the MCR.	not observed when the pump starts. MCR display indicates the speed of each obtains both minimum and maximum pump speeds. Audible and visible water hammer are not observed when the pump starts.	
vi.	Verify radiation isolation on discharge to the utility water discharge basin high radiation, low dilution flow or underground pipe break.	Initiate the following a real or simulated signals: i. LRWS discharge to the utility water discharge basin high radiation signal. ii. LRWS discharge to the utility water discharge basin low dilution flow signal. iii. LRWS discharge to the utility water discharge basin low guard pipe pressure signal.	MCR display and local, visual observation indicate the following: i. The LRWS discharge to the utility water discharge basin isolation valves close. ii. The LRWS discharge to the utility water discharge basin isolation valves close. iii. The LRWS discharge to the utility water discharge basin isolation valves close. iii. The LRWS discharge to the utility water discharge basin isolation valves close. [ITAAC 03.09.07] (items i through iii)	
vii.	Verify tank valves operate to ensure uninterrupted waste receiving.	Simulate an in-service tank high level signal for each of the following tanks: low-conductivity waste (LCW) collection tank A and B high-conductivity waste (HCW) collection tank A and B LCW sample tank A and B HCW sample tank A and B	MCR display and local, visual observation indicate the in-service tank fill valve is closed and the standby tank fill valve is open.	
viii	. Verify degasifier valves operate to ensure uninterrupted waste receiving.	 i. Initiate a simulated high degasifier level signal. ii. Initiate a simulated high degasifier pressure signal. 	i and ii. MCR display and local, visual observation indicate the in-service degasifier fill valve is closed and the standby degasifier fill valve is open.	

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Table 14.2-35: Liquid Radioactive Waste System Test # 35 (Continued)

ix.	Verify LRW pumps automatically operate to prevent tank overflow.	Align the LRWS to allow each of the following LRW transfer pumps to automatically transfer effluent to one of its design locations. Degasifier transfer pump A and B LCW collection tank transfer pump A and B HCW collection tank transfer pump A and B LCW sample tank transfer pump A and B HCW sample tank transfer pump A and B Detergent waste collection tank transfer	MCR displays and local, visual observation indicate the following: i. The transfer pump starts and transfers effluent to its design location. ii. The transfer pump stops.
		pump Demineralized water break tank transfer pump i. Simulate a HI HI level signal in each of the above tanks. ii. Simulate a low level signal in each of the above tanks.	
x.	Verify a local grab sample can be obtained from a LRWS grab sample device indicated on the LRW piping and instrumentation diagram.	Place the system in service to allow flow through the grab sampling device.	A local grab sample is successfully obtained.
xi.	Verify SRWS dewatering skid effluent can be transferred to LRW high-conductivity waste (HCW) collection tanks.	Align SRWS dewatering skid discharge to one of the LRW high-conductivity waste collection tanks. Fill the SRWS dewatering skid high integrity container (HIC) to above the low level pump stop setpoint. Start the SRWS dewatering skid diaphragm pump.	SRWS dewatering skid effluent is transferred to the LRW high-conductivity waste collection tank. The SRWS dewatering skid diaphragm pump is stopped.
xii.		Initiate a single real or simulated instrument signal from each LRWS transmitter.	 i. The instrument signal is displayed on an MCR workstation or recorded by the applicable control system historian. ii. The instrument signal is displayed on an RSS workstation or recorded by the applicable control system historian if the instrument signal is designed to be displayed in the RSS. iii. The instrument signal is displayed on an MCR module-specific safety display instrument monitor or an MCR common safety display instrument monitor if the instrument signal is designed to be displayed on a safety display instrument monitor.

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Table 14.2-35: Liquid Radioactive Waste System Test # 35 (Continued)

System Level Test #35-1				
Test Objective	Test Method	Acceptance Criteria		
i. Verify LRWS can process a gaseous waste stream.	Align LRWS to receive pressurizer gaseous waste from the pressurizer during plant startup.	i. The LRW degasifier removes condensable gases and vents waste to the RBVS or GRWS.		
	Process the pressurizer gaseous waste through the LRW degasifier.	ii. The LRW degasifier liquid transfer pumps transfer the liquid condensate waste to the low conductivity waste collection tanks.		
System Level Test #35-2				
Test Objective	Test Method	Acceptance Criteria		
i. Verify LRWS can process a liquid waste stream.	 Align LRWS to receive liquid waste from a liquid waste stream. i. Process the liquid waste stream through the low-conductivity waste (LCW) waste process. ii. Process the liquid waste stream through the HCW process. 	The waste treatment streams are successfully processed through the following processes: • filtration • tubular filtration skid • LCW processing skid • HCW processing skid • demineralization • transfer to LCW or HCW sample tanks • transfer from LCW or HCW sample tanks to the UWS discharge basin.		

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Table 14.2-36: Gaseous Radioactive Waste System Test # 36

Preoperational test is required to be performed once.			
The GRWS is described in Section 11.3 and 11.5.2.2.6 and the functions verified by this test are:			
•		System Function Categorization	Function Verified by Test #
1.	The GRWS supports the LRWS by receiving and / or collecting potentially radioactive and hydrogen-bearing waste gases which require processing prior to release to the environment.	nonsafety-related	Test #36-1
	The GRWS supports the CES by receiving and / or collecting potentially radioactive and hydrogen-bearing waste gases which require processing prior to release to the environment.	nonsafety-related	Test #36-1
Pr	erequisites		
		completed, with approved records and wi	thin all calibration due dates, for all
	struments required to perform this test.		
	omponent Level Tests		T
	st Objective	Test Method	Acceptance Criteria
i.	Verify each GRWS remotely-operated valve can be operated remotely.	Operate each valve from the (main control room) MCR and local control panel (if design has local valve control).	MCR display and local, visual observation indicate each valve fully opens and fully closes.
ii.	Verify each GRWS air-operated valve fails to its safe position on loss of air.	Place each valve in its non-safe position. Isolate and vent air to the valve.	MCR display and local, visual observation indicate each valve fails to its safe position.
	Verify each GRWS air-operated valve fails to its safe position on loss of electrical power to its solenoid. Verify GRWS valves automatically operate to maintain vessel volume.	Isolate electrical power to each air- operated valve. i. Initiate a real or simulated high GRWS moisture separator level.	MCR display and local, visual observation indicate each valve fails to its safe position. MCR display and local, visual observation indicate the following: i. The moisture separator drain valve open. ii. The moisture separator drain valve closed.
v.	Verify GRWS inlet isolation valves automatically close and nitrogen purge valve opens on high inlet stream oxygen concentration.	Simulate a GRWS inlet stream oxygen concentration high signal.	MCR display and local, visual observation indicate the following: i. The inlet stream isolation valves are closed. ii. The nitrogen purge valve is open.
	Verify GRWS isolates upon loss of RWBV exhaust flow.	Simulate a loss of RWBVS exhaust flow.	MCR display and local, visual observation indicate the GRWS isolation valves are closed.
viii	. Verify radiation isolation of GRWS charcoal decay beds upon detection of decay bed discharge flow high radiation level.	 i. Initiate a real or simulated GRWS train A decay bed discharge flow high radiation signal. ii. Initiate a real or simulated GRWS train B decay bed discharge flow high radiation signal. 	MCR display and local, visual observation indicate the following: i. GRWS train A charcoal decay bed discharge isolation valve is closed. [ITAAC 03.09.04] ii. GRWS train B charcoal decay bed discharge isolation valve is closed.

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[ITAAC 03.09.05]

Table 14.2-36: Gaseous Radioactive Waste System Test # 36 (Continued)

viii. Verify radiation isolation of GRWS discharge to the RWBVS exhaust upon detection of a high radiation level. ix. Verify a local grab sample can be obtained from a GRWS grab sample device indicated on the GRWS piping and instrumentation diagram.	Initiate a real or simulated GRWS discharge to the RWBVS exhaust high radiation signal. Place the system in service to allow flow through the grab sampling device.	MCR display and local, visual observation indicate the GRWS discharge to the RWBVS exhaust isolation valves are closed. [ITAAC 03.09.06] A local grab sample is successfully obtained.
x. Verify each GRWS instrument is monitored in the MCR and the RSS, if the signal is designed to be displayed in the RSS. (Test not required if the instrument calibration verified the MCR and RSS display)	Initiate a single real or simulated instrument signal from each GRWS transmitter.	 i. The instrument signal is displayed on an MCR workstation or recorded by the applicable control system historian. ii. The instrument signal is displayed on an RSS workstation or recorded by the applicable control system historian if the instrument signal is designed to be displayed in the RSS. iii. The instrument signal is displayed on an MCR module-specific safety display instrument monitor or an MCR common safety display instrument monitor if the instrument signal is designed to be displayed on a safety display instrument monitor.
System Level Test #36-1 Test Objective	Test Method	Acceptance Criteria
Verify GRWS can process a gaseous waste stream.	Align GRWS to receive gaseous waste from a gaseous waste stream. Process the gaseous waste stream through the gaseous waste process.	The gaseous waste stream is successfully processed through the following processes: gas cooler moisture separator charcoal drying heater charcoal guard bed
		charcoal decay beds RWB exhaust

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Table 14.2-37: Solid Radioactive Waste System Test # 37

Preoperational test is required to be performed once.			
The SRWS is described in Section 11.4 and the functions verified by this test are:			
System Function	System Function Categorization	Function Verified by Test #	
1. The SRWS supports the LRWS by	nonsafety-related	Test #37-1	
receiving spent resin and carbon bed	d	Test #37-4	
from LRW processing skids.		Test #37-6	
		Test #37-7	
2. The SRWS supports the CVCS by	nonsafety-related	Test #37-2	
receiving spent resin from CVCS ion		Test #37-5	
exchange vessels.		Test #37-7	
3. The SRWS supports the PCUS by	nonsafety-related	Test #37-3	
receiving spent resin and sludge		Test #37-5	
from PCUS ion exchange vessels.		Test #37-7	
4. The SRWS supports the CRVS by	nonsafety-related	Test #37-8	
receiving exhausted HEPA filters to			
be compacted and shipped off site.			
5. The SRWS supports the RWBVS by	nonsafety-related	Test #37-8	
receiving exhausted HEPA filters to			
be compacted and shipped off site.			
6. The SRWS supports the RBVS by	nonsafety-related	Test #37-8	
receiving exhausted HEPA filters and	!		
charcoal bed from RXB and normal			
control room HVAC, to be compacted	d		
and shipped off site.			

Prerequisites

Verify an instrument calibration has been completed, with approved records and within all calibration due dates, for all instruments required to perform this test.

Component Level Tests

Te	st Objective	Test Method	Acceptance Criteria
i.	Verify each SRWS remotely-operated	Operate each valve from the MCR and	MCR display and local, visual
	valve can be operated remotely.	local control panel (if design has local	observation indicate each valve fully
		valve control).	opens and fully closes.
ii.	Verify each SRWS air-operated valve	Place each valve in its non-safe position.	MCR display and local, visual
	fails to its safe position on loss of air.	Isolate and vent air to the valve.	observation indicate each valve fails to
			its safe position.
iii.	Verify each SRWS air-operated valve	Place each valve in its non-safe position.	MCR display and local, visual
	fails to its safe position on loss of	Isolate electrical power to each air-	observation indicate each valve fails to
	electrical power to its solenoid.	operated valve.	its safe position.
iv.	Verify each SRWS pump can be	Align the SRWS to allow for pump	MCR display and local, visual
	started and stopped remotely.	operation.	observation indicate each pump starts
		Stop and start each pump from the MCR.	and stops.
			Audible and visible water hammer are
			not observed when the pump starts.
٧.	Verify the speed of each SRWS	Align the SRWS to provide a flow path to	MCR display indicates the speed of each
	variable-speed pump can be	operate a selected pump.	obtains both minimum and maximum
	manually controlled.	Vary the SRWS pump speed from	pump speeds.
		minimum to maximum from the MCR.	Audible and visible water hammer are
			not observed when the pump starts.
vi.	Verify each SRWS transfer pump	Align the SRWS to allow for transfer	MCR display and local, visual
	automatically stops to protect the	pump operation. Place a transfer pump	observation indicate each transfer pump
	pump.	in service. Initiate a simulated tank low	stopped.
		level signal.	

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Table 14.2-37: Solid Radioactive Waste System Test # 37 (Continued)

vii. Verify a local grab sample can be obtained from a SRWS grab sample device indicated on the SRWS piping and instrumentation diagram.	Place the system in service to allow flow through the grab sampling device.	A local grab sample is successfully obtained.			
viii. Verify each SRWS instrument is monitored in the MCR and the RSS, if the signal is designed to be displayed in the RSS. (Test not required if the instrument calibration verified the MCR and RSS display).	Initiate a single real or simulated instrument signal from each SRWS transmitter.	 i. The instrument signal is displayed on an MCR workstation or recorded by the applicable control system historian. ii. The instrument signal is displayed on an RSS workstation or recorded by the applicable control system historian if the instrument signal is designed to be displayed in the RSS. iii. The instrument signal is displayed on an MCR module-specific safety display instrument monitor or an MCR common safety display instrument monitor if the instrument signal is designed to be displayed on a safety display instrument monitor. 			
· ·	System Level Test #37-1				
Test Objective	Test Method	Acceptance Criteria			
Verify spent resin from the LRWS demineralizers can be transferred to the SRWS phase separator tanks.	Align the LRWS and SRWSs to transfer LRWS demineralizer resin to a SRWS phase separator tank. Start a phase separator transfer pump.	The waste management control room (WMCR) displays and local, visual observation verifies LRWS demineralizer resins transferred to a SRWS phase separator tank.			
System Level Test #37-2					
Test Objective	Test Method	Acceptance Criteria			
Verify spent resin from the CVCS ion exchangers can be transferred to the SRWS spent resin storage tanks.	Align the CVCS and SRWSs to transfer CVCS ion exchanger resin to a SRWS spent resin storage tank. Start a SRWS spent resin storage tank transfer pump.	WMCR displays and local, visual observation verifies CVCS ion exchanger resin transferred to a SRWS spent resin storage tank.			
System Level Test #37-3					
Test Objective	Test Method	Acceptance Criteria			
Verify spent resin from the PCUS demineralizers can be transferred to the SRWS spent resin storage tanks.	Align the PCUS and SRWSs to transfer PCUS demineralizer resin to a SRWS spent resin storage tank. Start a SRWS spent resin storage tank transfer pump.	WMCR displays and local, visual observation verifies PCUS demineralizer resins transferred to a SRWS spent resin storage tank.			
System Level Test #37-4	T				
Test Objective	Test Method	Acceptance Criteria			
Verify spent resin from the SRWS phase separator tanks can be transferred to a dewatering station HIC.	Align a SRW phase separator tank and the SRW dewatering station to transfer spent resin to the dewatering station HIC using service air (SA).	WMCR displays and local, visual observation verifies phase separator tank resins are transferred to a dewatering station HIC.			
	Open SA isolation valve to the SRW phase separator tank.				

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Table 14.2-37: Solid Radioactive Waste System Test # 37 (Continued)

System Level Test #37-5			
Test Objective	Test Method	Acceptance Criteria	
Verify spent resin from the SRW spent	Align an SRWS spent resin storage tank	WMCR displays and local, visual	
resin storage tanks can be transferred to	and the SRWS dewatering station to	observation verifies spent resin storage	
a dewatering station HIC.	transfer spent resin to the dewatering	tank resins are transferred to a	
	station HIC using service air.	dewatering station HIC.	
	Open service air isolation valve to the		
	spent resin storage tank.		
System Level Test #37-6			
Test Objective	Test Method	Acceptance Criteria	
Verify granulated activated charcoal from	Align a LRWS and SRWSs to granulated	WMCR displays and local, visual	
the LRW granulated activated charcoal	activated charcoal to the dewatering	observation verifies spent resin storage	
filter can be transferred to a dewatering	station HIC using the clean in place	tank resins are transferred to a	
station HIC.	system.	dewatering station HIC.	
System Level Test #37-7		•	
Test Objective	Test Method	Acceptance Criteria	
Verify the dewatering skid pump	Align the dewatering skid pump to a	Free-standing water in the HIC has been	
removes standing water in the HIC with	LRWS high conductivity waste tank and	removed.	
spent resin in the dewatering station HIC.	start the dewatering skid pump.		
System Level Test #37-8	•		
Test Method	Acceptance Criteria		
Verify the SRWS waste compactor	Place solid radioactive waste in	The waste has been compacted.	
compacts solid radioactive waste.	compactor and start compactor.		

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Table 14.2-38: Chemical and Volume Control System Test # 38

Preoperational test is required to be performed for each NPM. The CVCS is described in Section 9.3.4 and 11.5.2.2.11 and the functions verified by this test are:			
nonsafety-related	Test #38-1		
nonsafety-related	Test #38-1		
nonsafety-related	Test #38-2		
nonsafety-related	Test #38-3		
nonsafety-related	Test #38-3		
nonsafety-related	Test #38-1		
ests are:	<u> </u>		
nonsafety-related	MPS Test #63-12		
nonsafety-related	TG Test #33-1		
safety-related	MPS Test #63-6		
	and 11.5.2.2.11 and the functions ver System Function Categorization nonsafety-related nonsafety-related nonsafety-related nonsafety-related nonsafety-related ests are: nonsafety-related nonsafety-related		

Prerequisites

- Verify an instrument calibration has been completed, with approved records and within all calibration due dates, for all instruments required to perform this test.
- ii. Verify a pump curve test has been completed and approved for the CVCS pumps.

Component Level Tests Test Objective Test Method Acceptance Criteria Verify each CVCS remotely-operated Operate each valve from the MCR and MCR display and local, visual local control panel (if design has local observation indicate each valve fully valve can be operated remotely. valve control). opens and fully closes. Verify each CVCS air-operated valve Place each valve in its non-safe position. MCR display and local, visual observation indicate each valve fails to fails to its safe position on loss of Isolate electrical power to each airelectrical power to its solenoid. operated valve. its safe position. iii. Verify each CVCS ASME Code Class 3 Operate each valve from the MCR. MCR display verifies the valve opens and air-operated valve changes position closes under preoperational under preoperational temperature, temperature, differential pressure, and differential pressure, and flow flow conditions. conditions. [ITAAC 02.02.03] iv. Verify each CVCS ASME Code Class 3 MCR display and local, visual Place each valve in its non-safe position. air-operated valve fails to its safe Isolate and vent air to the valve. observation indicate each valve fails to position on loss of air under its safe position under preoperational preoperational temperature, temperature, differential pressure, and differential pressure, and flow flow conditions. conditions. [ITAAC 02.02.05]

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Table 14.2-38: Chemical and Volume Control System Test # 38 (Continued)

V.	air-operated valve fails to its safe position on loss of electrical power to its solenoid under preoperational temperature, differential pressure, and flow conditions.	Isolate electrical power to the valve.	MCR display and local, visual observation indicate each valve fails to its safe position under preoperational temperature, differential pressure, and flow conditions. [ITAAC 02.02.05]
vi.	Verify each CVCS ASME Code Class check valve will fully close under preoperational temperature, differential pressure and flow conditions.	The check valves are tested in accordance with the requirements of ASME OM Code, ISTC-5220, Check Valves.	Each CVCS ASME Code Class check valve strokes fully open and closed under forward and reverse flow conditions, respectively. [ITAAC 02.02.04]
vii.	Verify the speed of each CVCS variable-speed pump can be manually controlled.	operate a selected pump.	MCR display indicates the speed of each obtains both minimum and maximum pump speeds. Audible and visible water hammer are not observed when the pump starts.
	Verify each CVCS operating makeup pump automatically stops to protect the pump and the standby pump starts.	Align the CVCS to allow for pump operation. Place a makeup pump in service. Initiate a simulated signal for the following system conditions. i. Pump low suction pressure. ii. Pump high discharge pressure. iii. Makeup filter high differential pressure.	MCR display and local, visual observation indicate the operating pump stops and the standby pump starts. Audible and visible water hammer are not observed when the pump starts.
ix.	Verify each CVCS recirculation pump automatically stops to protect the pump and the standby pump starts.	Align the CVCS to allow for pump operation. Place a recirculation pump in service. Initiate a simulated signal for the following system conditions. i. Pump low suction pressure. ii. Pump discharge high flow. iii. High pump discharge pressure.	MCR display and local, visual observation indicate the following: i. Operating pump stops and the standby pump starts. ii. Operating pump stops and the standby pump starts. iii. Operating pump stops. Audible and visible water hammer are not observed when the pump starts.
x.	high flow to protect plant equipment.	Initiate a simulated CVCS high letdown flow signal.	MCR display and local, visual observation indicate the following: LRWS letdown flow control valve and LRWS letdown isolation valves (3) are closed.
	isolates on low injection pressure to protect plant equipment.	Initiate a simulated CVCS low hydrogen injection pressure signal.	MCR display and local, visual observation indicate the following: CVCS hydrogen injection pressure regulating valve and hydrogen injection isolation valve are closed.
xii.	Verify ion exchanger isolation on non-regenerative heat exchanger high outlet temperature to protect plant equipment.	Initiate a simulated high non- regenerative heat exchanger outlet temperature signal.	MCR display and local, visual observation indicate the following: i. CVCS purification bypass diverting valve is in the bypass position. ii. Mixed bed ion exchanger A inlet isolation valves (2) are closed. iii. Auxiliary ion exchanger inlet isolation valve is closed. iv. Cation exchanger inlet isolation valve is closed.

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Table 14.2-38: Chemical and Volume Control System Test # 38 (Continued)

xiii. Verify the CVCS automatically responds to mitigate a release of radioactivity. xiv. Verify the CVCS automatically responds to mitigate a release of radioactivity.	Initiate a real or simulated high radiation signal for the auxiliary boiler steam flow to the 6A MHS heat exchanger. Initiate a real or simulated high radiation signal for the auxiliary boiler steam flow to the 6B MHS heat exchanger.	i. CVCS module heatup system 6A heat exchanger inlet and outlet isolation valves are closed. [This component-level test is required to be performed once for each CVCS associated with the MHS 6A heat exchanger.] [ITAAC 02.07.03] MCR display verifies the following: i. CVCS module heatup system 6B heat exchanger inlet and outlet isolation valves are closed. [This component-level test is required to be performed once for each CVCS associated with the MHS 6B heat exchanger.]
xv. Verify the CVCS automatically responds to mitigate a release of radioactivity.	Initiate a real or simulated high radiation signal for the RCS discharge flow to the regenerative heat exchanger.	[ITAAC 02.07.04] MCR display verifies the following: i. chemical and volume control RCS discharge to process sampling isolation valve closed. [This component-level test is required to be performed once for each CVCS.]
the signal is designed to be displayed in the RSS. (Test not required if the instrument calibration verified the MCR and RSS display)	Initiate a single real or simulated instrument signal from each CVCS transmitter.	 [ITAAC 02.07.02] i. The instrument signal is displayed on an MCR workstation or recorded by the applicable control system historian. ii. The instrument signal is displayed on an RSS workstation or recorded by the applicable control system historian if the instrument signal is designed to be displayed in the RSS. iii. The instrument signal is displayed on an MCR module-specific safety display instrument monitor or an MCR common safety display instrument monitor if the instrument signal is designed to be displayed on a safety display instrument monitor.
System Level Test #38-1 Test Objective Verify proper operation of the automatic pressurizer level control.	Test Method This test will be performed in conjunction with turbine generator test #33-1, which heats the RCS from ambient conditions to no less than 425°F but as high as reasonably achievable. Use the module control system (MCS) data historian to review pressurizer level at maximum-obtained RCS temperature.	Acceptance Criteria MCS data indicates that automatic pressurizer level control is maintained within the design operating level band.

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Table 14.2-38: Chemical and Volume Control System Test # 38 (Continued)

System Level Test #38-2				
Test Objective	Test Method	Acceptance Criteria		
Verify proper operation of the automatic pressurizer pressure control.	This test will be performed in conjunction with turbine generator test #33-1 which heats the RCS from ambient conditions to no less than 425°F but as high as reasonably achievable. Use the MCS data historian to review pressurizer pressure at maximumobtained RCS temperature.	MCS data indicates that automatic pressurizer pressure control is maintained within the design operatin pressure band.		
System Level Test #38-3				
Test Objective	Test Method	Acceptance Criteria		
Verify proper operation of CVCS automatic dilution and boration control.	This test will be performed in conjunction with turbine generator test #33-1 which heats the RCS from ambient conditions to no less than 425°F but as high as reasonably achievable. Ensure that RCS low flow rate alarm is clear to ensure adequate mixing for dilution and boration. i. Use the MCS automation and operator permission to decrease to a target RCS boron concentration. ii. Use the MCS and operator permission to increase to a target RCS boron concentration.	 i. MCS data indicates that the dilution of the RCS results in a decreased boron concentration within acceptable limits of the target concentration. ii. MCS data indicates that the boratio of the RCS results in a increased boron concentration within acceptable limits of the target concentration. 		
System Level Test #38-4				
Test Objective	Test Method	Acceptance Criteria		
Verify the CVCS can provide borated water to the RCS during a beyond design basis accident.	Refer to Test #63-11	Refer to Test #63-11		

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Table 14.2-39: Boron Addition System Test # 39

Preoperational test is required to be performed for each NPM.									
The boron addition system (BAS) is described in Section 9.3.4. The BAS function verified by this test is:									
System Function									
The BAS supports the SFPCS by providing borated water to the RXB pools.	nonsafety-related	component-level test xii							
The BAS function verified by other test	is:								
System Function	System Function Categorization	Function Verified by Test #							
The BAS supports the CVCS by providing uniformly mixed borated water on demand.	nonsafety-related	CVC Test #38-3							

Prerequisites

i. Verify an instrument calibration has been completed, with approved records and within all calibration due dates, for all instruments required to perform this test.

ii.	Verify a pump curve test has been con	mpleted and approved for the BAS pumps			
	mponent Level Tests				
Te	st Objective	Test Method	Acceptance Criteria		
i. ii.	Verify each BAS remotely-operated valve can be operated remotely. Verify each BAS air-operated valve	MCR display and local, visual observation indicate each valve fully opens and fully closes. MCR display and local, visual			
	fails to its safe position on loss of air.	Isolate and vent air to the valve.	observation indicate each valve fails to its safe position.		
	Verify each BAS air-operated valve fails to its safe position on loss of electrical power to its solenoid.	Place each valve in its non-safe position. Isolate electrical power to each air- operated valve.	MCR display and local, visual observation indicate each valve fails to its safe position.		
	Verify the BAS transfer pump can be started and stopped remotely.	Align the BAS to allow for pump operation. Stop and start the transfer pump from the MCR.	MCR display and local, visual observation indicate the pump starts and stops. Audible and visible water hammer are not observed when the pump starts.		
v.	Verify the speed of the BAS variable- speed pumps can be manually controlled.	Align the BAS to provide a flow path to operate a selected pump. Vary the BAS pump speed from minimum to maximum from the MCR.	MCR display indicates the speed of eac pump obtains both minimum and maximum pump speeds. Audible and visible water hammer are not observed when the pump starts.		
vi.	Verify BAS valves automatically operate to protect plant equipment.	 i. Initiate a real or simulated high BAS batch tank level signal. ii. Initiate a real or simulated high BAS storage tank level signal. 	MCR display and local, visual observation indicate the following: i. The batch tank fill and return valves are fully closed. ii. The storage tank fill and recirculation valves are fully closed.		
vii.	Verify the BAS transfer pump stops automatically to protect plant equipment.	Align the BAS to allow for pump operation. i. Place the BAS transfer pump in service on recirculation to the BAS batch tank. Initiate a simulated a low batch tank level signal. ii. Place the BAS transfer pump in service on recirculation to the BAS storage tank. Simulate a low storage tank level signal.	MCR display and local, visual observation indicate the following: i. The transfer pump stops. ii. The transfer pump stops.		

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Table 14.2-39: Boron Addition System Test # 39 (Continued)

viii	Verify BAS supply pumps stop automatically to protect plant	Align the BAS to allow for pump operation.	MCR display and local, visual observation indicate the following:
	equipment.	 Place a BAS supply pump in service on recirculation to the BAS batch bank. Initiate a simulated a low batch tank level signal. 	i. The supply pump stops. ii. The supply pump stops.
		ii. Place a supply pump in service on recirculation to the BAS storage tank. Initiate a simulated low storage tank level signal.	
ix.	Verify BAS flow capability by	Align the BAS to allow for pump	MCR display and local, visual
	automatic start of each BAS supply pump while in standby mode.	operation. Place a supply pump in service. Initiate a simulated low pump	observation indicate the standby pump starts.
	parity write in standay mode.	discharge pressure signal.	Audible and visible water hammer are
			not observed when the pump starts.
x.	Verify supply pump low flow	Align the BAS to allow a BAS supply	MCR displays and local, visual
	protection.	pump flow sufficient to close the pump	observation verifies the following:
		recirculation valve to the storage tank. i. Manually throttle a valve in the pump	 The pump recirculation valve is open.
		flow path until the flow rate reaches	ii. The pump recirculation valve is
		the pump minimum flow setpoint.	closed.
		ii. Open the throttled valve	
xi.	Verify a local grab sample can be obtained from a BAS grab sample	Place the system in service to allow flow through the grab sampling device.	A local grab sample is successfully obtained.
vii	device. Verify the BAS automatically adds a	i. Verify the BAS batch tank contains a	MCR displays and local, visual
ļ	specified quantity of borated water	sufficient volume of water to conduct	
	from the BAS batch tank to the RXB	this test.	i. The BAS to SFPCS valve initially
	pools.	ii. Align the BAS and the SFPCS to supply water from the BAS to the	opens to supply water from the BAS to the SFPCS pump suction.
		SFPCS pump suction.	ii. The BAS to SFPCS valve
		 Enter a BAS batch tank target level to terminate batch operation to the spent fuel pool. 	automatically closes when the BAS batch tank obtains the target level.
xiii.	Verify each BAS instrument is	Initiate a single real or simulated	i. The instrument signal is displayed
		instrument signal from each BAS transmitter.	on an MCR workstation or recorded by the applicable control system historian.
	(Test not required if the instrument		ii. The instrument signal is displayed
	calibration verified the MCR and RSS		on an RSS workstation or recorded
	display)		by the applicable control system historian if the instrument signal is
			designed to be displayed in the RSS.
			iii. The instrument signal is displayed
			on an MCR module-specific safety
			display instrument monitor or an MCR common safety display
			instrument monitor if the
			instrument signal is designed to be
			displayed on a safety display instrument monitor.
Sys	stem Level Tests		matument monitor.
No			

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Table 14.2-40: Module Heatup System Test # 40

Preoperational test is required to be performed for each NPM.							
The MHS is described in Section 9.3.4.2	2. MHS functions are not verified by N	NHS tests. MHS functions verified by other					
tests are:							
System Function	System Function Categorization	Function Verified by Test #					
The MHS supports the CVCS by adding	nonsafety-related	TG Test #33-1					
heat to primary coolant.							
Prerequisites							
Prerequisites associated with MHS testing	g are identified in the referenced test al	bstract cited under the "Function Verified by					
Test #" heading.	_	·					
Component Level Tests							
None							
System Level Tests							
None							

Table 14.2-41: Containment Evacuation System Test # 41

Preoperational test is required to be performed for each NPM.							
The CES is described in Sections 9.3.6, 11.5.2.2.7 and 5.2.5 and the functions verified by this test are:							
System Function	System Function Categorizat	ion Function Verified by Test #					
The CES supports the CN removing water vapor frocontainment vessel (CNV)	om the	Test #41-1 Test #41-2 Test #41-3					
The CES supports the CN condensing water vapor from the CNV in the cont evacuation condenser.	removed	Test #41-1 Test #41-2 Test #41-3					
The CES supports the CN removing non-condensa from the CNV.	· · · · · · · · · · · · · · · · · · ·	Test #41-1 Test #41-2 Test #41-3					
 The CES supports the MC providing a radioactivity 		Test #41-2					
The CES supports the RC providing RCS leak detec monitoring capability.	•	Test #41-3					

Prerequisites

Verify an instrument calibration has been completed, with approved records and within all calibration due dates, for all instruments required to perform this test.

								_
Component Level 1	l ests	/el l	Lev	ent	on	mn	റ	•

Tor	st Objective	Test Method	Accontance Criteria
res	-		Acceptance Criteria
i.	Verify each CES remotely-operated	Operate each valve from the MCR and	MCR display and local, visual
	valve can be operated remotely.	local control panel (if design has local	observation indicate each valve fully
		valve control).	opens and fully closes.
ii.	Verify each CES air-operated valve	Place each CES valve in its non-safe	MCR display and local, visual
	fails to its safe position on loss of air.	position. Isolate and vent air to the valve.	observation indicate each valve fails to
			its safe position.
iii.	Verify each CES air-operated valve	Place each CES valve in its non-safe	MCR display and local, visual
	fails to its safe position on loss of	position. Isolate electrical power to each	observation indicate each valve fails to
	electrical power to its solenoid.	CES air-operated valve.	its safe position.
iv.	Verify each CES pump can be started	Stop and start each pump from the MCR.	MCR display and local, visual
	and stopped remotely.		observation indicate each pump starts
			and stops.
٧.	Verify the speed of each CES variable-	Vary the speed of each pump from the	MCR display indicates pump speed
	speed pump can be manually	MCR and local control panel (if design	varies from minimum to maximum
	controlled.	has local pump control).	speed.
vi.	Verify each CES pump automatically	Place a pump in operation. Initiate a real	MCR displays and local, visual
	stops to protect plant equipment.	or simulated signal for each pump trip	observation verifies the pump stops.
		condition.	
vii.	Verify each CES pump suction and	Open the pump suction and discharge	Each pump suction and discharge valve
		valves.	closes on each real or simulated valve
	to protect the CES equipment.	Initiate a real or simulated signal for each	close condition.
		valve close conditions.	
viii.	Verify a local grab sample can be	Place the system in service to allow flow	A local grab sample is successfully
	obtained from a CES grab sample	through the grab sampling device.	lobtained.
	device indicated on the CES piping	acvice.	
	and instrumentation diagram.		

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Table 14.2-41: Containment Evacuation System Test # 41 (Continued)

	Initiate a single real or simulated instrument signal from each CES transmitter.	i. The instrument signal is displayed on an MCR workstation or recorded by the applicable control system historian.
(Test not required if the instrument calibration verified the MCR and RSS display)		ii. The instrument signal is displayed on an RSS workstation or recorded by the applicable control system historian if the instrument signal is designed to be displayed in the RSS.
		iii. The instrument signal is displayed on an MCR module-specific safety display instrument monitor or an MCR common safety display instrument monitor if the instrument signal is designed to be displayed on a safety display instrument monitor.
System Level Test #41-1		
Test Objective	Test Method	Acceptance Criteria
Verify the automatic operation of the CES to establish and maintain design vacuum for the CNV.	3	The automated control establishes and maintains vacuum in the CNV.
System Level Test #41-2		
Test Objective	Test Method	Acceptance Criteria
Verify radiation isolation and flow diversion on high radiation level in the CES.	The reactor module is in hot functional testing with the RCS at normal operating pressure. The CES is operating in automatic control with a CNV steady-state vacuum pressure indicating the noncondensable gases have been	 i. The CES effluent flow path to the RBVS is isolated and diverted to GRWS. [ITAAC 02.07.01] ii. The CES effluent to process sample
	removed from the CNV. Initiate a real or simulated high radiation signal for the CES vacuum pump discharge.	panel isolation valve is closed. [ITAAC 02.07.01]
		iii. The CES purge air solenoid valves to the vacuum pumps are closed. [ITAAC 02.07.01]

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Table 14.2-41: Containment Evacuation System Test # 41 (Continued)

Test Objective Test Method i. Verify the CES level instrumentation i. The reactor module is in hot	Acceptance Criteria
i. Verify the CES level instrumentation ii. The reactor module is in hot	
supports RCS leakage detection. ii. Verify the CES pressure instrumentation supports RCS leakage detection. functional testing with the RCS at normal operating pressure and the maximum operating temperature achievable by heating the RCS with the MHS. ii. The CES is operating in automatic control with a CNV steady-state vacuum pressure indicating the noncondensable gasses have been removed from the CNV. iii. Record the MCS baseline leakage rate into the CNV. iv. Isolate the CFDS to CNTS spool piece to allow test equipment to be connected to the spool piece. v. Inject water at a flow rate less than or equal to one gpm. This test may be done in conjunction Test #41-2.	 i. The CES detects a level increase in the CES sample tank, which correlates to a detection of an unidentified RCS leakage rate of one gpm within one hour, by providing an alarm signal to the MCR within one hour of the start of water injection into the CNV indicating the baseline leakage rate has been exceeded. [ITAAC 02.03.01] ii. The CES detects a pressure increase in the sample vessel inlet pressure instrumentation that correlates to a detection of an unidentified RCS leakage rate of one gpm within one hour, by providing an alarm signal to the MCR within one hour of the start of water injection into the CNV indicating the baseline leakage rate has been exceeded. [ITAAC 02.03.02]

Table 14.2-42: Containment Flooding and Drain System System Test # 42

Preoperational test component level testing is required to be performed for the 6A CFDS and for the 6B CFDS. System level testing is required to be performed as indicated for each system level test.

The 0	CFDS	is de	scribed	in Se	ction 9.	3.6 and	11.	5.2.2.9	and t	he funct	ions ver	ified l	by this test are:	
-------	------	-------	---------	-------	----------	---------	-----	---------	-------	----------	----------	---------	-------------------	--

Sy	stem Function	System Function Categorization	Function Verified by Test #
1.	The CFDS supports the CNTS by flooding the CNV in preparation for refueling operations.	nonsafety-related	Test #42-1
2.	The CFDS supports the CNTS by draining the CNV in preparation for startup operations.	nonsafety-related	Test #42-2
3.	The CFDS supports the RCS by providing borated coolant inventory for the removal of core heat during a beyond design basis accident.	nonsafety-related	Test #42-3

Prerequisites

Verify an instrument calibration has been completed, with approved records and within all calibration due dates, for all instruments required to perform this test.

Co	mponent Level Tests				
Te	st Objective	Test Method	Acceptance Criteria		
i.	Verify each CFDS remotely-operated valve can be operated remotely.	Operate each valve from the MCR and local control panel (if design has local valve control).	MCR display and local, visual observation indicate each valve fully opens and fully closes.		
ii.	Verify each CFDS air-operated valve fails to its safe position on loss of air.	Place each CFDS valve in its non-safe position. Isolate and vent air to the valve.	MCR display and local, visual observation indicate each valve fails to its safe position.		
iii.	Verify each CFDS air-operated valve fails to its safe position on loss of electrical power to its solenoid.	Place each CFDS valve in its non-safe position. Isolate electrical power to each CFDS air-operated valve.	MCR display and local, visual observation indicate each valve fails to its safe position.		
iv.	Verify each CFDS pump can be started and stopped remotely.	Stop and start each pump from the MCR.	MCR display and local, visual observation indicate each pump starts and stops.		
	Verify each CFDS pump automatically stops to protect plant equipment.	Place a pump in operation. Initiate a real or simulated signal for each pump trip condition.	MCR displays and local, visual observation verifies the pump stops.		
vi.	Verify each CFDS instrument is monitored in the MCR and the RSS, if the signal is designed to be displayed in the RSS.	Initiate a single real or simulated instrument signal from each CFDS transmitter.	 The instrument signal is displayed on an MCR workstation or recorded by the applicable control system historian. 		
	(Test not required if the instrument calibration verified the MCR and RSS display.)		ii. The instrument signal is displayed on an RSS workstation or recorded by the applicable control system historian if the instrument signal is designed to be displayed in the RSS		
			iii. The instrument signal is displayed on an MCR module-specific safety display instrument monitor or an MCR common safety display instrument monitor if the instrument signal is designed to be displayed on a safety display instrument monitor.		

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Table 14.2-42: Containment Flooding and Drain System System Test # 42 (Continued)

System Level Test #42-1				
Test Objective	Test Method	Acceptance Criteria		
Verify the CFDS can automatically drain	Drain the CNTS using CFDS automatic	The CNTS is drained using CFDS		
the CNTS.	operation and designed manual	automatic controls.		
	operation.	(This test is required to be performed for each NPM.)		
System Level Test #42-2				
Test Objective	Test Method	Acceptance Criteria		
Verify the CFDS can automatically flood the CNTS.	Drain the CNTS using CFDS automatic operation and designed manual	The CNTS is flooded using CFDS automatic controls.		
	operation.	(This test is required to be performed for each NPM.)		
System Level Test #42-3				
Test Objective	Test Method	Acceptance Criteria		
Verify the CFDS can provide borated	Refer to Test #63-11	Refer to Test #63-11		
water to the containment during a				
beyond design basis accident.				
System Level Test #42-4				
Test Objective	Test Method	Acceptance Criteria		
Verify the 6A CFDS automatically	While the 6A CFDS is draining the CNTS	The 6A CFDS containment drain		
responds to mitigate a release of	initiate a real or simulated high radiation	separator gaseous discharge to RBVS		
radioactivity.	signal on the gaseous effluent of the 6A	isolation valve is closed.		
	CFDS containment drain separator tank.	[ITAAC 03.17.01]		
System Level Test #42-5				
Test Objective	Test Method	Acceptance Criteria		
Verify the 6B CFDS automatically	While the 6B CFDS is draining the CNTS	The 6B CFDS containment drain		
responds to mitigate a release of	initiate a real or simulated high radiation	separator gaseous discharge to RBVS		
radioactivity.	signal on the gaseous effluent of the 6B	isolation valve is closed.		
	CFDS containment drain separator tank.	[ITAAC 03.18.01]		

Table 14.2-43: Containment System Test # 43

Preoperational test is required to be pe The CNTS is described in Section 6.2 and		
	System Function Categorization	Function Verified by Test #
The CNTS supports the RXB by providing a barrier to contain mass, energy, and fission product release from a degradation of the reactor coolant pressure boundary.	safety-related	Test #43-1
The CNTS supports the ECCS operations by providing a sealed containment.	safety-related	Test #43-1
The CNTS functions verified by other te		
	System Function Categorization	Function Verified by Test #
The CNTS supports the DHRS by closing containment isolation valves (CIVs) for the main steam and feedwater systems when actuated by the MPS for DHRS operation.	safety-related	MPS Test #63-6
The CNTS supports the RCS by closing the CIVs for pressurizer spray, RCS injection, RCS discharge, and reactor pressure vessel (RPV) high point degasification when actuated by the MPS for RCS isolation.	safety-related	MPS Test #63-6
a barrier to contain mass, energy, and fission product release by closure of the CIVs upon a containment isolation signal.	safety-related	MPS Test #63-6
The CNTS supports the Reactor Building crane (RBC) by providing lifting attachment points that the RBC can connect to so that the module can be lifted.	non-safety related, risk-significant	RBC Test #52-1 RBC Test #52-2
	non-safety related	SDI Test #66-2
Prerequisites		
Verify an instrument calibration has been instruments required to perform this test.	completed, with approved records and wi	thin all calibration due dates, for all
Component Level Tests	Tota Mathad	A
i. Verify the CNTS safety-related check valves change position under design	Test Method The check valves are tested in accordance with the requirements of ASME OM code, ISTC-5220, check valves.	Acceptance Criteria Each CNTS safety-related check valve strokes fully open and closed under forward and reverse flow conditions, respectively. [ITAAC 02.01.21]

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Table 14.2-43: Containment System Test # 43 (Continued)

System Level Test #43-1							
Test Objective	Test Method	Acceptance Criteria					
Verify the leaktightness of the containment system.	of the CNTS in accordance with the	Local leak rate tests are completed on containment penetrations listed in Table 6.2-9 which require Appendix J, Type B or C testing.					
		[ITAAC 02.01.07]					

Table 14.2-44: Control Rod Drive System Flow-Induced Vibration Test # 44

The control rod drive system (CRDS) flow-induced vibration (FIV) testing is performed during startup testing. There are no preoperational tests for CRDS.

The CRDS flow-induced vibration testing is performed consistent with the requirements of the NuScale "Comprehensive Vibration Assessment Program" as described in the "Comprehensive Vibration Assessment Program (CVAP) Technical Report," TR-0716-50439. The CVAP is addressed in DCD Section 3.9.2. The CRDS is discussed in DCD Section 4.6.

System Function	System Function Categorization	Function Verified by Test #		
None	N/A	N/A		
Prerequisites:				
N/A				
Component Level Tests				
None				

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Table 14.2-45: Reactor Vessel Internals Flow-Induced Vibration Test # 45

Reactor vessel internals (RVI) flow-induced vibration testing is performed during startup testing. There are no preoperational tests for RVI.

RVI flow induced vibration testing is performed consistent with the requirements of the NuScale "Comprehensive Vibration Assessment Program" as described in the "Comprehensive Vibration Assessment Program (CVAP) Technical Report," TR-0716-50439. The CVAP is addressed in DCD Section 3.9.2. Reactor vessel internals are discussed in DCD Section 5.1.3.3

System Function	System Function Categorization	Function Verified by Test #						
None	N/A	N/A						
Prerequisites:	•	•						
N/A	N/A							
Component Level Tests								
None								

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Table 14.2-46: Reactor Coolant System Test # 46

Preoperational test is required to be pe		
The RCS is described in Section 5.4 and		
-	System Function Categorization	Function Verified by Test #
The RCS supports the CNTS by supplying the reactor coolant pressure boundary and a fission product boundary via the RPV and other appurtenances.	safety-related, risk-significant	Component Tests i. and ii.
The RCS functions verified by other test	ts are:	
	System Function Categorization	Function Verified by Test #
	safety-related, risk-significant	MPS Test #63-1
The RCS supports the MPS by providing instrument information signals for low temperature overpressure protection actuation.	safety-related	MPS Test #63-1
The RCS supports the MPS by providing PAM instrument information signals.	nonsafety-related	SDI Test #66-2
Prerequisites Verify an instrument calibration has been of instruments required to perform this test. Component Level Tests	completed, with approved records and wi	thin all calibration due dates, for all
	Test Method	Acceptance Criteria
valves change position under design	The check valves are tested in accordance with the requirements of ASME OM Code, ISTC-5220, Check Valves.	Each RCS safety-related check valve strokes fully open and closed under forward and reverse flow conditions, respectively. [ITAAC 02.01.16]
flow check valves change position under design flow.	The check valves are tested in accordance with the requirements of ASME OM Code, ISTC-5220, Check Valves.	Each RCS safety-related excess flow check valve strokes fully closed under excess flow conditions. [ITAAC 02.01.17]
monitored in the MCR and the RSS, if the signal is designed to be displayed in the RSS.	Initiate a single real or simulated instrument signal from each RCS transmitter.	i. The instrument signal is displayed on an MCR workstation or recorded by the applicable control system historian.
(Test not required if the instrument calibration verified the MCR and RSS display)		 The instrument signal is displayed on an RSS workstation or recorded by the applicable control system historian if the instrument signal is designed to b displayed in the RSS.
		iii. The instrument signal is displayed on an MCR module-specific safety display instrument monitor or an MCR common safety display instrument monitor if the instrument signal is designed to be displayed on a safety display instrument monitor.

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Table 14.2-47: Emergency Core Cooling System Test # 47

Preoperational test is required to be p	erformed for each NPM.	
The ECCS is described in Section 6.3. The	ne ECCS functions are not verified by	ECCS tests. The ECCS functions verified by
other tests are:		
System Function	System Function Categorization	Function Verified by Test #
 The ECCS supports the RCS by opening the ECCS reactor vent valves and reactor recirculation valves when their respective trip valve is actuated by the MPS. 		MPS Test #63-6
The ECCS supports the RCS by providing recirculated coolant from the containment to the RPV for the removal of core heat.	safety-related	MPS Test #63-6
 The ECCS supports the RCS by providing low temperature overpressure protection (LTOP) for maintaining the reactor coolant pressure boundary. 	safety-related	MPS Test #63-6
 ECCS supports MPS by providing instrumentation information signals. 	nonsafety-related	MPS Test #63-1
The ECCS supports MPS by providing post accident monitoring instrument information signals.		SDI Test #66-2
Prerequisites		·
Test #" heading.	g are identified in the referenced test a	bstract cited under the "Function Verified by
Component Level Tests	,	
None	,	
System Level Tests		
None	·	

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Table 14.2-48: Decay Heat Removal System Test # 48

Preoperational test is required to be po		
	HRS functions are not verified by DH	RS tests. DHRS functions verified by othe
tests are: System Function	System Function Categorization	Function Verified by Test #
The DHRS supports the RCS by opening the DHRS actuation valves for DHRS operation.	safety-related	MPS Test #63-6
The DHRS supports the MPS by providing MPS actuation instrument information signals.	safety-related	MPS Test #63-1
 The DHRS supports the MPS by providing PAM instrument information signals. 	nonsafety-related	SDI Test #66-2
Prerequisites		•
N/A		
Component Level Tests		
None		
System Level Tests		
None		

Table 14.2-49: Incore Instrumentation Test # 49

Preoperational test is required to be pe	erformed for each NPM.				
The in-core instrumentation system (IC	IS) is described in Section 7.0.4.7 and th	e function verified by this test is:			
System Function	System Function Categorization	Function Verified by Test #			
The IICIS supports the MPS by providing	nonsafety-related	Test #49-1			
reactor core (RXC) temperature					
information.					
The ICIS functions verified by another t	test is:				
System Function	System Function Categorization	Function Verified by Test #			
The ICIS supports the MPS by providing	nonsafety-related	Test #66-2			
RXC temperature information.					
Prerequisites					
i. The ICIS instrument strings are inserte	ed into the core.				
i. Verify an instrument calibration has b	een performed on all ICIS thermocouples l	by cross-calibrating the thermocouple to			
the RCS narrow range resistance temp	perature detectors (RTDs) prior to RCS heat	tup.			
Component Level Tests					
None					
System Level Test #49-1					
Test Objective	Test Method	Acceptance Criteria			
Verify proper temperature indication is	Heat the RCS from ambient conditions to	MCS data indicates that the ICIS			
obtained from the ICIS thermocouples.	normal operating temperature.	thermocouples respond properly.			
	Use the MCS data historian to cross-				
	check the ICIS thermocouples to each				
	other and the RCS narrow-range and				
	wide range RTDs.				

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Table 14.2-50: Module Assembly Equipment Test # 50

	tests for module assembly equipment (MAE). import trolley, the upender, and the inspection	n rack.
System Function	System Function Categorization	Function Verified by Test #
None	None	None
Prerequisites	,	•
N/A		
Component Level Tests		
None		
System-Level Tests		
None		
110		

Table 14.2-51: Fuel Handling Equipment System Test # 51

Component-level testing is required to be performed once.

System Level Test #51-1 and Test #51-2 are required to be performed once.

System Level Test #51-3 and Test #51-4 are required to be performed once.

The	e fue	el hand	ling e	quipmen	t (FHE) sy	/stem is	describe	ed in	Section	9.1.4	and th	e function	s verified b	by this test are:	

Sy	stem Function	System Function Categorization	Function Verified by Test #
1.	The FHE system supports new fuel by providing ability to visually inspect fuel.	nonsafety-related	Test #51-1 Test #51-2
2.	The FHE system supports the RXC by moving fuel within the core.	nonsafety-related	Test #51-3 Test #51-4
3.	The FHE system supports the spent fuel storage system (SFSS) by moving fuel into the spent fuel storage system.	nonsafety-related	Test #51-4

Prerequisites

- i. An FHE system factory acceptance test has been successfully completed and approved.
- ii. A rated-load test has been successfully completed and approved on theFHE system on the following equipment in accordance with ASME NOG-1 paragraph 7423.
 - a. Fuel handling machine (FHM) main hoist
 - b. FHM auxiliary hoists
- iii. Verify an instrument calibration has been completed, with approved records and within all calibration due dates, for all instruments required to perform this test.

Component Level Tests

Tes	t Objective	Test Method	Acceptance Criteria
i.	Verify the operation of FHE controls	Actuate or simulate actuation of the	The FHE equipment controls limit
	that limit motion and speed.	interlocks contained in Table 14.2-51a.	motion and speed per design.
ii.	the signal is designed to be displayed in the RSS. (Test not required if the instrument calibration verified the MCR and RSS	instrument signal from each FHE system	 i. The instrument signal is displayed on an MCR workstation or recorded by the applicable control system historian. ii. The instrument signal is displayed on an RSS workstation or recorded
	display.)		by the applicable control system historian if the instrument signal is designed to be displayed in the RSS.
			iii. The instrument signal is displayed on an MCR module-specific safety display instrument monitor or an MCR common safety display instrument monitor if the
			instrument signal is designed to be
			displayed on a safety display
			instrument monitor.
_	tem Level Test #51-1		
	t Objective	Test Method	Acceptance Criteria
	ify the proper operation of the new	Transfer a dummy fuel assembly from its	
fue	jib crane.	receipt shipping container to the new	successfully transferred to the new

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fuel inspection stand and from the new

fuel inspection stand to the new fuel

elevator.

fuel inspection stand.

fuel elevator.

A dummy fuel assembly is

successfully transferred to the new

Table 14.2-51: Fuel Handling Equipment System Test # 51 (Continued)

Test Objective	Test Method	Acceptance Criteria
Verify the proper operation of the new fuel elevator.	Lower a dummy fuel assembly in the new fuel elevator.	A dummy fuel assembly is successfully lowered to the position where it can be retrieved by the FHM mast.
System Level Test #51-3		
Test Objective	Test Method	Acceptance Criteria
Verify the proper operation of the FHM.	 Transfer the dummy fuel assembly from the new fuel elevator to the FHM mast. 	i. The dummy fuel assembly is successfully transferred to the FHM mast.
	ii. Transfer the dummy fuel assembly from the new fuel elevator location to a designated RXC location.iii. Seat the dummy fuel assembly.	ii. The dummy fuel assembly is successfully transferred to its designated core location and partially inserted.
	iii. Seat the daminy raci assembly.	iii. The dummy fuel assembly is fully seated.
System Level Test #51-4		
Test Objective	Test Method	Acceptance Criteria
Verify the proper operation of the FHM.	 i. Withdraw the dummy fuel assembly to a position where the FHM can automatically transfer the assembly. Transfer the dummy fuel assembly from the RXC to a designated spent fuel storage location. (Manual operation of the fuel assembly is required for final fuel insertion.) ii. Seat the dummy fuel assembly. 	 i. The dummy fuel assembly is successfully transferred to its designated storage location and partially inserted. ii. The dummy fuel assembly is fully seated.
System Level Test #51-5		1
Test Objective	Test Method	Acceptance Criteria
Verify the FHM maintains at least 10 feet of water above the top of the fuel assembly when lifted to its maximum height with the pool level at the lower limit of the normal operating low water level.	Perform a test of the FHM mast mechanical stop limit switch.	The FHM maintains at least 10 feet of water above the top of the fuel assembly when lifted to its maximum height with the pool level at the lower limit of the normal operating low water level. [ITAAC 03.04.05]

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Table 14.2-51a: FHE System Interlock Testing

Equipment	Emergency Stop	Bridge and Trolley End of Travel	Crane Zone Limits	Hoist Underload (Underweight / Slack Rope) (Lower)	Hoist Overload (Overweight) (Raise)	Hoist Up- Position (Upper Travel Limit)	Hoist Down- Position (Lower Travel Limit)	Rotation and Gripper	Hoist, Bridge, Trolley Slow Zones	Overspeed Limit	Mis-reeve Limit Switch
FHM bridge	X	X	X						Х		
FHM trolley	Х	Х	Х						Х		
FHM main hoist/mast	Х			Х	Х	Х	Х	Х	Х	Х	Х
FHM auxiliary hoist	Х				Х	Х	Х				Х
New fuel jib crane trolley	Х	Х						Х			
New fuel jib crane hoist	Х				Х	Х	Х			Х	Х
New fuel elevator	Х				Х	Х	Х				Х

Table 14.2-52: Reactor Building CranesTest # 52

Pre	Preoperational test is required to be performed once.					
The RBC system is described in Section 9.1.5 and the functions verified by this test are:						
Sys	tem Function	System Function Categorization	Function Verified by Test #			
	The RBC supports the NPM by providing structural support and mobility while moving from refueling, inspection and operating bay.	nonsafety-related, risk-significant	Test #52-1 Test #52-2			
	MAE bolting supports the CNT by providing material handling to allow for disassembly and reassembly of the CNV lower flange.	nonsafety-related	Test #52-2			
	MAE bolting supports the RPV actively by providing material handling to allow for disassembly and reassembly of the RPV lower flange.	nonsafety-related	Test #52-2			
	The CNTS supports the RBC by providing lifting attachment points that the RBC can connect to so that the module can be lifted.	nonsafety-related	Test #52-1 Test #52-2			

Prerequisites

- i. An RBC site acceptance test has been completed and approved.
- ii. A rated-load test has been completed and approved on the RBC on the following equipment in accordance with ASME NOG-1 paragraph 7423.
 - a. RBC main hoist
 - b. RBC auxiliary hoists
 - c. RBC wet hoist
- iii. Verify an instrument calibration has been completed, with approved records and within all calibration due dates, for all instruments required to perform this test.

Component Level Tests

_			I		
Te	st Objective	Test Method	Acceptance Criteria		
i.	Verify RBC controls that limit RBC motion and speed.	Actuate or simulate actuation of the RBC interlocks contained in Table 14.2-52a.	Local visual observation indicates that the interlocks limit RBC motion and speed.		
ii.	Verify RBC remains in current position on loss of control or power or seismic event.	Initiate the following real or simulated signals: i. Loss of control. ii. Loss of power. iii. Seismic switch actuation.	Local visual observation indicates that the bridge, trolley, main hoist, wet hoist, auxiliary hoist trolley and auxiliary hoist brakes are set.		
iii.	Verify each RBC system instrument is monitored in the MCR, if designed to be monitored in the MCR. (Test not required if the instrument calibration verified the MCR display)	Initiate a single real or simulated instrument signal from each RBC system transmitter.	i.The instrument signal is displayed on an MCR workstation or recorded by the applicable control system historian.		

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Table 14.2-52: Reactor Building CranesTest # 52 (Continued)

Syste	m Level Test #52-1					
Test (Objective	Test Method	Acceptance Criteria			
Test (i. Vo an ii. Vo of	Pobjective erify RBC load path and removal of a NPM from a reactor bay. erify RBC load path and installation from NPM in a reactor bay. Verify the NPM can be disassembled using the CNV support stand and the RPV support stand and associated tooling. Verify the RBC semi-automatic controls can be used to transport the NPM through the disassembly process.	Place the module lifting adaptor on the RBC. Lift an NPM and move the RBC with the attached NPM to its design home location. i. Use the RBC semi-automatic programmed controls to install the NPM in the lead NPM bay location and return the RBC to the design home location ii. Use the RBC semi-automatic	i. ii. iv. v.	The bridge and trolley speeds do not exceed maximum design speeds. The bridge and trolley does not move at the same time. The bridge and trolley maximum allowable speed is toggled from full-speed to microspeed when the RBC hook gets within the design distance of a predefined reference location. The main hoist only moves within the predefined elevation zones. The reactor module is positioned at the design rotation at predefined reference locations. The reactor module is fully seated in the reactor bay receiver. a. Verify the NPM can be disassembled using the CNV support stand and associated tooling. b. Verify the RBC semi-automatic controls can be used to transport the NPM through the disassembly process. a. Verify the NPM can be assembled using the CNV support stand and the RPV support stand and associated tooling. b. Verify the RBC semi-automatic controls can be used to transport stand and the RPV support stand and associated tooling. b. Verify the RBC semi-automatic controls can be used to transport the NPM through the assembly process.		

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Table 14.2-52: Reactor Building CranesTest # 52 (Continued)

Test Objective	Test Method	Acceptance Criteria
	ii. Use the RBC semi-automati programmed controls to m NPM and MLA from the des location to the module insp rack and attach the upper N MLA.	ove the ign home section
	Use the RBC semi-automati programmed controls to m upper NPM from the modul inspection rack to the RPV s stand and seat the upper NI lower RPV and RPV support Install and tension the lower closure bolts.	ove the le support PM on the stand.
	Use the RBC semi-automati programmed controls to m upper NPM from the RPV sustand to the CNV support st seat the upper NPM on the CNV and CNV support standand tension the lower CNV bolts.	ove the upport tand and lower d. Install
	Use the RBC semi-automati programmed controls move and NPM from the CNV sup stand to the design home lo	e the RBC port

Table 14.2-52a: RBC System Interlock Testing

Equipment	Emergency Stop	Bridge and Trolley End of Travel	Crane Zone Limits	Hoist Underload (Underweight / Slack Rope) (Lower)	Hoist Overload (Overweight) (Raise)	Hoist Up- Position (Upper Travel Limit)	Hoist Down- Position (Lower Travel Limit)	-	Mis-reeve Limit Switch	Unbalanced Load	Two- Blocking
RBC trolley	Х	X	Х								
RBC bridge	Х	Х	Х								
RBC main hoist	Х			Х	Х	Х	Х	Х	Х	Х	Х
RBC aux hoist trolley 1 & 2	Х	Х									
RBC aux hoist 1 & 2	Х			Х	Х	Х	Х	Х	Х	Х	
Wet hoist	X			X	X	Χ	Х	X	Х	Х	Χ

Table 14.2-53: Process Sampling System Test # 53

Preoperational test is required to be performed for each NPM. The PSS is described in Section 9.3.2 and the functions verified by this test are:				
	stem Function	System Function Categorization	Function Verified by Test #	
	The PSS supports the RCS during normal operations by providing sampling and analysis of reactor coolant discharge (letdown) liquid.	nonsafety-related	Test #53-1	
2.	The PSS supports the CVCS by providing sampling of reactor coolant at process points in the CVCS.	nonsafety-related	Test #53-1	
3.	The PSS supports the RCS during accident conditions by providing post-accident grab sample of the reactor coolant.	nonsafety-related	Test #53-1	
	The PSS supports the CNTS during normal operations by providing sampling of containment gas and analysis of hydrogen and oxygen concentration in containment.	nonsafety-related	Test #53-2	
5.	The PSS supports the condensate and FWS by providing sampling and analysis of condensate and feedwater.	nonsafety-related	Test #53-3	
6.	The PSS supports the MSS by providing sampling and analysis of main steam.	nonsafety-related	Test #53-3	
7.	The PSS system supports the ABS by providing sampling and analysis of the auxiliary boiler steam and feedwater.	nonsafety-related	Test #53-3	
	PSS supports the CNTS during accident condition by providing sampling of containment gas and analysis of hydrogen and oxygen concentration in containment to respond to emergencies.	nonsafety-related	Test #53-2	

Prerequisites

Verify an instrument calibration has been completed, with approved records and within all calibration due dates, for all instruments required to perform this test.

Component Level Tests

Te	st Objective	Test Method	Acceptance Criteria	
i.	Verify each PSS remotely-operated valve can be operated remotely.	local control panel (if design has local	MCR display and local, visual observation indicate each valve fully opens and fully closes.	
ii.	,	Isolate and vent air to the valve.	MCR display and local, visual observation indicate each valve fails to its safe position.	
iii.	Verify each PSS air-operated valve fails to its safe position on loss of electrical power to its solenoid.		MCR display and local, visual observation indicate each valve fails to its safe position.	

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Table 14.2-53: Process Sampling System Test # 53 (Continued)

monitored in the MCR and the RSS, if	Initiate a single real or simulated instrument signal from each PSS transmitter.	 i. The instrument signal is displayed on an MCR workstation or recorded by the applicable control system historian. ii. The instrument signal is displayed on an RSS workstation or recorded by the applicable control system historian if the instrument signal is designed to be displayed in the RSS iii. The instrument signal is displayed on an MCR module-specific safety display instrument monitor or an MCR common safety display
		instrument monitor if the instrument signal is designed to be displayed on a safety display
		instrument monitor.
System Level Test #53-1		
Test Objective	Test Method	Acceptance Criteria
sampling points.	 i. The reactor module is in hot functional testing with the reactor coolant system at normal operating pressure and the maximum operating temperature achievable by heating the RCS with the MHS. The RCS supply and discharge flow is in service. Align the CVCS and PSS to provide continuous sampling flow to the PSS analysis panel. ii. The RCS discharge line is in service. Align the RCS and PSS to provide sampling flow to the primary sampling ion chromatography units. iii. Open the PSS grab sample panel manual valve to obtain an RCS injection flow pressurized grab sample. iv. Open the PSS grab sample panel manual valve to obtain an RCS discharge flow pressurized grab 	 i. The PSS analysis panel instruments provide indication of the water analysis. ii. The primary sampling ion chromatography unit monitors for the programmed ion. iii. An RCS injection flow grab sample is successfully obtained. iv. An RCS discharge flow grab sample is successfully obtained. v. A CVCS demineralizer discharge flow grab sample is successfully obtained.

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Table 14.2-53: Process Sampling System Test # 53 (Continued)

System Level Test #53-2				
Test Objective	Test Method	Acceptance Criteria		
Verify sampling capability of the containment sampling points.	The reactor module is in hot functional testing with the RCS at normal operating pressure and the maximum operating temperature achievable by heating the RCS with the MHS.	The PSS containment gas sample panel instruments provide indication of the gas analysis.		
	The CES is in service.			
	Align the CES and PSS to provide			
	continuous sampling flow to the PSS			
5	containment gas sample panel.			
System Level Test #53-3 Test Objective	Test Method	Accontance Critoria		
		Acceptance Criteria		
Verify sampling capability of the secondary sampling points.	i. The reactor module is in hot functional testing with the RCS at normal operating pressure and the maximum operating temperature achievable by heating the RCS with the MHS. The FWS and MSS are in service. Align the FWS, MSS, and PSS to provide continuous sampling flow to the PSS secondary sampling system feedwater/main steam sample panel. ii. Open the manual feedwater/main steam ion chromatography analysis panel valve to obtain a feedwater to SG sample. iii. Open the manual feedwater/main steam ion chromatography analysis panel valve to obtain an SG-1 steam sample. iv. Open the manual feedwater/main steam ion chromatography analysis panel valve to obtain a SG-2 steam sample. v. Open the manual feedwater/main steam ion chromatography analysis panel valve to obtain a SG-2 steam sample. v. Open the manual feedwater/main steam ion chromatography analysis panel valve to obtain a condensate pump discharge sample.	 i. The PSS secondary sampling system feedwater/main steam sample panel instruments provide indication of the water and steam analysis. ii. The feedwater/main steam ion chromatography analysis panel monitors the programmed ion. iii. The feedwater/main steam ion chromatography analysis panel monitors the programmed ion. iv. The feedwater/main steam ion chromatography analysis panel monitors the programmed ion. v. The feedwater/main steam ion chromatography analysis panel monitors the programmed ion. v. The feedwater/main steam ion chromatography analysis panel monitors the programmed ion. 		

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control to the auxiliary AC power

Table 14.2-54: 13.8kV and Switchyard System Test # 54

Preoperational test is required to be performed once for the 6A 13.8 kV and switchyard system (EHVS) and once for the 6B EHVS.

The EHVS is described in Sections 8.1.2.1 and 8.3.1.1, and the functions verified by this test are:				
System Function	System Function Categorization	Function Verified by Test #		
The EHVS supports the EMVS by providing electrical power.	nonsafety-related	Component level tests		
The EHVS supports the TGS by providing electrical protection and control.	nonsafety-related	Component level tests		
3. The EHVS supports the BPSS by providing electrical protection and	nonsafety-related	Component level tests		

source. Prerequisites

- Verify an instrument calibration has been performed on all EHVS instruments that provide information signals to the plant control system (PCS) for the bus and main power transformer under test.
- ii. Verify an instrument calibration has been completed, with approved records and within all calibration due dates, for all instruments required to perform this test.
- iii. Verify all protective devices associated with the EHVS bus and main power transformer under test is tested before that bus is energized

	bus is energized				
Co	Component Level Tests				
Te	st Objective	Test Method	Acceptance Criteria		
i.	Verify each EHVS breaker can be operated locally.	Operate each breaker from the local control panel while the breaker is in the test position.	MCR display and local, visual observation indicate each breaker opens and closes.		
ii.	Verify each EHVS breaker can be operated remotely.	Operate each breaker from the MCR while the breaker is in the test position.	MCR display and local, visual observation indicate each breaker opens and closes.		
	Verify each EHVS breaker trips on its fault conditions.	Simulate each fault condition for a breaker when the breaker is in the test position.	MCR display and local, visual observation indicate each breaker opens on each fault condition.		
iv.	by offsite power via its main power transformer.	Energize each EHVS bus from its main power transformer.	Bus voltage is within design limits.		
	(Test not required if an offsite power system is not provided.)				
V.	Verify each EHVS instrument is monitored in the MCR and the RSS, if the signal is designed to be displayed in the RSS.	Initiate a single real or simulated instrument signal from each EHVS transmitter.	 The instrument signal is displayed on an MCR workstation or recorded by the applicable control system historian. 		
	(Test not required if the instrument calibration verified the MCR and RSS display.)		ii. The instrument signal is displayed on an RSS workstation or recorded by the applicable control system historian if the instrument signal is designed to be displayed in the RSS.		
			iii. The instrument signal is displayed on an MCR module-specific safety display instrument monitor or an MCR common safety display instrument monitor if the instrument signal is designed to be displayed on a safety display		

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Table 14.2-54: 13.8kV and Switchyard System Test # 54 (Continued)

System Level Tests	
None	

Table 14.2-55: Medium Voltage AC Electrical Distribution System Test # 55

Preoperational test is required to be performed once for the 6A medium voltage AC electrical distribution system (EMVS) and once for the 6B EMVS. The testing of each EMVS bus which provides power to 00 loads (common system loads) is performed with NPM number 1 EMVS loads.

Th	The EMVS is described in Sections 8.1.2.1 and 8.3.1.1 and the functions verified by this test are:				
System Function		System Function Categorization	Function Verified by Test #		
1.	The EMVS supports the ELVS by providing electrical power.	nonsafety-related	component-level tests		
2.	The EMVS supports the circulating water system (CWS) by providing electrical power to loads.	nonsafety-related	component-level tests		
3.	The EMVS supports the CHWS by providing electrical power to loads.	nonsafety-related	component-level tests		
4.	The EMVS supports the SCWS by providing electrical power to loads.	nonsafety-related	component-level tests		

Prerequisites

- i. Verify an instrument calibration has been completed, with approved records and within all calibration due dates, for all instruments required to perform this test.
- ii. Verify all protective devices associated with the EMVS bus and unit auxiliary transformer under test are tested before that bus is energized. Approved test records indicate each protective device has been calibrated within its required test interval.

	interval.				
Co	Component Level Tests				
Te	st Objective	Test Method	Acceptance Criteria		
i.	Verify each EMVS breaker can be operated locally.	Operate each breaker from the local control panel while the breaker is in the test position.	MCR display and local, visual observation indicate each breaker opens and closes.		
ii.	Verify each EMVS breaker can be operated remotely.	Operate each breaker from the MCR while the breaker is in the test position.	MCR display and local, visual observation indicate each breaker opens and closes.		
iii.	Verify each EMVS breaker trips on its fault conditions.	Simulate each fault condition for a breaker when the breaker is in the test position.	MCR display and local, visual observation indicate each breaker opens on each fault condition.		
	Verify each EMVS bus can be powered via its unit auxiliary transformer and adjacent EMVS bus. (Test not required if an offsite power system is not provided.)	Energize each EMVS bus from its unit auxiliary transformer and its adjacent EMV bus.	Bus voltage is within design limits.		
v.	Verify each EMVS instrument is monitored in the MCR and the RSS, if the signal is designed to be displayed in the RSS. (Test not required if the instrument calibration verified the MCR and RSS display.)	Initiate a single real or simulated instrument signal from each EMVS transmitter.	 i. The instrument signal is displayed on an MCR workstation or recorded by the applicable control system historian. ii. The instrument signal is displayed on an RSS workstation or recorded by the applicable control system historian if the instrument signal is designed to be displayed in the RSS. iii. The instrument signal is displayed on an MCR module-specific safety display instrument monitor or an MCR common safety display instrument monitor if the instrument signal is designed to be displayed on a safety display instrument monitor. 		

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Table 14.2-55: Medium Voltage AC Electrical Distribution System Test # 55 (Continued)

vi.	Verify the automatic transfer of each	Simulate all conditions that require an	MCR display and local, visual
	EMVS bus to its adjacent EMVS bus.	automatic bus transfer to an adjacent	observation indicate the required tie
		bus.	breaker from the adjacent bus closes.
		This test may be performed with the	
		EMVS bus energized or deenergized.	
Sy	stem Level Tests		
No	ne		

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Table 14.2-56: Low Voltage AC Electrical Distribution System Test # 56

Preoperational test is required to be performed in support of the testing of each NPM. The testing of each ELVS bus, which provides power to common system loads and 6A loads, is performed with NPM number 1 ELVS loads.

The ELVS is described in Section 8.1.2.1 and 8.3.1.1, and the functions verified by this test are:

Sy	stem Function	System Function Categorization	Function Verified by Test #
1.	The ELVS provides AC power to system loads via ELVS buses.	nonsafety-related	component-level tests
2.	The ELVS supports the EMVS by providing AC power to the system's auxiliary equipment.	nonsafety-related	component-level tests
3.	The ELVS supports the high voltage AC electrical distribution system (EHVS) by providing AC power to the system's auxiliary equipment.	nonsafety-related	component-level tests

Prerequisites

- i. Verify an instrument calibration has been completed, with approved records and within all calibration due dates, for all instruments required to perform this test.
- ii. Verify all protective devices associated with the ELVS bus and unit auxiliary transformer under test are tested before that bus is energized.

Component Level Tests

Te	st Objective	Test Method	Acceptance Criteria
i.	Verify each ELVS breaker can be operated locally.	Operate each breaker from the local control panel while the breaker is in the test position.	MCR display and local, visual observation indicate each breaker opens and closes.
ii.	Verify each ELVS breaker can be operated remotely.	Operate each breaker from the MCR while the breaker is in the test position.	MCR display and local, visual observation indicate each breaker opens and closes.
iii.	Verify each ELVS breaker trips on its fault conditions.	Simulate each fault condition for a breaker when the breaker is in the test position.	MCR display and local, visual observation indicate each breaker opens on each fault condition.
iv.	Verify each ELVS bus can be powered by offsite power via its unit auxiliary transformer. (Test not required if an offsite power system is not provided.)	Energize each ELVS bus from its unit auxiliary transformer.	Bus voltage is within design limits.
v.	Verify automatic bus transfer of each ELVS bus.	Perform the following test for each of the ELVS buses. Open the ELVS supply breaker to a given ELVS bus.	The ELVS bus tie breaker is closed and the bus voltage is within design limits.

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Table 14.2-56: Low Voltage AC Electrical Distribution System Test # 56 (Continued)

vi. Verify each ELVS instrument is	Initiate a single real or simulated	i.	The instrument signal is displayed
monitored in the MCR and the RSS, if	instrument signal from each ELVS		on an MCR workstation or recorded
the signal is designed to be displayed	transmitter.		by the applicable control system
in the RSS.			historian.
(Test not required if the instrument		ii.	The instrument signal is displayed
calibration verified the MCR and RSS			on an RSS workstation or recorded
display.)			by the applicable control system
			historian if the instrument signal is
			designed to be displayed in the RSS.
		iii.	The instrument signal is displayed
			on an MCR module-specific safety
			display instrument monitor or an
			MCR common safety display
			instrument monitor if the
			instrument signal is designed to be
			displayed on a safety display
			instrument monitor.
System Level Tests			
None			

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Table 14.2-57: Highly Reliable DC Power System Test # 57

Preoperational test is required to be performed for each NPM.				
The EDSS is described in Sections 8.1.2.2, 8.1.4.2 and 8.3.2.1.1, and the functions verified by this test are:				
System Function	System Function Categorization	Function Verified by Test #		
The highly reliable DC power system (EDSS) supports the following systems by providing DC electrical power. • MPS — poutron monitoring system (NMS)	nonsafety-related	The Site Acceptance Test criteria in the prerequisites satisfies the functional verification.		
 neutron monitoring system (NMS) fixed area radiation monitoring system (RMS) plant lighting system (PLS) 				
• PPS				
safety display information systemCRVS				
EDS system functions verified by other	tests are:			
System Function	System Function Categorization	Function Verified by Test #		
EDSS supports the MPS by providing EDSS module-specific operating parameter information signals.	nonsafety-related	Reference 14.2-66 Component level test		
EDSS supports the PPS by providing EDSS common operating parameter information signals. Description	nonsafety-related	Reference 14.2-66 Component level test		

Prerequisites

- i. Verify an instrument calibration has been completed, with approved records and within all calibration due dates, for all instruments required to perform this test.
- ii. Verify a valve-regulated lead-acid battery acceptance tests has been performed on all EDSS batteries to confirm battery capacity in accordance with IEEE Standard 1188 Sections 6 and 7.
- iii. Verify battery charger performance testing has been completed by the manufacturer or a site acceptance test has been completed in accordance with manufacturer instructions.

	completed in accordance with manufacturer instructions.				
Co	Component Level Tests				
Te	st Objective	Test Method	Acceptance Criteria		
i.	Verify on loss of power each EDSS battery charger ELVS input breaker automatically opens.	De-energize the ELVS motor control center feed to a EDSS battery charger. Repeat test for remaining EDSS battery chargers.	The battery charger ELVS input breaker is open.		
ii.	Verify each EDSS instrument is monitored in the MCR and the RSS, if the signal is designed to be displayed in the RSS.	_	 The instrument signal is displayed on an MCR workstation or recorded by the applicable control system historian. 		
	(Test not required if the instrument calibration verified the MCR and RSS display.)		ii. The instrument signal is displayed on an RSS workstation or recorded by the applicable control system historian if the instrument signal is designed to be displayed in the RSS.		
			iii. The instrument signal is displayed on an MCR module-specific safety display instrument monitor or an MCR common safety display instrument monitor if the instrument signal is designed to be displayed on a safety display instrument monitor.		

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Table 14.2-57: Highly Reliable DC Power System Test # 57 (Continued)

S	ystem Level Tests	l
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Table 14.2-58: Normal DC Power System Test # 58

Preoperational test is required to be performed for each NPM. EDNS is described in Sections 8.1.2.2, 8.1.4.2 and 8.3.2.1.2 and the functions verified by this test are:							
System Function	,						
The normal DC power system supports the following systems by providing DC electrical power for instrumentation and control power.	nonsafety-related	Functions verified by prerequisite and component test.					
 13.8KV and SWYD medium voltage AC electrical distribution system low voltage AC electrical distribution system PCS MCS communication systems RMS meteorological and environmental monitoring system FDS FPS Seismic monitoring system (SMS) TGS Turbine Building HVAC system (TBVS) RBVS plant-wide video monitoring system CRDS 							

Prerequisites

- i. Verify an instrument calibration has been completed, with approved records and within all calibration due dates, for all instruments required to perform this test.
- ii Verify a valve-regulated lead-acid battery acceptance tests has been performed on all EDN batteries to confirm battery capacity in accordance with IEEE Standard 1188 Sections 6 and 7.
- iii. Verify battery charger performance testing has been completed by the manufacturer or a site acceptance test has been completed in accordance with manufacturer instructions.

Component Level Tests

Test Objective		Test Method	Acceptance Criteria
i.	Verify on loss of power each EDNS	De-energize the ELVS motor control	The battery charger ELVS input breaker
	, , ,	center feed to a EDNS battery charger.	is open.
	automatically opens.	Repeat test for remaining EDNS battery	
		chargers.	

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Table 14.2-58: Normal DC Power System Test # 58 (Continued)

ii. Verify each EDNS instrument is	Initiate a single real or simulated	i.	The instrument signal is displayed	
monitored in the MCR and the RSS, if	instrument signal from each EDNS		on an MCR workstation or recorded	
the signal is designed to be displayed	transmitter.		by the applicable control system	
in the RSS.			historian.	
(Test not required if the instrument calibration verified the MCR and RSS display)		ii.	The instrument signal is displayed on an RSS workstation or recorded by the applicable control system historian if the instrument signal is	
			designed to be displayed in the RSS.	
		iii.	The instrument signal is displayed on an MCR module-specific safety display instrument monitor or an MCR common safety display instrument monitor if the instrument signal is designed to be displayed on a safety display instrument monitor.	
System Level Tests				
None				

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Table 14.2-59: Backup Power Supply Test # 59

Pr	Preoperational test is required to be performed for 6A NPMs and 6B NPMs.				
The BPSS is described in Sections 8.1.2.1 and 8.1.2.2 and the functions verified by this test are:					
Sy	stem Function	System Function Categorization	Function Verified by Test #		
1.	The BPSS supports ELVS by providing diesel generator backup electrical power to 480V B-6000 motor control centers.	nonsafety-related	Test #59-1		
2.	The BPSS supports ELVS by providing diesel generator backup electrical power to the operation selected RXB exhaust fan A and B.	nonsafety-related	Test #59-1		
3.	The BPSS supports ELVS by providing diesel generator backup electrical power to the operation selected normal DC power system.	nonsafety-related	Test #59-1		

Prerequisites

- Verify an instrument calibration has been completed, with approved records and within all calibration due dates, for all
 instruments required to perform this test.
- ii. Verify all protective devices associated with the BPSS diesel generators have been tested before performing this test.

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_	st Objective	Test Method	Acceptance Criteria
:	-		-
۱.	Verify each BPSS remotely-operated	Operate each valve from the MCR and	MCR display and local, visual
	valve can be operated remotely.	local control panel (if design has local	observation indicate each valve fully
		valve control).	opens and fully closes.
ii.	Verify each BPSS air-operated valve	Place each valve in its non-safe position.	MCR display and local, visual
	fails to its safe position on loss of air.	Isolate and vent air to the valve.	observation indicate each valve fails to
			its safe position.
iii.	Verify each BPSS air-operated valve	Place each valve in its non-safe position.	MCR display and local, visual
	fails to its safe position on loss of	Isolate electrical power to each air-	observation indicate each valve fails to
	electrical power to its solenoid.	operated valve.	its safe position.
iii.	Verify each BPSS pump can be	Align the BPSS to allow for pump	MCR display and local, visual
	started and stopped remotely.	operation.	observation indicate each pump starts
		Stop and start each pump from the MCR.	and stops.
		otop and start cach pamp nom and mem	Audible and visible water hammer are
			not observed when the pump starts.
iv	Verify the BPSS diesel generator can	Align the BPSS to allow for diesel	i. and ii.
	be started and stopped remotely.	generator operation.	MCR display and local, visual
	se started and stopped remotely.		observation indicate the diesel
		 Start and stop the diesel generator from the MCR. 	
			generator started and stopped.
		ii. Start and stop the diesel generator	
		locally.	
٧.	Verify the BPSS diesel generator fuel	Align the fuel oil transfer pump to	MCR display and local, visual
	oil transfer pump automatically	provide oil to the day tank.	observation indicate the transfer pump
	maintains day tank level.	Simulate a low level in the day tank.	starts.
vi.	Verify protective features of the BPSS	Align the BPSS to allow for diesel	MCR display and local, visual
	diesel generator.	generator operation. Start a diesel	observation indicate the diesel
	-	generator.	generator stops.
		Initiate a simulated fault signal for each	
		diesel generator fault condition.	
		dieser generator fault condition.	

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Table 14.2-59: Backup Power Supply Test # 59 (Continued)

System Level Test #59-1					
Test Objective	Test Method	Acceptance Criteria			
automatically starts and achieves rated voltage and frequency.	generator operation. Initiate a real or simulated loss of power	MCR display and local, visual observation indicate the diesel generator started and achieved rated voltage and frequency.			

Table 14.2-60: Plant Lighting System Test # 60

Preoperational test is required to be performed once.				
The plant lighting system (PLS) is described in Section 9.5.3 and the functions verified by this test are:				
System Function	System Function Categorization	Function Verified by Test #		
 PLS supports the CRB by providing normal lighting. 	nonsafety-related	component-level test i.		
The PLS supports the CRB by providing emergency lighting in the main control room.	nonsafety-related	component-level test ii.		
The PLS supports the RXB by providing normal lighting.	nonsafety-related	component-level test i.		
 The PLS supports the RXB by providing emergency lighting for the remote shutdown station. 	nonsafety-related	component-level test ii.		

Prerequisites

Verify an instrument calibration has been completed, with approved records and within all calibration due dates, for all

	struments required to perform this test				
Component Level Tests					
Te	st Objective	Test Method	Ac	cep	tance Criteria
i.	Verify the PLS provides normal illumination of the MCR and RSS operator workstations, and the MCR safety display information panel.	With normal MCR and RSS lighting in service, measure the light at each MCR and RSS workstation.	i.		The PLS provides at least 100 foot-candles illumination at the MCR operator workstations and at least 50 foot-candles at the MCR auxiliary panels. 103.08.01]
			i.	b.	The PLS provides at least 100 foot-candles illumination at the RSS operator workstations.
			-		03.08.01]
ii.	The PLS provides emergency illumination of the MCR and RSS operator workstations and the MCR safety display information panel.	With MCR and RSS emergency illumination in service, measure the light at each MCR and RSS workstation and MCR safety display information panel.	ii.	a.	The PLS provides at least 10 foot-candles of illumination at the MCR operator workstations and the RSS auxiliary panels.
			[IT	AAC	03.08.02]
			ii.	b.	The PLS provides at least 10 foot-candles at the RSS operator workstations.
					03.08.02]
iii.	Verify the eight-hour battery pack emergency lighting fixtures provide illumination for post-fire safe- shutdown activities performed by operators outside the MCR and RSS.	With no AC power available, measure the light at each eight-hour battery pack emergency lighting fixture target area.		illu foc out fire per	re required target areas are iminated to provide at least one ot-candle illumination in the areas tside the MCR or RSS where poster safe-shutdown activities are reformed.

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Table 14.2-60: Plant Lighting System Test # 60 (Continued)

iv. Verify each PLS instrument is monitored in the MCR and the RSS, if the signal is designed to be displayed in the RSS. (Test not required if the instrument	_	iv.		displayed on an MCR workstation or recorded by the applicable control system historian.
calibration verified the MCR and RSS display.)			b.	The instrument signal is displayed on an RSS workstation or recorded by the applicable control system historian if the instrument signal is designed to be displayed in the RSS.
			C.	The instrument signal is displayed on an MCR module-specific safety display instrument monitor or an MCR common safety display information monitor if the instrument signal is designed to be displayed on a safety display information monitor.
System Level Tests				
None				

Table 14.2-61: Module Control System Test # 61

Preoperational test is required to be performed as indicated by tests for MCS-controlled systems and systems providing data to the MCS.

The MCS is described in Section 7.0.4.5.

On-site testing of the system is performed by an MCS site acceptance test (SAT).

The MCS is a distributed control system which allows monitoring and control of NPM-specific plant components. The MCS includes all manual controls and visual display units necessary to provide operator interaction with the process control mechanism.

The boundary of the MCS is at the terminations on the MCS hardware. The MCS supplies nonsafety inputs to the human-system interfaces (HSIs) for nonsafety displays in the MCR, the remote shutdown station, and other locations where module control system HSIs are necessary. There are two boundaries between MCS and MPS, the fiber-optic isolated portion and the hard-wired module boundary. The MCS has a direct, bi-directional interface with the PCS.

A complete staging and testing of system hardware and software configurations will be conducted. This factory acceptance testing will be conducted in accordance with a written test procedure for testing the software and hardware of the MCS prior to installation in the plant. Following installation, site acceptance testing shall be completed in accordance with developed procedures to ensure the MCS is installed and fully functional as designed.

To ensure the MCS communicates with module-specific plant components, component-level testing is performed on all systems controlled by MCS to manually operate the associated components from the main control room and remote shutdown station. These component-level tests are described in the test abstracts of the systems that contain the actuated components.

In addition, it is verified that each instrument supplying data to the MCS is component tested in preoperational test abstracts to ensure the signal is displayed in the MCR and RSS if applicable. These component-level tests are described in the test abstracts of the systems that contain the instrument.

System Function	System Function Categorization	Function Verified by Test #
Verify each MCS-controlled system instrument is monitored in the MCR and the RSS, if the signal is designed to be displayed in the RSS.	Initiate a single real or simulated instrument signal from each MCS-controlled system transmitter.	i. The instrument signal is displayed on an MCR workstation or recorded by the applicable control system historian.
(Test not required if the instrument calibration verified the MCR and RSS display.)		ii. The instrument signal is displayed on an RSS workstation or recorded by the applicable control system historian if the instrument signal is designed to be displayed in the RSS.
		iii. The instrument signal is displayed on an MCR module-specific safety display instrument monitor or an MCR common safety display instrument monitor if the instrument signal is designed to be displayed on a safety display instrument monitor.

Prerequisites

Prerequisites associated with MCS testing are identified in the test abstracts that contain module-specific components that ensure communication with the MCS.

Component Level Tests

None

System Level Tests

None

Table 14.2-62: Plant Control System Test # 62

Preoperational test is required to be performed as indicated by tests for PCS-controlled systems and systems providing data to the PCS.

The PCS is described in Section 7.0.4.6.

On-site testing of the system is performed by a PCS site acceptance test (SAT).

The PCS is a distributed control system which allows monitoring and control of virtually all module-specific plant components. The PCS includes all manual controls and visual display units necessary to provide operator interaction with the process control mechanism.

The boundary of the PCS is at the terminations on the PCS hardware. The PCS supplies nonsafety inputs to the video display units (VDUs) for nonsafety displays in the MCR, the RSS, and other locations where PCS video display units are necessary. The boundary between the PPS and PCS is at the output connection of the safety-related optical isolators in the PPS, and on the terminals of the equipment interface module for each input from the PCS to the PPS.

The PCS has a direct, bidirectional interface with the MCS. The network interface devices for the PCS domain controller/historian provide the interface between the human machine interface network layer and the control network layer.

A complete staging and testing of system hardware and software configurations will be conducted. This factory acceptance testing will be conducted in accordance with a written test procedure for testing the software and hardware of the PCS prior to installation in the plant. Following installation, site acceptance testing shall be completed in accordance with developed procedures to ensure the PCS is installed and fully functional as designed.

To ensure the PCS communicates with module-specific plant components, component-level testing is performed on all systems controlled by PCS to manually operate the associated components from the main control room and remote shutdown station. These component-level tests are described in the test abstracts of the systems that contain the actuated components.

In addition, it is verified that each instrument supplying data to the PCS is component tested in preoperational test abstracts to ensure the signal is displayed in the MCR and RSS if applicable. These component-level tests are described in the test abstracts of the systems that contain the instrument.

System Function	System Function Categorization	Function Verified by Test #
Verify each PCS-controlled system instrument is monitored in the main control room (MCR) and the remote shutdown station (RSS), if the signal is	Initiate a single real or simulated instrument signal from each PCS-controlled system transmitter.	 The instrument signal is displayed on an MCR workstation or recorded by the applicable control system historian.
designed to be displayed in the RSS. (Test not required if the instrument calibration verified the MCR and RSS display.)		 The instrument signal is displayed on an RSS workstation or recorded by the applicable control system historian if the instrument signal is designed to be displayed in the RSS.
		iii. The instrument signal is displayed on an MCR module-specific safety display instrument monitor or an MCR common safety display instrument monitor if the instrument signal is designed to be displayed on a safety display instrument monitor.

Prerequisites

Prerequisites associated with PCS testing are identified in the test abstracts that contain module-specific components that ensure communication with or are controlled by the PCS.

Component	Leve	Tests
p		

None

System Level Tests

None

Table 14.2-63: Module Protection System Test #63

Preoperational test is required to be performed for each NPM. The MPS is described in Sections 7.0, 7.1, and 7.2 and the functions verified by this test are:			
System Function	System Function Categorization	Function Verified by Test #	
The MPS supports the CNTS by removing	safety-related	Test #63-4	
electrical power to the trip solenoids of	·	Test #63-6	
the following CIVs on a containment			
system isolation actuation signal:			
RCS injection containment isolation			
valves			
RCS discharge containment isolation			
valves			
Pressurizer spray containment isolation valves			
RPV high point degasification			
containment isolation valves			
Feedwater containment isolation			
valves			
Main steam containment isolation			
valves			
Main steam bypass valves			
CES containment isolation valves			
RCCWS containment isolation valves			
CFDS containment isolation valves			
The MPS supports the CNTS by removing	safety-related	Test #63-4	
electrical power to the trip solenoids of		Test #63-6	
the following valves on a DHRS actuation			
signal.			
DHRS actuation valves			
Main steam isolation valves			
Main steam bypass isolation valves			
• Feedwater isolation valves			
The MPS supports the ECCS by removing	safety-related	Test #63-4	
electrical power to the trip solenoids of the following valves on an ECCS		Test #63-6	
actuation signal.			
Reactor vent valves			
Reactor recirculation valves			
The MPS supports the Containment	safety-related	Test #63-4	
system by removing electrical power to	salety-related		
the trip solenoids of the following		Test #63-6	
containment isolation valves on a CVCS			
isolation actuation signal:			
RCS injection containment isolation			
valves			
 RCS discharge containment isolation valves 			
PZR pressurizer spray CIVs			
RPV high point degasification			
containment isolation valves			

Table 14.2-63: Module Protection System Test #63 (Continued)

The MPS supports the CVCS by removing	safety-related	Test #63-4
electrical power to the trip solenoids of		Test #63-6
the DWS supply isolation valves on a		. 651 65
DWS isolation actuation signal		
The MPS supports the ECCS by removing	safety-related	Test #63-4
electrical power to the trip solenoids of	·	Test #63-6
the reactor vent valves on an LTOP		1636 #03 0
actuation signal.		
The MPS supports the ELVS by removing	safety-related	Test #63-4
electrical power to the pressurizer	,	Test #63-6
heaters on a pressurizer heater trip		163t #03-0
actuation signal.		
The MPS supports the EDNS by removing	safety-related	Test #63-4
electrical power to the CRDS for a reactor		Test #63-5
trip.		162(#03-3
The DHRS supports the RCS by opening	safety-related	Test #63-6
the DHRS actuation valves on a DHRS	surety related	rese nos o
actuation signal for DHRS operation.		
The CNTS supports the DHRS by closing	safety-related	Test #63-6
CIVs for the main steam and feedwater	safety related	1636 #03 0
systems when actuated by the MPS.		
The CNTS supports the RCS by closing	safety-related	Test #63-6
the CIVs for pressurizer spray, RCS	salety-related	1est #05-0
injection, RCS letdown, and RPV high		
point degasification when actuated by		
the MPS.		
The CNTS supports the RXB by providing	safety-related	Test #63-6
a barrier to contain mass, energy, and	safety-related	1est #05-0
fission product release by closure of the		
CIVs upon a containment isolation		
signal.		
_	and the malata d	Toot #62.6
The ECCS supports the RCS by opening	safety-related	Test #63-6
the ECCS reactor vent valves and reactor		
recirculation valves when their		
respective trip valve is actuated by the MPS.		
		T + #62.6
The ECCS supports the RCS by providing	safety-related	Test #63-6
recirculated coolant from the		
containment to the RPV for the removal		
of core heat.		
The ECCS supports the RCS by providing	safety-related	Test #63-6
LTOP for maintaining the reactor coolant		
pressure boundary.		
The CVCS supports the RCS by isolating	safety-related	Test #63-6
dilution sources.		
The FWS supports the CNTS by providing	nonsafety-related	Test #63-6
secondary isolation of the feedwater		
lines.		
The MSS supports the CNTS by providing	nonsafety-related	Test #63-6
secondary isolation of the main steam	·	
lines.		

Table 14.2-63: Module Protection System Test #63 (Continued)

The FWS supports the DHRS by providing secondary isolation of the feedwater lines, ensuring required boundary conditions for DHRS operation.	nonsafety-related	Test #63-6
The NMS supports the MPS by providing neutron flux data for various reactor trips.	safety-related	Test #63-4
ECCS supports MPS by providing instrumentation information signals.	nonsafety-related	Test #63-1
The DHRS supports the MPS by providing MPS actuation instrument information signals.	safety-related	Test #63-1
The RCS supports the MPS by providing instrument information signals.	nonsafety-related	Test #63-1
The RCS supports the MPS by providing instrument information signals for LTOP actuation	safety-related	Test #63-1
The CVCS supports ECCS valves by providing water to reset the ECCS valves.	nonsafety-related	Test #63-6

Prerequisite

Verify an instrument calibration has been completed, with approved records and within all calibration due dates, for all instruments required to perform this test.

Component Level Tests

None

System Level Test #63-1

Test Objective	Test Method	Acceptance Criteria
Verify the instrument signals of MPS monitored variables are displayed in the MCR.	Table 7.1-2 lists all of sensors which input to MPS. This test may be performed concurrently with safety display and indication system (SDIS) test #66 -2 for PAM Type B and Type C testing described in Section 14.2.12.	Each MPS monitored signal is displayed on an MCR workstation and the module-specific safety display instrument panel (if designed for safety display instrument display).
	Inject a single signal as close as practical for each sensor listed in Table 7.1-2 and monitor its response on an MCR workstation and the module-specific safety display instrument panel (if designed for safety display instrument display).	
	If the sensor signal is designed to be disconnected when the reactor module is moved then it will be necessary to test the signal from the sensor to the disconnect and then from the disconnect to the MCR display.	

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Table 14.2-63: Module Protection System Test #63 (Continued)

System Level Test #63-2					
Test Objective	Test Method	Acceptance Criteria			
 i. Verify the reactor trip logic fails to a safe state such that loss of electrical power to an MPS separation group results in a reactor trip state for that separation group. ii. Verify the ESF logic fails to a safe state such that loss of electrical power to an MPS separation group results in a predefined safe state for that separation group. 	This test will verify initiation of a trip state for MPS separation groups on loss of power to that separation group. Component actuation is not required or verified. i. Remove power from one separation group of one reactor trip function listed in Table 7.1-3 to provide a trip state for that separation group. Repeat tests for all separation groups for all reactor trip functions. ii. Remove power from one separation group of one ESF actuation function listed in Table 7.1-3 to provide a predefined state for that separation group. Repeat tests for all separation groups	 i. Loss of electrical power in a separation group results in a reactor trip state for that separation group. [ITAAC 02.05.14] ii. Loss of electrical power in a separation group results in the predefined state for that separation group. [ITAAC 02.05.15] 			
Contain Local Total #62.2	for all ESF actuation functions.				
System Level Test #63-3	I=	In			
Test Objective	Test Method	Acceptance Criteria			
 i. Verify MPS operating bypass interlocks are automatically established when the associated interlock condition is satisfied and automatically removed when the condition is not satisfied. ii. Verify MPS operating bypasses can be manually established when the associated permissive condition is satisfied and automatically removed when the condition is not satisfied. iii. Verify MCR alarms when operating bypasses are established. 	 This test will verify operation of each operating bypass interlock and operating bypass permissive. Component actuation is not required or verified. Table 7.1-5 contains the following information: The identification of each operating bypass interlock and operating bypass permissive and their logic. The function of the operating bypass i. a. Simulate the logic for an operating bypass interlock. b. Remove the logic. Repeat test for all operating bypass interlocks. ii. a. Simulate the logic for an operating bypass permissive and manually establish the operating bypass. b. Remove the logic. Repeat test for all operating bypass. b. Remove the logic. Repeat test for all operating bypass permissives. 	 i. a. The operating bypasses are automatically established. b. The operating bypasses are automatically removed. [ITAAC 02.05.18] ii. a. The operating bypasses can be manually established. b. The operating bypasses are automatically removed. [ITAAC 02.05.19] iii. Each established operating bypass is alarmed in the MCR. [ITAAC 02.05.22] 			

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Table 14.2-63: Module Protection System Test #63 (Continued)

Test Objective		Test Method	Acceptance Criteria
i.			 i. A reactor trip signal is displayed in the MCR for all 2 out of 4 logic combinations of each reactor trip function. [ITAAC 02.05.08] ii. An ESF actuation signal is displayed in the MCR for all 2 out of 4 logic combinations each reactor ESF actuation function. [ITAAC 02.05.09]
_	rstem Level Test #63-5 est Objective	Test Method	Acceptance Criteria
i.	Verify the MPS manually actuates a reactor trip. Verify the MPS automatically actuates a reactor trip.	This test will verify the automatic and manual reactor trips. Reactor trip actuation is verified by reactor trip breaker actuation. Only one trip function is required to perform the automatic reactor trip,	i. The reactor trip breakers open. [ITAAC 02.05.12] ii. The reactor trip breakers open. [ITAAC 02.05.10]
		i. Initiate a manual reactor trip from the MCR. ii. Initiate an automatic reactor trip signal by simulating any single reactor trip function.	

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Table 14.2-63: Module Protection System Test #63 (Continued)

System Level Test #63-6

Test 63-6 is performed at hot functional testing concurrently with TGS test #33-1 (reference 14.2.12.33) to allow testing of ESF actuations at normal operating pressure and elevated temperatures. Test #33-1 heats the RCS from ambient conditions to the highest temperature achievable by MHS heating. These hot functional testing conditions provide the highest differential pressure and temperature conditions that can be achieved prior to fuel load.

Te	st Objective	Tes	st Method	Acc	:ep	tance Criteria
i.	Verify the MPS can manually actuate ESF equipment from the MCR. Verify deliberate operator action is	sigi	ure 7.1-1 identifies all ESF actuation nals such as CVCS isolation and CNTS lation.	i.	to	e MPS actuates the ESF equipment perform its safety-related function described in Table 7.
	required to return the ESF actuated equipment to its non-actuated position.	Tab Thi	ole 7.1-4 lists all of the ESF functions. Is test will verify the design response ESF actuation signals using both a		Eac of a	ch ECCS valve opens after receipt an ESF signal and after RCS essure is decreased to the
iii.	 Verify the MPS can automatically actuate ESF equipment from all ESF actuation signals. 	sing fun act	gle manual ESF signal and a single ESF nction to provide an automatic ESF uation signal. All manual and tomatic ESF actuation signals are		the des 6.3	eshold pressure for operation of e inadvertent actuation block scribed in described in Section .2.2.
		tes	ted.	[ITA	۱AC	02.01.13]
			, 3,	[ITA	AAC	02.01.14]
			oplying bypass steam to the ndenser.	[ITA	AAC	02.01.15]
				[ITA	AAC	02.01.18]
		i.	Initiate a manual ESF actuation signal from the MCR.	[ITA	AAC	02.01.19]
		ii.		[ITA	AAC	02.01.20]
				[ITA	AAC	02.05.13]
			b. Remove the manual ESF	[ITA	AAC	02.05.16]
			actuation signal.	ii.	a.	The actuated equipment cannot
			c. Use the MCR enable nonsafety			be operated from the MCR.
			control switch to allow operation of the ESF actuated equipment		b.	The actuated equipment cannot be operated from the MCR.
			from the MCR. Repeat for all MCR manual ESF		c.	The ESF equipment can be operated from the MCR.
				[ITAAC 02.01.13] [ITAAC 02.01.14]		02.01.13]
		III.	Initiate an automatic ESF actuation signal. The test may be performed			02.01.14]
			with the RCS at ambient conditions.	[ITA	AAC	02.01.15]
			Repeat for all ESF actuation signals.	[ITA	AAC	02.05.16]
				iii.	ESF rela	e MPS automatically actuates the equipment to perform its safety- ated function as described in ole 7.1-4.
				[ITA	AAC	02.01.13]
				[ITA	AAC	02.01.14]
				[ITA	AAC	02.01.15]
				[ITA	AAC	02.01.18]
				[ITAAC 02.01.20]		02.01.20]
				[ITA	AAC	02.05.11]
				[ITA	۸AC	02.05.16]

Table 14.2-63: Module Protection System Test #63 (Continued)

System Level Test #63-7

Test #63-7 is performed concurrently with Test #63-6 which operates all of the ESF actuation valves during hot functional

Test #63-7 records the stroke times of containment isolation valves (CIVs) as they travel to their ESF-actuated position with the RCS pressure at normal operating pressure.

Test Objective	Test Method	Acceptance Criteria	
Verify the CIVs operate to satisfy their ESF-actuated design stroke time.	Table 6.2-10 contains the design closure time for containment isolation valves. Time the operation of all CIVs as they actuate to their ESF position during the manual ESF actuation testing in Test #63-6.	 i. Each containment isolation valve travels from fully open to fully closed in less than or equal to the time listed in Section 6.2.4.3 after receipt of a containment isolation signal. [ITAAC 02.01.08] [ITAAC 02.05.17] 	

System Level Test #63-8

This test will verify the time response of MPS reactor trip and ESF actuation signals. The reactor trip test verifies response time through reactor trip breaker actuation. The ESF response time is tested through the de-energization of the associated solenoid valve or the opening of the pressurizer heater supply breaker. ESF valve response times are tested in Test #63-7.

Test Objective	Test Method	Acceptance Criteria
Verify the MPS response times from	Section 7.1.4 contains a description of	The MPS reactor trip functions listed in
sensor output through:	design basis event actuation delays	Table 7.1-3 and ESF functions listed in
reactor trip function.	listed in Table 7.1-6. The actuation delays do not include ESF actuated component	,
valves. iii. opening of the pressurizer heater supply breaker for the pressurizer heater trip.	Perform a time response test for the actuation signals listed in Table 7.1-6.	[ITAAC 02.05.17]
	Response time testing for ESF actuated CNTS, DHRS, ECCS and DWS valves are found in Test #63-7.	

Test Objective	Test Method	Acceptance Criteria
	actions required to modify tunable	All actions described in Section 7.2.9.1 are required to modify tunable parameters.
	A test will be performed to verify that all manual actions described in Section 7.2.9.1 are required to modify tunable parameters.	[ITAAC 02.05.02]

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Table 14.2-63: Module Protection System Test #63 (Continued)

Sy	stem Level Test #63-10			
Test Objective		Test Method	Acceptance Criteria	
i.	functions when one of its separation	Section 7.2.4.2 discusses the operation of the MPS maintenance bypass operation for the MPS safety function module	no trip to the respective scheduling and voting module.	
	groups is placed in maintenance bypass.	(SFM).	b. There is no change to the 2 out of 4 voting logic for the separation	
ii.	Verify MPS maintenance bypasses	Place an SFM in maintenance bypass by	group.	
	are indicated in the main control	using the out of service and trip/bypass	[ITAAC 02.05.21]	
	room.	switches associated with the SFM.	ii. The inoperable status of the SFM is provided in the MCR.	
		Repeat tests for all SFMs.	[ITAAC 02.05.23]	
Sy	stem Level Test #63-11			
Te	st Objective	Test Method	Acceptance Criteria	
	,	i. A test will be performed to verify the	i. Water is added to the RCS.	
	erator workstations in the MCR	CVCS can add water to the RCS after	ii. Water is added to containment.	
	erate to perform important human tions.	a containment isolation signal using the O-1 override switch and MCR	[ITAAC 02.05.20]	
acı	lions.	controls.	[ITAAC 02.05.26]	
		 ii. A test will be performed to verify the CFDS can add water to containment after a containment isolation signal using the O-1 override switch and MCR controls. 	(i. and ii.)	

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Table 14.2-64: Plant Protection System Test # 64

Preoperational test is required to be performed once. The PPS is described in Section 7.0.4.3. PPS functions are not verified by PPS tests. PPS functions verified by other tests are:				
 The PPS supports the CRVS by providing actuation and control signals to the CRE isolation dampers. 	nonsafety-related	CRHS Test #18-1		
 The PPS supports the control room habitability system (CRHS) by providing actuation and control signals. 	nonsafety-related	CRHS Test #18-1		
 The PPS supports the CRVS by providing actuation and control signals to the outside air isolation dampers. 	nonsafety-related	CRVS Test #19-3		
Prerequisites				
Prerequisites associated with PPS testing Test #" heading.	are identified in the referenced test abs	stract cited under the "Function Verified by		
Component Level Tests				
None				
System Level Tests	,			
None				

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Table 14.2-65: Neutron Monitoring System Test # 65

Preoperational test is required to be performed for each NPM.					
The NMS is described in Section 7.0.4.2 and the functions verified by this test are:					
System Function Function Verified by Test #					
 The NMS supports the MPS by providing neutron flux data for various reactor trips. 	safety-related	Test #63-4			
The NMS supports the MPS by providing information signals for PAM.	nonsafety-related	Test #66-2			
 The NMS supports the MPS by providing information signals for PAM during CNV flooded conditions. 	nonsafety-related	Test #66-2			
Prerequisites					
Prerequisites associated with NMS testing Test #" heading.	g are identified in the referenced test al	ostract cited under the "Function Verified by			
Component Level Tests					
None					
System Level Tests					
None					

Table 14.2-66: Safety Display and Indication Test # 66

Test #66 Component-level testing for the module-specific SDIS is required to be performed for each NPM.

Test # 66 Component-level testing for the common SDIS is required to be performed once.

Test #66-1 System-level testing for the module-specific SDIS is required to be performed for each NPM to verify proper trending of RCS pressure and temperature.

Test #66-2 System-level testing for the module-specific SDIS is required to be performed for each NPM to verify PAM variables are displayed and alarms retrieved.

SDIS is described in Section 7.0.4.4 and the functions verified by this test are:

System Function	System Function Categorization	Function Verified by Test #
The SDIS actively supports the CRB by providing the main control roon accident monitoring plant conditions.	nonsafety-related	 i. Module-specific SDIS component-level tests ii. Common SDIS component-level tests iii. Test #66-1 iv. Test #66-2
2. The SDIS actively supports the PCS is providing plant status and indication data to the plant data historian.		 i. Module-specific SDIS component-level tests ii. Common SDI component-level tests iii. Test #66-1 iv. Test #66-2
The ICIS supports the MPS by providing RXC temperature information.	nonsafety-related	Test #66-2
4. The ECCS supports MPS by providir PAM instrument information signal		Test #66-2
5. The RCS supports the MPS by providing PAM instrument information signals.	nonsafety-related	Test #66-2
6. The CNTS supports the MPS by providing PAM information signals.	nonsafety-related	Test #66-2
7. The RMS supports the RXB by monitoring radiation levels in the building in proximity of the bioshield.	nonsafety-related	Test #66-2
8. The NMS supports the MPS by providing information signals for PAM.	nonsafety-related	Test #66-2
The NMS supports the MPS by providing information signals for PAM during CNV flooded condition	nonsafety-related s.	Test #66-2
10. The DHRS supports the MPS by providing PAM instrument information signals.	nonsafety-related	Test #66-2
11. The EDSS supports the PPS by providing common EDSS operating parameter information signals.	nonsafety-related	Component-level test: Common SDIS test iii.
12. The EDSS supports the MPS by providing module-specific EDSS operating parameter information signals.	nonsafety-related	Component-level test: Module-Specific SDIS test iii.

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Table 14.2-66: Safety Display and Indication Test # 66 (Continued)

Prerequisites

Verify an instrument calibration has been completed, with approved records and within all calibration due dates, for all instruments required to perform this test.

Note:

Testing of PAM Type B and Type C displays and alarms is performed in Test #66-1.

Note:

Testing of reactor module level, pressure, and temperature and flow instruments is performed in Test #66-2.

		and temperature and flow instruments is p	performed in Test #66-2.
	mponent Level Tests: Common SDIS		
	st Objective	Test Method	Acceptance Criteria
i.	Verify the proper valve position indication for each valve that provides input to the PPS.	Open and close each valve listed in Table 7.1-8.	The valve opens and closes as indicated by a common SDIS display and an MCR workstation display.
ii.		and ELVS voltmeter monitored by PPS	The radiation signal is displayed by a common SDIS display and an MCR workstation.
iii.		Provide a simulated signal for each EDSS and ELVS voltmeter monitored by PPS listed in Table 7.1-8.	The voltage signal is displayed by a common SDIS display and an MCR workstation.
iv.		Provide a simulated signal for each instrument monitored by PPS listed in Table 7.1-8.	The instrument signal is displayed by a common SDIS display and an MCR workstation.
Co	mponent Level Tests: Module Specif	ic SDI Test	
Tes	st Objective	Test Method	Acceptance Criteria
i.	Verify the proper valve position indication for each ESF valves that provide input to MPS.	 i. With the reactor module assembled, open and close the valves listed in Table 7.1-2. ii. Provide a real or simulated signal for each reactor safety valve position (Table 7.1-2). 	 i. The valves open and close as indicated by a module-specific SDIS display and an MCR workstation display. ii. The valve opens and closes as indicated by a module-specific SDIS display and an MCR workstation display.
ii.	Verify radiation monitor indication is obtained in the MCR for each radiation monitor that provides input to the MPS.	radiation monitor monitored by MPS	The radiation monitor signal is displayed by a module-specific SDIS display and an MCR workstation.
	indication is obtained in the MCR for each voltmeter that provide input to the MPS.	and ELVS voltmeter monitored by MPS (Table 7.1-2).	The voltage signal is displayed by a module-specific SDIS display and an MCR workstation.
	obtained in the MCR for each radiation monitor that provides input to the MPS.		The neutron flux signal is displayed by a module-specific SDIS display and an MCR workstation display.
v.	Verify a neutron flux instrument fault indication is obtained in the MCR for each signal that provides input to the MPS.	neutron flux instrument fault monitored	The neutron flux instrument fault is displayed by a module-specific SDIS display and an MCR workstation display.

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Table 14.2-66: Safety Display and Indication Test # 66 (Continued)

Test Objective	Test Method	Acceptance Criteria
Verify that the output signals from the reactor module level, pressure, temperature and flow instruments listed in Table 7.1-2 properly trend while increasing RCS temperature and pressure. Note: This is not a verification of instrument calibrations.	Increase RCS temperature from ambient to the highest temperature achievable by MHS heating. Using the MCS historian record the engineering values for the output of the instruments described in the test objective. Record data at approximately 50 °F intervals from ambient temperature to the maximum RCS temperature. Note: Instrument signals are provided to the module-specific SDIS display and the main control room workstations.	Trended data shows agreement between the two divisional instruments or the four safety group instruments monitoring the same variable.
System Level Test #66-2		
Test Objective	Test Method	Acceptance Criteria
Type B and C variables are retrieved in the MCR. iii. Verify module-specific PAM Type D	PAM Type B and C variables listed in Table 7.1-7. ii. Increase and/or decrease a simulated injection signal for the PAM Type B and C variables listed in Table 7.1-7 to obtain its associated alarm. iii. Simulate an injection signal for the PAM Type D variables listed in Table 7.1-7	 i. The PAM Type B and C variables listed in Table 7.1-7 are retrieved and displayed on the SDI displays in the MCR. [ITAAC 02.05.25] ii. The alarms associated with the PAM Type B and C variables listed in Table 7.1-7.are retrieved and displayed or the SDI displays in the MCR. iii. The PAM Type D variables listed in Table 7.1-7 are retrieved and displayed on the SDIS displays in the

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Table 14.2-67: Fixed Area Radiation Monitoring System Test # 67

The fixed-area radiation monitoring sy	stem is described in Section 12.3.4 and t	the function verified by this test is:
System Function	System Function Categorization	Function Verified by Test #
The fixed-area radiation monitoring system supports the following buildings by monitoring radiation levels:	nonsafety-related	Component-level test
ANB CRB RWB TGB		
RMS function verified by another test is	s:	
System Function	System Function Categorization	Function Verified by Test #
The RMS supports the RXB by monitoring radiation levels in the building in	nonsafety-related	Test #66-2
proximity of the bioshield.		
-		
proximity of the bioshield. Prerequisites Verify an instrument calibration has been instruments required to perform this test. Component Level Tests	completed, with approved records and wi	thin all calibration due dates, for all
Prerequisites Verify an instrument calibration has been instruments required to perform this test.		thin all calibration due dates, for all Acceptance Criteria
Prerequisites Verify an instrument calibration has been instruments required to perform this test. Component Level Tests Test Objective	Test Method Actuate the check source on a fixed	
Prerequisites Verify an instrument calibration has been instruments required to perform this test. Component Level Tests Test Objective i. Verify each fixed airborne radiation monitor's response to a known	Test Method Actuate the check source on a fixed airborne radiation monitor listed in Table 12.3-10. Repeat test for the remainder of fixed airborne radiation monitors. Actuate the check source on a fixed area	Acceptance Criteria MCR display and local, visual observation indicate the following: i. The main control room audible and visual alarms are received. ii. The local readout, audible alarm and

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Table 14.2-68: Communication SystemTest # 68

Preoperational test is required to be performed after construction turnover of the communication system (COMS The COMS is described in Section 9.5.2 and the function verified by this test is:			
System Function	System Function Categorization	Function Verified by Test #	
The COMS supports the following locations by providing voice and data communications within the building and surrounding areas.	nonsafety-related	Component-level tests i. through iv	
 RXB TGB RWB CRB Security Buildings ANB Diesel Generator Building Administrative and Training Building Central Utility Building Warehouse Building Fire Water Building 			

Prerequisites

i. Required communications system site acceptance tests have been completed and approved.

Component Level Tests

Co	Component Level Tests			
Te	st Objective	Test Method	Acceptance Criteria	
i.	Verify plant public address/general alarm (PA/GA) system can be heard throughout the plant site.	Station test personnel in each required test area of the plant to monitor the PA/GA system. i. Use the public address to provide a test announcement. ii. Use the general alarm system to provide a test alarm.	 i. The test announcement is heard at each test site. ii. The test emergency alarm is heard at each test site. 	
ii.	Verify plant radio communications can be heard throughout the plant site.	Station test personnel in each required test area of the plant to communicate using plant radios.	The plant radio communication is obtained at each test site.	
iii.	Verify the sound powered telephone system can be used for voice communication.	Test each sound powered telephone.	All channels of each sound powered telephone can be used to communicate with another sound powered telephone.	
iv.	Verify wireless communication throughout the plant site.	Station test personnel in each required test area of the plant to communicate using voice and data communication.	The voice and data communication is obtained at each test site.	
v.	Verify the central alarm station is equipped with a conventional (landline) telephone service which can be used to communicate with the control room and local law enforcement authorities.	Test the conventional (landline) service from the central alarm station to the control room and local law enforcement authorities.	The conventional service connects with the control room and the local law enforcement authorities. [ITAAC 03.16.11]	

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Table 14.2-68: Communication SystemTest # 68 (Continued)

vi.	Verify that plant radio communications maintains continuous communications	Test communications with the plant radio system in areas described in the physical protection program boundaries	The radios will provide continuous communications in all test areas.		
		and areas described in the contingency response event areas.	[ITAAC 03.16.12]		
vii.	Verify all nonportable communication devices (including conventional telephone systems) in the central alarm station remain operable during the loss of normal power.	Remove normal power from the central alarm station nonportable communication devices.	The nonportable communication devices establish connections with the normal power removed. [ITAAC 03.16.13]		
Sys	System Level Tests				
No	ne				

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Table 14.2-69: Seismic Monitoring System Test # 69

The SMS is described in Section 3.7.4. The SMS is a site-specific system, and the SMS design is the responsibility of the COL applicant as indicated by COL item 3.7-1.

COL Item 14.2-6: A COL applicant that references the NuScale Power Plant design certification will provide a test abstract for the SMS pre-operational testing.

System Function	System Function Categorization	Function Verified by Test #
As described in Section 3.7.4	nonsafety-related	Provided by COL applicant
Prerequisites	<u> </u>	<u> </u>
Provided by COL applicant		
Component Level Tests		
Provided by COL applicant		
System Level Tests		
Provided by COL applicant		

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Table 14.2-70: Hot Functional Testing Test # 70

The following identifies the te	ests employed in support of th	ne performance of hot functional testing.	
Hot Functional Testing Tests	Test Objective	Verified by Test #	Tested Function Categorization
CES	 i. Verifies the automatic operation of the CES to establish and maintain design vacuum for the CNV. ii. Verify radiation isolation on high radiation level in 	i. CE Test #41-1 ii. CE Test #41-2 iii. CE Test #41-3	nonsafety-related
	the ABS. iii. Verifies the CES supports RCS leakage detection.		
CFD	 i. Verifies the CFDS can automatically drain the CNTS. This test may be completed as a prerequisite to hot functional testing because the completion of the test does not require elevated water temperatures. ii. Verifies the CFDS can automatically flood the CNTS. This test may be completed as a prerequisite to hot functional testing because the completion of the test does not require elevated water temperatures. iii. Verifies the CFDS can provide borated water to the RCS during a beyond design basis accident. (Important human action). iv. Verifies the CFDS responds to high radiation conditions. 		nonsafety-related
CVC	i. Verifies CVCS automatic makeup to maintain pressurizer level. ii. Verifies automatic pressurizer pressure control.	i. CVCS Test #38-1 ii. CVCS Test #38-2 iii. CVCS Test #38-3	nonsafety-related
	iii. Verifies CVCS automatic boration and dilution of the RCS.		

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Table 14.2-70: Hot Functional Testing Test # 70 (Continued)

ECCS	Each ECCC walve among -ft - "	: MDC Tost #62.6	noncafoty related
ECCS	Each ECCS valve opens after	i. MPS Test #63-6	nonsafety-related
	receipt of an ESF signal and	1	
	after RCS pressure is decreased		
	to the threshold pressure for		
	operation of the inadvertent		
	actuation block.		
FWS	i. Verifies the FWS	i. Test TG #33-1	nonsafety-related
	automatically controls flow	/ ii. Test TG #33-1	
	to the SGs to maintain SG		
	inventory.		
	ii. Verifies the FWS		
	automatically cools the		
	turbine generator bypass		
	steam flow in the main		
	steam desuperheater.		
ICIS	Verifies proper temperature	Test ICI #49-1	nonsafety-related
	indication is obtained from the	2	
	ICIS thermocouples.		
MHS	i. Verifies the MHS is capable	i. TG Test #33-1	nonsafety-related
	of heating the RCS to a	ii. TG Test #33-1	
	temperature sufficient to	iii. TG Test #33-1	
	obtain criticality.	11. 13 1636 #33 1	
	ii. Verifies the MHS is capable		
	of heating the RCS to		
	establish natural		
	circulation flow sufficient		
	to obtain criticality.		
	iii. Verifies a local grab sample	2	
	can be obtained from an		
	MHS grab sample device		
	indicated on the MHS		
	piping and		
	instrumentation diagram.		
MPS	i. Verifies design responses	i. Test #63-6	safety-related
5	to manual ESF signals.		Salety Telated
	_	ii. Test #63-7	
		iii. Test #63-6	
	isolation valves closure times.	iv. Test #63-4	
		v. Test #63-5	
	iii. Verifies design responses	vi. Test #63-6	
	to automatic ESF signals.		
	iv. Verifies design responses		
	to automatic reactor trip		
	signals.		
	v. Verifies automatic enabling	9	
	and reset of operational		
	bypasses.		
	vi. Verifies the ECCS valves		
	closes when the CVCS		
	provides water to reset the	<u> </u>	
	ECCS valves.	-	
	Eccs valves.		

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Table 14.2-70: Hot Functional Testing Test # 70 (Continued)

PSS	i. Verifies sampling capability	Test #53-1	nonsafety-related
	of the primary sampling	Test #53-2	
	points.	Test #53-3	
	ii. Verifies sampling capability		
	of the containment		
	sampling points.		
	ii. Verifies sampling capability		
	of the secondary sampling		
	points.		
SDIS	Verify that the output signals	Test #66-1	nonsafety-related
	from the reactor module level,		
	pressure, temperature, and		
	flow instruments listed in Table		
	7.1-2 properly trend while		
	increasing RCS temperature		
	and pressure.		
TG	i. Verifies the TGS	i. Test #33-1	nonsafety-related
		ii. Test #33-2	
	turbine bypass flow to the		
	main condenser.		
	ii. Verifies the turbine		
	generator can obtain		
	synchronous speed.		

Prerequisites

Prerequisites associated with performing hot functional testing are identified in the referenced test abstract cited under the "Verified by Test #" heading.

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Table 14.2-71: Module Assembly Equipment Bolting Test # 71

Preoperational test is required to be	performed once.			
The MAE bolting is described in Section	on 9.1.5. MAE bolting functions are no	t verified by MAE bolting tests. MAE		
bolting functions verified by other tests are:				
System Function	System Function Categorization	Function Verified by Test #		
 MAE bolting supports the CNTS actively by providing material handling to allow for disassembly and reassembly of the CNV lower flange. 	nonsafety-related	Test #52-2		
 MAE bolting supports the RPV actively by providing material handling to allow for disassembly and reassembly of the RPV lower flange. 	nonsafety-related	Test #52-2		
Prerequisites	•			
Prerequisites associated with MAE bolting Verified by Test #" heading.	ng testing are identified in the referenced	d test abstract cited under the "Function		
Component Level Tests				
None				
System-Level Tests				
None				

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None

Table 14.2-72: Steam Generator Flow-Induced Vibration Test # 72

SG flow-induced vibration testing is performed during startup testing. There are no preoperational tests for SG.				
SG flow-induced vibration testing is performed consistent with the requirements of the NuScale "Comprehensive Vibration				
Assessment Program" as described in the "Comprehensive Vibration Assessment Program (CVAP) Technical Report," TR-				
0716-50439. The CVAP is addressed in DCD Section 3.9.2. The steam generators are discussed in DCD Section 5.4.1.				
System Function	System Function Categorization	Function Verified by Test #		
None	N/A	N/A		
Prerequisites:				
N/A				
Component Level Tests				

Table 14.2-73: Security Access Control Test # 73

Security access control is described in NuScale Power, LLC, "NuScale Design of Physical Security Systems", TR-0416-48929, Revision 0.				
System Function	System Function Categorization	Function Verified by Test #		
The security access controls support the security plan described in "NuScale Design of Physical Security Systems", TR-0416-48929, Revision 0.	security-related	Component level test i.		
Prerequisites				
 Security access control boundary for t established. 	he protected and vital areas, described in	the security technical report, are		
Component Level Tests				
Component reser 16212				
· · · · · · · · · · · · · · · · · · ·	Test Method	Acceptance Criteria		
Test Objective i. Verify an access control system with a numbered photo identification badge system which will control access to vital areas within the RXB and CRB to authorized personnel.		i. The access points do not allow access to unauthorized badges. ii. The access points allow authorized personnel. [ITAAC 03.16.04]		
Test Objective i. Verify an access control system with a numbered photo identification badge system which will control access to vital areas within the RXB	Use authorized and unauthorized identification badges in all vital area access points in the RXB and CRB identified in "NuScale Design of Physical Security Systems", TR-0416-48929,	 i. The access points do not allow access to unauthorized badges. ii. The access points allow authorized personnel. 		

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Table 14.2-74: Security Detection and Alarm-Test # 74

Preoperational test is required to be performed once. Security detection and alarm is described in NuScale Power, LLC, "NuScale Design of Physical Security Systems", TR-0416-48929, Revision 0.				
acts to satisfy t requirements o	he functional described in "NuScale ical Security Systems", TR-	security-related	Component level test i-v	
i. Required so	ecurity system site accepta	nce tests have been completed and appro	ved.	
Component L	evel Tests			
Test Objective)	Test Method	Acceptance Criteria	
i. Unoccupie designed v intrusion d annunciate station.	d vital areas will be vith locking devices and etection devices that e in the central alarm	Access to all unoccupied vital areas that are identified in the "NuScale Design of Physical Security Systems", TR-0416- 48929, Revision 0.	 i. Verify the access door is locked. ii. Upon entry into the room verify an intrusion alarm is received in the central alarm station. [ITAAC 03.16.05] 	
transmissio	arm devices including on lines to annunciators -indicating and self-	 a. Insert a signal real or simulated tamper signal. b. Insert a signal real or simulated of a component failure for all alarm devices and transmission lines in the RXB and CRB. c. Place all security alarm devices in the RXB and CRB on standby power. 	Verify alarm annunciation is received in the central alarm station for each test method. The alarm must indicate the type and location of the alarm. [ITAAC 03.16.07]	
systems pr	etection and assessment ovides visual and audible unciation in the central on.	Put all intrusion detection equipment described in "NuScale Design of Physical Security Systems", TR-0416-48929, Revision 0 into an alarm state.	Verify an audible and visual alarm is received in the central alarm station. [ITAAC 03.16.08]	
equipment alarm annu alarm, alari indication a location, al	,	Place all intrusion detection equipment	Verify the intrusion detection system recording system records each alarm to include: a. Location of the alarm b. Type of alarm c. Alarm circuit d. Date e. Time (this test can be done in conjunction with audible and visual alarm testing) [ITAAC 03.16.09] i. Verify the locking device prevents	
will be alar detection of locking dev	rexits in the RXB and CRB med with intrusion devices and secured by vices that allow prompt ng an emergency.	ii. Exit each of the RXB and CRB exits.	ii. Verify the exit allows for prompt exit of the building and alarms in the central alarm station when opened.	

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Table 14.2-75: Initial Fuel Loading Precritical Test (Test #75)

Startup test is required to be performed for each NPM.

This test is performed after initial fuel loading but prior to initial criticality.

Test Objectives

- i. Identify the sequence for precritical testing (after fuel load and prior to criticality).
- ii. The pre-critical tests are:
 - a. Reactor Coolant System Flow Measurement Test (Test #77)
 - b. Reactor Module Temperatures Test (Test #78)
 - c. Primary and Secondary System Chemistry Test (Test #79)
 - d. Control Rod Drive System Manual Operation, Rod Speed, and Rod Position Indication Test (Test #80)
 - e. Control Rod Assembly (CRA) Drop Time Test (Test #81)
 - f. Pressurizer Spray Bypass Flow Test (Test #82)

Prerequisites

None

Test Method

- Identify the specific plant conditions required for each precritical test procedure to maintain technical specification operability.
- ii. Identify the prerequisites required for each precritical test procedure.
- iii. Determine the test sequence for precritical testing based on technical specification requirements and test prerequisites.

Acceptance Criterion

The sequence for precritical testing has been determined.

Table 14.2-76: Initial Fuel Load Test (Test #76)

The Initial Fuel Load Test is required to be performed for each NPM.

This test is performed prior to initial fuel load.

Test Objectives

- i. Conduct initial fuel load with no inadvertent criticality.
- ii. Install fuel assemblies and control components at the locations specified by the design of the initial RXC.

Prerequisites

- i. Plant systems required for initial fuel loading have completed preoperational testing.
- ii. Plant systems required for initial fuel loading have been aligned per operations procedures.
- The design of the initial RXC that specifies the final core configuration of fuel assemblies and control components is completed.
- iv. A core load sequence has been approved.
- v. Neutron monitoring data from a previous NPM initial fuel loading or calculations showing the predicted response of monitoring channels are available for evaluating monitoring data.
- vi. The lower RPV is installed in the RPV support stand.
- vii. Control room communications are established.
- viii. RXB radiation monitors are functional.

Test Method

- i. The overall process of initial fuel loading will be supervised by a licensed senior reactor operator with no other concurrent duties.
- ii. Install fuel and control components per approved procedures.
- iii. Monitor boron concentration inside the RPV periodically during fuel load to ensure it satisfies TS.
- iv. Monitor neutron counts during the load of each fuel assembly and plot an independent inverse count rate ratio for each source range detector after each fuel load assembly is loaded.
- v. Verify neutron count data are consistent with calculations showing the predicted response. For fuel loading of the second NPM and all subsequent NPMs use data obtained from previous fuel loadings.
- vi. Demonstrate the inverse count rate ratio does not show significant approach to criticality.
- vii. Maintain the status of the core loading.
- viii. Maintain communication between fuel handling personnel and the MCR.

Acceptance Criterion

Each fuel assembly and control component is installed in the location specified by the design of the initial RXC.

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Table 14.2-77: Reactor Coolant System Flow Measurement Test (Test #77)

The Reactor Coolant System Flow Measurement test is required to be performed for each NPM.

This test is performed after initial fuel loading but prior to initial criticality.

Test Objective

Verify that the RCS flow is sufficient to ensure adequate boron mixing in the RCS coolant.

Prerequisites

- i. The core is installed.
- ii. The NPM is fully assembled.
- iii. The RCS is at hot zero power (RCS at normal operating pressure with RCS temperature at the maximum temperature obtainable when heated only by the MHS).
- iv. The RCS flow meters have been calibrated.

Test Method

Record RCS flow using MCR indication.

Acceptance Criterion

The RCS flow at hot zero power (HZP) satisfies the minimum RCS flow assumed in the safety analysis.

Table 14.2-78: Reactor Module Temperatures Test (Test #78)

Startup test is required to be performed for each NPM.

This test is performed after initial fuel loading but prior to initial criticality.

Test Objectives

- i. Perform a cross calibration of the RTDs monitored by the MPS listed in Table 7.1-2.
- ii. Verify incore thermocouple resistance leakage satisfies manufacturer's criteria.

Prerequisites

- The core is installed.
- ii. The NPM is fully assembled.
- iii. The calibration of reactor coolant system RTDs has been completed.

Test Method

- i. With the RCS at ambient temperature and isothermal conditions record the following data:
 - · Main control room indication of RTD temperatures monitored by MPS
 - Main control room indication of incore thermocouples temperatures
 - · Leakage resistance of the incore thermocouples
- ii. Increase RCS temperature by approximately 50°F.
- iii. Record RTD and incore thermocouple data at isothermal conditions.
- iv. Repeat data collection until RCS temperature is at the highest temperature obtainable using only the MHS.
- v. Cross-calibrate RTD temperatures monitored by MPS that monitor the same variable.

Acceptance Criteria

- i. The cross calibration of the reactor coolant system RTDs has been completed.
- ii. The leakage resistance of the fixed incore detectors satisfies manufacturer's recommendations.

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Table 14.2-79: Primary and Secondary System Chemistry Test (Test #79)

Startup test is required to be performed for each NPM.

This test is performed at approximately 25, 50, 75, and 100 percent reactor thermal power.

Test Objective

Verify water quality in the primary system and secondary system using the PSS.

Prerequisites

- i. The PSS instruments have been calibrated.
- ii. The NPM is fully assembled.
- iii. The RCS is at hot zero power (RCS at normal operating pressure and RCS temperature at the maximum temperature obtainable when heated only by the MHS).

Test Method

- i. Use the PSS to sample the normal primary system sample points listed in Table 9.3.2-1.
- ii. Use the PSS to sample the normal secondary system sample points listed in Table 9.3.2-3.
- iii. To the extent practical, responses of PSS radiation monitors should be verified by laboratory analyses of grab samples taken at the same process location.
- iv. Conduct the test at steady-state condition at approximately 25, 50, 75, and 100% reactor thermal power.

Acceptance Criterion

The sample analysis satisfies the limits specified in plant procedures.

Table 14.2-80: Control Rod Drive System - Manual Operation, Rod Speed, and Rod Position Indication Test (Test #80)

Startup test is required to be performed for each NPM.

This test is performed after initial fuel loading but prior to initial criticality.

Test Objectives

- i. Verify the ability to manually fully insert and fully withdraw individual control rod assemblies (CRAs) from the MCR.
- ii. Verify CRA rod position indications provide indication of rod movement.
- iii. Verify individual CRA position indications are within the required number of steps of their associated group position.
- iv. Verify the rod insertion and withdrawal speeds are within design limits.

Prerequisites

- The core is installed.
- ii. The NPM is fully assembled.
- iii. The RCS is at hot zero power (RCS at normal operating pressure and RCS temperature at the maximum temperature obtainable when heated only by the MHS).
- iv. All RCS temperatures satisfy the minimum technical specification temperature for criticality.
- v. The nuclear instrumentation system is calibrated and operable.
- vi. The SDM is within the limits specified in the core operating limits report.

Test Method

- i. Individually withdraw and insert each shutdown bank and regulating bank from the MCR a sufficient number of steps to verify that the individual CRA positions are within the required number of steps of their group position as required by TS. Only the tested bank will be withdrawn. All other banks are fully inserted. Repeat the test until all shutdown banks and regulating banks are tested.
- ii. With all shutdown and regulating banks fully inserted, fully withdraw and then fully insert one CRA. Repeat these steps until all CRAs are tested.

- i. All CRAs can be individually fully withdrawn and fully inserted from the MCR.
- ii. Individual CRA positions agree with the control rod demand position within design limits for the full range of CRA travel.
- iii. Individual CRA position indications are within the number of steps of their associated group position as required by TS.
- iv. The CRA insertion and withdrawal speeds are within design limits.

Table 14.2-81: Control Rod Assembly Drop Time Test (Test #81)

Startup test is required to be performed for each NPM.

This test is performed after initial fuel loading but prior to initial criticality.

Test Objective

Verify each CRA satisfies the CRA drop time acceptance criteria for RCS flow at 0% reactor thermal power.

Prerequisites

- The core is installed.
- ii. The NPM is fully assembled.
- iii. The RCS is at hot zero power (RCS at normal operating pressure and RCS temperature at the maximum temperature obtainable when heated only by the MHS).
- iv. All RCS temperatures satisfy the minimum technical specification temperature for criticality.
- v. The nuclear instrumentation system is calibrated and operable.
- vi. The SDM is within the limits specified in the core operating limits report.
- vii. A CRA drop time acceptance criteria for 0% thermal reactor power has been developed and is in agreement with the technical specification CRA drop time surveillance requirement.

Test Method

- i. Withdraw each individual CRA.
- ii. Interrupt the electrical power to the associated CRDM.
- iii. Measure the CRA drop time.

- i. Each CRA drop time is less than or equal to the CRA drop time acceptance criteria for HZP.
- ii. The arithmetic average of all CRA drop times is within TS limits.

Table 14.2-82: Pressurizer Spray Bypass Flow Test (Test #82)

Startup test is required to be performed for each NPM.

This test is performed after initial fuel loading but prior to initial criticality.

Test Objective

Verify the pressurizer spray bypass flow rate is adequate to prevent thermal fatigue of the spray line components and provide sufficient mixing in the pressurizer to maintain pressurizer water chemistry similar to the rest of the RCS while avoiding unnecessary energization of the pressurizer heaters.

Prerequisites

- i. The core is installed.
- ii. The NPM is fully assembled.
- iii. The RCS is at hot zero power (RCS at normal operating pressure and RCS temperature at the maximum temperature obtainable when heated only by the MHS).

Test Method

- i. With the automatic pressurizer spray valve closed, adjust the manual spray bypass valve to maintain a continuous spray bypass flow of approximately one gpm.
- ii. If the continuous bypass spray flow requires the operation of the pressurizer backup heaters to maintain the pressurizer pressure setpoint, throttle close the bypass valve until pressurizer pressure is maintained by the proportional heaters.

Acceptance Criterion

The spray bypass valve is throttled to maintain the required bypass flow.

Table 14.2-83: Initial Criticality Test (Test #83)

Startup test is required to be performed for each NPM.

This test is performed after initial fuel loading.

Test Objective

Achieve initial criticality in a controlled manner.

Prerequisites

- i. The RCS is at hot zero power (RCS at normal operating pressure and RCS temperature at the maximum temperature obtainable when heated only by the MHS).
- ii. All RCS temperatures satisfy the minimum technical specification temperature for criticality.
- iii. The nuclear instrumentation system is calibrated and operable.
- iv. The SDM is within the limits specified in the core operating limits report.
- v. An estimated critical position (calculation) has been performed.
- vi. RCS measured boron is at or near the desired estimated critical position value.
- vii. The shutdown banks and the regulating banks are fully inserted.

Test Method

- i. Shutdown banks are withdrawn in sequence using the sequence of a normal plant startup. Gather data to plot the inverse count rate ratio. The inverse count rate ratio is used to monitor reactivity.
- ii. Once all shutdown banks are fully withdrawn, then the regulating bank is withdrawn using the sequence of a normal plant startup. The inverse count rate ratio is plotted to monitoring reactivity for the approach to criticality.
- iii. After criticality is obtained, the regulating bank is confirmed to be above the TS regulating group insertion limit.
- iv. Should criticality be reached with the regulating bank below the insertion limit specified by the core operating limits requirement, the limiting condition of operation test exception is invoked. The RCS boron will be increased until the regulating bank is withdrawn sufficiently to meet the insertion limit.

Acceptance Criterion

The reactor is critical with the regulating banks above their technical specification insertion limit.

Table 14.2-84: Post - Critical Reactivity Computer Checkout Test (Test #84)

Startup test is required to be performed for each NPM.

This test is performed after initial criticality.

Test Objective

Verify proper operation of the reactivity computer to measure reactivity changes in the core during low-power testing.

Prerequisites

- i. The reactor is critical with the neutron flux level within the range for low-power physics testing.
- ii. The RCS temperature and pressure are stable at the normal no-load values.
- iii. The neutron flux level and RCS boron concentration are stable.
- iv. The reactivity computer is installed and internal reactivity computer checks have been completed.

Test Method

- i. Withdraw the regulating bank to achieve a positive startup rate below TS limits.
- ii. Measure the reactor period or doubling time.
- iii. Reinsert the regulating bank to re-establish the initial steady-state neutron flux.
- iv. Measure the negative reactor period or halving time.
- v. Validate the core response against the reactivity computer input delayed neutron fractions and prompt neutron lifetime using pre-determined test criteria.
- vi. Adjust and recalibrate reactivity computer until acceptance criteria is met.

Acceptance Criterion

The reactivity computer is calibrated.

Table 14.2-85: Low Power Test Sequence (Test #85)

Startup test is required to be performed for each NPM.

This test is performed before initial criticality.

Test Objectives

- . Identify the sequence for low-power testing.
- ii. The low-power tests are:
 - a. Determination of Zero-Power Physics Testing Range Test (Test #86)
 - b. All Rods Out (ARO) Boron Endpoint Determination Test (Test #87)
 - c. Isothermal Temperature Coefficient Measurement Test (Test #88)
 - d. Bank Worth Measurement Test (Test #89)

Prerequisites

None

Test Method

For each of the tests identified in the test objectives above:

- Identify the specific plant conditions required for each low-power test procedure to maintain technical specification operability.
- ii. Identify the prerequisites required for each low-power test procedure.
- iii. Determine the test sequence for low-power testing based on technical specification requirements and test prerequisites.

Acceptance Criterion

The sequence for low-power testing has been determined.

Table 14.2-86: Determination of Zero-Power Physics Testing Range Test (Test #86)

Startup test is required to be performed for each NPM.

This test is performed after initial criticality.

Test Objectives

- i. Determine the reactor flux level at which the point of nuclear heating is detectable.
- ii. Establish the range of neutron flux in which HZP reactivity measurements are to be performed.

Prerequisites

- i. The reactor is critical with the neutron flux level at steady-state below the expected level of nuclear heating.
- ii. The RCS temperature and pressure is steady-state at the normal HZP conditions.
- iii. The RCS boron concentration is steady-state.
- iv. The reactivity computer is operational and recording the core average neutron flux level.
- v. The regulating bank is positioned to allow reactivity changes by rod motion alone.

Test Method

- i. Withdraw the regulating bank to establish a slow startup rate allowing neutron flux level to increase until nuclear heating is observed.
- ii. Record the reactivity computer neutron flux level and the corresponding MCR flux indication at which nuclear heating occurs.
- Insert the regulating bank to establish a reactivity computer flux level about one-third of the value at which nuclear heating was observed. This flux level becomes the maximum value for the zero-power testing range.

Acceptance Criterion

The zero power testing range flux level is determined.

Table 14.2-87: All Rods Out Boron Endpoint Determination Test (Test #87)

Startup test is required to be performed for each NPM.

This test is performed after initial criticality.

Test Objective

Determine the critical RCS boron concentration for ARO (fully withdrawn shutdown banks and regulating banks) at HZP.

Prerequisites

- i. The reactor is critical with the neutron flux level at steady-state below the expected level of nuclear heating.
- ii. The RCS temperature and pressure is steady-state at the normal HZP conditions.
- iii. The RCS boron concentration is steady-state.
- iv. The reactivity computer is operational and recording the core average neutron flux level.

Test Method

- i. Add a pre-determined volume of borated water to the RCS and withdraw the regulating bank to maintain critical conditions. The final regulating bank position will be near fully withdrawn and will limit the usable positive reactivity remaining in the rods with the reactor critical.
- ii. Measure the just-critical boron concentration by chemical analysis.
- iii. Fully withdraw the regulating bank without adjusting the boron concentration. Measure and calculate the change in reactivity for ARO and the RCS temperature difference from program T_{AVG}, due to an equivalent change in boron concentration. Add the equivalent boron change to the just-critical boron concentration to yield the endpoint for ARO.

Acceptance Criterion

The measured value for the ARO boron endpoint satisfies the design value contained within the test acceptance criteria.

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Table 14.2-88: Isothermal Temperature Coefficient Measurement Test (Test #88)

Startup test is required to be performed for each NPM.

This test is performed after initial criticality.

Test Objectives

- i. Determine the isothermal temperature coefficient.
- ii. Calculate the moderator temperature coefficient.

Prerequisites

- i. The reactor is critical with the neutron flux level at steady-state below the expected level of nuclear heating.
- ii. The RCS temperature and pressure is steady-state at the normal HZP conditions.
- iii. The RCS boron concentration is steady-state.
- iv. The reactivity computer is operational and recording the core average neutron flux level.
- v. The regulating rod bank is positioned near fully withdrawn (near their ARO position).

Test Method

- i. Vary RCS temperature (heatup/cooldown) while maintaining rods and boron concentration constant.
- ii. Monitor reactivity results and determine the isothermal temperature coefficient.
- iii. Calculate the moderator temperature coefficient using the isothermal temperature coefficient and design values.

Acceptance Criterion

The moderator temperature coefficient is within the limits specified in the core operating limits report.

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Table 14.2-89: Bank Worth Measurement Test (Test #89)

Startup test is required to be performed for each NPM.

This test is performed after initial criticality.

Test Objectives

- i. Measure the integral and differential worth of the reference bank (the test bank with the highest predicted worth).
- ii. Measure the worth of the remaining shutdown and regulating banks by control rod exchange (rod swap).

Prerequisites

- i. The reactor is critical with the neutron flux level at steady-state within the range for HZP physics testing.
- ii. The RCS temperature and pressure is steady-state at the normal HZP conditions.
- iii. The RCS boron concentration is steady-state.
- iv. The reactivity computer is operational and recording the core average neutron flux level.
- v. The regulating rod banks are positioned near fully withdrawn (near their ARO position).

Test Method

- i. The referenced bank rod worth measurement is made by performing a slow controlled boron dilution while the reference bank is inserted to maintain criticality. The rod worth is measured using the reactivity computer. During boron dilution the reference bank step insertions maintain neutron flux within the zero-power physics test range until the referenced bank is fully inserted.
- ii. A test bank rod worth measurement is made by inserting the test bank while the reference bank is withdrawn. The test bank worth is determined by the final position of the referenced bank.

Acceptance Criterion

The measured worth for each individual bank, and sum of bank worths, is consistent with the predicted value within the test acceptance criteria.

Table 14.2-90: Power-Ascension Test (Test #90)

Startup test is required to be performed for each NPM.

This test is performed prior to power-ascension testing.

Test Objective

Identify the sequence for the following power-ascension tests.

- a. Core Power Distribution Map Test (Test #91)
- b. Neutron Monitoring System Power Range Flux Calibration Test (Test #92)
- c. Reactor Coolant System Temperature Instrument Calibration Test (Test #93)
- d. Reactor Coolant System Flow Calibration Test (Test# 94)
- e. Radiation Shield Survey Test (Test #95)
- f. Reactor Building Ventilation System Capability Test (Test #96)
- g. Thermal Expansion Test (Test #97)
- h. Control Rod Assembly Misalignment Test (Test #98)
- i. Steam Generator Level Control System Test (Test #99)
- j. Ramp Change in Load Demand Test (Test #100)
- k. Step Change in Load Demand Test (Test #101)
- I. Loss of Feedwater Heater Test (Test #102)
- m. 100 Percent Load Rejection Test (Test #103)
- n. Reactor Trip from 100 Percent Power Test (Test #104)
- o. Loss of Offsite Power Test (Test #105)
- p. Remote Shutdown Workstation Test (Test #106)

Prerequisites

None

Test Method

- Identify the specific plant conditions required for each power-ascension test procedure to maintain technical specification operability.
- ii. Identify the prerequisites required for each power-ascension test procedure.
- Determine the test sequence for power-ascension testing based on technical specification requirements and test prerequisites.

Acceptance Criterion

The sequence for power-ascension testing has been determined.

Table 14.2-91: Core Power Distribution Map Test (Test #91)

Startup test is required to be performed for each NPM.

This test is performed at approximately 25, 50, 75, and 100 percent reactor thermal power

Test Objectives

- i. Obtain a core power distribution map during power ascension.
- ii. Using the data from the core power distribution map verify core power distribution is consistent with design predictions and associated technical specifications limits.

Prerequisites

- i. The ICIS is operational.
- ii. The NPM is operating in a steady-state condition at the specified power level.
- iii. Maintain reactor power, T_{AVG}, and pressurizer level constant during data collection.

Test Method

- With the plant at power levels of approximately 25, 50, 75, and 100 percent of reactor thermal power, obtain a core power distribution map during power ascension using the MCS and instrument input from the in-core self-powered neutron detectors.
- ii. Use data from the in-core maps to verify that core power distribution is consistent with design predictions and technical specifications limits.

Acceptance Criterion

Core power distribution is consistent with design predictions and technical specifications limits.

Table 14.2-92: Neutron Monitoring System Power Range Flux Calibration Test (Test #92)

Startup test is required to be performed for each NPM.

This test is performed at approximately 25, 50, 75 and 100 percent reactor thermal power.

Test Objective

Calibrate the NMS power range neutron flux signals during power ascension.

Prerequisites

- i. The ICIS is operational.
- ii. The NPM is operating in a steady-state condition at the specified power level.

Test Method

- i. With the plant at power levels of approximately 25, 50, 75 and 100 percent of reactor thermal power, record the following data:
 - power range neutron flux from the ICIS self-powered neutron detectors
 - NMS power range (linear power) signal
- ii. Maintain reactor power, T_{AVG}, and pressurizer level constant during data collection.
- iii. Calibrate the NMS neutron flux power range (linear power) signal using the recorded data.

Acceptance Criterion

The NMS neutron flux power range (linear power) signal has been calibrated.

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Table 14.2-93: Reactor Coolant System Temperature Instrument Calibration Test (Test #93)

Startup test is required to be performed for each NPM.

This test is performed at approximately 25, 50, 75, and 100 percent reactor thermal power.

Test Objective

Calibrate narrow range RCS hot leg temperature instruments, wide range RCS hot leg temperature instruments, and narrow range RCS cold leg temperature instruments.

Prerequisites

- i. The ICIS is operational.
- ii. The NPM is operating in a steady-state condition at the specified power level.

Test Method

- i. With the plant at power levels of approximately 25, 50, 75, and 100 percent of reactor thermal power, record the following data:
 - NMS flux power range (linear power) signal
 - RCS narrow range hot leg temperature
 - RCS wide range hot leg temperature
 - RCS narrow range cold leg temperature
 - ICIS core inlet and outlet temperature
- ii. Maintain reactor power, T_{AVG}, and pressurizer level at steady-state during data collection.
- Calibrate the RCS narrow range and wide range hot leg temperature instruments and the RCS narrow range cold leg temperature using the recorded data.

Acceptance Criterion

The RCS hot and cold let temperature instruments have been calibrated.

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Table 14.2-94: Reactor Coolant System Flow Calibration Test (Test #94)

Startup test is required to be performed for each NPM.

This test is performed at approximately 25, 50, 75, and 100 percent reactor thermal power.

Test Objective

Calibrate the RCS flow instruments during power ascension.

Prerequisites

- The ICIS is operational.
- ii. The NPM is operating in a steady-state condition at the specified power level.

Test Method

- i. With the plant at power levels of approximately 25, 50, 75, and 100 percent of reactor thermal power, record the following data:
 - NMS flux power range (linear power) signal
 - RCS narrow range hot leg temperature
 - RCS narrow range cold leg temperature
 - ICIS core inlet and outlet temperature
- ii. Maintain reactor power, T_{AVG}, and pressurizer level at steady state during data collection.
- iii. Calibrate the RCS flow instruments using the recorded data.

Acceptance Criterion

The RCS flow instruments have been calibrated.

Table 14.2-95: Radiation Shield Survey Test (Test #95)

Startup test is required to be performed for each NPM.

This test is performed at approximately 25, 50, and 100 percent reactor thermal power.

Test Objective

Verify the adequacy of concrete radiation shields in the RXB designed to protect personnel from radiation originating from sources within the reactor vessel.

Prerequisites

- i. Radiation survey instruments are calibrated.
- ii. The NPM is operating in a steady-state condition at the specified power level.

Test Method

- Measure gamma and neutron radiation dose rates at designated locations at approximately 25, 50, and 100 percent reactor thermal power.
- ii. The designated locations are the accessible areas outside permanent concrete radiation shields in the RXB. (reference Figure 12.3-1a for the RXB radiation zone map)

Acceptance Criterion

Radiation dose rates are consistent with design expectations.

Table 14.2-96: Reactor Building Ventilation System Capability (Test #96)

Startup test is required to be performed for each NPM.

This test is performed at approximately 50 and 100 percent reactor thermal power.

Test Objective

Verify that the RXB ventilation system maintains the design environment in areas containing equipment that is environmentally qualified for a harsh or mild environment.

Prerequisite

The NPM is operating in a steady-state condition at the specified power level.

Test Method

- With the plant at power levels of approximately 50 and 100% of reactor thermal power and RXB ventilation system in normal lineup, record temperature and humidity for the environmental qualification zones listed in Table 3.11-2 that are not under the bioshield.
- ii. With the plant at power levels of approximately 50 and 100% of reactor thermal power and RXB ventilation system in normal lineup, record the temperature and humidity in the rooms containing electrical equipment qualified for a mild environment.

Acceptance Criteria

- i. Room temperature and humidity in environmental qualification zones listed in Table 3.11-2 that are not under the bioshield satisfy the indoor design conditions for the RXB ventilation system contained in Table 9.4.2-2.
- ii. Room temperature and humidity in rooms containing electrical equipment qualified for a mild environment satisfy the indoor design conditions for the RXB ventilation system contained in Table 9.4.2-2.

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Table 14.2-97: Thermal Expansion Test (Test #97)

Startup test is required to be performed for each NPM.

This test is performed during plant heatup and cooldown.

Test Objectives

- i. Verify that ASME Code Class 1, 2, and 3 system piping can expand without obstruction and that expansion is within design limits. All ASME Code Class 1, 2, and 3 system piping is within the RXB.
- ii. Verify that high-energy piping inside the RXB can expand without obstruction and that expansion is within design limits.

Prerequisite

Temporary instrumentation is installed on piping outside the NPM as required to monitor the deflections for the piping under test.

Test Method

- i. Thermal expansion testing is performed in accordance with ASME OM Standard, Part 7 as discussed in Section 3.9.2.1.2.
- ii. Record deflection data during plant heatup and cooldown.
- iii. Identify support movements by recording hot and cold positions of the supports.
- iv. All tested piping is within the RXB.
- v. All tested piping is outside the NPM.
- vi. All tested piping is contained within the MSS, FWS, ABS, PSS, and CVCS.

Acceptance Criteria

For the piping systems tested:

- i. There is no evidence of blocking of the thermal expansion of piping or component, other than by installed supports, restraints, and hangers.
- ii. Spring hanger movements must remain within the hot and cold setpoints and supports must not become fully retracted or extended.
- iii. Piping and components return to their approximate baseline cold position.

Table 14.2-98: Control Rod Assembly Misalignment (Test #98)

Startup test is required to be performed for each NPM.

This test is performed between 30 and 50 percent reactor thermal power.

Test Objectives

- i. Verify that core thermal and nuclear parameters at 50% reactor thermal power are in accordance with predictions with a single high-worth rod fully inserted, during rod movement, and following return of the rod to its bank position.
- ii. Verify the capability of the in-core neutron flux instrumentation to detect a control rod misalignment equal to or less than the technical specification limits at 50% and 100% reactor thermal power.
- iii. Monitor the power distribution following the recovery of a misaligned CRA.

Prerequisites

- i. The reactor is operating at approximately 50% reactor thermal power and has been at that power for a sufficient time to reach xenon equilibrium.
- ii. The reactor power level, reactor coolant system boron concentration, and temperature are stable.
- iii. The regulating and shutdown banks are positioned as required for the specific measurement, near fully withdrawn for CRA insertion, and at their respective insertion limits for CRA withdrawal.

Test Method

- For the CRA insertion, insert a group of selected CRAs, one at a time, first to the limit of misalignment specified in TS, then
 fully inserted, and finally restored to the bank position. Compensate for reactivity changes by dilution and boration as
 required.
- ii. For the CRA withdrawal, withdraw one or more selected CRAs, one at a time, to the fully withdrawn position. Compensate for reactivity changes by boration and dilution as required.
- iii. Record incore and excore instrumentation signals to determine their response and to determine the power distribution and power peaking factors prior to control rod assembly misalignment, at partial misalignment, at full misalignment, and periodically after restoration to normal.

Acceptance Criteria

Measured power distributions and power peaking factors are within technical specification limits and are consistent with the predictions.

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Table 14.2-99: Steam Generator Level Control Test (Test #99)

Startup test is required to be performed for each NPM.

This test is performed at approximately 25, 50, 75, and 100 percent reactor thermal power.

Test Objective

Verify the stability of the automatic SG level control system by introducing simulated transients at various power levels during the ascension to full power.

Prerequisite

The NPM is operating in a steady-state condition at the specified power level.

Test Method

- i. Simulate an SG level transient by changing the level setpoint at approximately 25, 50, 75, and 100% reactor thermal power.
- ii. Record the steam generator level control response when the control system is returned to automatic control.
- iii. Adjustments to the control systems are made, if necessary, prior to proceeding to the next power plateau.

- i. During recovery from a simulated steam generator level transient, SG level control response is consistent with the design for the following:
 - a. overshoot or undershoot to the new level.
 - b. time required to achieve the new level.
 - c. error between the actual level and control setpoint.
 - d. feedwater pump discharge pressure oscillations.
- ii. Water hammer indications:
 - a. Audible indications of water hammer are not observed.
 - b. No damage to pipe supports or restraints.
 - c. No damage to equipment.
 - d. No equipment leakage as a result of the steam generator level transient.

Table 14.2-100: Ramp Change in Load Demand (Test #100)

Startup test is required to be performed for each NPM.

This test is performed at approximately 25, 50, 75, and 100 percent reactor thermal power.

Test Objectives

- i. Verify the ability of the plant automatic control systems to sustain a ramp increase in load demand.
- ii. Assess the dynamic response of the plant for ramp increase in load demand.

Prerequisites

- i. The NPM is operating in a steady-state condition at the designated power level.
- ii. The plant's electrical distribution system is aligned for normal operation.
- iii. Reactor, turbine, and secondary control systems are in automatic mode.

Test Method

- i. Use the main control room turbine controls to provide a 5% of full power per minute load increase in demand at approximately 25, 50, and 75% reactor thermal power.
- ii. Use the main control room turbine controls to provide a 5% of full power per minute load decrease in demand at approximately 25, 50, and 75, and 100% reactor thermal power.

- i. The turbine does not trip.
- ii. The reactor does not trip.
- iii. The main steam safety valves do not open.
- iv. The turbine does not overspeed.
- The primary and secondary control systems, with no manual intervention, maintain reactor power, reactor coolant
 system temperatures, pressurizer pressure and level, and SG levels and pressures within acceptable ranges during and
 following the transient.
- vi. Control system response is reviewed and compared to expected performance. Necessary adjustments to the control systems have been made prior to proceeding to the next power plateau.
- vii. Water hammer indications
 - a. Audible indications of water hammer are not observed.
 - b. No damage to pipe supports or restraints.
 - c. No damage to equipment.
 - d. No equipment leakage as a result of the ramp change.

Table 14.2-101: Step Change in Load Demand Test (Test #101)

Startup test is required to be performed for each NPM.

This test is performed at approximately 25, 50, 75, and 100 percent reactor thermal power.

Test Objectives

- i. Verify the ability of the plant automatic control systems to sustain step load increases and step load decreases in demand.
- ii. Assess the dynamic response of the plant for a load step demand.

Prerequisites

- . The NPM is operating in a steady-state condition at the specified power level.
- ii. The plant's electrical distribution system is aligned for normal operation.
- iii. Reactor, turbine, and secondary control systems are in automatic mode.

Test Method

- i. Use the MCR turbine controls to provide a 10% step load increase in demand at approximately 25, 50, and 75% reactor thermal power.
- ii. Use the MCR turbine controls to provide a 10% step load decrease in demand at approximately 25, 50, 75, and 100% reactor thermal power.

- i. The turbine does not trip.
- ii. The reactor does not trip.
- iii. The main steam safety valves do not open.
- iv. The turbine does not overspeed.
- v. The primary and secondary control systems, with no manual intervention, maintain reactor power, RCS temperatures, pressurizer pressure and level, and SG levels and pressures within acceptable ranges during and following the transient.
- vi. Control system response is reviewed and compared to expected performance. Necessary adjustments to the control systems have been made prior to proceeding to the next power plateau.
- vii. Water hammer indications
 - a. Audible indications of water hammer are not observed.
 - b. No damage to pipe supports or restraints.
 - c. No damage to equipment.
 - d. No equipment leakage as a result of the step load change.

Table 14.2-102: Loss of Feedwater Heater Test (Test #102)

Startup test is required to be performed for each NPM.

This test is performed at approximately 50 and 90 percent reactor thermal power.

Test Objectives

- i. Verify the ability of the plant automatic control systems to sustain a loss of the high pressure feedwater heater during power operation.
- ii. Assess the dynamic response of the plant for the loss of the high pressure feedwater heater.

Prerequisites

- i. The NPM is operating in a steady-state condition at the specified power level.
- ii. The plant's electrical distribution system is aligned for normal operation.
- iii. Reactor, turbine, and secondary control systems are in automatic mode.

Test Method

Close the turbine generator extraction steam supply isolation valve to the high pressure feedwater heater from the main control room at approximately 50 and 90% reactor thermal power.

Acceptance Criteria

- The reactor does not trip.
- ii. The turbine does not trip.
- iii. The main steam safety valves do not open.

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Table 14.2-103: 100 Percent Load Rejection Test (Test #103)

Startup test is required to be performed for each NPM.

This test is performed at approximately 100 percent reactor thermal power.

Test Objectives

- i. Verify the ability of the plant automatic control systems to sustain a 100% load rejection from full power.
- ii. Assess the dynamic response of the plant for a 100% power load rejection.

Prerequisites

- i. The NPM is operating in a steady-state condition at full reactor thermal power.
- ii. The plant's electrical distribution system is aligned for normal operation.
- iii. Reactor, turbine, and secondary control systems are in automatic mode.

Test Method

Manually trip the generator output breaker to provide a 100 percent load rejection.

- i. The turbine trips.
- ii. The reactor does not trip.
- iii. The main steam safety valves do not open.
- iv. The turbine does not overspeed beyond design limits.
- v. The turbine generator bypass valve opens and modulates steam flow to the condenser to maintain steam generator pressure.
- vi. The FWS automatically provides the necessary feedwater flow to the steam generator.
- vii. Water hammer indications
 - a. Audible indications of water hammer are not observed
 - b. No damage to pipe supports or restraints
 - c. No damage to equipment
 - d. No equipment leakage as a result of the load rejection.

Table 14.2-104: Reactor Trip from 100 Percent Power Test (Test #104)

Startup test is required to be performed for each NPM.

This test is performed at 100 percent reactor thermal power.

Test Objectives

- i. Verify the ability of the NPM to sustain a reactor trip from 100% reactor thermal power and automatically cool the RCS to mode 3 (all RCS temperatures < 420 °F).
- ii. Assess the dynamic response of the plant to the reactor trip.

Prerequisites

- . The NPM is operating in a steady-state condition at full reactor thermal power.
- ii. The plant's electrical distribution system is aligned for normal operation.

Test Method

- i. Manually trip the reactor from the MCR.
- ii. Allow the RCS to cool to mode 3.

- The reactor trips.
- ii. The CIVs close.
- iii. The decay heat removal valves open.
- iv. The turbine generator bypass valve operates to prevent opening of the main steam safety valve.
- v. The turbine speed does not exceed overspeed design limits.
- vi. The reactor vent valves do not open.
- vii. Water hammer indications
 - a. Audible indications of water hammer are not observed
 - b. No damage to pipe supports or restraints
 - c. No damage to equipment
 - d. No equipment leakage as a result of the reactor trip
- viii. The RCS cools to a stable condition in mode 3 without operator intervention.

Table 14.2-105: Island Mode Test for NuScale Power Module #1(Test #105)

This startup test is required to be performed for the first NPM #1. Startup Test #106 tests island mode for multiple NPMs.

This test is performed at 100 percent reactor thermal power. Island mode operation is described in Section 8.3.1.1.1

Test Objective for NPM #1

- Verify NPM #1 can operate independently from an offsite transmission grid after transition from the transmission grid to island mode.
- ii. Verify plant electrical loads may be transitioned from island mode to an offsite transmission grid without interruption to the operation of NPM Module #1.

Prerequisites

NPM #1 is in normal operation at 100 percent reactor thermal power.

Test Method

Simulate a loss of the transmission grid by opening the switchyard supply breakers (reference Figures 8.3-2a and 8.3-2b).

- a. Turbine Generator (TG #1) does not trip and changes from droop mode control to isochronous mode to control the loads on site.
 - b. NPM #1 remains at approximately 100 percent reactor thermal power using turbine generator bypass operation.
 - c. Electrical power to plant loads is uninterrupted without loss of voltage or automatic bus transfers.
 - d. The auxiliary AC power source starts automatically but does not automatically load its associated bus.
- ii. The plant electrical loads are transitioned back to the external offsite grid connection when it becomes available.

Table 14.2-106: Island Mode Test for Multiple NuScale Power Modules (Test #106)

This startup test is required to be performed once with multiple NPMs in operation. Startup Test #105 tests island mode for a single NPM.

COL Item 14.2-7: A COL applicant that references the NuScale Power Plant design certification will select the plant configuration to perform the Island Mode Test (number of NPMs in service).

This test is performed at 100 percent reactor thermal power for all NPMs under test. Island mode operation is described in Section 8.3.1.1.1

Test Objective for multiple NPM in operation:

- Verify all NPMs under test can operate independently from an offsite transmission grid after transition from the transmission grid to island mode.
- ii. Verify plant electrical loads may be transitioned from island mode to an offsite transmission grid without interruption to the operation of NPM #1.

Prerequisites

The NPMs selected for test are in normal operation at 100 percent reactor thermal power.

Test Method

Simulate a loss of the transmission grid by opening the switchyard supply breakers (reference Figures 8.3-2a and 8.3-2b).

- i. a. The service unit turbine generator transitions to island mode by changing from droop mode control to isochronous mode control to control the load on the 13.8kV bus it is supplying.
 - b. The service unit NPM remains at approximately 100 percent reactor thermal power using turbine generator bypass operation.
 - c. The non-service unit turbine generators trip.
 - d. The non-service unit NPMs power reduces to approximately 95% percent reactor thermal power using turbine generator bypass operation
 - e. Electrical power to plant loads is uninterrupted without loss of voltage or automatic bus transfers.
 - d. The auxiliary AC power source starts automatically but does not automatically load its associated bus.
- ii. The plant electrical loads are successfully transitioned back to an external offsite grid connection when it becomes available

Table 14.2-107: Remote Shutdown Workstation Test (Test #107)

Startup test is required to be performed for each NPM.

This test is performed at approximately 10 - 20 percent reactor thermal power.

Test Objectives

- i. Verify the NPM safety-related controls can be disabled at the remote shutdown station.
- ii. Verify the NPM nonsafety-related controls are functional at the remote shutdown station.

Prerequisites

- . Communication exists between the MCR and the remote shutdown station.
- ii. The reactor is operating in a steady-state condition at 10 20% reactor thermal power.

Test Method

- i. Using the appropriate operating procedure, the operator manually trips the reactor under test before leaving the MCR.
- ii. Using the appropriate operating procedure, the operator uses manual switches in the remote shutdown station to isolate the module protection system manual actuation switches, override switches, and the enable nonsafety control switches for each nuclear power modules' module protection system in the MCR to prevent spurious actuation of equipment due to fire damage.

Acceptance Criteria

i. An operator verifies that the module protection switch controls in the MCR have been disabled.

The displays in the remote shutdown station verify the following NPM status:

- ii. The reactor is tripped.
- iii. All CIVs are closed.
- iv. The DHRS actuation valves are open.
- v. All RCS temperatures cool to less than 420°F (mode 3, safe shutdown) without operator action.
- vi. Safety-related components cannot be operated from the remote shutdown station.
- vii. The nonsafety-related controls in the remote shutdown station controls can be used to place the plant in a configuration specified by the appropriate operating procedure.

Table 14.2-108: Reactor Module Vibration Test (Test #108)

This startup test is required to be performed once for NPM #1. This test supports FOAK testing described in Section 14.2.3.3.

This test is performed at 100 percent reactor thermal power. Reactor module vibration testing is described in Sections 3.9.2.1.1.1, 3.9.2.3 and 3.9.2.4. and Reference 3.9-5 NuScale Power, LLC, "Comprehensive Vibration Assessment Program (CVAP) Technical Report," TR-0716-50439.

Test Objective for NPM #1

- Perform vibration testing of DHRS steam piping at 100 percent reactor thermal power as described in TR-0716-50439, Section 4.3, to verify vibration amplitudes in the DHRS steam piping confirm the acoustic resonance analysis results described in TR-0716-50439 Section 4.3.
- ii. Perform visual testing of the reactor module components specified in Table 5-1 of TR-0716-50439.

Prerequisites

The DHRS steam piping is instrumented to obtain acoustic resonance (AR) data.

Test Method

- Operate the reactor module for a sufficient duration at 100 percent power to ensure one million vibration cycles for the component with the lowest structural natural frequency.
- ii. Monitor the vibration of the DHRS steam piping. If an unacceptable vibration response develops any time during initial startup testing, the test conditions will be adjusted to stop the vibration and the reason for the vibration anomaly will be investigated prior to continuing with the testing.
- iii. Disassemble the reactor module and performed a visual inspection of the reactor module components specified in Table 5-1 of TR-0716-50439.

Acceptance Criterion

- i. Measured vibration amplitudes in the DHRS steam piping confirm the acoustic resonance analysis results described in TR-0716-50439 Section 4.3.
- ii. Visual inspection results of reactor module components satisfy the acceptance criteria of Table 5-1 of TR-0716-50439.

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Table 14.2-109: List of Test Abstracts

Test Number	System Abbreviation	Test Abstract
1	SFPCS	Spent Fuel Pool Cooling System
2	PCUS	Pool Cleanup System
3	RPCS	Reactor Pool Cooling System
4	PSCS	Pool Surge Control System
5	UHS	Ultimate Heat Sink
6	PLDS	Pool Leakage Detection Systems
7	RCCWS	Reactor Component Cooling Water System
8	CHW	Chilled Water
9	ABS	Auxiliary Boiler System
10	CWS	Circulating Water System
11	SCW	Site Cooling Water
12	PWS	Potable Water System
13	UWS	Utility Water System
14	DWS	Demineralized Water System
15	NDS	Nitrogen Distribution System
16	SAS	Service Air System
17	IAS	Instrument Air System
18	CRHS	Control Room Habitability System
19	CRVS	Normal Control Room HVAC System
20	RBVS	Reactor Building HVAC System
21	RWBVS	Radioactive Waste Building HVAC System
22	TBVS	Turbine Building HVAC System
23	RWDS	Radioactive Waste Drain System
24	BPDS	Balance of Plant Drain System
25	FPS	Fire Protection System
26	FDS	Fire Detection System
27	MSS	Main Steam System
28		Condensate and Feedwater System
29		Feedwater Treatment System
30		Condensate Polishing System
31	HVD	Heater Vents and Drains
32		Condenser Air Removal System
33	TGS	Turbine Generator System
34		Turbine Lube Oil Storage System
35		Liquid Radioactive Waste Management System
36		Gaseous Radioactive Waste Management System
37		Solid Radioactive Waste Management System
38		Chemical and Volume Control System
39		Boron Addition System
40	MHS	Module Heatup System
41	CES	Containment Evacuation System
42	CFDS	Containment Flooding and Drain System
43	CNTS	Containment System
44		Control Rod Drive System
45		Reactor Vessel Internals
46		Reactor Coolant System
47	ECCS	Emergency Core Cooling System
48	DHRS	Decay Heat Removal System
49	ICIS	In-core Instrumentation System

Table 14.2-109: List of Test Abstracts (Continued)

Test Number	System Abbreviation	Test Abstract
50	MAE	Module Assembly Equipment
51	FHE	Fuel Handling Equipment
52	RBC	Reactor Building Cranes
53	PSS	Process Sampling System
54	EHVS	13.8 kV and switchyard system
55	EMVS	Medium Voltage AC Electrical Distribution System
56	ELVS	Low Voltage AC Electrical Distribution System
57	EDSS	Highly Reliable DC Power System
58	EDNS	Normal DC Power System
59	BPSS	Backup Power Supply System
60	PLS	Plant Lighting System
61	MCS	Module Control System
62	PCS	Plant Control System
63	MPS	Module Protection System
64	PPS	Plant Protection System
65	NMS	Neutron Monitoring System
66	SDIS	Safety Display and Indication System
67	RMS	Fixed Area Radiation Monitoring System
68	COMS	Communication Systems
69	SMS	Seismic Monitoring System
70	HFT	Hot Functional Testing
71	MAEB	Module Assembly Equipment-Bolting
72	SG	Steam Generator
73	N/A	Security Access Control
74	N/A	Security Alarm Architecture
75	N/A	Initial Fuel Loading-Precritical
76	N/A	Initial Fuel Load
77	N/A	Reactor Coolant System Flow Measurement
78	N/A	Reactor Module Temperatures
79	N/A	Primary and Secondary System Chemistry
80	N/A	Control Rod Drive System-Manual Operation and Rod Position Indication
81	N/A	Control Rod Assembly Drop Time
82	N/A	Pressurizer Spray Bypass Flow
83	N/A	Initial Criticality
84	N/A	Post-Critical Reactivity Computer Checkout
85	N/A	Low Power Test Sequence
86	N/A	Determination of Zero-Power Physics Testing Range
87	N/A	All Rods Out Boron Endpoint Determination
88	N/A	Isothermal Temperature Coefficient Measurement
89	N/A	Bank Worth Measurement
90	N/A	Power Ascension
91	N/A	Core Power Distribution Map
92	N/A	Nuclear Monitoring System Power Range Flux Calibration
93	N/A	Reactor Coolant System Temperature Instrument
94	N/A	Reactor Coolant System Flow Calibration
95	N/A	Radiation Shield Survey
96	N/A	Reactor Building Ventilation System Capability
97	N/A	Thermal Expansion
98	N/A	Control Rod Assembly Misalignment
99	N/A	Steam Generator Inventory Control
100	N/A	Ramp Change in Load Demand
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Table 14.2-109: List of Test Abstracts (Continued)

Test Number	System Abbreviation	Test Abstract
101	N/A	Step Change in Load Demand
102	N/A	Loss of Feedwater Heater
103	N/A	Load Rejection
104	N/A	Reactor Trip from 100% Power
105	N/A	Island Mode Test for NuScale Power Module #1
106	N/A	Island Mode Test for Multiple NuScale Power Modules
107	N/A	Remote Shutdown Workstation
108	N/A	Reactor Module Vibration Test

14.3 Certified Design Material and Inspections, Tests, Analyses, and Acceptance Criteria

14.3.1 Introduction

This section provides guidance regarding the development of certified design material (CDM) in Tier 1, including Inspections, Tests, Analyses, and Acceptance Criteria (ITAAC) required under Title 10 of the Code of Federal Regulations (10 CFR) 52.47(b)(1). The scope of ITAAC is sufficient to provide reasonable assurance that, if the ITAAC are successfully completed, the facility has been constructed and can be operated in accordance with the Atomic Energy Act, relevant Nuclear Regulatory Commission (NRC) regulations, and the combined license (COL). The successful completion of ITAAC constitutes the basis for the NRC determination to allow operation of a facility certified under 10 CFR 52.

Tier 1 information is the portion of the design-related information contained in the Final Safety Analysis Report that is approved and certified by the design certification rule. There are two material categories in Tier 1, the CDM and ITAAC. The CDM is in the form of design descriptions, design commitments, tables, and figures, and is binding for the lifetime of a facility. The ITAAC is used to verify the as-built design features. The ITAAC material expires at initial fuel loading.

The Tier 1 design description consists of the system description and design commitments, both of which contain top-level design features. A design feature is either a physical attribute or a performance characteristic of structures, systems, and components (SSC).

The design features in the system description are not verified by ITAAC. Only the design features in the design commitments are verified by ITAAC.

The sections below describe the criteria and methods by which specific technical entries for Tier 1 were selected. The contents of Tier 1 may not directly correspond to these guidelines in all cases because special considerations may warrant a different approach. In this regard, a case-by-case determination is made consistent with the principles inherent in 10 CFR 52 as well as NRC guidance regarding the content of design descriptions and ITAAC.

- COL Item 14.3-1: A COL applicant that references the NuScale Power Plant design certification will provide the site-specific selection methodology and Inspections, Tests, Analyses, and Acceptance Criteria for emergency planning.
- COL Item 14.3-2: A COL applicant that references the NuScale Power Plant design certification will provide the site-specific selection methodology and ITAAC for SSC within their scope.

14.3.2 Tier 1 Design Description and Inspections, Tests, Analyses, and Acceptance Criteria First Principles

General criteria that provide clarity on the scope and level of detail of design descriptions and ITAAC are discussed below. These criteria are consolidated and grouped into two sets of first principles: 1) Tier 1 design description scope first principles and 2) ITAAC scope first principles.

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The development of the scope of Tier 1 is determined based upon policies set forth by the NRC. A "first principles" approach is considered such that the design descriptions and ITAAC in Design Certification Applications are "necessary and sufficient." Thus, in order to determine the appropriate scope of ITAAC, it is important to apply both the first principles for determining the top-level design features that are included in Tier 1 design descriptions, and the first principles for determining whether a Tier 1 design description needs an ITAAC. Consistent with these first principles, the selection of the top-level design features for Tier 1 is based on the safety significance of SSC, their importance in various safety analyses, and their functions for defense-in-depth considerations.

The first principles for determining the scope of design descriptions and ITAAC are described in Section 14.3.2.1 and Section 14.3.2.2.

14.3.2.1 Tier 1 Design Description Scope First Principles

- Design description content is limited to the following:
 - top-level design features of safety-related SSC
 - top-level design features of safety-related or nonsafety-related SSC that protect safety-related components
 - top-level design features of security system physical SSC
 - top-level design features of risk-significant, nonsafety-related SSC determined by results of a probabilistic risk assessment (PRA)

Refer to Section 14.3.2.1.1 for further discussion of this principle.

- Design descriptions are derived solely from Tier 2 design information.
- The amount of detail in design descriptions is proportional to the safety significance of the system (i.e., a graded approach). Refer to Section 14.3.2.1.2 for further discussion of the graded approach.
- Not all safety-related design features are included in a design description. Refer to Section 14.3.2.1.3 for further discussion of this principle.
- Not all design features contained in the accident analyses must be included in design descriptions. Refer to Section 14.3.2.1.4 for further discussion of this principle.
- Operational programs and post-fuel load testing are not contained in design descriptions. Refer to Section 14.3.2.1.5 for further discussion of this principle.
- Design descriptions do not need to include every component for that system, but instead only includes those SSC that are required to perform the safety-related and risk-significant system functions. Refer to Section 14.3.2.1.6 for further discussion of this principle.
- Some risk-significant design features identified by the PRA do not need to be specifically addressed in the design description because they are indirectly addressed by design features that are addressed by other design commitments. Refer to Section 14.3.2.1.7 for further discussion of this principle.

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- To the extent that an SSC is already the subject of a design commitment by reason of design basis accident (DBA) mitigation function, a design commitment does not need to address the function of the SSC to mitigate severe accidents. Other design features that are not specifically installed for severe accident mitigation, but are used for severe accident mitigation do not need to be addressed in Tier 1. Refer to Section 14.3.2.1.8 for further discussion of this principle.
- Design descriptions only include fixed design features that are installed prior to fuel loading and are expected to be in place for the lifetime of the plant. Refer to Section 14.3.2.1.9 for further discussion of this principle.
- No new design information can be contained in Tier 1 that is not already in Tier 2.
- Tier 1 information is not relied upon for the NRC safety determination provided in a Safety Evaluation Report. The NRC safety determination is based solely on the Tier 2 design information. If a system or component function or design feature is not discussed in Tier 2, hence is not part of the NRC safety determination, it does not belong in Tier 1.
- Design descriptions do not contain a level of detail (e.g., minor dimensional details) that would restrict a licensee from making changes that do not affect a safety-related or risk-significant system function.
- Systems with no safety significance are not included in design descriptions.
- Design descriptions do not contain information that the NRC may designate as "Tier 2*". The NRC guidance in NUREG-0800, Section 14.3, states that Tier 2* information is generally not appropriate for treatment in Tier 1 because it is subject to change.
- Design descriptions do not contain processes that are used for designing and constructing a plant because the safety-related function of an SSC is dependent upon its final as-built condition and not the processes used to achieve that condition.
- Design descriptions do not contain discussions of single failures. Rather, the design description contains related top-level design features, such as physical separation and electrical isolation of Class 1E circuits.

14.3.2.1.1 Tier 1 Design Descriptions Are Limited to the Top-Level Design Features

The following describes the top-level design features for the NuScale Power Plant.

A design feature is either a physical attribute or a performance characteristic of an SSC. The top-level design features contained in Tier 1 design descriptions are:

- reactor coolant pressure boundary
- containment pressure boundary
- Seismic Category I Reactor Building (RXB) and Control Building (CRB)
- Radwaste Category RW-IIa Radioactive Waste Building (RWB)
- control room envelope (CRE)
- safety-related equipment qualification

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- safety-related component performance
- SSC providing protection of safety-related components
- safety-related protection system (reactor trip and engineered safety features actuation systems (ESFAS))
- components providing radiation protection for personnel and safety-related equipment
- new and spent fuel storage
- security system physical components

Examples of structures included in Tier 1 design descriptions are the Seismic Category I RXB and CRB, fire barriers, flood barriers, radiation shields, and fuel storage racks.

Examples of components included in Tier 1 design descriptions are valves, instruments, and piping systems.

Examples of physical attributes included in Tier 1 design descriptions are safety-related equipment qualification, location of fire barriers, and thickness of radiation shields.

Examples of performance characteristics included in Tier 1 design descriptions are building seismic performance, safety-related piping conformance to American Society of Mechanical Engineers (ASME) Code Section III requirements, valve stroke time, and safety-related components' automatic response to the module protection system (MPS).

14.3.2.1.2 Graded Approach

The extent to which a particular SSC is described in Tier 1 depends upon the safety significance of the SSC. A graded approach is used to determine the type of information and the level of detail in Tier 1 commensurate with the safety significance of the SSC for the design.

The graded approach reflects the wide variation in safety significance from system to system. It is unnecessary and would be inappropriate to provide the same level of detail for every system in Tier 1.

Top-level design information in Tier 1 is extracted from the more detailed design information presented in Tier 2. Limiting the Tier 1 contents to top-level information reflects the graded approach consistent with NRC guidance in NUREG-0800 and in Regulatory Guide (RG) 1.206.

Severe accident design features are described in the design description, and the ITAAC verify that they exist. In general, the capabilities of the design features need not be included in the ITAAC. For example, a design commitment may discuss that a severe accident containment flooding system exists, while the acceptance criteria

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would discuss that the severe accident containment flooding system exists, but would not specify the capabilities of associated pumps.

14.3.2.1.3 Not all Safety-Related Design Features are Included in a Design Description

Not all safety-related design features need to be explicitly addressed in design descriptions. Examples of safety-related component design features that generally do not warrant discussion in a design description include:

- instrument lines
- fill lines
- drains
- ASME Code Section III valves that have only a passive function
- piping pressure relief valves associated with thermal expansion and anticipated valve leakage
- interlocks aimed specifically at equipment protection for safety-related components
- local controls for safety-related components
- rebar and concrete properties for Seismic Category I structures

14.3.2.1.4 Top-Level Design Features

Not all design features are included in the design descriptions. Only the top-level design features are contained in the appropriate design description and verified by ITAAC. Table 14.3-1 and Table 14.3-2 present a matrix which correlates the top-level design features contained in design commitments with their treatment in Tier 1. Table 14.3-1 and Table 14.3-2 also contains the top-level design features that were developed based upon results of the following plant safety analyses:

- transient and accident analyses
- internal and external hazards analyses
- radiological analyses
- risk-significant design features as determined by the results of a PRA
- design features necessary or important to severe accident mitigation
- fire protection

By capturing the top level design features that are based upon results of plant safety analyses, the integrity of the fundamental analyses associated with the design as presented in Tier 2 are preserved in the certified design as presented in Tier 1.

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14.3.2.1.5 Design Descriptions do not Include Operational Programs and Post-Fuel Load Testing

Those aspects of the design that pertain to programs rather than the as-built plant (e.g., Appendix B to 10 CFR Part 50 requires a quality assurance program, and 10 CFR 50.65 requires a maintenance rule program) are not included in Tier 1.

The key aspects of the design are described in Tier 1. Those aspects of the design that cannot be verified until after fuel loading are not included in ITAAC. This is because 10 CFR 52 requires the ITAAC to be satisfied prior to fuel loading. For these, the Initial Test Program verifies various aspects of the design after fuel load, but prior to operation. Examples are the post-fuel load startup and power ascension test program verification of fuel, control rod, and core characteristics, as well as system and integrated plant operating characteristics. The treatment of these issues is similar to their treatment at facilities licensed under 10 CFR 50, in that verification of the satisfactory completion of these requirements are a condition of the license.

14.3.2.1.6 Design Commitments only include Components Required to Perform System Functions in the System Description

Not every design element specified in the certified design rule has a corresponding Tier 1 verification requirement. For example the safety classification of SSC are identified in the design descriptions, but are not verified by ITAAC because there is no specific test for this characteristic. Further, some ITAAC verify system function and do not address individual system components that together yield the required system functional performance.

14.3.2.1.7 Risk-Significant Design Features as Determined by the Results of a Probabilistic Risk Assessment

Some risk-significant design features identified by the PRA do not need to be specifically addressed in the design description because they are indirectly addressed by design features that are addressed by other design commitments. For example, some PRA studies are dependent upon an assessment of the ability of certain SSC to function during seismic events that are more severe than the design basis safe shutdown earthquake (SSE). If equipment is designed and qualified for the seismic design basis, the design process is such that the added capability assumed in the PRA will inherently be present.

The risk-significant design features that are included in the design descriptions and have associated ITAAC are listed in Table 14.3-1 and Table 14.3-2.

14.3.2.1.8 Design Features Necessary or Important to Severe Accident Mitigation

There are some SSC that mitigate DBAs as well as provide an important success path for severe accident mitigation. The severe accident analysis design features that are included in the design descriptions and have associated ITAAC are listed in Table 14.3-1 and Table 14.3-2.

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14.3.2.1.9 Design Descriptions Only Include Fixed Design Features Installed Prior to Fuel Loading and Expected to be in Place for the Lifetime of the Plant

Those aspects of the design that pertain to portable items or consumables rather than fixed design features are not included in Tier 1. Because hardware such as fuel cannot be installed in the reactor until after completion of the ITAAC and because the fuel will be periodically replaced, fuel is not an appropriate topic for ITAAC.

14.3.2.2 Inspections, Tests, Analyses, and Acceptance Criteria Scope First Principles

The following criteria are considered when determining which information warrants inclusion in the ITAAC entries:

- The design commitment is extracted directly from the design descriptions and differences in text are minimized, unless intentional.
- The NRC safety determination is based solely on the Tier 2 design information.
 ITAAC are not relied upon for the NRC safety determination provided in a Safety Evaluation Report.
- The ITAAC are an important part of the NRC construction verification program, but do not verify every design and construction feature included in the certified design. The ITAAC are not meant to be a one-for-one check of detailed design and construction features that are verified by the normal construction quality programs.
- An inspection, test, or analysis, or a combination thereof, may verify one or more provisions in the design commitment, as defined by the ITAAC.

14.3.3 Organization of Tier 1

The design descriptions, interface requirements, and site parameters are derived from Tier 2 information. Tier 1 information includes

- preamble material which includes a table of contents, a list of tables, and a list of figures.
- an introduction section (described in Section 14.3.4).
- unit-specific design descriptions and ITAAC (described in Section 14.3.5). This section includes
 - systems that are fully within the scope of the NuScale Power Plant design certification.
 - The in-scope portion of those systems that are only partially within the scope of the NuScale Power Plant design certification.
- shared or common SSC and non-SSC design descriptions and ITAAC (described in Section 14.3.6).
- interface material (described in Section 14.3.7).
- site parameters (described in Section 14.3.8).

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14.3.3.1 Design Descriptions (Certified Design Material)

The design descriptions serve as requirements for the lifetime of a plant to assure that the plant does not deviate from the certified design. The design descriptions use a system-based structure that is different than the structure of Tier 2. Consequently, developing the design description entries for a system is based on multiple Tier 2 chapters having technical information related to that system.

The design description consists of a system description and design commitments. System description tables and figures are used where appropriate.

The top-level design features in Tier 1 are extracted from the more detailed design information in Tier 2 using the first principles described in Section 14.3.2.1.

System Description and Design Commitments

The purpose of the system description is to provide a concise description of the safety-related and/or risk-significant system functions, safety classification, and general location. The system description only describes those portions of the system that perform safety-related and/or risk-significant functions.

The level of detail in system descriptions uses a graded approach commensurate with the safety and risk significance of a system.

Design commitments are provided in numbered paragraphs that are used to develop the design commitment column in the ITAAC table as discussed in Section 14.3.2.2. Design commitments cover design features, such as seismic and ASME Code classifications, Class 1E power sources and divisions, equipment to be qualified for harsh environments (and other than harsh for certain instrumentation and controls (I&C) equipment).

System Description Tables

A table may be used in cases where portions of the system description can be more concisely presented in tabular form. System description tables are generally only referenced in the ITAAC acceptance criteria. System description tables are used to identify design features such as ASME Code class, valve active functions, Class 1E classification of electrical equipment, or required response time of equipment.

System Description Figures

A figure may be included in Tier 1 if it is necessary to describe something that cannot be adequately described in the system description and tables. Figures are provided to convey information in support of system descriptions, in cases where information can be more concisely presented in a figure. Figures are intended to depict a simplified schematic arrangement of the significant SSC.

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14.3.3.2 Inspections, Tests, Analyses, and Acceptance Criteria Tables

A table of ITAAC entries is provided for each system that has design commitments in the design description. A three-column format for the ITAAC table is used. All three columns of the ITAAC table must be read and interpreted together.

The first column of the ITAAC table identifies the design commitment to be verified. This column contains the specific text of the design commitment, which is extracted from the design commitments contained in the design description.

The second column of the ITAAC table identifies the proposed method by which the licensee will verify the design commitment described in column 1. The methods used are inspections, tests, analyses, or a combination of the three.

- Inspections are used when verification can be done by visual observation, physical examination, or reviews of records based on visual observation or physical examination that compare a) the SSC condition to one or more design commitments or b) the program implementation elements to one or more program commitments, as applicable. Examples include walkdowns, configuration checks, measurements of dimensions, or nondestructive examinations.
- Tests mean actuation or operation, or establishment, of specified conditions to evaluate the performance or integrity of as-built SSC, unless explicitly stated otherwise, to determine whether an ITAAC acceptance criterion is met.
 - In addition to testing equipment at its final location, alternative testing methods may be used including factory testing, test facility testing, and laboratory testing. Testing can also include type testing such as might be performed to demonstrate qualification to meet environmental requirements. Type test means a test on one or more sample components of the same type and manufacturer to qualify other components of the same type and manufacturer. A type test is not necessarily a test of an as-built SSC.
- Analyses are used when verification can be done by calculation, mathematical computation, or engineering or technical evaluations.

The third column of the ITAAC table identifies the specific acceptance criteria for the inspections, tests, or analyses described in column 2 that, if met, demonstrate that the licensee has met the design commitments in column 1. Acceptance criteria are objective and clear to avoid confusion over whether or not acceptance criteria have been satisfied.

Using the criteria listed above, ITAAC table entries were developed for each selected system. This was achieved by evaluating the design features defined in the design descriptions and preparing an ITAAC table entry for each design description entry that satisfied the above selection criteria.

Having established the design features for which ITAAC are appropriate, the ITAAC table was completed by selecting the method to be used for verification (either an inspection, a test, or an analysis, or a combination of these) and the acceptance criteria

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against which the as-built design features are measured. The proposed verification activity is identified in the second column of the ITAAC table.

Where ITAAC is verified by a preoperational test, the test will be established in accordance with the Initial Test Program described in Section 14.2 and RG 1.68. Conversion or extrapolation of test results from the test conditions to design condition may be necessary to satisfy specific ITAAC.

Selection of acceptance criteria is dependent upon the specific design characteristic being verified by the ITAAC table entry. In most cases the appropriate acceptance criteria are self- evident and are based upon the design descriptions. For many of the ITAAC, the acceptance criterion is a statement that the as-built facility has the design feature identified in the design description. A guiding principle for acceptance criteria preparation is the recognition that the criteria should be objective and unambiguous.

In some cases, the ITAAC contain numerical values from Tier 2 that are not specifically identified in the design description or the design commitment column of the ITAAC table. This is acceptable because the design description defines the important design feature that merits Tier 1 treatment. The numerical value in the acceptance criterion is a measurement standard for determining if the as-built facility is in compliance with the design commitment.

The use of objective and unambiguous terms for the acceptance criteria minimizes opportunities for multiple, subjective (and potentially conflicting) interpretations as to whether an acceptance criterion has, or has not, been met. In some cases, the acceptance criteria may be more general because the detailed supporting information in Tier 2 does not lend itself to concise verification. Numerical values for SSC are specified as ITAAC acceptance criteria when values consistent with the design commitments are possible, or when failure to meet the stated acceptance criterion would clearly indicate a failure to properly implement the design or meet the safety analysis.

Where appropriate, the detailed design information provided in Tier 2 includes supporting information for various inspections, tests, and analyses that is used to satisfy the acceptance criteria. This information describes an acceptable means of satisfying an ITAAC.

The details in Tier 2 are not referenced in Tier 1 and are not part of the CDM.

For numerical values in the acceptance criteria, ranges or tolerances are generally included. This is necessary and acceptable because:

- Specification of a single-value acceptance criterion is impractical because minute deviations would represent noncompliance.
- Tolerances recognize that legitimate site variations can occur in complex construction projects.
- Minor variations in plant parameters within the tolerance bounds have no effect on plant safety.

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14.3.3.3 Systems Within the Scope of Tier 1

The results of the ITAAC screenings of SSC that are either fully or partially within the scope of the NuScale Power Plant design certification are provided in Table 14.3-1 and Table 14.3-2. These tables identify those SSC that are addressed in Tier 1.

Tier 1 does not include systems that have been determined to not require design descriptions or ITAAC.

14.3.4 Tier 1 Chapter 1, Introduction

Tier 1 Chapter 1 contains the definitions and general provisions used in design descriptions and ITAAC. The intent of these entries is to avoid ambiguities and misinterpretations by providing front-end guidance to users of Tier 1.

Definitions are included for terms used in Tier 1 that could be subject to various interpretations. The intent is to be consistent with Tier 2 information and to reflect NRC guidance regarding various terms. Should questions on terminology arise, the definitions would aid in understanding the intent of the information in Tier 1.

General provisions are included for treatment of individual items, implementation of ITAAC (including ITAAC format), discussion of matters related to operations, and interpretation of figures. The rated reactor core thermal power is not specified because the maximum power level with any special conditions will be specified in the operating license.

Tier 2 Table 1.1-1 is used to interpret Tier 1. The information in Table 1.1-1 will not be duplicated in Tier 1 Chapter 1 in order to prevent the treatment of acronyms and abbreviations as Tier 1 CDM.

The figure legend contained in Tier 2 Chapter 1 is used to interpret Tier 1 system description figures. The information in Figures 1.7-1 through 1.7-3 will not be duplicated in Tier 1 Chapter 1 in order to prevent the treatment of figure legends as Tier 1 CDM.

14.3.5 Tier 1 Chapter 2, Unit-Specific Structures, Systems, and Components Design Descriptions and Inspections, Tests, Analyses, and Acceptance Criteria

Tier 1 Chapter 2 contains design descriptions and associated ITAAC for unit-specific systems that support a single NuScale Power Module (NPM). The unit-specific system design is identical between units. If a unit-specific system meets the first principles for entry into Tier 1 as described in Section 14.3.2.1, then its design description and ITAAC are entered into Tier 1. Tier 1 Chapter 2 includes an entry for each unit-specific system that is either fully or partially within the scope of the NuScale Power Plant design certification as identified in Table 14.3-1.

The design descriptions of a given unit-specific system are the same for all units.

However, unlike single-unit facility designs, each ITAAC for a given unit-specific system must be completed for each unit.

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The design description for a unit-specific system will only be recorded once in Tier 1, but the ITAAC for that system must be completed for each unit.

14.3.6 Tier 1 Chapter 3, Shared Structures, Systems, and Components and Non-Structures, Systems, and Components Design Descriptions and Inspections, Tests, Analyses, and Acceptance Criteria

Tier 1 Chapter 3 contains design descriptions and associated ITAAC for systems that support multiple NPMs (shared or common systems). If a shared or common system meets the first principles for entry into Tier 1 as described in Section 14.3.2.1, then its design description and ITAAC are entered into Tier 1. Tier 1 Chapter 3 includes an entry for the shared or common systems that are either fully or partially within the scope of the NuScale Power Plant design certification as identified in Table 14.3-2. Additionally, Tier 1 Chapter 3 addresses non-SSC design and construction activities that are applicable to more than one system or NPM such as human factors engineering.

Shared or common systems that must be completed to support the operation of the first NPM have their ITAAC completed once. If shared or common systems require a portion of the system to be completed to support the operation of the first NPM, then the applicable ITAAC will be in Tier 1 Chapter 2 and must be completed for each associated NPM.

Entries in this chapter of Tier 1 have the same structure as the unit-specific material discussed in Section 14.3.5; that is, design description text, tables, figures, and a table of ITAAC entries.

14.3.7 Tier 1 Chapter 4, Interface Requirements

Tier 1 Chapter 4 provides the interface requirements. Interface requirements are design features that are met by the site-specific portions of a facility that are not within the scope of the certified design. The interface requirements define the design features that ensure the site-specific portion of the design is in conformance with the certified design. The site-specific portions of the design are those portions of the design that are dependent on characteristics of the site.

Tier 1 Chapter 4 also identifies the scope of the design to be certified by specifying the systems that are completely or partially out of scope of the certified design. Thus, interface requirements are defined for: (a) systems that are entirely outside the scope of the certified design, and (b) the out-of-scope portions of those systems that are only partially within the scope of the certified design.

The NuScale Power Plant relies upon passive safety features physically located within NuScale Power Plant buildings and structures. No interfaces need to be identified between or among these portions of the facility. Tier 1 Chapter 4 does not include ITAAC or a requirement for COL developed ITAAC for interface requirements.

14.3.8 Tier 1 Chapter 5, Site Parameters

Tier 1 Chapter 5 provides bounding values for site parameters that a COL applicant referencing the NuScale Power Plant design certification will use in the design of a specific site. Compliance with these site parameters is verified during the COL application process,

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so no ITAAC are necessary for site parameters. Chapter 2 provides a discussion of the envelope of site design parameters used for the NuScale Power Plant design. The corresponding Tier 1 Chapter 5 is based on Table 2.0-1. Tier 1 Chapter 5 is limited to a tabular entry; no supporting text material is required.

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Table 14.3-1: Module-Specific Structures, Systems, and Components Based Design Features and Inspections, Tests, Analyses, and Acceptance Criteria Cross Reference

ITAAC No.	System	Discussion	DBA	Internal/External Hazard	Radiological	PRA & Severe Accident	FP
02.01.01	NPM	As required by ASME Code Section III NCA-1210, each ASME Code Class 1, 2 and 3 component (including piping systems) of a nuclear power plant requires a Design Report in accordance with NCA-3550. NCA-3551.1 requires that the drawings used for construction be in agreement with the Design Report before it is certified and be identified and described in the Design Report. It is the responsibility of the N Certificate Holder to furnish a Design Report for each component and support, except as provided in NCA-3551.2 and NCA-3551.3. NCA-3551.1 also requires that the Design Report be certified by a registered professional engineer when it is for Class 1 components and supports, Class CS core support structures, Class MC vessels and supports, Class 2 vessels designed to NC-3200 (NC-3131.1), or Class 2 or Class 3 components designed to Service Loadings greater than Design Loadings. A Class 2 Design Report shall be prepared for Class 1 piping NPS 1 or smaller that is designed in accordance with the rules of Subsection NC. NCA-3554 requires that any modification of any document used for construction, from the corresponding document used for design analysis, shall be reconciled with the Design Report. An ITAAC inspection is performed of the NuScale Power Module ASME Code Class 1, 2 and 3 as-built piping system Design Report to verify that the requirements of ASME Code Section III are met.	X				

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Table 14.3-1: Module-Specific Structures, Systems, and Components Based Design Features and Inspections, Tests, Analyses, and Acceptance Criteria Cross Reference (Continued)

ITAAC No.	System	Discussion	DBA	Internal/External Hazard	Radiological	PRA & Severe Accident	FP
02.01.02	NPM	The ASME Code Section III requires that documentary evidence be available at the construction or installation site before use or installation to ensure that ASME Code Class 1, 2 and 3 components conform to the requirements of the Code. As defined in NCA-9000, a component can be a vessel, pump, pressure relief valve, line valve, storage tank, piping system, or core support structure that is designed, constructed, and stamped in accordance with the rules of Section III. The NuScale Power Module ASME Code Class 1 and 2 components require a Data Report as specified by NCA-1210. The Data Report is prepared by the certificate holder or owner and signed by the certificate holder or owner and the inspector as specified by NCA-8410. The type of individual Data Report forms necessary to record the required code data is specified in Table NCA-8100-1. An ITAAC inspection is performed of the Data Reports for NuScale Power Module ASME Code Class 1 and 2 as-built components listed in Tier 1 Table 2.1-2 and interconnecting piping to (1) ensure that the appropriate Data Reports have been provided as specified in Table NCA-8100-1, (2) ensure that the certificate holder or owner and the authorized nuclear inspector have signed the Data Reports, and (3) verify that the requirements of ASME Code met.	X			X	

ITAAC No. Svstem DBA Internal/External Radiological PRA & Severe Hazard Accident 02.01.03 NPM The ASME Code Section III requires that documentary evidence be Χ available at the construction or installation site before use or installation to ensure that ASME Code CS components conform to the requirements of the Code. The ASME Code Class CS components require a Data Report as specified by NCA-1210. The Data Report is prepared by the certificate holder or owner and signed by the certificate holder or owner and the Inspector as specified by NCA-8410. The type of individual Data Report Forms necessary to record the required Code Data is identified in Table NCA-8100-1. An ITAAC inspection is performed of the Data Reports for the ASME Code Class CS as-built components listed in Tier 1 Table 2.1-2 to (1) ensure that the appropriate Data Reports have been provided as specified in Table NCA-8100-1, (2) ensure that the certificate holder or owner and the inspector have signed the Data Reports, and (3) verify that the requirements of ASME Code Section III are met. 02.01.04 NPM Section 3.6, Protection against Dynamic Effects Associated with Χ Χ Postulated Rupture of Piping, provides the design bases and criteria for the analysis required to demonstrate that safety-related SSC are not impacted by the adverse effects of a high-and moderate-energy pipe failure within the plant. Table 3.6-2: Postulated Break Locations, lists the high-and moderate-energy pipe break locations. An ITAAC inspection is performed to verify that the as-built protective features credited in the reconciled Pipe Break Hazards Analysis Report such as pipe whip restraints, pipe whip or jet impingement barriers, jet impingement shields, or quard pipe have been installed in accordance with design drawings of sufficient detail to show the existence and location of the protective hardware. The as-built inspection is intended to verify that changes to postulated pipe failure locations and protective features or protected equipment made during construction do not adversely affect the safety-related functions of the protected equipment.

Table 14.3-1: Module-Specific Structures, Systems, and Components Based Design Features and Inspections, Tests, Analyses, and Acceptance Criteria Cross Reference (Continued)

ITAAC No.	System	Discussion	DBA	Internal/External Hazard	Radiological	PRA & Severe Accident	FP
02.01.05	NPM	Section 3.6.3, Leak-Before-Break Evaluation Procedures, describes the application of the mechanistic pipe break criteria, commonly referred to as leak-before-break (LBB), to the evaluation of pipe ruptures. The LBB analysis eliminates the need to consider the dynamic effects of postulated pipe breaks for high-energy piping that qualify for LBB.	Х				
		An analysis, which includes material properties of piping and welds, stress analyses, leakage detection capability, and degradation mechanisms, confirms that the as-designed LBB analysis is bounding for the ASME Code Class 2 as-built piping listed in Tier 1 Table 2.1-1 and interconnected equipment nozzles. A summary of the results of the plant specific LBB analysis, including material properties of piping and welds, stress analyses, leakage detection capability, and degradation mechanisms is provided in the as-built LBB analysis report.					
02.01.06	NPM	Section 5.3.1.5, Fracture Toughness, discusses the fracture toughness properties of the reactor pressure vessel (RPV) beltline material and the Material Surveillance Program. A Charpy V-Notch test of the RPV beltline material specimen is performed by the vendor to ensure that the initial RPV beltline Charpy upper-shelf energy is no less than 75 ft-lb.	Х				
02.01.07	NPM	Section 6.2.6, Containment Leakage Testing, provides a discussion of the leakage testing requirements of the containment vessel (CNV), which serves as an essentially leak-tight barrier against the uncontrolled release of radioactivity to the environment. As discussed in Section 6.2.6, the NuScale CNV is exempted from the integrated leak rate testing specified in the General Design Criterion (GDC) 52. In accordance with Table 14.2-43, a preoperational test	Х				
		demonstrates that the leakage rate for local leak rate tests (Type B and Type C) for pressure containing or leakage-limiting boundaries and containment isolation valves (CIVs) meet the leakage acceptance criterion of 10 CFR Part 50, Appendix J.					

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Table 14.3-1: Module-Specific Structures, Systems, and Components Based Design Features and Inspections, Tests, Analyses, and Acceptance Criteria Cross Reference (Continued)

ITAAC No.	System	Discussion	DBA	Internal/External Hazard	Radiological	PRA & Severe Accident	FP
02.01.08	NPM	Section 6.2.4.3, Design Evaluation, provides a discussion of how the containment system (CNTS) containment isolation valves close within the required closure time after receipt of a containment isolation signal to meet containment isolation requirements following a radiological release in the CNV.	Х				
		In accordance with Table 14.2-63, a preoperational test demonstrates that each automatic CIV listed in Tier 1 Table 2.1-3 travels from the full open to full closed position in less than or equal to the time listed in Table 6.2-4 after receipt of a containment isolation signal.					
02.01.09	NPM	Section 6.2.4.2.2, Component Description, provides a discussion of the isolation valves outside containment that are located as close to the containment as practical in accordance with the requirements of 10 CFR Part 50, Appendix A, GDC 55, 56 and 57.	Х				
		An ITAAC inspection is performed to verify the length of piping between each containment penetration and its associated outboard CIVs is less than or equal to the length identified in Tier 1 Table 2.1-1.					
02.01.10	NPM	Section 8.1.5.3 General Design Criteria, NRC Regulations, RGs, and Branch Technical Positions, NUREG Reports, SECY Papers, and NRC Bulletins, discusses that the NPM Class 1E containment electrical penetration assemblies are sized to power their design loads as demonstrated by satisfying the guidance of RG 1.63.	Х				
		An analysis determines the required design electrical rating needed to power the design loads of each NPM Class 1E containment electrical penetration assembly listed in Tier 1 Table 2.1-3.					
		An ITAAC inspection is performed to verify that the electrical rating of each NPM Class 1E containment electrical penetration assembly listed in Tier 1 Table 2.1-3 is greater than or equal to the required design electrical rating. This ITAAC inspection may be performed any time after manufacture of the Class 1E containment electrical penetration assemblies.					

Table 14.3-1: Module-Specific Structures, Systems, and Components Based Design Features and Inspections, Tests, Analyses, and Acceptance Criteria Cross Reference (Continued)

ITAAC No.	System	Discussion	DBA	Internal/External Hazard	Radiological	PRA & Severe Accident	FP
02.01.11	NPM	Sections 7.1.2, Independence, discusses the independence of the MPS Class 1E instrumentation and control current-carrying circuits per the guidance of RG 1.75, which endorses Institute of Electrical and Electronics Engineers (IEEE) Std. 384-1992. Physical separation is provided to maintain the independence of Class 1E I&C current-carrying circuits so that the safety functions required during and following any design basis event can be accomplished. Minimum separation distance (as defined in IEEE Std. 384-1992), or barriers or any combination thereof may achieve physical separation as specified in IEEE Std. 384-1992. Separate ITAAC inspections are performed to verify the independence provided by physical separation and the independence of Class 1E current-carrying circuits by physical separation. The scope of this commitment includes the cables from the NPM disconnect box to the instrument. An ITAAC inspection is performed of physical separation of the MPS Class 1E current-carrying circuits. The physical separation ITAAC inspection results verify that the following physical separation criteria are met: i. Physical separation between redundant divisions of the MPS Class 1E I&C current-carrying circuits is provided by a minimum separation distance, or by barriers (where the minimum separation distances cannot be maintained), or by a combination of	X	THE STATE OF THE S			
		separation distance and barriers; and such physical separation satisfies the criteria of RG 1.75. The configuration of each as-built barrier agrees with its associated as-built drawing. ii. Physical separation between the MPS Class 1E I&C current-carrying circuits and non-Class 1E I&C current-carrying circuits is provided by a minimum separation distance, or by barriers (where the minimum separation distances cannot be maintained), or by a combination of separation distance and barriers; and such physical separation satisfies the criteria of RG 1.75. The configuration of each as-built barrier agrees with its associated as-built drawing.					

Table 14.3-1: Module-Specific Structures, Systems, and Components Based Design Features and Inspections, Tests, Analyses, and Acceptance Criteria Cross Reference (Continued)

ITAAC No.	System	Discussion	DBA	Internal/External Hazard	Radiological	PRA & Severe Accident	FP
02.01.12	NPM	Section 5.3.1.6, Material Surveillance, discusses the use of specimen capsules installed in specimen guide baskets.	Х				
		An ITAAC inspection is performed to verify that the correct number of guide baskets are attached to the outer surface of the core barrel at about the mid height of the core support assembly at approximately 90-degree intervals.					
02.01.13	NPM	The CNTS safety-related valves are tested by remote operation to demonstrate the capability to perform their function to transfer open and transfer closed under preoperational temperature, differential pressure, and flow conditions.	Х				
		In accordance with Table 14.2-63, a preoperational test demonstrates that the CNTS safety-related valves listed in Table 2.1-2 stroke fully open and fully closed by remote operation under preoperational test conditions.					
		Preoperational test conditions are established that approximate design-basis temperature, differential pressure, and flow conditions to the extent practical, consistent with preoperational test limitations.					
02.01.14	NPM	The emergency core cooling system (ECCS) safety-related valves are tested by remote operation to demonstrate the capability to perform their function to transfer open and transfer closed under preoperational temperature, differential pressure, and flow conditions.	Х				
		In accordance with Table 14.2-63, a preoperational test demonstrates that the ECCS safety-related valves listed in Table 2.1-2 stroke fully open and fully closed by remote operation under preoperational test conditions.					
		Preoperational test conditions are established that approximate design-basis temperature, differential pressure, and flow conditions to the extent practical, consistent with preoperational test limitations.					

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Table 14.3-1: Module-Specific Structures, Systems, and Components Based Design Features and Inspections, Tests, Analyses, and Acceptance Criteria Cross Reference (Continued)

ITAAC No.	System	Discussion	DBA	Internal/External Hazard	Radiological	PRA & Severe Accident	FP
02.01.15	NPM	The decay heat removal system (DHRS) safety-related valves are tested by remote operation to demonstrate the capability to perform their function to transfer open and transfer closed under preoperational temperature, differential pressure, and flow conditions.	Х				
		In accordance with Table 14.2-63, a preoperational test demonstrates that the DHRS safety-related valves listed in Table 2.1-2 stroke fully open and fully closed by remote operation under preoperational test conditions.					
		Preoperational test conditions are established that approximate design basis temperature, differential pressure, and flow conditions to the extent practical, consistent with preoperational test limitations.					
02.01.16	NPM	The reactor coolant system (RCS) safety-related check valves are tested to demonstrate the capability to perform their function to transfer open and transfer closed (under forward and reverse flow conditions, respectively) under preoperational temperature, differential pressure, and flow conditions. Check valves are tested in accordance with the requirements of the ASME OM Code, ISTC-5220, Check Valves.	X				
		In accordance with Table 14.2-46, a preoperational test demonstrates that the RCS check valves listed in Table 2.1-2 strokes fully open and closed under forward and reverse flow conditions, respectively.					
		Preoperational test conditions are established that approximate design-basis temperature, differential pressure and flow conditions to the extent practical, consistent with preoperational test limitations.					

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Table 14.3-1: Module-Specific Structures, Systems, and Components Based Design Features and Inspections, Tests, Analyses, and Acceptance Criteria Cross Reference (Continued)

ITAAC No.	System	Discussion	DBA	Internal/External Hazard	Radiological	PRA & Severe Accident	FP
02.01.17	NPM	The RCS safety-related excess flow check valves are tested to demonstrate the capability to perform their function to stroke fully closed under excess flow conditions under preoperational temperature, differential pressure, and flow conditions. Check valves are tested in accordance with the requirements of the ASME OM Code, ISTC-5220, Check Valves.	Х		Х		
		In accordance with Table 14.2-46, a preoperational test demonstrates that the RCS check valves listed in Table 2.1-2 strokes fully closed under forward flow conditions.					
		Preoperational test conditions are established that approximate design-basis temperature, differential pressure and flow conditions to the extent practicable, consistent with preoperational test limitations.					
02.01.18	NPM	The CNTS safety-related hydraulic-operated valves are tested to demonstrate the capability to perform their function to fail to or maintain their safety-related position on loss of motive power under preoperational temperature, differential pressure, and flow conditions.	Х				
		In accordance with Table 14.2-63, a preoperational test demonstrates that each CNTS safety-related hydraulic-operated valves listed in Table 2.1-2 repositions to or maintains its safety-related position on loss of motive power (electric power to the valve actuating solenoid(s) is lost, or hydraulic pressure to the valve(s) is lost).					
		Preoperational test conditions are established that approximate design-basis temperature, differential pressure, and flow conditions to the extent practicable, consistent with preoperational test limitations.					

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Table 14.3-1: Module-Specific Structures, Systems, and Components Based Design Features and Inspections, Tests, Analyses, and Acceptance Criteria Cross Reference (Continued)

ITAAC No.	System	Discussion	DBA	Internal/External Hazard	Radiological	PRA & Severe Accident	FP
02.01.19	NPM	The ECCS safety-related reactor recirculation valves and reactor vent valves are tested to demonstrate the capability to perform their function to fail to or maintain their safety-related position on loss of electrical power under preoperational temperature, differential pressure, and flow conditions.	Х		Х		
		In accordance with Table 14.2-63, a preoperational test demonstrates that each ECCS safety-related reactor recirculation valve and reactor vent valve listed in Table 2.1-2 fails open on loss of electrical power to its corresponding trip valve.					
		Preoperational test conditions are established that approximate design-basis temperature, differential pressure, and flow conditions to the extent practicable, consistent with preoperational test limitations.					
02.01.20	NPM	The DHRS safety-related hydraulic-operated valves are tested to demonstrate the capability to perform their function to fail to or maintain their safety-related position on loss of motive power under preoperational temperature, differential pressure, and flow conditions.	Х				
		In accordance with Table 14.2-63, a preoperational test demonstrates that each DHRS safety-related hydraulic-operated valves listed in Table 2.1-2 fails open loss of motive power (electric power to the valve actuating solenoid(s) is lost, or hydraulic pressure to the valve(s) is lost).					
		Preoperational test conditions are established that approximate design basis temperature, differential pressure, and flow conditions to the extent practicable, consistent with preoperational test limitations.					

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Table 14.3-1: Module-Specific Structures, Systems, and Components Based Design Features and Inspections, Tests, Analyses, and Acceptance Criteria Cross Reference (Continued)

ITAAC No.	System	Discussion	DBA	Internal/External Hazard	Radiological	PRA & Severe Accident	FP
02.01.21	NPM	The CNTS safety-related check valves are tested to demonstrate the capability to perform their function to transfer open and transfer closed (under forward and reverse flow conditions, respectively) under preoperational temperature, differential pressure, and flow conditions. Check valves are tested in accordance with the requirements of the ASME OM Code, ISTC-5220, Check Valves. In accordance with Table 14.2-43, a preoperational test demonstrates that the CNTS check valves listed in Tier 1 Table 2.1-2 strokes fully open and closed under forward and reverse flow conditions, respectively.	Х				
		Preoperational test conditions are established that approximate design basis temperature, differential pressure and flow conditions to the extent practicable, consistent with preoperational test limitations.					
02.01.22	NPM	Section 8.3.1.2.2, Circuit Protection and Coordination, discusses instantaneous and thermal overload fault protection to limit the loss of equipment due to postulated fault conditions. A circuit interrupting device coordination analysis confirms that the as-built Class 1E containment electrical penetration assemblies listed in Tier 1 Table 2.1-3 can withstand fault currents for the time required to clear the fault from its power source.	Х				

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Table 14.3-1: Module-Specific Structures, Systems, and Components Based Design Features and Inspections, Tests, Analyses, and Acceptance Criteria Cross Reference (Continued)

ITAAC No.	System	Discussion	DBA	Internal/External Hazard	Radiological	PRA & Severe Accident	FP
02.02.01	CVCS	As required by ASME Code Section III NCA-1210, each ASME Code Class 1, 2 and 3 component (including piping systems) of a nuclear power plant requires a Design Report in accordance with NCA-3550. NCA-3551.1 requires that the drawings used for construction be in agreement with the Design Report before it is certified and be identified and described in the Design Report. It is the responsibility of the N certificate holder to furnish a Design Report for each component and support, except as provided in NCA-3551.2 and NCA-3551.3. NCA-3551.1 also requires that the Design Report be certified by a registered professional engineer when it is for Class 1 components and supports, Class CS core support structures, Class MC vessels and supports, Class 2 vessels designed to NC-3200 (NC-3131.1), or Class 2 or Class 3 components designed to service loadings greater than design loadings. A Class 2 Design Report shall be prepared for Class 1 piping NPS 1 or smaller which is designed in accordance with the rules of Subsection NC. NCA-3554 requires that any modification of any document used for construction, from the corresponding document used for design analysis, shall be reconciled with the Design Report. An ITAAC inspection is performed of the chemical and volume control system (CVCS) ASME Code Class 3 as-built piping system Design Report to verify that the requirements of ASME Code Section III are met.	X				

Table 14.3-1: Module-Specific Structures, Systems, and Components Based Design Features and Inspections, Tests, Analyses, and Acceptance Criteria Cross Reference (Continued)

ITAAC No.	System	Discussion	DBA	Internal/External Hazard	Radiological	PRA & Severe Accident	FP
02.02.02	CVCS	The ASME Code Section III requires that documentary evidence be available at the construction or installation site before use or installation to ensure that ASME Code Class 1, 2 and 3 components conform to the requirements of the Code. As defined in NCA-9000, a component can be a vessel, pump, pressure relief valve, line valve, storage tank, piping system, or core support structure that is designed, constructed, and stamped in accordance with the rules of Section III. The chemical and volume control system ASME Code Class 3 components require a Data Report as specified by NCA-1210. The Data Report is prepared by the certificate holder or owner and signed by the certificate holder or owner and signed by the certificate holder or owner and the inspector as specified by NCA-8410. The type of individual Data Report forms necessary to record the required code data is specified in Table NCA-8100-1. An ITAAC inspection is performed of the Data Reports for the chemical and volume control system ASME Code Class 3 as-built components listed in Tier 1 Table 2.2-2 and interconnecting piping that is described in Section 9.3.4 to (1) ensure that the appropriate Data Reports have been provided as specified in Table NCA-8100-1, (2) ensure that the certificate holder or owner and the authorized nuclear inspector have signed the Data Reports, and (3) verify that the requirements of ASME Code Section III are met.	X				

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Table 14.3-1: Module-Specific Structures, Systems, and Components Based Design Features and Inspections, Tests, Analyses, and Acceptance Criteria Cross Reference (Continued)

ITAAC No.	System	Discussion	DBA	Internal/External Hazard	Radiological	PRA & Severe Accident	FP
02.02.03	cvcs	The chemical and volume control ASME Code Class 3 valves are tested by remote operation to demonstrate the capability to perform their function to transfer open and transfer closed under preoperational temperature, differential pressure, and flow conditions.	Х				
		In accordance with the information provided in Table 14.2-38, a preoperational test demonstrates that the chemical and volume control system ASME Code Class 3 valves listed in Tier 1 Table 2.2-2 stroke fully open and fully closed by remote operation under preoperational test conditions.					
		Preoperational test conditions are established that approximate design basis temperature, differential pressure, and flow conditions to the extent practicable, consistent with preoperational test limitations.					
02.02.04	CVCS	The chemical and volume control system ASME Code Class 3 check valves are tested to demonstrate the capability to perform their function to transfer closed (under reverse flow conditions) under preoperational temperature, differential pressure, and flow conditions. Check valves are tested in accordance with the requirements of the ASME OM Code, ISTC-5220, Check Valves.	Х				
		In accordance with the information provided in Table 14.2-38, a preoperational test demonstrates that the chemical and volume control system ASME Code Class 3 check valves listed in Tier 1 Table 2.2-2 stroke fully closed under reverse flow conditions.					
		Preoperational test conditions are established that approximate design basis temperature, differential pressure and flow conditions to the extent practicable, consistent with preoperational test limitations.					

	ITAAC No.	System	Discussion	DBA	Internal/External Hazard	Radiological	PRA & Severe Accident	FP
	02.02.05	CVCS	The chemical and volume control system ASME Code Class 3 air- operated valves are tested to demonstrate the capability to perform their function to fail to or maintain their position on loss of motive power under preoperational temperature, differential pressure, and flow conditions.	Х				
			In accordance with Table 14.2-38, a preoperational test demonstrates that each chemical and volume control system ASME Code Class 3 air-operated valves listed in Tier 1 Table 2.2-2 fails closed on loss of motive power (electric power to the valve actuating solenoid(s) is lost, or pneumatic pressure to the valve(s) is lost).					
14			Preoperational test conditions are established that approximate design-basis temperature, differential pressure, and flow conditions to the extent practicable, consistent with preoperational test limitations.					
14 3-28	02.03.01	CES	Section 5.2.5 Reactor Coolant Pressure Boundary Leakage Detection, discusses that RCS leakage detection systems are designed to detect and, to the extent practicable, identify the source of reactor coolant leakage. The RCS leakage detection systems conform to the guidance of RG 1.45, regarding detection, monitoring, quantifying, and identification of reactor coolant leakage.	Х				
			In accordance with the information provided in Table 14.2-41, a preoperational test demonstrates that the containment evacuation system (CES) detects a level increase in the CES sample vessel, which correlates to a detection of an unidentified RCS leakage rate of one gpm within one hour.					
Revision 0			Water vapor and non-condensable gases are removed from the containment vessel by the CES. The water vapor is collected and condensed in the CES sample vessel where it is monitored using level and temperature instrumentation. The CES sample vessel level instrumentation is used to quantify and trend leak rates in the containment.					

Table 14.3-1: Module-Specific Structures, Systems, and Components Based Design Features and Inspections, Tests, Analyses, and Acceptance Criteria Cross Reference (Continued)

ITAAC No.	System	Discussion	DBA	Internal/External Hazard	Radiological	PRA & Severe Accident	FP
02.03.02 CES	CES	Section 5.2.5, Reactor Coolant Pressure Boundary Leakage Detection, discusses that RCS leakage detection systems are designed to detect and, to the extent practicable, identify the source of reactor coolant leakage. The RCS leakage detection systems conform to the guidance of RG 1.45, regarding detection, monitoring, quantifying, and identification of reactor coolant leakage.	Х				
		In accordance with Table 14.2-41, a preoperational test demonstrates that the CES is capable of detecting a pressure increase in the CES inlet pressure instrumentation (PIT-1001/PIT-1019), which correlates to a detection of an unidentified RCS leakage rate of one gpm within one hour.					
02.04.01	TG	Section 10.2.2.3.3, Overspeed Protection, provides a description of the turbine generator system and its redundant independent turbine overspeed protection systems (OSPs), i.e., the governor overspeed detection circuit and the turbine emergency trip system. An ITAAC inspection is performed of the turbine overspeed protection arrangement to verify that the trip circuitry for the governor overspeed detection circuit and the turbine emergency trip system are supplied from different power sources and do not share common equipment.	Х				
02.04.02	TG	Section 10.1.2.4, Turbine Overspeed Protection, discusses the turbine stop valve and turbine control valves and the associated turbine trip signals. In accordance with the information provided in Table 14.2-33, a preoperational test will be performed to verify the turbine stop valve and turbine control valves close on a turbine overspeed trip signal from both the turbine emergency trip system and the governor overspeed detection circuit.	Х				

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Table 14.3-1: Module-Specific Structures, Systems, and Components Based Design Features and Inspections, Tests, Analyses, and Acceptance Criteria Cross Reference (Continued)

ITAAC No.	System	Discussion	DBA	Internal/External Hazard	Radiological	PRA & Severe Accident	FP
02.05.01	MPS	Section 7.2.1.1, I&C Safety System Development Process, discusses the software lifecycle phases for the MPS. The purpose is to verify software implementation based on licensing commitments to 10 CFR Part 50, Appendix A, GDC 1 (Quality), Appendix B (Quality Assurance Criteria), RGs 1.28, 1.152, 1.168, 1.169, 1.170, 1.171, 1.172, and 1.173, and the associated IEEE standards. The licensee shall perform analyses for each phase and generate technical reports to conclude that the lifecycle phases were implemented per the licensing commitments. Per RG 1.152, a generic waterfall software life cycle model consists of the following phases: (1) concepts, (2) requirements, (3) design, (4) implementation, (5) test, (6) installation, checkout, and acceptance testing, (7) operation, (8) maintenance, and (9) retirement. The ITAAC verifies that output documentation of each Software Lifecycle phase satisfies the requirements of that phase for the MPS	X				
		and that software were implemented per licensing commitments to 10 CFR Part 50, Appendix A, GDC1 (Quality), Appendix B (Quality Assurance Criteria), RGs 1.28, 1.152, 1.168, 1.169, 1.170, 1.171, 1.172, and 1.173, and the associated IEEE standards.					
02.05.02	MPS	Section 7.2.9, Control of Access, Identification, and Repair, discusses the protective measures that prevent modification of the MPS tunable parameters without proper configuration and authorization. Guidance on this issue is provided in DI&C-ISG-04 Revision 1, "Highly-Integrated Control Rooms - Communications Issues," under interdivisional communications, staff position 10.	Х				
		In accordance with Table 14.2-63, a preoperational test demonstrates that protective measures restrict modification to the MPS tunable parameters without proper configuration and authorization. This test will be performed by attempting to modify the tunable parameters with the MPS not in the correct configuration or without authorization.					

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Table 14.3-1: Module-Specific Structures, Systems, and Components Based Design Features and Inspections, Tests, Analyses, and Acceptance Criteria Cross Reference (Continued)

ITAAC No.	System	Discussion	DBA	Internal/External Hazard	Radiological	PRA & Severe Accident	FP
02.05.03	MPS	Sections 7.1.2, Independence, discusses the independence of the MPS Class 1E I&C current-carrying circuits per the guidance of RG 1.75, which endorses IEEE Std. 384-1992. Physical separation is provided to maintain the independence of Class 1E I&C current-carrying circuits so that the safety functions required during and following any design basis event can be accomplished. Minimum separation distance (as defined in IEEE Std. 384-1992), or barriers or any combination thereof may achieve physical separation as specified in IEEE Std. 384-1992. Separate ITAAC inspections are performed to verify the independence provided by physical separation and the independence provided by electrical isolation. This ITAAC verifies the independence of Class 1E current-carrying circuits by physical separation. An ITAAC inspection is performed of physical separation of the MPS Class 1E current-carrying circuits. The physical separation ITAAC inspection results verify that the following physical separation between redundant divisions of the MPS Class 1E I&C current-carrying circuits is provided by a minimum separation distance, or by barriers (where the minimum separation distance and barriers; and such physical separation satisfies the criteria of RG 1.75. The configuration of each as-built barrier agrees with its associated as-built drawing. ii. Physical separation between the MPS Class 1E I&C current-carrying circuits is provided by a minimum separation distance, or by barriers (where the minimum separation distance, or by barriers; and such physical separation separation distance, or by barriers (where the minimum separation distance, or by barriers; and such physical separation separation distance, or by barriers (where the minimum separation distances cannot be maintained), or by a combination of separation distance and barriers; and such physical separation satisfies the criteria of RG 1.75. The configuration of each as-built barrier agrees with its associated as-built drawing.	X				

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Table 14.3-1: Module-Specific Structures, Systems, and Components Based Design Features and Inspections, Tests, Analyses, and Acceptance Criteria Cross Reference (Continued)

ITAAC No.	System	Discussion	DBA	Internal/External Hazard	Radiological	PRA & Severe Accident	FP
02.05.04	MPS	Sections 7.1.2, Independence, discusses the independence of the MPS Class 1E I&C circuits per the criteria of RG 1.75, which endorses IEEE Std. 384-1992. Electrical isolation is provided between the redundant divisions of the MPS Class 1E I&C circuits, and between Class 1E I&C circuits and non-Class 1E I&C circuits by Class 1E isolation devices so a failure in an I&C circuit does not prevent safety-related function completion in a different Class 1E I&C circuit.	Х				
		An ITAAC inspection is performed to verify the following electrical isolation criteria are met:					
		 i. Class 1E electrical isolation devices that satisfy the criteria of RG 1.75 are installed between redundant divisions of the MPS Class 1E l&C circuits. 					
		 ii. Class 1E electrical isolation devices that satisfy the criteria of RG 1.75 are installed between the MPS Class 1E I&C circuits and non-Class 1E I&C circuits. 					
02.05.05	MPS	Sections 7.1.2, Independence, discusses the independence of MPS Class 1E circuits per the criteria of RG 1.75, which endorses IEEE Std. 384-1992. Electrical isolation is provided between Class 1E circuits and non-Class 1E circuits by Class 1E isolation devices so a failure in a non-Class 1E circuit does not prevent the safety-related function completion in the Class 1E circuit.	Х				
		 i. The ITAAC verifies that: (1) an equipment qualification data report exists for the Class 1E isolation devices, and (2) the equipment qualification data report concludes that the Class 1E isolation devices performs its safety-related function under the design basis environmental conditions specified in the equipment qualification data report. 					
		 ii. An ITAAC inspection is performed to verify that Class 1E electrical isolation devices are installed between MPS Class 1E circuits and non-Class 1E circuits, which satisfy the guidance of RG 1.75. 					

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Table 14.3-1: Module-Specific Structures, Systems, and Components Based Design Features and Inspections, Tests, Analyses, and Acceptance Criteria Cross Reference (Continued)

IT	AAC No.	System	Discussion	DBA	Internal/External Hazard	Radiological	PRA & Severe Accident	FP
0	02.05.06	MPS	Section 7.1.2, Independence, discusses the communication independence between redundant Class 1E digital communication system divisions. The purpose is to verify proper data isolation between redundant divisions. Requirements for independence are given in IEEE Std. 603-1991. Guidance for providing independence between redundant divisions of the Class 1E digital communication system is provided in Digital I&Cs Interim Staff Guidance (ISG) 04. A vendor test demonstrates that independence between redundant divisions of the Class 1E MPS is provided.	Х				
0	02.05.07	MPS	Section 7.1.2, Independence, discusses the communication independence between Class 1E digital communication systems and non-Class 1E digital communication systems. The purpose is to verify that logical or software malfunction of the nonsafety-related system cannot affect the functions of the safety system. Requirements for independence are given in IEEE Std. 603-1991. Guidance for providing independence between the Class 1E digital communication system and non-Class 1E digital communication systems is provided in Digital Instrumentation and Controls ISG 04. A vendor test demonstrates that independence between the Class	Х				
0)2.05.08	MPS	Section 7.1.1.2.1, Protection Systems, describes automatic and manual reactor trips, variables that are monitored to provide input into automatic reactor trip signals, and the features of the reactor trip system (RTS). The reactor trip functions are listed in Table 7.1-3: Reactor Trip Functions. The reactor trip logic for the monitored variables is provided in Figure 7.1-1. The MPS initiates an automatic reactor trip signal when the associated plant condition(s) exist. In accordance with Table 14.2-63, a preoperational test demonstrates that a reactor trip signal is automatically initiated for each reactor trip function listed in Tier 1 Table 2.5-1. The actuation of reactor trip breakers (RTBs) is not required for this test. The verification of the existence of a reactor trip signal is accomplished using main control room (MCR) displays.	X				

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Table 14.3-1: Module-Specific Structures, Systems, and Components Based Design Features and Inspections, Tests, Analyses, and Acceptance Criteria Cross Reference (Continued)

ITAAC No.	System	Discussion	DBA	Internal/External Hazard	Radiological	PRA & Severe Accident	FP
02.05.09	MPS	Section 7.1.1.2.1, Protection Systems, describes automatic and manual engineered safety features (ESFs) actuations, variables that are monitored to provide input into automatic ESFs signals, and the features of the ESF systems. The ESFs functions are listed in Table 7.1-4: Module Protection System Engineered Safeguards Functions. The ESFs logic for the monitored variables is provided in Figure 7.1-1. The MPS initiates an automatic ESF actuation signal when the associated plant condition(s) exist.	Х				
		In accordance with Table 14.2-63, a preoperational test demonstrates that an automatic ESF actuation signal is automatically initiated for each of the ESF functions listed in Tier 1 Table 2.5-2.					
		The actuation of ESFs equipment is not required for this test. The verification of the existence of an ESF actuation signal is accomplished using MCR displays.					
02.05.10	MPS	Section 7.1.1.2.1, Protection Systems, describes automatic and manual reactor trips, variables that are monitored to provide input into automatic reactor trip signals, and the features of the RTS. The reactor trip functions are listed in Table 7.1-3: Reactor Trip Functions. The reactor trip logic for the monitored variables is provided in Figure 7.1.	Х				
		The MPS initiates an automatic reactor trip signal for the reactor trip functions when the associated plant condition(s) exist.					
		In accordance with Table 14.2-63, a preoperational test demonstrates that the RTBs open when any one of the automatic reactor trip functions is initiated from the MCR. The RTBs are only opened once to satisfy this test objective.					

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Table 14.3-1: Module-Specific Structures, Systems, and Components Based Design Features and Inspections, Tests, Analyses, and Acceptance Criteria Cross Reference (Continued)

ITAAC No.	System	Discussion	DBA	Internal/External Hazard	Radiological	PRA & Severe Accident	FP
02.05.11	MPS	Section 7.1.1.2.1, Protection Systems, describes automatic and manual ESFs actuations, variables that are monitored to provide input into automatic ESFs signals, and the features of the engineered safety feature systems. The ESFs functions are listed in Table 7.1-4: Module Protection System Engineered Safeguards Functions. The ESFs logic for the monitored variables is provided in Figure 7.1.	Х				
		The MPS initiates an automatic ESF actuation signal for the functions listed in Tier 1 Table 2.5-2 when the associated plant condition(s) exist.					
		In accordance with Table 14.2-63, a preoperational test demonstrates that ESF equipment automatically actuates to perform its safety-related function listed in Tier 1 Table 2.5-2 upon an injection of a single simulated MPS signal.					
02.05.12	MPS	Section 7.1.1.2.1, Protection Systems, describes automatic and manual reactor trips, variables that are monitored to provide input into automatic reactor trip signals, and the features of the RTS. A manual reactor trip is one of the MPS manually actuated functions. In accordance with Table 14.2-63, a preoperational test	Х				
		demonstrates that the RTBs open when a reactor trip is manually initiated from the MCR.					
02.05.13	MPS	Section 7.1.1.2.1, Protection Systems, describes manual ESFs actuation, variables that are monitored to provide input into automatic ESFs signals, and the features of the ESF system. The ESFs functions that can be manually actuated are shown in Figure 7.1-1	Х				
		In accordance with Table 14.2-63, a preoperational test demonstrates that the MPS actuates the ESF equipment to perform its safety-related function listed in Tier 1 Table 2.5-3 when manually initiated.					

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Table 14.3-1: Module-Specific Structures, Systems, and Components Based Design Features and Inspections, Tests, Analyses, and Acceptance Criteria Cross Reference (Continued)

ITAAC No.	System	Discussion	DBA	Internal/External Hazard	Radiological	PRA & Severe Accident	FP
02.05.14	MPS	Section 7.1.6, Safety Evaluation, describes the MPS conformance to the GDC in 10 CFR 50 Appendix A. Guidance provided in Design Specific Review Standard Section 7.2.3, Reliability, Integrity, and Completion of Protective Action, states that the design incorporate protective measures that provide for I&C safety systems to fail in a safe state, or into a state that has been demonstrated to be acceptable on some other defined basis, if conditions such as disconnection of the system, loss of power, or adverse environments, are experienced.	Х				
		Section 7.1.6 describes that consistent with GDC 23, the MPS is designed, with sufficient functional diversity as to prevent the loss of a protection function, to fail into a safe state or into a state demonstrated to be acceptable on some other defined basis if conditions such as disconnection of the system, loss of power, or postulated adverse environments are experienced. Section 7.2.3.2, System Integrity Characteristics, states that the MPS is designed such that in the event of a condition such as a system disconnection or loss of power the MPS fails into a safe state. In accordance with Table 14.2-63, a preoperational test					
		demonstrates that when the loss of electrical power is detected in a separation group of the MPS that separation group fails to a safe state resulting in a reactor trip state for that separation group.					

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Table 14.3-1: Module-Specific Structures, Systems, and Components Based Design Features and Inspections, Tests, Analyses, and Acceptance Criteria Cross Reference (Continued)

ITAAC No.	System	Discussion	DBA	Internal/External Hazard	Radiological	PRA & Severe Accident	FP
02.05.15	MPS	Section 7.1.6, Safety Evaluation, describes the MPS conformance to the GDC in 10 CFR 50 Appendix A. Guidance provided in Design Specific Review Standard Section 7.2.3, Reliability, Integrity, and Completion of Protective Action, states that the design incorporate protective measures that provide for I&C safety systems to fail in a safe state, or into a state that has been demonstrated to be acceptable on some other defined basis, if conditions such as disconnection of the system, loss of power, or adverse environments, are experienced.	Х				
		Section 7.1.6 describes that consistent with GDC 23, the MPS is designed, with sufficient functional diversity as to prevent the loss of a protection function, to fail into a safe state or into a state demonstrated to be acceptable on some other defined basis if conditions such as disconnection of the system, loss of power, or postulated adverse environments are experienced. Section 7.2.3.2, System Integrity Characteristics, states that the MPS is designed such that in the event of a condition such as a system disconnection or loss of power the MPS fails into a safe state. For an ESF function this predefined safe state may be that the actuated component remains as-is.					
		In accordance with Table 14.2-63, a preoperational test demonstrates that when the loss of electrical power is detected in a separation group of the MPS that separation group fails to a safe state for that separation group.					

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Table 14.3-1: Module-Specific Structures, Systems, and Components Based Design Features and Inspections, Tests, Analyses, and Acceptance Criteria Cross Reference (Continued)

ITAAC No.	System	Discussion	DBA	Internal/External Hazard	Radiological	PRA & Severe Accident	FP
02.05.16	MPS	Section 7.2.3.3, Completion of Protective Action, describes compliance with requirements for completion of protective actions, which requires that, once initiated, the reactor trip and ESF proceed to completion and remain in their required position/condition until the actuation system is reset and operator action is taken. IEEE 603-1991 Clause 5.2 states that `The safety systems shall be designed so that, once initiated automatically or manually, the intended sequence of protective actions of the execute features shall continue until completion. Deliberate operation action shall be required to return the safety systems to normal. This requirement shall not preclude the use of equipment protective devices identified in [Clause] 4.11 of the design basis or the provisions for deliberate operator interventions. Seal-in of individual channels is not required."	X				
		 i. upon an MPS reactor trip signal listed in Tier 1 Table 2.5-1, the RTBs open and the RTBs do not automatically close when the MPS reactor trip signal clears. ii. upon an MPS engineered safety feature actuation signal listed in Tier 1 Table 2.5-2, the ESF equipment actuates to perform its safety-related function and continues to maintain its safety-related position and perform its safety-related function when the MPS engineered safety feature actuation signal clears. 					

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Table 14.3-1: Module-Specific Structures, Systems, and Components Based Design Features and Inspections, Tests, Analyses, and Acceptance Criteria Cross Reference (Continued)

ITAAC No.	System	Discussion	DBA	Internal/External Hazard	Radiological	PRA & Severe Accident	FP
02.05.17	MPS	Section 7.2.12.1, Automatic Control, describes the signals and initiating logic for each reactor trip and required response times. Reactor trip response time is defined in technical specification Section 1.1, Definitions, as RTS RESPONSE TIME is that time interval from when the monitored parameter exceeds its RTS trip setpoint at the channel sensor until loss of stationary gripper coil voltage.	Х				
		In accordance with Table 14.2-63, a preoperational test demonstrates that the measured time for the reactor trip functions listed in Tier 1 Table 2.5-1 is less than or equal to the maximum values assumed in the accident analysis. Technical specification Section 1.1, Definitions, states that the response time may be measured by means of any series of sequential, overlapping, or total steps so that the entire response time is measured.					
		Section 7.2.12.1, Automatic Control, describes the signals and initiating logic for each ESF and the required response times. The ESF response time is defined in technical specification Section 1.1, Definitions, as ESF RESPONSE TIME is that time interval from when the monitored parameter exceeds its actuation setpoint at the channel sensor until the ESF equipment is capable of performing its safety function (i.e., the valves travel to their required positions).					
		In accordance with Table 14.2-63, a preoperational test demonstrates that the measured time for the ESF functions listed in Tier 1 Table 2.5-2 is less than or equal to the maximum values assumed in the accident analysis. Technical specification Section 1.1, Definitions, states that the response time may be measured by means of any series of sequential, overlapping, or total steps so that the entire response time is measured.					

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Table 14.3-1: Module-Specific Structures, Systems, and Components Based Design Features and Inspections, Tests, Analyses, and Acceptance Criteria Cross Reference (Continued)

ITAAC No.	System	Discussion	DBA	Internal/External Hazard	Radiological	PRA & Severe Accident	FP
02.05.18	MPS	Section 7.2.4.1, Operating Bypasses, describes MPS operating bypasses for reactor trip functions. Section 7.2.4.1, Operating Bypasses, describes MPS operating bypasses for ESF actuations. The operating bypasses are applied automatically when plant conditions dictate that the safety function is not needed, or that the safety function prevents proper plant operation at a specific mode of operation. In accordance with Table 14.2-63, a preoperational test demonstrates that the MPS interlocks listed in Tier 1 Table 2.5-4 automatically establish an operating bypass for the specified reactor trip or ESF actuations when a real or simulated signal simulates that the associated interlock condition is met; and are automatically removed when the real or simulated signal simulates	Х				
02.05.19	MPS	that the associated permissive condition is no longer satisfied. Section 7.2.4.1, Operating Bypasses, describes MPS operating bypasses for reactor trip functions. Section 7.2.4.1, Operating Bypasses, describes MPS operating bypasses for ESF actuations. The operating bypasses are applied automatically when plant conditions dictate that the safety function is not needed, or that the safety function prevents proper plant operation at a specific mode of operation.	X				
		In accordance with Table 14.2-63, a preoperational test demonstrates that the MPS permissives listed in Tier 1 Table 2.5-4 allows the manual bypass of the specified reactor trip or ESF actuations when a real or simulated signal simulates that the associated permissive condition is met; and are automatically removed when the real or simulated signal simulates that the associated permissive condition is no longer satisfied.					

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Table 14.3-1: Module-Specific Structures, Systems, and Components Based Design Features and Inspections, Tests, Analyses, and Acceptance Criteria Cross Reference (Continued)

ITAAC No.	System	Discussion	DBA	Internal/External Hazard	Radiological	PRA & Severe Accident	FP
02.05.20	MPS	Section 7.2.4.1, Operating Bypasses, describes MPS operating bypasses for reactor trip functions. Section 7.2.4.1, Operating Bypasses, describes MPS operating bypasses for ESF actuations. The operating bypasses are applied automatically when plant conditions dictate that the safety function is not needed, or that the safety function prevents proper plant operation at a specific mode of operation.	Х				
		In accordance with Table 14.2-63, a preoperational test demonstrates that the MPS overrides listed in Tier 1 Table 2.5-4 are established when the manual override switch is active and a real or simulated RT-1 interlock is established.					
02.05.21	MPS	Section 7.2.4.2, Maintenance Bypass, describes the MPS maintenance bypass operation mode. An individual protection channel can be placed in a maintenance bypass operation mode to allow manual testing and maintenance during power operation, while ensuring that the minimum redundancy required by the Technical Specifications is maintained. The reactor trip functions are listed in Table 7.1-3: Reactor Trip Functions. The ESFs functions are listed in Table 7.1-4: Module Protection System Engineered Safeguards Functions.	Х				
		In accordance with Table 14.2-63, a preoperational test demonstrates that with a safety function module out of service switch activated, the safety function is placed in trip or bypass based on the position of the safety function module trip/bypass switch. Each separation group of the reactor trip functions listed in Tier 1 Table 2.5-1 and each separation group of the ESFs signals listed in Tier 1 Table 2.5-2 is tested by placing the separation group in maintenance bypass.					

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Table 14.3-1: Module-Specific Structures, Systems, and Components Based Design Features and Inspections, Tests, Analyses, and Acceptance Criteria Cross Reference (Continued)

ITAAC No.	System	Discussion	DBA	Internal/External Hazard	Radiological	PRA & Severe Accident	FP
02.05.22	MPS	Section 7.2.4.2, Maintenance Bypass, describes the MPS maintenance bypass operation mode. An individual protection channel can be placed in a maintenance bypass operation mode to allow manual testing and maintenance during power operation, while ensuring that the minimum redundancy required by the technical specifications is maintained. Section 7.2.4.2 discusses the status indication of MPS manual or automatic bypasses placed in maintenance bypass operation mode. In accordance with Table 14.2-63, a preoperational test demonstrates that each operational MPS manual or automatic	Х				
02.05.23	MPS	bypass is indicated in the MCR. Section 7.2.4.2, Maintenance Bypass, describes the MPS maintenance bypass operation mode. An individual protection channel can be placed in a maintenance bypass operation mode to allow manual testing and maintenance during power operation, while ensuring that the minimum redundancy required by the technical specifications is maintained. Section 7.2.4.2 discusses the status indication of MPS maintenance bypasses placed in maintenance bypass operation mode. In accordance with Table 14.2-63, a preoperational test demonstrates that each MPS maintenance bypass is indicated in the MCR.	Х				

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Table 14.3-1: Module-Specific Structures, Systems, and Components Based Design Features and Inspections, Tests, Analyses, and Acceptance Criteria Cross Reference (Continued)

ITAAC No.	System	Discussion	DBA	Internal/External Hazard	Radiological	PRA & Severe Accident	FP
02.05.24	MPS	This ITAAC is intended to address self-testing features credited towards surveillance or other operational testing. Given the nature of this ITAAC, it is acceptable to verify ITAAC completion during the factory acceptance testing (FAT). Self-testing features include, but are not limited to, watchdog timers, automated channel checks, and signal input comparisons.	Х				
		Section 7.2.15.3, Fault Detection and Self-diagnostics, discusses the self-testing features of the MPS, including the types of faults that should be detected, the system responses to such faults, the required response times, and the ability for alarms and displays in the MCR to provide indication of such faults' existence.					
		These tests of the MPS self-testing features ensure that a) faults requiring detection are detected, b) the system responds appropriately to each fault based on the type of fault, c) the response occurs within a sufficient timeframe to ensure safety function is not lost, and d) that alarms and indications in the main control room indicate the type of fault present.					
		A vendor test demonstrates and a report exists and concludes that:					
		 self-testing features verify that faults requiring detection are detected. self-testing features verify that upon detection, the system responds according to the type of fault. self-testing features verify that faults are detected and responded within a sufficient timeframe to ensure safety function is not lost. self-testing features verify that detected faults are indicated by alarms and displays. 					

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Table 14.3-1: Module-Specific Structures, Systems, and Components Based Design Features and Inspections, Tests, Analyses, and Acceptance Criteria Cross Reference (Continued)

ITAAC No.	System	Discussion	DBA	Internal/External Hazard	Radiological	PRA & Severe Accident	FP
02.05.25	MPS	Section 7.1.1.2.2, Post Accident Monitoring, and Section 7.2.13, Displays and Monitoring, describe the post-accident monitoring (PAM) Type B and C displays and alarms indicated on the safety display and indication system (SDIS) displays in the MCR. PAM Type B and C variables are developed in accordance with the guidance in RG 1.97, Revision 4, "Criteria for Accident Monitoring Instrumentation for Nuclear Power Plants" which endorses (with certain clarifying regulatory positions specified in Section C of this guide) IEEE Std. 497-2002.1, "IEEE Standard Criteria for Accident Monitoring Instrumentation for Nuclear Power Generating Stations."	Х				
		In accordance with Table 14.2-66, a preoperational test demonstrates the ability to retrieve and display the various PAM Type B and C parameters and alarms at the as-built safety display indication displays in the main control room. The intent is to verify that the displays and alarms function during testing of the integrated as-built system; however, separate testing of the actual operation of the PAM alarms and displays using simulated signals may be acceptable where this is not practical.					
02.05.26	MPS	Section 18.6, Treatment of Important Human Actions, provides a summary of the treatment of important human actions (TIHA) objectives, scope, methodology, and results. The TIHA methodology and the results are documented in the TIHA results summary report. The TIHA approach is consistent with the applicable provisions of NUREG-0711, Revision 3. In accordance with Table 14.2-63, a preoperational test demonstrates that the minimum inventory of controls identified by the human factors engineering process is can be manually operated from the operator workstation in the MCR.	Х				

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Table 14.3-1: Module-Specific Structures, Systems, and Components Based Design Features and Inspections, Tests, Analyses, and Acceptance Criteria Cross Reference (Continued)

ITAAC No.	System	Discussion	DBA	Internal/External Hazard	Radiological	PRA & Severe Accident	FP
02.05.27	MPS	Section 7.0.4.1.2, Reactor Trip System, discusses the arrangement of the protection system RTBs. Figure 7.0-6: Reactor Trip Breaker Arrangement provides the arrangement of the RTBs.	Х				
		This ITAAC verifies that the RTBs conform to the arrangement indicated in Tier 1 Figure 2.5-1. In addition, the ITAAC inspection verifies proper connection of the shunt and undervoltage trip mechanisms and other auxiliary contacts.					
02.05.28	MPS	Section 7.1.5.1, Application of NUREG/CR-6303 Guidelines, discusses that two of the four separation groups and one of the two divisions of RTS and ESFAS will utilize a different programmable technology. A ITAAC inspection is performed to verify that MPS separation	Х				
		groups A & C and Division I of RTS and ESFAS utilize a different programmable technology from separation groups B & D and Division II of RTS and ESFAS.					
02.05.29	MPS	Section 7.1.3.3, Redundancy in Nonsafety I&C System Design, discusses that when operators evacuate the MCR and occupy the RSS, two manual isolation switches for the MPS divisions are provided to isolate the MPS manual actuation switches in the MCR to prevent fires in the MCR from causing spurious actuations of associated equipment.	Х				
		An ITAAC inspection is performed of each MCR isolation switch location to verify that the switch exists in the RSS.					

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Table 14.3-1: Module-Specific Structures, Systems, and Components Based Design Features and Inspections, Tests, Analyses, and Acceptance Criteria Cross Reference (Continued)

ITAAC No.	System	Discussion	DBA	Internal/External Hazard	Radiological	PRA & Severe Accident	FP
02.06.01	NMS	Section 7.1.2.2, Electrical Independence, discusses the independence of the neutron monitoring system (NMS) Class 1E circuits. Electrical isolation is provided between Class 1E circuits and non-Class 1E circuits by Class 1E isolation devices so a failure in a non-Class 1E circuit does not prevent the safety-related function completion in the Class 1E circuit.	Х				
		A type test, analysis, or a combination of type test and analysis will be performed of the Class 1E isolation devices to verify that the Class 1E circuit does not degrade below defined acceptable operating levels when the non-Class 1E side of the isolation device is subjected to the maximum credible voltage, current transients, shorts, grounds, or open circuits.					
		An ITAAC inspection is performed to verify that Class 1E electrical isolation devices are installed between NMS Class 1E circuits and non-Class 1E circuits.					

Table 14.3-1: Module-Specific Structures, Systems, and Components Based Design Features and Inspections, Tests, Analyses, and Acceptance Criteria Cross Reference (Continued)

ITAAC No.	System	Discussion	DBA	Internal/External Hazard	Radiological	PRA & Severe Accident	FP
02.06.02	NMS	Sections 7.0.3.2, Safety-Related Systems, 7.1.2.1, Physical Independence, and 7.1.2.4.1, Independence between Redundant Portions of a Safety System, discuss the independence of the NMS Class 1E I&C current-carrying circuits per the guidance of RG 1.75, which endorses IEEE Std. 384-1992. Physical separation is provided to maintain the independence of Class 1E I&C current-carrying circuits so that the safety functions required during and following any design basis event can be accomplished. Minimum separation distance (as defined in IEEE Std. 384-1992), or barriers or any combination thereof may achieve physical separation as specified in IEEE Std. 384-1992.	Х				
		Separate ITAAC inspections are performed to verify the independence provided by physical separation and the independence provided by electrical isolation. This ITAAC verifies the independence of Class 1E current-carrying circuits by physical separation. An ITAAC inspection is performed of physical separation of the NMS Class 1E current-carrying circuits. The physical separation ITAAC inspection results verify that the following physical separation criteria are met:					
		i. Physical separation between redundant divisions of the NMS Class 1E I&C current-carrying circuits is provided by a minimum separation distance, or by barriers (where the minimum separation distances cannot be maintained), or by a combination of separation distance and barriers; and such physical separation satisfies the criteria of RG 1.75. The configuration of each as-built barrier agrees with its associated as-built drawing.					
		ii. Physical separation between the NMS Class 1E I&C current-carrying circuits and non-Class 1E I&C current-carrying circuits is provided by a minimum separation distance, or by barriers (where the minimum separation distances cannot be maintained), or by a combination of separation distance and barriers. The configuration of each as-built barrier agrees with its associated as-built drawing.					

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Table 14.3-1: Module-Specific Structures, Systems, and Components Based Design Features and Inspections, Tests, Analyses, and Acceptance Criteria Cross Reference (Continued)

System	Discussion	DBA	Internal/External Hazard	Radiological	PRA & Severe Accident	FP
NMS	Sections 7.0.3.2, Safety-Related Systems, 7.1.2.2, Electrical Independence, and 7.1.2.4.1, Independence between Redundant Portions of a Safety System, discuss the independence of the NMS Class 1E I&C circuits per the criteria of RG, which endorses IEEE Std. 384-1992. Electrical isolation is provided between the redundant divisions of the NMS Class 1E I&C circuits, and between Class 1E I&C circuits and non-Class 1E I&C circuits by Class 1E isolation devices so a failure in an I&C circuit does not prevent safety-related function completion in a different Class 1E I&C circuit. An ITAAC inspection is performed to verify the following electrical isolation criteria are met: i. Class 1E electrical isolation devices that satisfy the criteria of RG 1.75 are installed between redundant divisions of the NM system Class 1E I&C circuits.	Х				
	ii. Class 1E electrical isolation devices that satisfy the criteria of RG 1.75 are installed between the NMS Class 1E I&C circuits and non-Class 1E I&C circuits.					
	Section 11.5.2.2.7, Containment Evacuation System, discusses the operation of the CES. For each high radiation signal listed in Tier 1 Table 2.7-1, the CES automatically aligns the components identified in Tier 1 Table 2.7-1 to the required positions identified in the table. In accordance with Table 14.2-41, a preoperational test demonstrates the CES automatically aligns the components identified in Tier 1 Table 2.7-1 to the required positions identified in the table upon initiation of a real or simulated CES high radiation			X		
		NMS Sections 7.0.3.2, Safety-Related Systems, 7.1.2.2, Electrical Independence, and 7.1.2.4.1, Independence between Redundant Portions of a Safety System, discuss the independence of the NMS Class 1E I&C circuits per the criteria of RG, which endorses IEEE Std. 384-1992. Electrical isolation is provided between the redundant divisions of the NMS Class 1E I&C circuits, and between Class 1E I&C circuits and non-Class 1E I&C circuits by Class 1E isolation devices so a failure in an I&C circuit does not prevent safety-related function completion in a different Class 1E I&C circuit. An ITAAC inspection is performed to verify the following electrical isolation criteria are met: i. Class 1E electrical isolation devices that satisfy the criteria of RG 1.75 are installed between redundant divisions of the NM system Class 1E I&C circuits. ii. Class 1E electrical isolation devices that satisfy the criteria of RG 1.75 are installed between the NMS Class 1E I&C circuits and non-Class 1E I&C circuits. Section 11.5.2.2.7, Containment Evacuation System, discusses the operation of the CES. For each high radiation signal listed in Tier 1 Table 2.7-1, the CES automatically aligns the components identified in Tier 1 Table 2.7-1 to the required positions identified in the table. In accordance with Table 14.2-41, a preoperational test demonstrates the CES automatically aligns the components identified in Tier 1 Table 2.7-1 to the required positions identified in	NMS Sections 7.0.3.2, Safety-Related Systems, 7.1.2.2, Electrical Independence, and 7.1.2.4.1, Independence between Redundant Portions of a Safety System, discuss the independence of the NMS Class 1E I&C circuits per the criteria of RG, which endorses IEEE Std. 384-1992. Electrical isolation is provided between the redundant divisions of the NMS Class 1E I&C circuits, and between Class 1E I&C circuits and non-Class 1E I&C circuits by Class 1E isolation devices so a failure in an I&C circuit does not prevent safety-related function completion in a different Class 1E I&C circuit. An ITAAC inspection is performed to verify the following electrical isolation criteria are met: i. Class 1E electrical isolation devices that satisfy the criteria of RG 1.75 are installed between redundant divisions of the NM system Class 1E I&C circuits. ii. Class 1E electrical isolation devices that satisfy the criteria of RG 1.75 are installed between the NMS Class 1E I&C circuits and non-Class 1E I&C circuits. Section 11.5.2.2.7, Containment Evacuation System, discusses the operation of the CES. For each high radiation signal listed in Tier 1 Table 2.7-1, the CES automatically aligns the components identified in Tier 1 Table 2.7-1 to the required positions identified in the table. In accordance with Table 14.2-41, a preoperational test demonstrates the CES automatically aligns the components identified in Tier 1 Table 2.7-1 to the required positions identified in the table upon initiation of a real or simulated CES high radiation	NMS Sections 7.0.3.2, Safety-Related Systems, 7.1.2.2, Electrical Independence, and 7.1.2.4.1, Independence between Redundant Portions of a Safety System, discuss the independence of the NMS Class 1E I&C circuits per the criteria of RG, which endorses IEEE Std. 384-1992. Electrical isolation is provided between the redundant divisions of the NMS Class 1E I&C circuits, and between Class 1E I&C circuits and non-Class 1E I&C circuits by Class 1E isolation devices so a failure in an I&C circuit does not prevent safety-related function completion in a different Class 1E I&C circuit. An ITAAC inspection is performed to verify the following electrical isolation criteria are met: i. Class 1E electrical isolation devices that satisfy the criteria of RG 1.75 are installed between redundant divisions of the NM system Class 1E I&C circuits. ii. Class 1E electrical isolation devices that satisfy the criteria of RG 1.75 are installed between the NMS Class 1E I&C circuits and non-Class 1E I&C circuits. Section 11.5.2.2.7, Containment Evacuation System, discusses the operation of the CES. For each high radiation signal listed in Tier 1 Table 2.7-1, the CES automatically aligns the components identified in Tier 1 Table 2.7-1 to the required positions identified in the table. In accordance with Table 14.2-41, a preoperational test demonstrates the CES automatically aligns the components identified in tier 1 Table 2.7-1 to the required positions identified in the table upon initiation of a real or simulated CES high radiation	NMS Sections 7.0.3.2, Safety-Related Systems, 7.1.2.2, Electrical Independence, and 7.1.2.4.1, Independence between Redundant Portions of a Safety System, discuss the independence of the NMS Class IE I&C circuits per the criteria of RG, which endorses IEEE Std. 384-1992. Electrical isolation is provided between the redundant divisions of the NMS Class 1E I&C circuits, and between Class 1E I&C circuits and non-Class 1E I&C circuits by Class 1E isolation devices so a failure in an I&C circuit does not prevent safety-related function completion in a different Class 1E I&C circuit. An ITAAC inspection is performed to verify the following electrical isolation criteria are met: i. Class 1E electrical isolation devices that satisfy the criteria of RG 1.75 are installed between redundant divisions of the NM system Class 1E I&C circuits. ii. Class 1E electrical isolation devices that satisfy the criteria of RG 1.75 are installed between the NMS Class 1E I&C circuits and non-Class 1E I&C circuits. Section 11.5.2.2.7, Containment Evacuation System, discusses the operation of the CES. For each high radiation signal listed in Tier 1 Table 2.7-1, the CES automatically aligns the components identified in Tier 1 Table 2.7-1 to the required positions identified in the table. In accordance with Table 14.2-41, a preoperational test demonstrates the CES automatically aligns the components identified in tier 1 Table 2.7-1 to the required positions identified in the table upon initiation of a real or simulated CES high radiation	NMS Sections 7.0.3.2, Safety-Related Systems, 7.1.2.2, Electrical Independence, and 7.1.2.4.1, Independence between Redundant Portions of a Safety System, discuss the independence of the NMS Class 1E I&C circuits per the criteria of RG, which endorses IEEE Std. 384-1992. Electrical isolation is provided between the redundant divisions of the NMS Class 1E I&C circuits, and between Class 1E I&C circuits and non-Class 1E I&C circuits by Class 1E isolation devices so a failure in an I&C circuit does not prevent safety-related function completion in a different Class 1E I&C circuit. An ITAAC inspection is performed to verify the following electrical isolation criteria are met: i. Class 1E electrical isolation devices that satisfy the criteria of RG 1.75 are installed between redundant divisions of the NM system Class 1E I&C circuits. ii. Class 1E electrical isolation devices that satisfy the criteria of RG 1.75 are installed between the NMS Class 1E I&C circuits and non-Class 1E I&C circuits. Section 11.5.2.2.7, Containment Evacuation System, discusses the operation of the CES. For each high radiation signal listed in Tier 1 Table 2.7-1, the CES automatically aligns the components identified in Tier 1 Table 2.7-1 to the required positions identified in the table. In accordance with Table 14.2-41, a preoperational test demonstrates the CES automatically aligns the components identified in the table upon initiation of a real or simulated CES high radiation

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Table 14.3-1: Module-Specific Structures, Systems, and Components Based Design Features and Inspections, Tests, Analyses, and Acceptance Criteria Cross Reference (Continued)

ITAAC No.	System	Discussion	DBA	Internal/External Hazard	Radiological	PRA & Severe Accident	FP
02.07.02		Section 11.5.2.2.11, Chemical and Volume Control System, discusses the operation of the CVCS. For each high radiation signal listed in Tier 1 Table 2.7-1, the CVCS automatically aligns the components identified in Tier 1 Table 2.7-1 to the required positions identified in the table.			Х		
		In accordance with Table 14.2-38, a preoperational test demonstrates the CVCS automatically aligns the components identified in Tier 1 Table 2.7-1 to the required positions identified in the table upon initiation of a real or simulated CVCS high radiation signal from CVC-RT-3016.					
02.07.03		Section 11.5.2.2.14, Auxiliary Boiler System, discusses the operation of the auxiliary boiler system (ABS) and the CVCS. For each high radiation signal listed in Tier 1 Table 2.7-1, the CVCS automatically aligns the components identified in Tier 1 Table 2.7-1 to the required positions identified in the table.			х		
		In accordance with Table 14.2-38, a preoperational test demonstrates the CVCS automatically aligns the components identified in Tier 1 Table 2.7-1 to the required positions identified in the table upon initiation of a real or simulated ABS high radiation signal from 6A-AB-RT-0142.					
02.07.04		Section 11.5.2.2.14, Auxiliary Boiler System, discusses the operation of the ABS and the CVCS. For each high radiation signal listed in Tier 1 Table 2.7-1, the CVCS automatically aligns the components identified in Tier 1 Table 2.7-1 to the required positions identified in the table.			Х		
		In accordance with Table 14.2-38, a preoperational test demonstrates the CVCS automatically aligns the components identified in Tier 1 Table 2.7-1 to the required positions identified in the table upon initiation of a real or simulated ABS high radiation signal from 6B-AB-RT-0141.					

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Table 14.3-1: Module-Specific Structures, Systems, and Components Based Design Features and Inspections, Tests, Analyses, and Acceptance Criteria Cross Reference (Continued)

ITAAC No.	System	Discussion	DBA	Internal/External Hazard	Radiological	PRA & Severe Accident	FP
02.08.01	EQ	Section 3.10, Seismic and Dynamic Qualification of Mechanical and Electrical Equipment, presents information to demonstrate that the Seismic Category I equipment, including its associated supports and anchorages, is qualified by type test, analysis, or a combination of type test and analysis to perform its safety function under the design basis seismic loads during and after an SSE. The qualification method employed for the Seismic Category I equipment is the same as the qualification method described for that type of equipment in Section 3.10. This method conforms to IEEE-344-2004 and ASME QME-1-2007 (or later editions), as accepted by the NRC staff in RG 1.100 Revision 3 (or later revision), with specific revision years and numbers as presented in Section 3.10.	X				
		The ITAAC verifies that: (1) a seismic qualification record form exists for each Seismic Category I component type, and (2) the seismic qualification record form concludes that the Seismic Category I equipment listed in Tier 1 Table 2.8-1, including its associated supports and anchorages, performs its function under the seismic design basis load conditions specified in the seismic qualification record form.					
		After installation in the plant, an ITAAC inspection is performed to verify that the Seismic Category I equipment listed in Tier 1 Table 2.8-1, including its associated supports and anchorages, is installed in its design location in a Seismic Category I structure in a configuration bounded by the seismic qualification record form.					

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Table 14.3-1: Module-Specific Structures, Systems, and Components Based Design Features and Inspections, Tests, Analyses, and Acceptance Criteria Cross Reference (Continued)

ITAAC No.	System	Discussion	DBA	Internal/External Hazard	Radiological	PRA & Severe Accident	FP
02.08.02	EQ	Section 3.10, Seismic and Dynamic Qualification of Mechanical and Electrical Equipment, presents information to demonstrate that the Seismic Category I equipment, including its associated supports and anchorages, is qualified by type test, analysis, or a combination of type test and analysis to perform its safety function under the design basis seismic loads during and after an SSE. The qualification method employed for the Seismic Category I equipment is the same as the qualification method described for that type of equipment in Section 3.10. This method conforms to IEEE-344-2004 and ASME QME-1-2007 (or later editions), as accepted by the NRC staff in RG 1.100 Revision 3 (or later revision), with specific revision years and numbers as presented in Section 3.10.	X				
		for each Seismic Category I component type, and (2) the seismic qualification record form concludes that the Seismic Category I equipment listed in Tier 1 Table 2.8-1, including its associated supports and anchorages, performs its function under the seismic design basis load conditions specified in the seismic qualification record form.					
		After installation in the plant, an ITAAC inspection is performed to verify that the Seismic Category I equipment listed in Tier 1 Table 2.8-1, including its associated supports and anchorages, is installed in its design location in a Seismic Category I structure in a configuration bounded by the seismic qualification record form.					

Table 14.3-1: Module-Specific Structures, Systems, and Components Based Design Features and Inspections, Tests, Analyses, and Acceptance Criteria Cross Reference (Continued)

ITAAC No.	System	Discussion	DBA	Internal/External Hazard	Radiological	PRA & Severe Accident	FP
02.08.03	EQ	Section 3.11 presents information to demonstrate that the non-metallic parts, materials, and lubricants used in safety-related mechanical equipment located in a harsh environment are qualified using a type test or a combination of type test and analysis to perform their safety-related function up to the end of their qualified life in design basis harsh environmental conditions experienced during normal operations, anticipated operational occurrences, DBAs, and post-accident conditions. Environmental conditions include both internal service conditions and external environmental conditions for the non-metallic parts, materials, and lubricant. The qualification method employed for the equipment is the same as the qualification method described for that type of equipment in Section 3.11. The ITAAC verifies that: (1) an equipment qualification record form or ASME QME-1 report exists for the non-metallic parts, materials, and lubricants used in safety-related mechanical equipment designated for a harsh environment, and (2) the qualification record form concludes that the non-metallic parts, materials, and lubricants used in safety-related mechanical equipment listed in Tier 1 Table 2.8-1 perform their intended function up to the end of its qualified life under the design basis environmental conditions (both internal service conditions and external environmental conditions) specified in the qualification record form.	X				

Table 14.3-1: Module-Specific Structures, Systems, and Components Based Design Features and Inspections, Tests, Analyses, and Acceptance Criteria Cross Reference (Continued)

ITAAC No.	System	Discussion	DBA	Internal/External Hazard	Radiological	PRA & Severe Accident	FP
02.08.04	EQ	Section 3.11, Environmental Qualification of Mechanical and Electrical Equipment, and Appendix 3C, Methodology for Environmental Qualification of Electrical and Mechanical Equipment, presents information to demonstrate that the Class 1E computer-based I&C systems located in a mild environment is qualified by type test or a combination of type test and analysis to perform its safety-related function under the design basis mild environmental conditions. The qualification method employed for the equipment is the same as the qualification method described for that type of equipment in Section 3.11 and Appendix 3C. This method conforms to IEEE-323-2003 (or later editions), as accepted by the NRC staff in RG 1.209, Revision 0 (or later revision), with specific revision years and numbers as presented in Section 3.10. The ITAAC verifies that: (1) an equipment qualification record form exists for the Class 1E computer-based I&C systems listed in Tier 1 Table 2.8-1, and (2) the equipment qualification record form concludes that the Class 1E computer-based I&C systems performs its safety-related function under the design basis mild environmental conditions specified in Section 3.11 and Appendix 3C and the equipment qualification record form. After installation in the plant, an ITAAC inspection is performed to verify that the Class 1E computer-based I&C systems listed in Tier 1 Table 2.8-1 is installed in its design location in a configuration bounded by its equipment qualification record form.	X				

Table 14.3-1: Module-Specific Structures, Systems, and Components Based Design Features and Inspections, Tests, Analyses, and Acceptance Criteria Cross Reference (Continued)

ITAAC No.	System	Discussion	DBA	Internal/External Hazard	Radiological	PRA & Severe Accident	FP
02.08.05	EQ	Section 3.11, Environmental Qualification of Mechanical and Electrical Equipment, presents information to demonstrate that the Class 1E digital equipment is qualified using a type test, analysis, or a combination of type test and analysis to perform its safety-related function when subjected to electromagnetic interference, radio frequency interference, and electrical surges that would exist before, during, and following a DBA. The qualification method employed for Class 1E digital equipment is the same as the qualification method described for that type of equipment in Section 3.11. The ITAAC verifies that: (1) an equipment qualification record form exists for the Class 1E digital equipment listed in Tier 1 Table 2.8-1, and (2) the equipment qualification record form concludes that the Class 1E digital equipment withstands the design basis electromagnetic interference, radio frequency interference, and	X				
02.08.06	EQ	electrical surges that would exist before, during, and following a DBA without loss of safety-related function. Section 3.9.6.1, Functional Design and Qualification of Pumps, Valves, and Dynamic Restraints, and Section 3.10.2, Methods and Procedures for Qualifying Mechanical and Electrical Equipment and Instrumentation, discuss that the functional qualification of safety-related valves is performed in accordance with ASME QME-1-2007(or later edition), as accepted in RG 1.100 Revision 3 (or later	Х				
		revision), with specific revision years and numbers as presented in Section 3.9.6.1. The qualification method employed for the valves agrees with the qualification method described in Section 3.10.2. The ITAAC verifies that: (1) A Functional Qualification Report exists for the safety-related valves listed in Tier 1 Table 2.8-1, and (2) the Functional Qualification Report concludes that safety-related valves are capable of performing their safety-related function under the full range of fluid flow, differential pressure, electrical conditions, and temperature conditions up to and including DBA					

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Table 14.3-1: Module-Specific Structures, Systems, and Components Based Design Features and Inspections, Tests, Analyses, and Acceptance Criteria Cross Reference (Continued)

ITAAC No.	System	Discussion	DBA	Internal/External Hazard	Radiological	PRA & Severe Accident	FP
02.08.07	EQ	Section 3.9.3.2, Design and Installation of Pressure Relief Devices, discusses that relief valves provide overpressure protection in accordance with the ASME Code Section III. The ITAAC verifies that: (1) the test for each relief valve listed in Tier 1 Table 2.8-1 meets the set pressure, capacity, and overpressure design requirements; and (2) each relief valve listed in Tier 1 Table 2.8-1 is provided with an ASME Code Certification Mark that	Х				
02.08.08	EQ	identifies the valve's set pressure, capacity, and overpressure. Section 5.4.2, Decay Heat Removal System, discusses that the DHRS passive condensers provide the safety-related function of transferring their design heat load from the DHRS during shutdown. After manufacture of the DHRS passive condensers, a type test or a combination of type test and analysis is performed to validate that the DHRS passive condensers are capable of meeting the specified heat transfer performance requirements. Section 5.4.2 discusses the design heat transfer capability of the DHR system passive condensers. The ITAAC verifies that the safety-related passive condensers listed in Tier 1 Table 2.8-1 have a heat removal capacity sufficient to transfer their design heat load.	Х				

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Table 14.3-2: Shared/Common Structures, Systems, and Components and Non-Structures, Systems, and components Based Design Features and Inspections, Tests, Analyses, and Acceptance Criteria Cross Reference

ITAAC No.	System	Discussion	DBA	Internal/External Hazard	Radiological	PRA & Severe Accident	FP
03.01.01	CRH	Testing is performed on the CRE in accordance with RG 1.197, "Demonstrating Control Room Envelope Integrity at Nuclear Power Reactors," Revision 0, to demonstrate that air exfiltration from the CRE is controlled. RG 1.197 allows two options for CRE testing; either integrated testing (tracer gas testing) or component testing. Section 6.4 Control Room Habitability, describes the testing requirements for the CRE habitability program. Section 6.4 provides the maximum air exfiltration allowed from the CRE. In accordance with Table 14.2-18, a preoperational test using the tracer gas test method demonstrates that the air exfiltration from the CRE does not exceed the assumed unfiltered leakage rate provided in Table 6.4-1: Control Room Habitability System Design Parameters. Tracer gas testing in accordance with ASTM E741 will be performed to measure the unfiltered in-leakage into the CRE with the control room habitability system (CRHS) operating.			X		
03.01.02	CRH	The CRHS valves are tested by remote operation to demonstrate the capability to perform their function to transfer open and transfer closed under preoperational temperature, differential pressure, and flow conditions. In accordance with Table 14.2-18, a preoperational test demonstrates that each CRHS valve listed in Tier 1 Table 3.1-1 strokes fully open and fully closed by remote operation under preoperational test conditions. Preoperational test conditions are established that approximate design-basis temperature, differential pressure, and flow conditions to the extent practicable, consistent with preoperational test limitations.			X		

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Table 14.3-2: Shared/Common Structures, Systems, and Components and Non-Structures, Systems, and components Based Design Features and Inspections, Tests, Analyses, and Acceptance Criteria Cross Reference (Continued)

System	Discussion	DBA	Internal/External Hazard	Radiological	PRA & Severe Accident	FP
CRH	The CRHS solenoid-operated valves are tested to demonstrate the capability to perform their function to fail open on loss of motive power under preoperational temperature, differential pressure, and flow conditions.			X		
	In accordance with Table 14.2-18 a preoperational test demonstrates that each CRHS solenoid-operated valve listed in Tier 1 Table 3.1-1 repositions to the open position on loss of motive power (electric power to the valve actuating solenoid(s) is lost, or pneumatic pressure to the valve(s) is lost).					
	Preoperational test conditions are established that approximate design basis temperature, differential pressure, and flow conditions to the extent practicable, consistent with preoperational test limitations.					
CRH	Section 6.4.4, Design Evaluation, discusses the thermal mass of the CRB and its contents limit the temperature increase as shown in Table 6.4-3 within the CRE within an acceptable range for the first 72 hours following a DBA.			X		
	An analysis confirms that the CRE bulk average air temperature is acceptable on a loss of active cooling for the first 72 hours following a DBA.					
CRH	Section 6.4.3.2, Off-Normal Operation, discusses the operation of the CRHS, which maintains a positive pressure in the MCR relative to the adjacent areas. Table 6.4-1: Control Room Habitability System Design Parameters provides the required positive pressure in the MCR relative to the adjacent areas. In accordance with Table 14.2-18, a preoperational test demonstrates that the CRHS maintains a positive pressure of greater than or equal to 1/8 inches water gauge in the MCR relative to adjacent areas, while			X		
	CRH	CRH The CRHS solenoid-operated valves are tested to demonstrate the capability to perform their function to fail open on loss of motive power under preoperational temperature, differential pressure, and flow conditions. In accordance with Table 14.2-18 a preoperational test demonstrates that each CRHS solenoid-operated valve listed in Tier 1 Table 3.1-1 repositions to the open position on loss of motive power (electric power to the valve actuating solenoid(s) is lost, or pneumatic pressure to the valve(s) is lost). Preoperational test conditions are established that approximate design basis temperature, differential pressure, and flow conditions to the extent practicable, consistent with preoperational test limitations. CRH Section 6.4.4, Design Evaluation, discusses the thermal mass of the CRB and its contents limit the temperature increase as shown in Table 6.4-3 within the CRE within an acceptable range for the first 72 hours following a DBA. An analysis confirms that the CRE bulk average air temperature is acceptable on a loss of active cooling for the first 72 hours following a DBA. CRH Section 6.4.3.2, Off-Normal Operation, discusses the operation of the CRHS, which maintains a positive pressure in the MCR relative to the adjacent areas. Table 6.4-1: Control Room Habitability System Design Parameters provides the required positive pressure in the MCR relative to the adjacent areas. In accordance with Table 14.2-18, a preoperational test demonstrates that the CRHS maintains a positive pressure of greater than or equal to 1/8 inches	CRH The CRHS solenoid-operated valves are tested to demonstrate the capability to perform their function to fail open on loss of motive power under preoperational temperature, differential pressure, and flow conditions. In accordance with Table 14.2-18 a preoperational test demonstrates that each CRHS solenoid-operated valve listed in Tier 1 Table 3.1-1 repositions to the open position on loss of motive power (electric power to the valve actuating solenoid(s) is lost, or pneumatic pressure to the valve(s) is lost). Preoperational test conditions are established that approximate design basis temperature, differential pressure, and flow conditions to the extent practicable, consistent with preoperational test limitations. CRH Section 6.4.4, Design Evaluation, discusses the thermal mass of the CRB and its contents limit the temperature increase as shown in Table 6.4-3 within the CRE within an acceptable range for the first 72 hours following a DBA. An analysis confirms that the CRE bulk average air temperature is acceptable on a loss of active cooling for the first 72 hours following a DBA. CRH Section 6.4.3.2, Off-Normal Operation, discusses the operation of the CRHS, which maintains a positive pressure in the MCR relative to the adjacent areas. Table 6.4-1: Control Room Habitability System Design Parameters provides the required positive pressure in the MCR relative to the adjacent areas. In accordance with Table 14.2-18, a preoperational test demonstrates that the CRHS maintains a positive pressure of greater than or equal to 1/8 inches water gauge in the MCR relative to adjacent areas, while	CRH The CRHS solenoid-operated valves are tested to demonstrate the capability to perform their function to fail open on loss of motive power under preoperational temperature, differential pressure, and flow conditions. In accordance with Table 14.2-18 a preoperational test demonstrates that each CRHS solenoid-operated valve listed in Tier 1 Table 3.1-1 repositions to the open position on loss of motive power (electric power to the valve actuating solenoid(s) is lost, or pneumatic pressure to the valve(s) is lost). Preoperational test conditions are established that approximate design basis temperature, differential pressure, and flow conditions to the extent practicable, consistent with preoperational test limitations. CRH Section 6.4.4, Design Evaluation, discusses the thermal mass of the CRB and its contents limit the temperature increase as shown in Table 6.4-3 within the CRE within an acceptable range for the first 72 hours following a DBA. An analysis confirms that the CRE bulk average air temperature is acceptable on a loss of active cooling for the first 72 hours following a DBA. CRH Section 6.4.3.2, Off-Normal Operation, discusses the operation of the CRHS, which maintains a positive pressure in the MCR relative to the adjacent areas. Table 6.4-1: Control Room Habitability System Design Parameters provides the required positive pressure in the MCR relative to the adjacent areas. In accordance with Table 14.2-18, a preoperational test demonstrates that the CRHS maintains a positive pressure of greater than or equal to 1/8 inches water gauge in the MCR relative to adjacent areas, while	CRH The CRHS solenoid-operated valves are tested to demonstrate the capability to perform their function to fail open on loss of motive power under preoperational temperature, differential pressure, and flow conditions. In accordance with Table 14.2-18 a preoperational test demonstrates that each CRHS solenoid-operated valve listed in Tier 1 Table 3.1-1 repositions to the open position on loss of motive power (electric power to the valve actuating solenoid(s) is lost, or pneumatic pressure to the valve(s) is lost). Preoperational test conditions are established that approximate design basis temperature, differential pressure, and flow conditions to the extent practicable, consistent with preoperational test limitations. CRH Section 6.4.4, Design Evaluation, discusses the thermal mass of the CRB and its contents limit the temperature increase as shown in Table 6.4-3 within the CRE within an acceptable range for the first 72 hours following a DBA. An analysis confirms that the CRE bulk average air temperature is acceptable on a loss of active cooling for the first 72 hours following a DBA. CRH Section 6.4.3.2, Off-Normal Operation, discusses the operation of the CRHS, which maintains a positive pressure in the MCR relative to the adjacent areas. Table 6.4-1: Control Room Habitability System Design Parameters provides the required positive pressure in the MCR relative to the adjacent areas. In accordance with Table 14.2-18, a preoperational test demonstrates that the CRHS maintains a positive pressure of greater than or equal to 1/8 inches water gauge in the MCR relative to adjacent areas, while	CRH The CRHS solenoid-operated valves are tested to demonstrate the capability to perform their function to fail open on loss of motive power under preoperational temperature, differential pressure, and flow conditions. In accordance with Table 14.2-18 a preoperational test demonstrates that each CRHS solenoid-operated valve listed in Tier 1 Table 3.1-1 repositions to the open position on loss of motive power (electric power to the valve actuating solenoid(s) is lost, or pneumatic pressure to the valve(s) is lost). Preoperational test conditions are established that approximate design basis temperature, differential pressure, and flow conditions to the extent practicable, consistent with preoperational test limitations. CRH Section 6.4.4, Design Evaluation, discusses the thermal mass of the CRB and its contents limit the temperature increase as shown in Table 6.4-3 within the CRE within an acceptable range for the first 72 hours following a DBA. An analysis confirms that the CRE bulk average air temperature is acceptable on a loss of active cooling for the first 72 hours following a DBA. CRH Section 6.4.3.2, Off-Normal Operation, discusses the operation of the CRHS, which maintains a positive pressure in the MCR relative to the adjacent areas. Table 6.4-1: Control Room Habitability System Design Parameters provides the required positive pressure of greater than or equal to 1/8 inches water gauge in the MCR relative to adjacent areas, while

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Table 14.3-2: Shared/Common Structures, Systems, and Components and Non-Structures, Systems, and components Based Design Features and Inspections, Tests, Analyses, and Acceptance Criteria Cross Reference (Continued)

ITAAC No.	System	Discussion	DBA	Internal/External Hazard	Radiological	PRA & Severe Accident	FP
03.02.01	CRV	The normal control room HVAC system (CRVS) control room envelope isolation dampers are tested to demonstrate the capability to perform their function to fail to the closed position on loss of motive power. In accordance with Table 14.2-19, a preoperational test demonstrates that each CRVS air-operated CRE isolation damper listed in Tier 1 Table 3.2-1 repositions to the closed position on loss of motive power (electric power to the valve actuating solenoid is lost, or pneumatic pressure to the damper is lost). Preoperational test conditions are established that approximate design differential pressure conditions to the extent practical, consistent with preoperational test limitations. A manual signal, actual automatic signal, or simulated automatic signal may be used to operate the valves because the control logic of the valves is not being verified by this ITAAC.			X		X
03.02.02	CRV	Section 9.4.1.2, System Description, discusses the operation of the CRVS, which maintains a positive pressure in the CRB relative to the outside environment. This is consistent with the requirements of 10 CFR Part 20, Subparts E and H and 10 CFR Part 50, Appendix I. In accordance with Table 14.2-19 a preoperational test demonstrates that the CRVS will maintain a positive pressure of greater than or equal to 1/8 inches water gauge in the CRB relative to the outside environment, while operating in a normal operating alignment.			Х		

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Table 14.3-2: Shared/Common Structures, Systems, and Components and Non-Structures, Systems, and components Based Design Features and Inspections, Tests, Analyses, and Acceptance Criteria Cross Reference (Continued)

ITAAC No.	System	Discussion	DBA	Internal/External Hazard	Radiological	PRA & Severe Accident	FP
03.02.03	CRV	Section 9.4.1.2.2.1, Normal Operation, provides a discussion of how the CRVS maintains the hydrogen concentration levels in the CRB battery rooms containing batteries below one percent by volume.			X		
	In accordance with Table 14.2-19, a preoperational test demonstrates that the airflow capability of the CRVS maintains the hydrogen concentration levels in the CRB battery rooms containing batteries below one percent by volume.						
03.03.01	RBV	Section 9.4.2.2.2.1, Normal Operation, and Section 9.4.2.2.2.2, Off-normal Operation, discuss the operation of the Reactor Building HVAC system (RBVS) which maintains a negative pressure in the RXB relative to the outside environment. This is consistent with the requirements of 10 CFR Part 20, Subparts E and H and 10 CFR Part 50, Appendix I. In accordance with Table 14.2-20, a preoperational test demonstrates that the RBVS will maintain a negative pressure in the RXB relative to the outside environment,			х		
03.03.02	RBV	while operating in a normal operating alignment. Section 9.4.2.2.2.1, Normal Operation, and Section 9.4.2.2.2.2, Off-normal Operation, discuss the operation of the RBVS which maintains a negative pressure in the RWB relative to the outside environment. This is consistent with the requirements of 10 CFR Part 20, Subparts E and H and 10 CFR Part 50, Appendix I. In accordance with Table 14.2-20, a preoperational test demonstrates that the RBVS will maintain a negative pressure in the RWB relative to the outside environment,			X		

Table 14.3-2: Shared/Common Structures, Systems, and Components and Non-Structures, Systems, and components Based Design Features and Inspections, Tests, Analyses, and Acceptance Criteria Cross Reference (Continued)

ITAAC No.	System	Discussion	DBA	Internal/External Hazard	Radiological	PRA & Severe Accident	FP
03.03.03	RBV	Section 9.4.2.2.2.1, Normal Operation, provides a discussion of how the RBVS maintains the hydrogen concentration levels in the RXB battery rooms containing batteries below one percent by volume. In accordance with Table 14.2-20, a preoperational test demonstrates that the airflow capability of the RBVS maintains the hydrogen concentration levels in the RXB battery rooms containing batteries below one percent by volume.			X		
03.04.01	FHE	Section 9.1.4, Light-Load Handling System (Related to Refueling), describes that the fuel handling machine (FHM) is classified as a Type I crane as defined by the ASME NOG-1, "Rules for Construction of Overhead and Gantry Cranes (Top Running Bridge, Multiple Girder)." An ITAAC inspection is performed of the FHM main and auxiliary hoists machinery arrangement to verify the	X				
		existence of the following single-failure proof features: (a) nonredundant structural components (bridge, trolley, wire rope drum, and hook) are designed to appropriate standards, constructed from base material demonstrated to meet appropriate material properties, and, (b) redundant design features to stop and hold the load following:					
		 specified component failures (e.g., wire rope, drive train, and control system) operator errors (e.g., two-blocking and overload) 					
		This ITAAC inspection may be performed any time after manufacture of the FHM (at the factory or later).					

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Table 14.3-2: Shared/Common Structures, Systems, and Components and Non-Structures, Systems, and components Based Design Features and Inspections, Tests, Analyses, and Acceptance Criteria Cross Reference (Continued)

ITAAC No.	System	Discussion	DBA	Internal/External Hazard	Radiological	PRA & Severe Accident	FP
03.04.02	FHE	Section 9.1.4, Light-Load Handling System (Related to Refueling), describes that the FHM is classified as a Type I crane as defined by the ASME NOG-1 Code, Rules for Construction of Overhead and Gantry Cranes (Top Running Bridge, Multiple Girder). The FHM main hoist is tested in accordance with the applicable requirements of NOG-1. An FAT demonstrates that the single failure proof FHM main hoist is rated load tested at 125% (+5%, -0%) of the manufacturer's rating.	Х				
03.04.03	FHE	Section 9.1.4, Light-Load Handling System (Related to Refueling), describes that the FHM is classified as a Type I crane as defined by the ASME NOG-1 Code, Rules for Construction of Overhead and Gantry Cranes (Top Running Bridge, Multiple Girder). In accordance with ASME NOG-1 paragraph 7422, the FHM auxiliary hoist is full load tested at a maximum of 100% of the hoist manufacturer's rating. After the full load test is completed, and prior to use of the crane to handle loads, the FHM auxiliary hoist is rated load tested at 125% (+5%, -0%) of the manufacturer's rating in accordance with ASME NOG-1 paragraph 7423. An FAT demonstrates that the single failure proof FHM auxiliary hoist is rated load tested at 125% (+5%, -0%) of the					
03.04.04	FHE	manufacturer's rating. Section 9.1.4, Light-Load Handling System (Related to Refueling), describes that the single failure proof FHM is classified as a Type I crane as defined by the ASME NOG-1 Code, Rules for Construction of Overhead and Gantry Cranes (Top Running Bridge, Multiple Girder). An ITAAC inspection is performed to verify that the ASME Type I as-built FHM welds are nondestructively examined in accordance with the standards of ASME NOG-1 paragraph 4251.4 and the FHM purchase specification.	х				
		This ITAAC inspection may be performed any time after manufacture of the single failure-proof FHM (at the factory or later).					

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Table 14.3-2: Shared/Common Structures, Systems, and Components and Non-Structures, Systems, and components Based Design Features and Inspections, Tests, Analyses, and Acceptance Criteria Cross Reference (Continued)

ITAAC No.	System	Discussion	DBA	Internal/External Hazard	Radiological	PRA & Severe Accident	FP
03.04.05	FHE	Section 9.1.4, Light-Load Handling System (Related to Refueling), provide descriptions of how the limit switches on the FHM gripper mast limits travel and that the fuel handling equipment (FHE) has provisions to limit maximum lift height of a fuel assembly to maintain a water inventory of 10 feet above the top of the fuel assembly for personnel shielding. In accordance with Table 14.2-51, a preoperational test demonstrates that the FHM maintains at least 10 feet of water above the top of the fuel assembly when lifted to its maximum height with the pool level at the lower limit of the normal operating low water level.					
03.05.01	SFS	The ASME Code Section III requires that documentary evidence be available at the construction or installation site before use or installation to ensure that ASME Code Class NF components conform to the requirements of the Code. The Fuel Storage system ASME Code Class NF components require a Data Report as specified by NCA-1210. The Data Report is prepared by the certificate holder or owner and signed by the certificate holder or owner and the Inspector as specified by NCA-8410. The type of individual Data Report Forms necessary to record the required Code Data is specified in Table NCA-8100-1.					
		An ITAAC inspection is performed of the Data Reports for Fuel Storage system ASME Code Class NF as-built fuel storage racks that are described in Section 9.1.2 to (1) ensure that the appropriate Data Reports have been provided as specified in Table NCA-8100-1 and (2) ensure that the certificate holder or owner and the authorized nuclear inspector have signed the Data Reports, and (3) verify that the requirements of ASME Code Section III are met.					

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Table 14.3-2: Shared/Common Structures, Systems, and Components and Non-Structures, Systems, and components Based Design Features and Inspections, Tests, Analyses, and Acceptance Criteria Cross Reference (Continued)

ITAAC No.	System	Discussion	DBA	Internal/External Hazard	Radiological	PRA & Severe Accident	FP
03.05.02	SFS	Section 9.1.1, Criticality Safety of Fresh and Spent Fuel Storage and Handling, discusses the criticality analysis of the fuel storage racks.	Х				
		An ITAAC inspection is performed to verify that the as-built fuel storage racks, including any neutron absorbers, conform to the design values for materials and dimensions and their tolerances, as presented in the approved criticality analysis.					
03.06.01	UHS	As required by ASME Code Section III NCA-1210, each ASME Code Class 1, 2 and 3 component (including piping systems) of a nuclear power plant requires a Design Report in accordance with NCA-3550. NCA-3551.1 requires that the drawings used for construction be in agreement with the Design Report before it is certified and be identified and described in the Design Report. It is the responsibility of the N certificate holder to furnish a Design Report for each component and support, except as provided in NCA-3551.2 and NCA-3551.3. NCA-3551.1 also requires that the Design Report be certified by a registered professional engineer when it is for Class 1 components and supports, Class CS core support structures, Class MC vessels and supports, Class 2 vessels designed to NC-3200 (NC-3131.1), or Class 2 or Class 3 components designed to service loadings greater than design loadings. NCA-3554 requires that any modification of any document used for construction, from the corresponding document used for design analysis, shall be reconciled with the Design Report. An ITAAC inspection is performed of the ultimate heat sink (UHS) ASME Code Class 3 as-built piping system Design Report to verify that the e requirements of ASME Code Section III are met.				X	

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Table 14.3-2: Shared/Common Structures, Systems, and Components and Non-Structures, Systems, and components Based Design Features and Inspections, Tests, Analyses, and Acceptance Criteria Cross Reference (Continued)

ITAAC No.	System	Discussion	DBA	Internal/External Hazard	Radiological	PRA & Severe Accident	FP
03.06.02	UHS	Section 9.1.2.2.2, Spent Fuel Storage, Section 9.1.3.2.1, Spent Fuel Pool Cooling System, and Section 9.1.3.2.2, Reactor Pool Cooling System, discuss spent fuel pool (SFP) and reactor pool cooling. No piping, openings, doors, or penetrations through the SFP, refueling pool, reactor pool and dry dock walls are installed below the minimum water level required for shielding, spent fuel cooling, DHRS cooling, or containment cooling. Gates, openings, or drains, permanently connected mechanical or hydraulic systems (piping), and other features that by maloperation or failure could reduce the coolant inventory to unsafe levels are not included in the design. An ITAAC inspection is performed to verify that the SFP, refueling pool, reactor pool and dry dock include no drains, piping or other systems below 80 ft building elevation (55 ft pool level as measured from the bottom of the SFP and					
03.07.01	FP	reactor pool). This inspection is performed by physical measurements in the as-built SFP and reactor pool. Section 9.5.1.2.6, Fire Protection Design Features, discusses how the fire protection system (FPS) meets the guidance provided by RG 1.189 and applicable NFPA standards. Two separate dedicated 100 percent capacity freshwater storage tanks are provided. An ITAAC inspection is performed to verify that the					Х
		minimum usable water volume of each firewater storage tank is greater than or equal to 300,000 gallons. If the storage tanks are also used as backup water sources for other non-fire emergencies, the ITAAC inspection verifies that the non-fire emergencies cannot drain the tank below the minimum dedicated useable water volume of 300,000 gallons required for firefighting.					

Table 14.3-2: Shared/Common Structures, Systems, and Components and Non-Structures, Systems, and components Based Design Features and Inspections, Tests, Analyses, and Acceptance Criteria Cross Reference (Continued)

ITAAC No.	System	Discussion	DBA	Internal/External Hazard	Radiological	PRA & Severe Accident	FP
03.07.02	FP	Section 9.5.1, Fire Protection Program, discusses how the capacity of each FPS pump is adequate to supply the total flow demand at the pressure required at the pump discharge. Section 9.5.1 provides the design flow of the fire pumps. i. An analysis confirms that the as-built fire pump for fire protection shall be selected so that the greatest single demand for any FPS connected to the pump is less than or equal to 150 percent of the rated capacity (flow) of the pump. ii. In accordance with Table 14.2-25, a preoperational test demonstrates that each fire pump delivers the design flow to the FPS while operating in the fire-fighting alignment.					X

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Table 14.3-2: Shared/Common Structures, Systems, and Components and Non-Structures, Systems, and components Based Design Features and Inspections, Tests, Analyses, and Acceptance Criteria Cross Reference (Continued)

ITAAC No.	System	Discussion	DBA	Internal/External Hazard	Radiological	PRA & Severe Accident	FP
03.07.03	FP	Section 9.5.1 discusses that (a) safe-shutdown can be achieved assuming that all equipment in any one fire area (except for the MCR and containment) is rendered inoperable by fire and that reentry into the fire area for repairs and operator actions is not possible, (b) that smoke, hot gases, or fire suppressant cannot migrate from the affected fire area into other fire areas to the extent that they could adversely affect safe shutdown capabilities, including operator actions, and (c) an independent alternative shutdown capability that is physically and electrically independent of the MCR exists. A safe shutdown analysis of the as-built plant will be performed, including a post-fire safe shutdown circuit analysis performed in accordance with RG 1.189 and NEI 00-01for all possible fire-induced failures that could affect the safe shutdown success path, including multiple spurious actuations.					X
		 The safe shutdown analysis will verify that: safe shutdown can be achieved assuming that all equipment in any one fire area (except for the MCR and containment) is rendered inoperable by fire and that reentry into the fire area for repairs and operator actions is not possible. smoke, hot gases, or fire suppressant cannot migrate from the affected fire area into other fire areas to the extent that they could adversely affect safe shutdown capabilities, including operator actions. an independent alternative shutdown capability that is physically and electrically independent of the MCR exists. 					

Table 14.3-2: Shared/Common Structures, Systems, and Components and Non-Structures, Systems, and components Based Design Features and Inspections, Tests, Analyses, and Acceptance Criteria Cross Reference (Continued)

ITAAC No.	System	Discussion	DBA	Internal/External Hazard	Radiological	PRA & Severe Accident	FP
03.07.04	FP	Appendix 9A, Fire Hazards Analysis, discusses the methodology and presents the fire hazards analysis (FHA) for each fire area. The FHA must reflect the as-built configuration of the plant. The FHA is an analysis of the fire hazards, including combustible loading and ignition sources, and analysis of the fire protection features required to mitigate each postulated fire.					Х
		An FHA of the as-built plant will be performed in accordance with RG 1.189, as described in Appendix 9A. The FHA will verify (1) combustible loads and ignition sources are accounted for, and (2) fire protection features are suitable for the hazards they are intended for.					
03.08.01	PL	Section 9.5.3, Lighting Systems, discusses the plant lighting system (PLS) which provides normal illumination of the operator workstations and SDIS panels in the MCR and RSS. The PLS is capable of delivering at least 100 foot-candles of illumination to the MCR seated operator stations and 50 foot-candles of illumination to the MCR primary operating areas and remote and auxiliary operating panels. Lower illumination levels may be used within these areas to ensure more favorable visual conditions, or for areas where critical tasks are not performed. In accordance with Table 14.2-60, a preoperational test demonstrates that the PLS provides at least: i. 100 foot-candles illumination at the MCR operator				X	
		workstations and at least 50 foot-candles at the MCR auxiliary panels. ii. 100 foot-candles illumination at the RSS operator workstations.					

Table 14.3-2: Shared/Common Structures, Systems, and Components and Non-Structures, Systems, and components Based Design Features and Inspections, Tests, Analyses, and Acceptance Criteria Cross Reference (Continued)

ITAAC No.	System	Discussion	DBA	Internal/External Hazard	Radiological	PRA & Severe Accident	FP
03.08.02	PL	Section 9.5.3 discusses the PLS which provides emergency illumination of the operator workstations and SDIS panels in the MCR and RSS.	Х			X	
		In accordance with Table 14.2-60, a preoperational test demonstrates that the PLS provides at least:					
		 i. 10 foot-candles of illumination at the MCR operator workstations and MCR auxiliary panels. 					
		ii. 10 foot-candles at the RSS operator workstations.					
03.08.03	PL	Section 9.5.3 discusses the use of eight-hour battery pack emergency lighting fixtures, which provide illumination of at least one foot-candle for post-fire safe shutdown activities outside of the MCR and RSS. These units should provide lighting for:	X			X	
		 areas required for power restoration / recovery to comply with the guidance of RG 1.189, Fire Protection for Nuclear Power Plants. 					
		 areas where normal actions are required for operation of equipment needed during fire; and 					
		 escape or access routes for firefighting and the remote shutdown area. 					
		In accordance with the requirements in Table 14.2-60, a preoperational test demonstrates that eight-hour battery pack emergency lighting fixtures illuminate their required target areas to provide at least one foot-candle illumination in the areas outside the MCR or RSS where post-fire safeshutdown activities are performed.					

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Table 14.3-2: Shared/Common Structures, Systems, and Components and Non-Structures, Systems, and components Based Design Features and Inspections, Tests, Analyses, and Acceptance Criteria Cross Reference (Continued)

ITAAC No.	System	Discussion	DBA	Internal/External Hazard	Radiological	PRA & Severe Accident	FP
03.09.01	RM	Section 11.5.2.2.1, Normal Control Room HVAC System, discusses the operation of the CRVS. For each high radiation signal listed in Tier 1 Table 3.9-1, the CRVS automatically aligns the components identified in Tier 1 Table 3.9-1 to the required positions identified in the table. In accordance with Table 14.2-19, a preoperational test			Х		
		demonstrates the CRVS automatically aligns the components identified in Tier 1 Table 3.9-1 to the required positions identified in the table upon initiation of a real or simulated CRVS high radiation signal from 00-CRV-RT-0503, 00-CRV-RT-0504, and 00-CRV-RT-0505.					
03.09.02	RM	Section 11.5.2.2.1, Normal Control Room HVAC System, and Section 11.5.2.2.2, Control Room Habitability System, discuss the operation of the CRVS and CRHS. For each high radiation signal listed in Tier 1 Table 3.9-1, the CRVS and the CRHS automatically align the components identified in Tier 1 Table 3.9-1 to the required positions identified in the table. In accordance with Table 14.2-18, a preoperational test demonstrates the CRVS and the CRHS automatically align the components identified in Tier 1 Table 3.9-1 to the required positions identified in the table upon initiation of a			X		
03.09.03	RM	real or simulated CRVS high radiation signal from 00-CRV-RT-0510 and 00-CRV-RT-0511. Section 11.5.2.2.3, Reactor Building HVAC System, discusses the operation of the RBVS. For each high radiation signal listed in Tier 1 Table 3.9-1, the RBVS automatically aligns the components identified in Tier 1 Table 3.9-1 to the required positions identified in the table. In accordance with Table 14.2-20, a preoperational test demonstrates the RBVS automatically aligns the components identified in Tier 1 Table 3.9-1 to the required positions identified in the table upon initiation of a real or simulated RBVS high radiation signal from 00-RBV-RE-0510,			X		

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Table 14.3-2: Shared/Common Structures, Systems, and Components and Non-Structures, Systems, and components Based Design Features and Inspections, Tests, Analyses, and Acceptance Criteria Cross Reference (Continued)

ITAAC No.	System	Discussion	DBA	Internal/External Hazard	Radiological	PRA & Severe Accident	FP
03.09.04	RM	Section 11.5.2.2.6, Gaseous Radioactive Waste System, discusses the operation of the gaseous radioactive waste system (GRWS). For each high radiation signal listed in Tier 1 Table 3.9-1, the GRWS automatically aligns the components identified in Tier 1 Table 3.9-1 to the required positions identified in the table.			Х		
		In accordance with Table 14.2-36, a preoperational test demonstrates the GRWS automatically aligns the components identified in Tier 1 Table 3.9-1 to the required positions identified in the table upon initiation of a real or simulated GRWS high radiation signal from 00-GRW-RIT-0046.					
03.09.05	RM	Section 11.5.2.2.6, Gaseous Radioactive Waste System, discusses the operation of the GRWS. For each high radiation signal listed in Tier 1 Table 3.9-1, the GRWS automatically aligns the components identified in Tier 1 Table 3.9-1 to the required positions identified in the table.			X		
		In accordance with Table 14.2-36, a preoperational test demonstrates the GRWS automatically aligns the components identified in Tier 1 Table 3.9-1 to the required positions identified in the table upon initiation of a real or simulated GRWS high radiation signal from 00-GRW-RIT-0060.					
03.09.06	RM	Section 11.5.2.2.6, Gaseous Radioactive Waste System, discusses the operation of the GRWS. For each high radiation signal listed in Tier 1 Table 3.9-1, the GRWS automatically aligns the components identified in Tier 1 Table 3.9-1 to the required positions identified in the table.			Х		
		In accordance with Table 14.2-36, a preoperational test demonstrates the GRWS automatically aligns the components identified in Tier 1 Table 3.9-1 to the required positions identified in the table upon initiation of a real or simulated GRWS high radiation signal from 00-GRW-RIT-0071.					

Table 14.3-2: Shared/Common Structures, Systems, and Components and Non-Structures, Systems, and components Based
Design Features and Inspections, Tests, Analyses, and Acceptance Criteria Cross Reference (Continued)

ITAAC No.	System	Discussion	DBA	Internal/External Hazard	Radiological	PRA & Severe Accident	FP
03.09.07	RM	Section 11.5.2.1.5, Liquid Radioactive Waste System, discusses the operation of the liquid radioactive waste system (LRWS). For each high radiation signal listed in Tier 1 Table 3.9-1, the LRWS automatically aligns the components identified in Tier 1 Table 3.9-1 to the required positions identified in the table. In accordance with Table 14.2-35, a preoperational test demonstrates the LRWS automatically aligns the components identified in Tier 1 Table 3.9-1 to the required positions identified in the table upon initiation of a real or simulated LRWS high radiation signal from 00-LRW-RIT-0569 and 00-LRW-RIT-0571.			X		
03.09.08	RM	Section 11.5.2.2.14, Auxiliary Boiler System, discusses the operation of the ABS. For each high radiation signal listed in Tier 1 Table 3.9-1, the ABS automatically aligns the components identified in Tier 1 Table 3.9-1 to the required positions identified in the table. In accordance with Table 14.2-9, a preoperational test demonstrates the ABS automatically aligns the components identified in Tier 1 Table 3.9-1 to the required positions identified in the table upon initiation of a real or simulated ABS high radiation signal from 00-AB-RT-0153.			х		
03.09.09	RM	Section 11.5.2.2.14, Auxiliary Boiler System, discusses the operation of the ABS. For each high radiation signal listed in Tier 1 Table 3.9-1, the ABS automatically aligns the components identified in Tier 1 Table 3.9-1 to the required positions identified in the table. In accordance with Table 14.2-9, a preoperational test demonstrates the ABS automatically aligns the components identified in Tier 1 Table 3.9-1 to the required positions identified in the table upon initiation of a real or simulated ABS high radiation signal from 00-AB-RT-0166.			X		

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Table 14.3-2: Shared/Common Structures, Systems, and Components and Non-Structures, Systems, and components Based Design Features and Inspections, Tests, Analyses, and Acceptance Criteria Cross Reference (Continued)

ITAAC No.	System	Discussion	DBA	Internal/External Hazard	Radiological	PRA & Severe Accident	FP
03.09.10	RM	Section 11.5.2.1.4, Pool Surge Control System, discusses the operation of the pool surge control system (PSCS). For each high radiation signal listed in Tier 1 Table 3.9-1, the PSCS automatically aligns the components identified in Tier 1 Table 3.9-1 to the required positions identified in the table. In accordance with Table 14.2-4, a preoperational test demonstrates the PSCS automatically aligns the components identified in Tier 1 Table 3.9-1 to the required positions identified in the table upon initiation of a real or simulated PSCS high radiation signal from 00-PSC-RE-1003.			x		
03.10.01	RBC	Section 9.1.5, Overhead Heavy Load Handling System, describes that the Reactor Building crane (RBC) main hoist is classified as a Type I crane as defined by the ASME NOG-1 Code, Rules for Construction of Overhead and Gantry Cranes (Top Running Bridge, Multiple Girder). An ITAAC inspection is performed of the RBC main hoist machinery arrangement to verify the existence of the following single-failure proof features: (a) nonredundant structural components (bridge, trolley, wire rope drum, and hook) are designed to appropriate standards, constructed from base material demonstrated to meet appropriate material properties, and, (b) redundant design features to stop and hold the load following: • specified component failures (e.g., wire rope, drive train, and control system) • operator errors (e.g., two-blocking and overload) This ITAAC inspection may be performed any time after manufacture of the RBC (at the factory or later).				X	

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Table 14.3-2: Shared/Common Structures, Systems, and Components and Non-Structures, Systems, and components Based Design Features and Inspections, Tests, Analyses, and Acceptance Criteria Cross Reference (Continued)

ITAAC No.	System	Discussion	DBA	Internal/External Hazard	Radiological	PRA & Severe Accident	FP
03.10.02	RBC	Section 9.1.5 describes that the RBC auxiliary hoists are classified as a Type I crane as defined by the ASME NOG-1 Code, Rules for Construction of Overhead and Gantry Cranes (Top Running Bridge, Multiple Girder). An ITAAC inspection is performed of the RBC auxiliary hoists machinery arrangement to verify the existence of the following single-failure proof features: (a) nonredundant structural components (wire rope drum, and hook) are designed to appropriate standards, constructed from base material demonstrated to meet appropriate material properties, and, (b) redundant design features to stop and hold the load following: • specified component failures (e.g., wire rope, drive train, and control system) • operator errors (e.g., two-blocking and overload) This ITAAC inspection may be performed any time after manufacture of the RBC auxiliary hoists (at the factory or later).				X	

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Table 14.3-2: Shared/Common Structures, Systems, and Components and Non-Structures, Systems, and components Based Design Features and Inspections, Tests, Analyses, and Acceptance Criteria Cross Reference (Continued)

ITAAC No.	System	Discussion	DBA	Internal/External Hazard	Radiological	PRA & Severe Accident	FP
03.10.03	RBC	Section 9.1.5 describes that the RBC wet hoist is classified as a Type I crane as defined by the ASME NOG-1 Code, Rules for Construction of Overhead and Gantry Cranes (Top Running Bridge, Multiple Girder).				X	
		An ITAAC inspection is performed of the RBC wet hoist arrangement to verify the existence of the following single-failure proof features: (a) nonredundant structural components (bridge, trolley, wire rope drum, and hook) are designed to appropriate standards, constructed from base material demonstrated to meet appropriate material properties, and, (b) redundant design features to stop and hold the load following: • specified component failures (e.g., wire rope, drive train,					
		 and control system) operator errors (e.g., two-blocking and overload) This ITAAC inspection may be performed any time after manufacture of the RBC wet hoist (at the factory or later). 					
03.10.04	RBC	Section 9.1.5 describes that the RBC main hoist is classified as a Type I crane as defined by the ASME NOG-1 Code, Rules for Construction of Overhead and Gantry Cranes (Top Running Bridge, Multiple Girder). In accordance with ASME NOG-1, the RBC main hoist is full load tested at a maximum of 100% of the hoist manufacturer's rating. After the full load test is completed, and prior to use of the crane to handle loads, the RBC is rated load tested at 125% (+5%, -0%) of the manufacturer's rating in accordance with ASME NOG-1, paragraph 7423.				x	
		An FAT demonstrates that the single failure-proof RBC main hoist is rated load tested at 125% (+5%, -0%) of the manufacturer's rating.					

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Table 14.3-2: Shared/Common Structures, Systems, and Components and Non-Structures, Systems, and components Based Design Features and Inspections, Tests, Analyses, and Acceptance Criteria Cross Reference (Continued)

ITAAC No.	System	Discussion	DBA	Internal/External Hazard	Radiological	PRA & Severe Accident	FP
03.10.05	RBC	Section 9.1.5 describes that the RBC auxiliary hoists are classified as a Type I crane as defined by the ASME NOG-1 Code, Rules for Construction of Overhead and Gantry Cranes (Top Running Bridge, Multiple Girder). In accordance with ASME NOG-1, each RBC auxiliary hoist is full load tested at a maximum of 100% of the hoist manufacturer's rating. After the full load test is completed, and prior to use of the RBC auxiliary hoists to handle loads, each RBC auxiliary hoist is rated load tested at 125% (+5%, -0%) of the manufacturer's rating in accordance with ASME NOG-1, paragraph 7423. An FAT demonstrates that the single failure proof RBC auxiliary hoists are rated load tested at 125% (+5%, -0%) of the manufacturer's rating.				X	
03.10.06	RBC	Section 9.1.5 describes that the RBC wet hoist is classified as a Type I crane as defined by the ASME NOG-1 Code, Rules for Construction of Overhead and Gantry Cranes (Top Running Bridge, Multiple Girder). In accordance with ASME NOG-1, the RBC wet hoist is full load tested at a maximum of 100% of the hoist manufacturer's rating. After the full load test is completed, and prior to use of the RBC wet hoist to handle loads, the RBC wet hoist is rated load tested at 125% (+5%, -0%) of the manufacturer's rating in accordance with ASME NOG-1, paragraph 7423. An FAT demonstrates that the single failure proof RBC wet hoist is rated load tested at 125% (+5%, -0%) of the manufacturer's rating.				X	

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Table 14.3-2: Shared/Common Structures, Systems, and Components and Non-Structures, Systems, and components Based Design Features and Inspections, Tests, Analyses, and Acceptance Criteria Cross Reference (Continued)

ITAAC No.	System	Discussion	DBA	Internal/External Hazard	Radiological	PRA & Severe Accident	FP
03.10.07	RBC	Section 9.1.5 discusses that the single failure-proof RBC is classified as a Type I crane as defined by the ASME NOG-1 Code, Rules for Construction of Overhead and Gantry Cranes (Top Running Bridge, Multiple Girder).				X	
		An ITAAC inspection is performed to verify that the ASME Type I as-built RBC welds are nondestructively examined in accordance with the standards of ASME NOG-1 paragraph 4251.4 and/or the RBC purchase specification.					
		This ITAAC inspection may be performed any time after manufacture of the single failure proof RBC (at the factory or later).					
03.10.08	RBC	Section 9.1.5 discusses that the single failure-proof RBC wet hoist is classified as a Type I crane as defined by the ASME NOG-1 Code, Rules for Construction of Overhead and Gantry Cranes (Top Running Bridge, Multiple Girder).				X	
		An ITAAC inspection is performed to verify that the ASME Type I as-built RBC wet hoist welds are nondestructively examined in accordance with the standards of ASME NOG-1 paragraph 4251.4 and/or the RBC wet hoist purchase specification.					
		This ITAAC inspection may be performed any time after manufacture of the single failure-proof RBC wet hoist (at the factory or later).					

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Table 14.3-2: Shared/Common Structures, Systems, and Components and Non-Structures, Systems, and components Based Design Features and Inspections, Tests, Analyses, and Acceptance Criteria Cross Reference (Continued)

ITAAC No.	System	Discussion	DBA	Internal/External Hazard	Radiological	PRA & Severe Accident	FP
03.11.01	RXB	Section 9.5.1, Fire Protection Program, discusses that fire and smoke barriers separate: (1) safety-related systems from any potential fires in nonsafety-related areas that could affect the ability of safety-related systems to perform their safety-related function; (2) redundant divisions or trains of safety-related systems from each other to prevent damage that could adversely affect a safe shutdown function from a single fire; (3) equipment within a single safety-related electrical division that present a fire hazard to equipment in another safety-related division; (4) electrical circuits (safety-related and nonsafety-related) whose fire-induced failure could cause a spurious actuation that could adversely affect a safe shutdown function. An ITAAC inspection is performed to verify that the following RXB as-built fire barriers and smoke barriers are installed in accordance with the FHA and are qualified for the fire rating specified in the FHA: • fire-rated doors • fire-rated dampers • smoke barriers The objective of the inspection is to verify that the fire and smoke barriers meet the design requirements, location requirements, and that they are qualified for their intended use based upon visual inspection and review of the as-built drawings and qualification documentation.		X			X

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Table 14.3-2: Shared/Common Structures, Systems, and Components and Non-Structures, Systems, and components Based Design Features and Inspections, Tests, Analyses, and Acceptance Criteria Cross Reference (Continued)

ITAAC No.	System	Discussion	DBA	Internal/External Hazard	Radiological	PRA & Severe Accident	FP
03.11.02	RXB	Section 3.4.1, Internal Flood Protection for Onsite Equipment Failures, discusses the features used to mitigate the consequences of internal flooding, which include structural enclosures, barriers, curbs, sills, and watertight seals. An ITAAC inspection is performed to verify that the following RXB as-built internal flooding barriers are installed in accordance with the internal flooding analysis report and are qualified as specified in the internal flooding analysis report: • flood resistant doors • curbs and sills • walls • water tight penetration seals • NEMA enclosures The objective of the inspection is to verify that the flooding barriers meet the design requirements, location requirements, and that they are qualified for their intended use based upon visual inspection and review of the as-built drawings and qualification documentation.		X			

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Table 14.3-2: Shared/Common Structures, Systems, and Components and Non-Structures, Systems, and components Based Design Features and Inspections, Tests, Analyses, and Acceptance Criteria Cross Reference (Continued)

ITAAC No.	System	Discussion	DBA	Internal/External Hazard	Radiological	PRA & Severe Accident	FP
03.11.03	RXB	Section 2.4.2, Floods, discusses that the site is properly graded to prevent localized flooding from the maximum precipitation event. Section 3.4.2.1, Probable Maximum Flood, states that the finished grade for all building structures except at the truck ramp is 6 inches below the nominal ground floor elevation. An ITAAC inspection is performed to verify that the RXB asbuilt floor elevation at ground entrances is located above the maximum external flood elevation to protect the RXB from external flooding. The inspection will compare the maximum external flood elevation against the RXB as-built design drawings to verify that the required margin discussed in Section 3.4.1 is met.		X			
03.11.04	RXB	Section 12.3, Radiation Protection Design Features, provides the design bases for radiation shielding, including type, form and material properties utilized in specific locations. Radiation shielding is provided to meet the radiation zone and access requirements for normal operation and post-accident conditions, and to demonstrate compliance with 10 CFR 50.49, GDC 4, and GDC 19. Compartment walls, ceilings, and floors, or other barriers provide shielding. An ITAAC inspection is performed to verify that the thickness of RXB radiation barriers is greater than or equal to the required thicknesses. The required thicknesses are specified in Tier 1 Table 3.11-1.			X		

Table 14.3-2: Shared/Common Structures, Systems, and Components and Non-Structures, Systems, and components Based Design Features and Inspections, Tests, Analyses, and Acceptance Criteria Cross Reference (Continued)

ITAAC No.	System	Discussion	DBA	Internal/External Hazard	Radiological	PRA & Severe Accident	FP
03.11.05	RXB	Section 12.3.2.2, Design Considerations, provides the design bases for radiation shielding. Radiation shielding is provided to meet the radiation zone requirements for normal operation and control room access requirements for post-accident conditions. Radiation attenuating doors must meet or exceed the radiation attenuation capability of the wall within which they are installed. An ITAAC inspection is performed to verify that the RXB radiation attenuating doors are installed in their design location and have a radiation attenuation capability that meets or exceeds that of the wall within which they are installed in accordance with the approved door schedule design.			X		

Table 14.3-2: Shared/Common Structures, Systems, and Components and Non-Structures, Systems, and components Based Design Features and Inspections, Tests, Analyses, and Acceptance Criteria Cross Reference (Continued)

ITAAC No.	System	Discussion	DBA	Internal/External Hazard	Radiological	PRA & Severe Accident	FP
03.11.06	RXB	Section 3.8.4.4, Design and Analysis Procedures, and Appendix 3B, NuScale Plant Critical Sections, provide descriptive information, including plans and sections of each Seismic Category I structure, to establish that there is sufficient information to define the primary structural aspects and elements relied upon for the structure to perform the intended safety functions. Critical dimensions are identified in Appendix 3B. The RXB and its design basis loads are discussed in Section 3.8.4.3, Loads and Load Combinations. Critical sections are the subcomponents of individual Seismic Category I structures (i.e., shear walls, floor slabs and roofs, structure-to-structure connections) that are analytically representative of an essentially complete design. Design basis load combinations are shown in Table 3.8.4-3 and Table 3.8.4-4 and may include:	X				
		 D = Dead loads, including piping, equipment, and partitions. F = Loads due to weight and pressures of fluids. H = Loads due to weight and static pressure of soil, water in soil, or other materials. L = Live loads due to occupancy and moveable equipment. Lr = Roof live load. Ro = Piping and equipment reaction loads. Ra = Piping and equipment reaction loads due to a postulated accident. 					
		 To = Thermal loads due to normal operating temperatures. Ta = Thermal loads due to accident condition temperatures. R = Rain load. 					

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Table 14.3-2: Shared/Common Structures, Systems, and Components and Non-Structures, Systems, and components Based Design Features and Inspections, Tests, Analyses, and Acceptance Criteria Cross Reference (Continued)

ITAAC No.	System	Discussion	DBA	Internal/External Hazard	Radiological	PRA & Severe Accident	FP
		• S = Snow load.					
		• Se = Extreme snow load.					
		• W = Straight line wind load.					
		• Wt = Loads due to the design basis tornado.					
		 Wh = Loads due to the design basis hurricane. Eo = Seismic load due to an operating basis earthquake. 					
		• Ess = Seismic load due to an SSE.					
		• Ccr = Loads due to the RBC.					
		• Pa = Pressure loads due to accident conditions.					
		 Yj = Jet impingement load generated by a postulated pipe break. 					
		 Yr = Loads on the structure generated by the reaction of the broken pipe during a postulated break. 					
		 Ym = Missile impact load, or related internal moments and forces, on the structure generated by a postulated pipe break. 					
		 B = Loads due to buoyant force. 					
		Guidance for the content and structure of the design report is provided in Standard Review Plan Section 3.8.4, Appendix C as shown in Table 3.B-2.					
		An ITAAC inspection and analysis is performed to ensure that deviations between the drawings used for construction and of the as-built RXB are reconciled and the RXB maintains its structural integrity under the design basis loads. The design report provides criteria for the reconciliation between design and as-built conditions.					
		An ITAAC inspection is performed of the as-built RXB to verify that the dimensions of the RXB critical sections conform to the approved design.					

Table 14.3-2: Shared/Common Structures, Systems, and Components and Non-Structures, Systems, and components Based Design Features and Inspections, Tests, Analyses, and Acceptance Criteria Cross Reference (Continued)

ITAAC No.	System	Discussion	DBA	Internal/External Hazard	Radiological	PRA & Severe Accident	FP
03.11.07	RXB	Section 3.2.1, Seismic Classification, discusses that per RG 1.29, some SSC that perform no safety-related functions could, if they failed under seismic loading, prevent or reduce the functioning of Seismic Category I SSC.	Х				
		An ITAAC inspection and analysis is performed to verify that the as-built non-Seismic Category I SSC where a potential for adverse interaction with a Seismic Category I SSC exists will not impair the ability of Seismic Category I SSC to perform their safety functions as demonstrated by one or more of the following criteria:					
		 Seismic Category I SSC are isolated from non-Seismic Category I SSC so that interaction does not occur. 					
		 Seismic Category I SSC are analyzed to confirm that the ability to perform their safety functions is not impaired as a result of impact from non-Seismic Category I SSC. 					
		 A non-Seismic Category I restraint system designed to Seismic Category I requirements is used to assure that no interaction occurs between Seismic Category I SSC and non-Seismic Category I SSC. 					
03.12.01	RWB	Section 12.3, Radiation Protection Design Features, provides the design bases for radiation shielding, including type, form and material properties utilized in specific locations. Radiation shielding is provided to meet the radiation zone requirement for normal operation and post-accident conditions and to demonstrate conformance with RG 4.21 and RG 8.8. Compartment walls, ceilings, and floors, or other barriers provide shielding.			X		
		An ITAAC inspection is performed to verify that the thickness of RWB radiation barriers is greater than or equal to the required thicknesses. The required thicknesses are specified in Tier 1 Table 3.12-1.					

Table 14.3-2: Shared/Common Structures, Systems, and Components and Non-Structures, Systems, and components Based Design Features and Inspections, Tests, Analyses, and Acceptance Criteria Cross Reference (Continued)

ITAAC No.	System	Discussion	DBA	Internal/External Hazard		PRA & Severe Accident	FP
03.12.02	RWB	Section 12.3.2.2, Design Considerations, provides the design bases for radiation shielding. Radiation shielding is provided to meet the radiation zone requirements for normal operation and post-accident conditions, and to demonstrate conformance to RG 4.21 and RG 8.8. Radiation attenuating doors must meet or exceed the radiation attenuation capability of the wall within which they are installed. An ITAAC inspection is performed to verify that the RWB radiation attenuating doors are installed in their design location and have a radiation attenuation capability that meets or exceeds that of the wall within which they are installed in accordance with the approved door schedule design.			X		

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Table 14.3-2: Shared/Common Structures, Systems, and Components and Non-Structures, Systems, and components Based Design Features and Inspections, Tests, Analyses, and Acceptance Criteria Cross Reference (Continued)

ITAAC No.	System	Discussion	DBA	Internal/External Hazard	Radiological	PRA & Severe Accident	FP
03.12.03	RWB	The RW-Ila RWB and its design basis loads are discussed in Section 3.8.4.1.3, Radioactive Waste Building. Guidance for the content and structure of the as-built design report is provided in Standard Review Plan Section 3.8.4, Appendix C.	Х		x		
		The scope of this ITAAC is a reconciliation of deviations between the issued for construction drawings that implement the seismic and dynamic analyses and the asbuilt structures. The design report provides criteria for the reconciliation. Design basis loads for RW-lla structures as listed in RG 1.143 are:					
		• earthquake					
		• wind					
		• tornado					
		tornado missile					
		• flood					
		• precipitation (rain, snow)					
		accidental explosion (fixed facility)					
		accidental explosion (transportation vehicle)					
		malevolent vehicle assault					
		small aircraft crash					
		An ITAAC inspection and reconciliation analysis is performed of the as-built RW-lla RWB to ensure that deviations between the drawings used for construction and the as-built RW-lla RWB are reconciled and the as-built RW-lla RWB maintains its structural integrity under the design basis loads. The design report provides criteria for the reconciliation between design and as-built conditions.					

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Table 14.3-2: Shared/Common Structures, Systems, and Components and Non-Structures, Systems, and components Based Design Features and Inspections, Tests, Analyses, and Acceptance Criteria Cross Reference (Continued)

ITAAC No.	System	Discussion	DBA	Internal/External Hazard	Radiological	PRA & Severe Accident	FP
03.13.01	CRB	Section 9.5.1, Fire Protection Program, discusses that fire and smoke barriers separate: (1) Safety-related systems from any potential fires in nonsafety-related areas that could affect the ability of safety-related systems to perform their safety-related function. (2) Redundant divisions or trains of safety-related systems from each other to prevent damage that could adversely affect a safe shutdown function from a single fire. (3) Equipment within a single safety-related electrical division that present a fire hazard to equipment in another safety-related division. (4) Electrical circuits (safety-related and nonsafety-related) whose fire-induced failure could cause a spurious actuation that could adversely affect a safe shutdown function. An ITAAC inspection is performed to verify that the following CRB as-built fire barriers and smoke barriers are installed in accordance with the FHA and are qualified for the fire rating specified in the FHA: • fire-rated doors • fire-rated dampers • smoke barriers The objective of the inspection is to verify that the fire and smoke barriers meet the design requirements, location requirements, and that they are qualified for their intended use based upon visual inspection and review of the as-built drawings and qualification documentation.		X			X

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Table 14.3-2: Shared/Common Structures, Systems, and Components and Non-Structures, Systems, and components Based Design Features and Inspections, Tests, Analyses, and Acceptance Criteria Cross Reference (Continued)

ITAAC No.	System	Discussion	DBA	Internal/External Hazard	Radiological	PRA & Severe Accident	FP
03.13.02	CRB	Section 3.4.1, Internal Flood Protection for Onsite Equipment Failures, discusses the features used to mitigate the consequences of internal flooding, which include structural enclosures, barriers, and watertight seals. An ITAAC inspection is performed to verify that the following CRB as-built internal flooding barriers are installed in accordance with the internal flooding analysis report and are qualified as specified in the internal flooding analysis report: • flood resistant doors • walls • water tight penetration seals • NEMA enclosures The objective of the inspection is to verify that the flooding barriers meet the design requirements, location requirements, and that they are qualified for their intended use based upon visual inspection and review of the as-built drawings and qualification documentation.		X			

Table 14.3-2: Shared/Common Structures, Systems, and Components and Non-Structures, Systems, and components Based Design Features and Inspections, Tests, Analyses, and Acceptance Criteria Cross Reference (Continued)

ITAAC No	o. System	Discussion	DBA	Internal/External Hazard	Radiological	PRA & Severe Accident	FP
03.13.03	CRB	Section 2.4.2, Floods, discusses that the site is properly graded to prevent localized flooding from the maximum precipitation event. Section 3.4.1, Internal Flood Protection for Onsite Equipment Failures, and Section 3.4.2, Protection of Structures against Flood from External Sources, discuss that Seismic Category I structures that may be subjected to the design basis flood are designed to withstand the maximum external flood level to protect safe shutdown equipment within the structure. Section 3.4.2.1, Probable Maximum Flood, states that the finished grade for all building structures except at the truck ramp is 6 inches		X		Accident	
		below the nominal ground floor elevation. An ITAAC inspection is performed to verify that the CRB asbuilt floor elevation at ground entrances is located above the maximum external flood elevation to protect the CRB from external flooding. The inspection will compare the maximum external flood elevation against the CRB as-built design drawings to verify that the required margin discussed in Section 3.4.1 is met.					
03.13.04	CRB	Section 3.8.4.4, Design and Analysis Procedures, and Appendix 3B, NuScale Plant Critical Sections, provide descriptive information, including plans and sections of each Seismic Category I structure, to establish that there is sufficient information to define the primary structural aspects and elements relied upon for the structure to perform the intended safety functions. Critical dimensions are identified in Appendix 3B. The CRB at Elevation 120'-0" and below and its design basis loads are discussed in Section 3.8.4.3, Loads and Load Combinations. Critical sections are the subcomponents of individual Seismic Category I structures (i.e., shear walls, floor slabs and roofs, structure-to-structure connections) that are analytically representative of an essentially complete design. Design basis loads load combinations are shown in Table 3.8.4-3 and Table 3.8.4-4 and may include:					

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Table 14.3-2: Shared/Common Structures, Systems, and Components and Non-Structures, Systems, and components Based Design Features and Inspections, Tests, Analyses, and Acceptance Criteria Cross Reference (Continued)

ITAAC No.	System	Discussion	DBA	Internal/External Hazard	Radiological	PRA & Severe Accident	FP
		 D = Dead loads, including piping, equipment, and partitions. 					
		• F = Loads due to weight and pressures of fluids.					
		 H = Loads due to weight and static pressure of soil, water in soil, or other materials. 					
		 L = Live loads due to occupancy and moveable equipment. 					
		• Lr = Roof live load.					
		• Ro = Piping and equipment reaction loads.					
		 Ra = Piping and equipment reaction loads due to a postulated accident. 					
		 To = Thermal loads due to normal operating temperatures. 					
		 Ta = Thermal loads due to accident condition temperatures. 					
		• R = Rain load.					
		• S = Snow load.					
		• Se = Extreme snow load.					
		• W = Straight line wind load.					
		• Wt = Loads due to the design basis tornado.					
		• Wh = Loads due to the design basis hurricane.					
		• Ess = Seismic load due to an SSE.					
		• Pa = Pressure loads due to accident conditions.					

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Table 14.3-2: Shared/Common Structures, Systems, and Components and Non-Structures, Systems, and components Based Design Features and Inspections, Tests, Analyses, and Acceptance Criteria Cross Reference (Continued)

ITAAC No.	System	Discussion	DBA	Internal/External Hazard	Radiological	PRA & Severe Accident	FP
		Guidance for the content and structure of the design report is provided in Standard Review Plan Section 3.8.4, Appendix C as shown in Table 3.B-2.					
		An ITAAC inspection and analysis is performed to ensure that deviations between the drawings used for construction and of the as-built CRB are reconciled. The design report provides criteria for the reconciliation between design and as-built conditions.					
		An ITAAC inspection is performed of the as-built CRB at Elevation 120'-0" and below to verify that the dimensions of the CRB critical sections conform to the approved design.					
03.13.05	CRB	Section 3.2.1, Seismic Classification, discusses that per RG 1.29, some SSC that perform no safety-related functions could, if they failed under seismic loading, prevent or reduce the functioning of Seismic Category I SSC.	Х				
		An ITAAC inspection and analysis is performed to verify that the as-built non-Seismic Category I SSC located where a potential for adverse interaction with a Seismic Category I SSC exists will not impair the ability of Seismic Category I SSC to perform their safety functions as demonstrated by one or more of the following criteria:					
		 The collapse of the non-Seismic Category I structure will not cause the non-Seismic Category I structure to strike a Seismic Category I SSC. 					
		 The collapse of the non-Category I structure will not impair the integrity of Seismic Category I SSC, nor result in incapacitating injury to control room occupants. 					
		 The non-Category I structure will be analyzed and designed to prevent its failure under SSE conditions. 					

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Table 14.3-2: Shared/Common Structures, Systems, and Components and Non-Structures, Systems, and components Based Design Features and Inspections, Tests, Analyses, and Acceptance Criteria Cross Reference (Continued)

ITAAC No.	System	Discussion	DBA	Internal/External Hazard	Radiological	PRA & Severe Accident	FP
03.14.01	EQ	Section 3.10, Seismic and Dynamic Qualification of Mechanical and Electrical Equipment, presents information to demonstrate that the Seismic Category I equipment, including its associated supports and anchorages, is qualified by type test, analysis, or a combination of type test and analysis to perform its safety function under the design basis seismic loads during and after an SSE. The qualification method employed for the Seismic Category I equipment is the same as the qualification method described for that type of equipment in Section 3.10. This method conforms to IEEE-344-2004 and ASME QME-1-2007 (or later editions), as accepted by the NRC staff in RG 1.100 Revision 3 (or later revision), with specific revision years and numbers as presented in Section 3.10.					
		The ITAAC verifies that: (1) a seismic qualification record form exists for each Seismic Category I component type, and (2) the seismic qualification record form concludes that the Seismic Category I equipment listed in Tier 1 Table 3.14-1, including its associated supports and anchorages, performs its function under the seismic design basis load conditions specified in the seismic qualification record form. After installation in the plant, an ITAAC inspection is performed to verify that the Seismic Category I equipment listed in Tier 1 Table 3.14-1, including its associated supports and anchorages, is installed in its design location in a					
		Seismic Category I structure in a configuration bounded by the seismic qualification record form.					

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Table 14.3-2: Shared/Common Structures, Systems, and Components and Non-Structures, Systems, and components Based Design Features and Inspections, Tests, Analyses, and Acceptance Criteria Cross Reference (Continued)

ITAAC No. Syst	stem	Discussion	DBA	Internal/External Hazard	Radiological	PRA & Severe Accident	FP
03.14.02 EQ		Section 3.11, Environmental Qualification of Mechanical and Electrical Equipment, presents information to demonstrate that the Class 1E electrical equipment, including its connection assemblies, located in a harsh environment is qualified by type test or a combination of type test and analysis to perform its safety-related function under design basis harsh environmental conditions, experienced during normal operations, anticipated operational occurrences, DBAs, and post-accident conditions in accordance with 10 CFR 50.49. As defined in IEEE-Std-572-2006, IEEE Standard for Qualification of Class 1E Connection Assemblies for Nuclear Power Generating Stations, a connection assembly is any connector or termination combined with related cables or wires as an assembly. The qualification method employed for the equipment is the same as the qualification method described for that type of equipment in Section 3.11. The ITAAC verifies that: (1) an equipment qualification record form exists for the Class 1E electrical equipment listed in Tier 1 Table 3.14-1 and addresses connection assemblies, (2) the equipment qualification record form concludes that the Class 1E electrical equipment, including its connection assemblies, performs its safety-related function under the environmental conditions specified in Section 3.11 and the equipment qualification record form, and (3) the required post-accident operability time for the Class 1E electrical equipment in the equipment qualification record form is in agreement with Section 3.11. After installation in the plant, an ITAAC inspection is performed to verify that the Class 1E electrical equipment listed in Tier 1 Table 3.14-1, including its connection assemblies, is installed in its design location in a configuration bounded by the equipment qualification	X			recident	

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Table 14.3-2: Shared/Common Structures, Systems, and Components and Non-Structures, Systems, and components Based Design Features and Inspections, Tests, Analyses, and Acceptance Criteria Cross Reference (Continued)

ITAAC No.	System	Discussion	DBA	Internal/External Hazard	Radiological	PRA & Severe Accident	FP
03.15.01 HFE	HFE	Section 18.10.2.3, Integrated System Validation, describes the integrated system validation (ISV), which provides a comprehensive performance-based assessment of the design of the human-system interface (HSI) resources, based on their realistic operation within a simulator-driven MCR. The ISV is part of the overall human factors engineering (HFE) program.					
		An ISV test is performed in accordance with the verification and validation implementation plan. The ISV uses a representative set of scenarios to assess the usability of the MCR and HSI resources and the tolerance of or susceptibility to error. The acceptance criteria associated with each test scenario are satisfied upon initial performance of the scenarios or upon remediation of failures.					
03.15.02	HFE	Section 18.10.2.2, Design Verification, describes the implementation of HFE aspects of the plant design. An ITAAC inspection is performed to verify that the as-built configuration of main control room HSIs is consistent with the as-designed configuration of main control room HSIs as modified by the Integrated System Validation Report.					
03.16.01	SEC	Section 13.6 discusses that the physical security system design provides the capabilities to detect, assess, impede, and delay threats up to and including the design basis threat, and to provide for defense-in-depth through the integration of systems, technologies, and equipment. Technical Report TR-0416-48929, "NuScale Design of Physical Security Systems," provides safeguards and security-related information that describes security design bases and requirements for security SSC. Vital equipment and vital area are discussed in the report.					
		equipment to verify that the equipment is located in a vital area.					

Table 14.3-2: Shared/Common Structures, Systems, and Components and Non-Structures, Systems, and components Based Design Features and Inspections, Tests, Analyses, and Acceptance Criteria Cross Reference (Continued)

ITAAC No.	System	Discussion	DBA	Internal/External Hazard	Radiological	PRA & Severe Accident	FP
03.16.02	SEC	Section 13.6 discusses that the physical security system design provides the capabilities to detect, assess, impede, and delay threats up to and including the design basis threat, and to provide for defense-in-depth through the integration of systems, technologies, and equipment. Technical Report TR-0416-48929, "NuScale Design of Physical Security Systems," provides safeguards and security-related information that describes security design bases and requirements for security SSC. Provisions for accessing vital equipment are discussed in the report. An ITAAC inspection is performed of the as built vital equipment location to verify that access to vital equipment, within the nuclear island and structures, requires passage through at least two physical barriers, or as otherwise identified in Technical Report TR-0416-48929, "NuScale					
03.16.03	SEC	Design of Physical Security Systems." Section 13.6 discusses that the physical security system design provides the capabilities to detect, assess,impede, and delay threats up to and including the design basis threat, and to provide for defense-in-depth through the integration of systems, technologies, and equipment. Technical Report TR-0416-48929, "NuScale Design of Physical Security Systems," provides safeguards and security-related information that describes security design bases and requirements for security SSC. A type test, analysis, or a combination of type test and analysis are performed of the bullet-resisting barriers used in the external walls, doors, ceilings and floors in the MCR, central alarm station, and the last access control function for access to the protected area. This qualification will demonstrate that the barriers are bullet-resistant, to Underwriters Laboratories Ballistic Standard 752, "The Standard of Safety for Bullet-Resisting Equipment," Level 4, or National Institute of Justice Standard 0108.01, "Ballistic Resistant Protective Materials," Type III.					

Table 14.3-2: Shared/Common Structures, Systems, and Components and Non-Structures, Systems, and components Based Design Features and Inspections, Tests, Analyses, and Acceptance Criteria Cross Reference (Continued)

ITAAC No.	System	Discussion	DBA	Internal/External Hazard	Radiological	PRA & Severe Accident	FP
03.16.04	SEC	Section 13.6 discusses that the physical security system design provides the capabilities to detect, assess, impede, and delay threats up to and including the design basis threat, and to provide for defense-in-depth through the integration of systems, technologies, and equipment. Technical Report TR-0416-48929, "NuScale Design of Physical Security Systems," provides safeguards and security-related information that describes security design bases and requirements for security SSC. The access control system which limits access to vital areas, within the nuclear island and structures, to individuals with unescorted access authorization is discussed in the report. In accordance with Table 14.2-73, a preoperational test demonstrates that the access control system provides authorized access to vital areas, within the nuclear island and structures, only to those individuals with authorization for unescorted access.					

Table 14.3-2: Shared/Common Structures, Systems, and Components and Non-Structures, Systems, and components Based Design Features and Inspections, Tests, Analyses, and Acceptance Criteria Cross Reference (Continued)

ITAAC No.	System	Discussion	DBA	Internal/External Hazard	Radiological	PRA & Severe Accident	FP
03.16.05 SE	SEC	Section 13.6 discusses that the physical security system design provides the capabilities to detect, assess, impede, and delay threats up to and including the design basis threat, and to provide for defense-in-depth through the integration of systems, technologies, and equipment. Technical Report TR-0416-48929, "NuScale Design of Physical Security Systems," provides safeguards and security-related information that describes security design bases and requirements for security SSC. The report discusses that unoccupied vital area portals, within the nuclear island and structures, are equipped with locking devices and alarms that annunciate in the central alarm station. In accordance with Table 14.2-74, a preoperational test, inspection, or a combination of test and inspection demonstrates that unoccupied vital areas, within the					
		nuclear island and structures, are locked and alarmed and intrusion is detected and annunciated in the central alarm station as described in Technical Report TR-0416-48929, "NuScale Design of Physical Security Systems."					
03.16.06	SEC	Section 13.6 discusses that the physical security system design provides the capabilities to detect, assess, impede, and delay threats up to and including the design basis threat, and to provide for defense-in-depth through the integration of systems, technologies, and equipment. Technical Report TR-0416-48929, "NuScale Design of Physical Security Systems," provides safeguards and security related information that describes security design bases and requirements for security SSC. The central alarm station and their location are discussed in the report.					
		An ITAAC inspection is performed of the as built central alarm station to verify that it is located inside the protected area and the interior is not visible from the protected area perimeter.					

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Table 14.3-2: Shared/Common Structures, Systems, and Components and Non-Structures, Systems, and components Based Design Features and Inspections, Tests, Analyses, and Acceptance Criteria Cross Reference (Continued)

ITAAC No.	System	Discussion	DBA	Internal/External Hazard	Radiological	PRA & Severe Accident	FP
03.16.07	SEC	Section 13.6 discusses that the physical security system design provides the capabilities to detect, assess, impede, and delay threats up to and including the design basis threat, and to provide for defense-in-depth through the integration of systems, technologies, and equipment. Technical Report TR-0416-48929, "NuScale Design of Physical Security Systems," provides safeguards and security-related information that describes security design bases and requirements for security SSC. Security alarms, within the nuclear island and structures, are discussed in the report.					
		In accordance with Table 14.2-74, a preoperational test demonstrates that: (1) alarm annunciation indicates the type of alarm and location. (2) security alarm devices, including transmission lines to annunciators, are tamper-indicating and self-checking. (3) an automatic indication is provided when failure of the alarm system or a component occurs or when the system is on standby power.					

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Table 14.3-2: Shared/Common Structures, Systems, and Components and Non-Structures, Systems, and components Based Design Features and Inspections, Tests, Analyses, and Acceptance Criteria Cross Reference (Continued)

ITAAC No.	System	Discussion	DBA	Internal/External Hazard	Radiological	PRA & Severe Accident	FP
03.16.08	SEC	Section 13.6 discusses that the physical security system design provides the capabilities to detect, assess, impede, and delay threats up to and including the design basis threat, and to provide for defense-in-depth through the integration of systems, technologies, and equipment. Technical Report TR-0416-48929, "NuScale Design of Physical Security Systems," provides safeguards and security-related information that describes security design bases and requirements for security SSC. The intrusion detection and assessment system, within the nuclear island and structures, is discussed in the report. In accordance with Table 14.2-74, a preoperational test demonstrates that the intrusion detection and assessment system, within the nuclear island and structures, provides visual and audible annunciation of alarms in the central alarm station.					
03.16.09	SEC	Section 13.6 discusses that the physical security system design provides the capabilities to detect, assess, impede, and delay threats up to and including the design basis threat, and to provide for defense-in-depth through the integration of systems, technologies, and equipment. Technical Report TR-0416-48929, "NuScale Design of Physical Security Systems," provides safeguards and security-related information that describes security design bases and requirements for security SSC. The intrusion detection and assessment system, within the nuclear island and structures, is discussed in the report. In accordance with Table 14.2-74, a preoperational test demonstrates that the intrusion detection and assessment system, within the nuclear island and structures, records each onsite security alarm annunciation, including each alarm, false alarm, alarm check, and tamper indication that identifies the type of alarm, location, alarm circuit, date, and time.					

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Table 14.3-2: Shared/Common Structures, Systems, and Components and Non-Structures, Systems, and components Based Design Features and Inspections, Tests, Analyses, and Acceptance Criteria Cross Reference (Continued)

ITAAC No.	System	Discussion	DBA	Internal/External Hazard	Radiological	PRA & Severe Accident	FP
03.16.10		Section 13.6 discusses that the physical security system design provides the capabilities to detect, assess, impede, and delay threats up to and including the design basis threat, and to provide for defense-in-depth through the integration of systems, technologies, and equipment. Technical Report TR-0416-48929, "NuScale Design of Physical Security Systems," provides safeguards and security-related information that describes security design bases and requirements for security SSC. Emergency exits vital area boundaries, within the nuclear island and structures, are discussed in the report. In accordance with Table 14.2-74, a preoperational test, inspection, or a combination of test and inspection demonstrates that emergency exits through the vital area boundaries, within the nuclear island and structures, are alarmed with intrusion detection devices and secured by locking devices that allow egress during an emergency as described in Technical Report TR-0416-48929, "NuScale Design of Physical Security Systems."					

Tier 2

Table 14.3-2: Shared/Common Structures, Systems, and Components and Non-Structures, Systems, and components Based Design Features and Inspections, Tests, Analyses, and Acceptance Criteria Cross Reference (Continued)

ITAAC No.	System	Discussion	DBA	Internal/External Hazard	Radiological	PRA & Severe Accident	FP
03.16.11	SEC	Section 13.6 discusses that the physical security system design provides the capabilities to detect, assess, impede, and delay threats up to and including the design basis threat, and to provide for defense-in-depth through the integration of systems, technologies, and equipment. Technical Report TR-0416-48929, "NuScale Design of Physical Security Systems," provides safeguards and security-related information that describes security design bases and requirements for security SSC. The central alarm station's landline telephone service is discussed in the report.					
		In accordance with Table 14.2-74, a preoperational test, inspection, or a combination of test and inspection demonstrates that the central alarm station is equipped with conventional landline telephone service with the MCR and with local law enforcement authorities as described in Technical Report TR-0416-48929, "NuScale Design of Physical Security Systems."					
03.16.12	SEC	Section 13.6 discusses that the physical security system design provides the capabilities to detect, assess, impede, and delay threats up to and including the design basis threat, and to provide for defense-in-depth through the integration of systems, technologies, and equipment. Technical Report TR-0416-48929, "NuScale Design of Physical Security Systems," provides safeguards and security-related information that describes security design bases and requirements for security SSC. The central alarm station's communication system is discussed in the report. In accordance with Table 14.2-74, a preoperational test, inspection, or a combination of test and inspection.					
		demonstrates that the central alarm station is capable of continuous communication with on-duty security force personnel as described in Technical Report TR-0416-48929, "NuScale Design of Physical Security Systems."					

Table 14.3-2: Shared/Common Structures, Systems, and Components and Non-Structures, Systems, and components Based Design Features and Inspections, Tests, Analyses, and Acceptance Criteria Cross Reference (Continued)

ITAAC No.	System	Discussion	DBA	Internal/External Hazard	Radiological	PRA & Severe Accident	FP
03.16.13	SEC	Section 13.6 discusses that the physical security system design provides the capabilities to detect, assess, impede, and delay threats up to and including the design basis threat, and to provide for defense-in-depth through the integration of systems, technologies, and equipment. Technical Report TR-0416-48929, "NuScale Design of Physical Security Systems," provides safeguards and security-related information that describes security design bases and requirements for security SSC. Nonportable communications equipment in the central alarm station is discussed in the report. In accordance with Table 14.2-74, a preoperational test, inspection, or a combination of test and inspection demonstrates that nonportable communications equipment in the central alarm station remains operable (without disruption) from an independent power source in the event of loss of normal power as described in Technical Report TR-0416-48929, "NuScale Design of Physical Security Systems."					
03.17.01	RM	Section 11.5.2.2.9, Containment Flooding and Drain System, discusses the operation of the containment flooding and drain system (CFDS). For each high radiation signal listed in Tier 1 Table 3.17-1, the CFDS automatically aligns the components identified in Tier 1 Table 3.17-1 to the required positions identified in the table. In accordance with the information presented in Table 14.2-42, a preoperational test demonstrates the CFDS automatically aligns the components identified in Tier 1 Table 3.17-1 to the required positions identified in the table upon initiation of a real or simulated CFDS high radiation signal from 6A-CFD-RT-1007.			X		

Table 14.3-2: Shared/Common Structures, Systems, and Components and Non-Structures, Systems, and components Based Design Features and Inspections, Tests, Analyses, and Acceptance Criteria Cross Reference (Continued)

ITAAC No.	System	Discussion	DBA	Internal/External Hazard	Radiological	PRA & Severe Accident	FP
03.17.02	RM	Section 11.5.2.2.15, Balance-of-Plant Drain System, discusses the operation of the balance-of-plant drain system (BPDS). For each high radiation signal listed in Tier 1 Table 3.17-1, the BPDS automatically aligns the components identified in Tier 1 Table 3.17-1 to the required positions identified in the table.			X		
		In accordance with the information presented in Table 14.2-24, a preoperational test demonstrates the BPDS automatically aligns the components identified in Tier 1 Table 3.17-1 to the required positions identified in the table upon initiation of a real or simulated BPDS high radiation signal from 6A-BPD-RIT-0552.					
03.17.03	RM	Section 11.5.2.2.15, Balance-of-Plant Drain System, discusses the operation of the BPDS. For each high radiation signal listed in Tier 1 Table 3.17-1, the BPDS automatically aligns the components identified in Tier 1 Table 3.17-1 to the required positions identified in the table. In accordance with the information presented in Table 14.2-24, a preoperational test demonstrates the BPDS automatically aligns the components identified in Tier 1 Table 3.17-1 to the required positions identified in the table upon initiation of a real or simulated BPDS high radiation			X		
03.17.04	RM	signal from 6A-BPD-RIT-0529. Section 11.5.2.2.15, Balance-of-Plant Drain System, discusses the operation of the BPDS. For each high radiation signal listed in Tier 1 Table 3.17-1, the BPDS automatically aligns the components identified in Tier 1 Table 3.17-1 to the required positions identified in the table. In accordance with the information presented in Table 14.2-24, a preoperational test demonstrates the BPDS automatically aligns the components identified in Tier 1 Table 3.17-1 to the required positions identified in the table upon initiation of a real or simulated BPDS high radiation signal from 6A-BPD-RIT-0705.			X		

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Table 14.3-2: Shared/Common Structures, Systems, and Components and Non-Structures, Systems, and components Based Design Features and Inspections, Tests, Analyses, and Acceptance Criteria Cross Reference (Continued)

ITAAC No.	System	Discussion	DBA	Internal/External Hazard	Radiological	PRA & Severe Accident	FP
03.18.01	RM	Section 11.5.2.2.9, Containment Flooding and Drain System, discusses the operation of the containment flooding and drain system (CFDS). For each high radiation signal listed in Tier 1 Table 3.18-1, the CFDS automatically aligns the components identified in Tier 1 Table 3.18-1 to the required positions identified in the table.			Х		
		In accordance with the information presented in Table 14.2-42, a preoperational test demonstrates the CFDS automatically aligns the components identified in Tier 1 Table 3.18-1 to the required positions identified in the table upon initiation of a real or simulated CFDS high radiation signal from 6B-CFD-RT-1007.					
03.18.02	RM	Section 11.5.2.2.15, Balance-of-Plant Drain System, discusses the operation of the BPDS. For each high radiation signal listed in Tier 1 Table 3.18-1, the BPDS automatically aligns the components identified in Tier 1 Table 3.18-1 to the required positions identified in the table. In accordance with the information presented in Table 14.2-24, a preoperational test demonstrates the BPDS automatically aligns the components identified in Tier 1			Х		
		Table 3.18-1 to the required positions identified in the table upon initiation of a real or simulated BPDS high radiation signal from 6B-BPD-RIT-0552.					
03.18.03	RM	Section 11.5.2.2.15, Balance-of-Plant Drain System, discusses the operation of the BPDS. For each high radiation signal listed in Tier 1 Table 3.18-1, the BPDS automatically aligns the components identified in Tier 1 Table 3.18-1 to the required positions identified in the table.			Х		
		In accordance with the information presented in Table 14.2-24, a preoperational test demonstrates the BPDS automatically aligns the components identified in Tier 1 Table 3.18-1 to the required positions identified in the table upon initiation of a real or simulated BPDS high radiation signal from 6B-BPD-RIT-0529.					