Appendix F

Pump Test # 8 Report



Marsland Hydrologic Testing Report - Test # 8

Marsland Expansion Area, Dawes County, NE

FINAL REPORT

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1. EXECUTIVE SUMMARY

As part of Cameco Resources U.S. Nuclear Regulatory Commission License Amendment Application to conduct In-Situ Recovery operations in the Marsland Expansion Area, a regional groundwater pumping test was completed to:

- 1. Demonstrate hydraulic communication between the production zone pumping well and the surrounding production zone observation wells;
- 2. Assess the hydrologic characteristics of the production zone aguifer within the test area;
- 3. Evaluate the presence or absence of hydrologic boundaries in the production zone; and
- 4. Demonstrate sufficient confinement between the production zone and the overlying aquifer for the purpose of ISR mining.

The pumping test at the Marsland Expansion Area utilized one pumping well (CPW-1A) and nine observation wells (CPW-1 and Monitor-2 through Monitor-8) completed in the Basal Chadron Sandstone, as well as three overlying observations wells (BOW-1 through BOW-3) completed in the Brule Formation. The total length of the test was 4.29 days. The average discharge rate was 27.08 gallons per minute (gpm).

During the test, drawdown of greater than 0.8 feet was observed in all Basal Chadron Sandstone observation wells included in the formal observation well network. Based on the drawdown response observed at the most distant observation well locations (Monitor-2 and Monitor-8), the radius of influence of the test is slightly more than 8,800 feet. The drawdown response measured in all Basal Chadron Sandstone observation wells demonstrates hydraulic communication between the production zone pumping well and the surrounding observation wells across the entire test area.

No drawdown was observed in overlying Brule Formation observation wells during the test period. This observation supports the conclusion that adequate confinement exists between the overlying Brule Formation and the Basal Chadron production zone.

Drawdown and recovery data collected from the monitor wells were graphically analyzed to determine the aquifer properties including transmissivity and storativity. The methods of analysis included the Theis (1935) drawdown and recovery methods, and the Jacob Straight-Line Distance-Drawdown method (Cooper and Jacob, 1946).

Transmissivities for the Basal Chadron Sandstone calculated from the drawdown and recovery data ranged from 230 ft²/day to 2,469 ft²/day, respectively. A value of 1,012 ft²/day is believed representative of the average transmissivity over the radius of influence. Based on an average net sand thickness of 40 feet, the average hydraulic conductivity of the Basal Chadron Sandstone is 25 ft/day. Hydraulic conductivities of the aquifer materials in the vicinity of the pumped well (including wells CPW-1A, CPW-1, and Monitor-3) were approximately 3 to 9 times less than those calculated for other wells in the pumping test area based on both the drawdown and recovery analyses, as indicated by an apparent higher conductivity boundary condition effect (flattening of drawdown and recovery curves) in these wells. The storativity calculated from the drawdown data ranged from 1.7E-03 to 8.32E-05, with an average value of 2.56E-04 for the entire test area.



The transmissivity of the Basal Chadron Sandstone within the Marsland Expansion Area investigated herein is higher on average than the existing Class III Permit Area and the Three Crow and North Trend Expansion Areas.

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2. INTRODUCTION

Cameco Resources intends to submit an U.S. Nuclear Regulatory Commission (NRC) License Amendment Application to conduct in-situ recovery (ISR) operations in the Marsland Expansion Area, which is located approximately seven miles southeast of the current Class III Underground Injection Control (UIC) permit area and about four miles northeast of Marsland, Nebraska (**Figure 1**). As part of the amendment application, and in accordance with Nebraska Department of Environmental Quality (NDEQ) regulations, a regional groundwater pumping test was completed in the Marsland Expansion Area as described herein.

2.1 Purpose and Objectives

As part of the NRC License Amendment Application to conduct ISR operations in the Marsland Expansion Area, a regional groundwater pumping test was completed to:

- 1. Demonstrate hydraulic communication between the production zone pumping well and the surrounding production zone observation wells;
- 2. Assess the hydrologic characteristics of the production zone aquifer within the test area;
- 3. Evaluate the presence or absence of hydrologic boundaries in the production zone; and
- 4. Demonstrate sufficient confinement between the production zone and the overlying aquifer for the purpose of ISR mining.

The pumping test described herein was performed in accordance with the NDEQ approved Regional Pumping Test Plan dated September 27, 2010 and subsequent approved changes to the Regional Pumping Test Plan dated March 16, 2011. In accordance with state regulations and Cameco Resources existing Class III UIC permit, the following information is included as part of the Hydrologic Test Report requirements:

- A description and maps of the proposed permit area;
- Construction details for pumping and observation wells;
- Description of site stratigraphy and hydrogeology;
- Geologic cross-sections;
- Description of pumping test configuration and equipment;
- Discussion of pumping test performance and methods used for data analysis;
- Presentation of the results of the pumping test, including best estimates of transmissivity, hydraulic conductivity, and storativity for all observation wells and the pumped well;
- Type-curve match for each monitoring well used to develop best estimates of aquifer parameters;
- Assessment demonstrating confinement of the ore-bearing aquifer;
- Contour map showing drawdown observed at the end of the pumping period;
- Calculation of radius of influence; and

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 Compilation of water level (drawdown) and barometric pressure data for all wells, including pre-test, pumping test, and recovery data

Upon approval of the Hydrologic Test Report and other related permit documentation, NDEQ will provide Cameco Resources the authority to commence mining operations within the radius of influence (ROI) defined by the results of this hydrologic test report. Additional pumping tests will be necessary if ISR occurs outside of the demonstrated ROI. Additional approval must be granted from the NRC. This report addresses only the hydrologic testing activities and results. Baseline water quality data and subsequent discussion will be submitted under a separate cover.

2.2 Report Organization

This report includes nine sections. Subsurface geology and site stratigraphy are discussed in **Section 3**. Section 4 presents historical pumping test results. Information related to the monitor well locations and completions is included in **Section 5**. Data Collection and Field Procedures are presented in **Section 6**. Test results and analytical procedures are presented in **Section 7**. Conclusions and references are included in **Sections 8 and 9**, respectively.



3. **GENERAL SITE STRATIGRAPHY**

The subsurface stratigraphy of the Marsland Expansion Area is based on preliminary test hole drilling conducted at the Marsland property and correlation of regional geologic formations observed at the current Class III permit area and proposed expansion areas. A generalized stratigraphic section and well completion intervals for the Marsland Expansion Area is provided in **Table 1**. A cross-section location map is provided in Figure 2. Geologic cross-sections are included in Figures 3 through 8. Structure contour maps of the top of the Basal Chadron Sandstone and underlying Pierre Shale are included in Figures 9 and 10, respectively. Isopach maps depicting the thickness of the Basal Chadron Sandstone and overlying Upper/Middle Chadron confining unit are included in Figures 11 and 12, respectively.

Ore-grade uranium deposits underlying the Marsland Expansion Area are located in the Basal Chadron Sandstone, which averages 50 feet in thickness (typically 40 feet net sand) and occurs at depths ranging from 900 to more than 1,100 feet below ground surface. Ore-grade deposits are generally located along a northwest-southeast trend in the Basal Chadron Sandstone. The width of the mineralized zone is generally less than 1,500 feet along this trend. Ore-grade deposits are located primarily in the lower portion of the Sandstone, although ore-grade deposits may occur locally throughout the section. Based on drilling to date, the highest concentration of mineralization is located in the north, northcentral, and southern portion of the expansion area.

The Basal Chadron Sandstone does not contain distinct clay layers that can be correlated over significant distances, and therefore represents a single sand "package" with some interbedded clay lenses. The Upper/Middle Chadron Formation (confining unit), consisting primarily of clay, claystone and siltstone, and separates the Basal Chadron Sandstone from the overlying Brule Formation. The Upper/Middle Chadron confining unit is approximately 700 feet thick in the Marsland Expansion Area. The overlying Brule Formation consists primarily of interbedded siltstone and clayey sandstone and is approximately 150 feet thick in the Marsland Expansion Area. The Brule Formation is overlain locally by the Arikaree Formation, a calcareous sandstone with interbedded siltstone and claystone generally less than 150 feet thick in the Text updated to 350-550 feet thick UM Chadron Confinement Marsland Expansion Area.

No significant sands have been identified within the Upper/Middle Chadron Formation that can be over any significant distance. Hence, wells installed in the overlying Brule Formation were monit overlying aguifers during the pumping test.



4. SUMMARY OF HISTORICAL TESTING RESULTS

During the initial permitting and development of the Crow Butte mine, four pumping tests (referred to as Tests #1 though #4) were performed in the current UIC Permit (NE0122611) area. The tests were performed to: 1) confirm confinement of the ore-bearing aquifer, and 2) assess the hydraulic characteristics of the Basal Chadron Sandstone. Three additional pumping tests (#5 though #7) were performed to characterize the Basal Chadron Sandstone in the North Trend and Three Crow expansion areas. **Table 2** summarizes historical testing results.

Results of previous testing indicate the Basal Chadron Sandstone is relatively homogeneous and isotropic within the current Class III UIC permit area (e.g. the hydraulic conductivity is reasonably uniform with respect to location and direction), although higher values of hydraulic conductivity (permeability) are observed in the southern portion of the Class III UIC permit area (Test #4).

In the Three Crow area, values of hydraulic conductivity, transmissivity, and storage are similar to the permitted Class III UIC area, although the Basal Chadron Sandstone at Three Crow is divided locally into Upper and Lower Basal Sand units. The stratigraphy of the Basal Chadron Sandstone in the North Trend area is more complex and anisotropic than observed at other test locations.

In addition to the aforementioned historical pumping tests, a failed pumping test was undertaken in the Marsland Expansion Area on November 18, 2010. The pumping test was terminated after only 19 hours of operation due to pump failure. Although data collected as part of the failed pumping test was not formally analyzed, information gained from the failed test was used to modify the Pumping Test Plan for the subsequent successful test described herein.



5. MONITORING WELL LOCATIONS, INSTALLATION AND COMPLETION

As part of the Marsland Pumping Test #8, Cameco Resources installed seven new wells in the Basal Chadron Sandstone (CPW-1, CPW-1A, Monitor-4A, Monitor-5 through Monitor-8) and redeveloped two existing wells (Monitor-2 and Monitor-3). Of these wells, only the pumped well (CPW-1A) and Monitor-3 through Monitor-7 were included in the formal Basal Chadron Sandstone observation well network. Cameco also installed three new wells in the overlying Brule Formation (BOW-1 through BOW-3). The pumping and observation wells are located in Sections 1, 2, and 12 of Township 29 North, Range 51 West, and Section 18 of Township 29 North, Range 50 West (**Figure 1**).

Because the underlying Pierre Shale is over 1,500 feet thick, no underlying monitoring wells were warranted. The depth to water in the Basal Chadron Sandstone is approximately 450 feet bgs.

Table 3 summarizes well construction details for all test wells and **Figure 13** illustrates the locations of these wells. **Appendix A** includes the NDEQ well completion reports. The nature and thickness of the subsurface formations encountered during the installation of monitoring wells is representative of the stratigraphic section presented in **Table 1**. Monitoring wells were located at various distances and directions from the pumping well (CPW-1A) such that sufficient drawdown would be observed to allow hydraulic properties of the Basal Chadron Sandstone to be determined over the entire test area.



6. FIELD PROCEDURES AND DATA COLLECTION

The following tasks were accomplished as part of the pumping test field data collection program:

- Installation of In-Situ brand Level TROLL[®] data loggers (vented) into the observation wells and pumping well to record changes in water levels during the test;
- Measurement of baseline (pre-test) water levels and barometric pressure for a period of at least one week prior to the test;
- Periodic measurement of the pumping rate from the pumping well, and
- Collection of water level and barometric pressure data throughout the background, pumping, and recovery periods.

6.1 Pumping Test Equipment

Marsland Pumping Test #8 was performed using a 4-inch diameter 10 horsepower electrical submersible pump powered by a portable generator. The pump was set in well CPW-1A at an approximate depth of 600 feet, or 150 feet below the static water level. Flow from the pump was controlled with a manual valve and surface flow measured with two flow/totalizer meters. Per NDEQ direction, discharge water was collected in FRAC tanks and trucked to the Crow Butte facility for disposal.

Water levels in the observation wells and the pumping well were measured and recorded with dedicated In-Situ brand Level TROLL® 500 and Level Troll® 700-series pressure transducers/data loggers equipped with vented cables (for barometric pressure compensation). The data loggers were programmed to automatically calibrate prior to the test, record an initial reference water level elevation (head), and measure and record water levels according to programmed linear time schedules. The pressure rating for the transducers ranged from 30 pounds per square inch (PSI) in the observation wells to 100 pounds PSI in the pumping well. A separate barometric pressure transducer/data logger was deployed near the pumping well in the center of the test area. **Table 4** summarizes the PSI range and model for each transducer deployed at the Site.

6.2 Data Collection

To assess pre-test baseline water level fluctuations, water level data and barometric pressure data were recorded prior to the pumping period (pre-test period). Pre-test baseline monitoring was initiated on May 6, 2011 and ran for a period of 7 days before initiating the pumping test.

All pressure transducers were programmed to record water levels every 4 minutes during the pre-test, pumping, and recovery periods with the exception of observation well CPW-1 and pumping well CPW-1A. These wells were programmed using an event schedule. The transducers checked the water level in these wells every 30 seconds and if the water level in CPW-1 changed by 0.1 feet a reading was recorded and if the water level in CPW-1A changed by 0.5 feet a reading was recorded otherwise readings were recorded every 4 minutes. **Table 4** summarizes the logging interval for each transducer deployed at the Site.

The pumping test was started at 05:00 hours on May 16, 2011 and was terminated at 12:00 hours on May 20, 2011. The total length of the test was 4.29 days. As shown in **Table 5** the average discharge rate was 27.08 gallons per minute (gpm).



6.3 Water Management

Pumped water was collected in on-site FRAC tanks and transported to the Crow Butte facility evaporation ponds for disposal. Approximately 167,300 gallons of groundwater was collected and disposed over the 4.29 day pumping period.



7. TEST RESULTS

7.1 Potentiometric Surface

Figure 14 presents the potentiometric surface for the Basal Chadron Sandstone aquifer based on the monitoring wells installed within the Marsland Expansion Area. Water levels were measured and recorded on November 12, 2010 and are summarized in **Table 6**. The pumping well for the test (CPW-1A) was installed after these measurements were recorded and is therefore not included in the data set presented in **Figure 14** and **Table 6**. The data are considered representative of static conditions within this aquifer. Based on these data, groundwater in the Basal Chadron Sandstone flows predominantly to the northwest toward the White River drainage at a lateral hydraulic gradient of 0.0004 ft/ft (slope of the potentiometric surface).

Figure 15 presents the potentiometric surface for the overlying Brule Formation aquifer based on monitoring wells installed within the Marsland Expansion Area. Water levels were measured and recorded on November 12, 2010 and are summarized in **Table 6**. All wells measured were utilized as observation wells during the test. The data are considered representative of static conditions within this aquifer. Based on these data, groundwater in this aquifer flows predominantly to the southeast toward the Niobrara River drainage at a lateral hydraulic gradient of 0.011 ft/ft.

7.2 Pre-Test Baseline Trends

As discussed in **Section 6.2**, water level data were collected for a period of approximately 7 days prior to the start of the pumping test. Graphs of the pre-test, pumping and recovery water level data and barometric pressure data vs. time are included in **Appendix B (Graphs B1** through **B12)**. Water levels were variable and did respond slightly to barometric fluctuations but were generally stable (+/- 0.9 feet) prior to the test in both the Basal Chadron Sandstone and Brule Formation aquifers.

7.3 Brule Formation Response (Overlying Unit)

During the test (pumping and recovery periods), no discernable drawdown or recovery response was observed in Brule observation wells. Observation wells BOW-1, BOW-2, and BOW-3 did exhibit small fluctuations in water levels during the test period; however, these fluctuations are directly related to atmospheric pressure variations and not due to drawdown from pumping, as illustrated by **Graphs B1** through **B3** in **Appendix B**.

7.4 Basal Chadron Sandstone Response (Production Zone)

Table 7 summarizes the corrected and uncorrected observed drawdown in the Basal Chadron Sandstone immediately prior to shutting off the pump. During the pumping portion of the test there was a low pressure event (cold front) that caused the observed drawdown to fluctuate by approximately 0.1 foot. **Figure 16** illustrates the drawdown immediately prior to shutting off the pump using the corrected drawdown values. With the exception of distal wells Monitor-2 and Monitor-8 (which are not part of the formal observation well network) drawdown of greater than 0.8 feet was observed in all of the observation wells, with a maximum drawdown of 23.40 feet observed in CPW-1A (pumping well).



7.5 Data Analysis

7.5.1 Analytical Methods

Drawdown data vs. time were plotted for each observation well, and based on the character of the curves it was determined that confined aquifer analytical methods were appropriate for the analysis of water level data. These methods are consistent with that proposed in the Pumping Test Workplan.

Drawdown and recovery data collected from the observation wells were graphically analyzed to determine aquifer properties including transmissivity and storativity. The methods of analysis included Theis drawdown and recovery methods (1935), and the Cooper-Jacob Distance-Drawdown method (Cooper and Jacob, 1946). The software used to graphically analyze the data was Aquifer win32 version 3 developed by Environmental Simulations, Inc.

The major assumptions inherent in the application of these analytical methods include:

- The aquifer is confined and has apparent infinite extent;
- The aquifer is homogeneous and isotropic, and of uniform effective thickness over the area influenced by pumping;
- The piezometric surface is horizontal prior to pumping;
- The well is pumped at a constant rate;
- Water removed from storage is discharged instantaneously with a decline in head;
- The pumping well is fully penetrating; and
- Well diameter is small, so well storage is negligible.

These assumptions are reasonably satisfied over the test area. Locally, the Basal Chadron Sandstone is not homogenous and isotropic; however, over the scale of the pumping test, it can be treated as such for analytical purposes.

As discussed previously, no background trend corrections were warranted; however, all of the water levels measured in the observation wells, with the exception of CPW-1 and CPW-1A, were corrected for atmospheric pressure fluctuations.

7.5.2 Barometric Pressure Correlations and Corrections

As discussed previously, all of the Level TROLL® data loggers used in the test were vented (gauged). The vent eliminates the impact of barometric pressure on the sensor; however, a change in water levels due to barometric changes will occur whether a vented sensor is used or not. Hence, use of vented equipment eliminates the barometric impact on the sensor, but does not correct the water level measurements for barometric effects on the aquifer. As such, the vented data loggers are barometrically compensated, but not corrected.



7.5.2.1. Barometric Corrections

To evaluate if corrections due to barometric fluctuations were necessary, graphs of barometric pressure and groundwater levels vs. time were prepared for all of the wells monitored during the test. These graphs include data from the pre-test, drawdown, and recovery periods and are presented in **Appendix B (Graphs B1** through **B12)**. In addition the barometric efficiency of the Basal Chadron Sandstone aquifer was estimated to better understand the relationship between a change in barometric pressure and a measurable change in groundwater levels.

The barometric efficiency is the water level change caused by a barometric pressure change divided by that barometric pressure change (Clark, 1967). In a confined aquifer like the Basal Chadron Sandstone, an increase in barometric pressure usually will cause a decrease in water level in an open well by an amount governed by the barometric efficiency (Todd, 1959; Ferris and others, 1962; Freeze and Cherry, 1979; Kruseman and de Ridder, 1991; Landmeyer, 1996; Rasmussen and Crawford, 1997; and Batu, 1998). There are several methods to estimate the barometric efficiency. For this analysis the slope method on water level and barometric pressure change was used (Ferris and others, 1962). Measurements of change in water level are plotted on the y-axis and measurements of change in barometric pressure are plotted on the x-axis. A line is fitted to the plotted points and the slope of the line is the estimate of barometric efficiency.

The barometric efficiency of the aquifer was estimated using the pre-test water level data from Monitor-3 and the Baro TROLL® as the barometric sensor was located near the Basal Chadron Sandstone observation well Monitor-3. **Figure 17** illustrates the change in barometric pressure vs. change in water level for the pre-test period. Based on the slope of the data a barometric efficiency of 0.33 or 33 percent was estimated.

During the drawdown and recovery phases of the test the atmospheric pressures were variable with both increasing and decreasing pressure events as shown by the graphs in **Appendix B**. All of the Basal Chadron Sandstone observation wells appear to demonstrate a small but discernable barometric water level response during the test (up to 0.3 feet of barometric water level variation over the entire test period). As a conservative measure, barometric water level corrections were made for all Basal Chadron Sandstone wells except the pumped well (CPW-1A) and the closest observation well (CPW-1), which experienced large drawdowns (greater than 6 feet) relative to much smaller barometric fluctuations (making corrections unnecessary in these wells). As shown in the graphs in **Appendix B**, barometric corrections did not significantly affect the data but did smooth water level trends during low and high pressure events. These transducers were set to log based on an event schedule as discussed in **Section 6.2**.

7.6 Analytical Test Results

Appendix C includes the type curve matches for the drawdown and recovery data. Water level data for all wells monitored, including the pre-test, pumping, and recovery phases of the test, are included in **Appendix D** on a CD ROM.

7.6.1 Distance Drawdown Analysis

A distance drawdown graph of the data was prepared as a preliminary estimate of transmissivity and storativity and is shown on **Figure 18**. Based on this simple analysis the average transmissivity over the area of influence is approximately 737 square feet per day (ft²/day) and the storativity is approximately 4.9E-



05. Based on an average net sand thickness of 40 feet, the average hydraulic conductivity over the area of influence is approximately 18.4 feet per day (ft/day)

7.6.2 Theis Drawdown Analysis

Transmissivity was calculated for all wells except for the pumping well using the Theis (1935) method for drawdown analysis in a confined aquifer. Type curve matches for the drawdown data are included in **Appendix C, Graphs C-1** through **C-8**. Type curve matching generally focused on late-time drawdown data since this data normally considered the most reliable indicator of overall aquifer response. Type curve matching for wells CPW-1A, CPW-1, and Monitor-3 focused on middle-time data for the drawdown phase of test due to the presence of a higher permeability boundary condition apparent in the late-time data for these wells. Log-log plots of drawdown data for wells CPW-1A, CPW-1, Monitor-3, and Monitor 5 are shown in **Figure 19**. The drawdown data for wells CPW-1A, CPW-1, and Monitor-3 show a late-time flattening of the curve (indicative of higher permeability boundary condition), whereas the drawdown data for Monitor-5 (and all other distant observation wells) exhibited a more typical confined aquifer drawdown response. Aquifer storativity ranged from 1.7E-03 to 8.32E-05, with an average value of 2.56E-04 for the entire test area (geometric mean of all values).

The flattening of the drawdown curve in wells located in the immediate vicinity of the pumping well (including wells CPW-1A, CPW-1, and Monitor-3) is believed to be related to a transmissivity contrast between lower permeability aquifer materials near the pumped well location, and higher permeability aquifer materials elsewhere within the radius of influence of the test. As illustrated by the structure contour and isopach maps of the Basal Chadron Sandstone (Figures 10 and 11), the pumping test area is located within a northwest trending ancient river channel system (paleochannel) incised into the underlying Pierre Shale. Coarsegrained sands and some gravel are present in drill cuttings and core in exploration boreholes installed west of the test area, as well as more localized areas north and south of the pumped well location (e.g. area between Monitor-2 and Monitor-6) (Mike Brost, Cameco Geologist, personal communication). This permeability contrast is believed to be responsible for the majority of the observed higher transmissivity boundary condition. In addition to the observed permeability contrast, the thickness of the Basal Chadron Sandstone increases to the west of the pumped well location (Figure 11), likely resulting in an incremental increase in transmissivity. As shown in Table 8, these observations are supported by higher transmissivity and hydraulic conductivity in more distant observation well locations.

Transmissivities calculated from the drawdown data ranged from 230 ft²/day at Monitor-3 to 1780 ft²/day in Monitor-2, with an average transmissivity of 892 ft²/day for the entire test area. Based on an average net sand thickness of 40 feet throughout the pumping test area, hydraulic conductivities ranged from 6 to 45 ft/day, with an average hydraulic conductivity of 22 ft/day for the entire test area. Transmissivity and hydraulic conductivity in the vicinity of the pumped well (including wells CPW-1A, CPW-1, and Monitor 3) were approximately 3 to 8 times lower than transmissivity measured elsewhere within the test area.

7.6.3 Theis Recovery Analysis

Transmissivity was calculated using the Theis (1935) Recovery method for all wells monitored during the test. Type curve matching of the recovery data generally focused on late-time data. However, type curve matching for wells CPW-1A, CPW-1, and Monitor-3 focused on middle-time data as a higher permeability

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boundary condition was apparent in the late-time data. The flattening of the recovery curve was also observed in the drawdown data, as discussed in the preceding section (Section 7.6.2). Type curve matches for the recovery data are included in **Appendix C**, **Graphs C9** through **C17**.

Transmissivities calculated from the recovery data ranged from 299 ft²/day at Monitor 3 to 2,470 ft²/day in Monitor 2, with an average transmissivity of 1,132 ft²/day for entire test area. Based on an average net sand thickness of 40 feet throughout the pumping test area, hydraulic conductivities ranged from 7 to 62 ft/day, with an average hydraulic conductivity of 28 ft/day for the entire test area. Transmissivity and hydraulic conductivity in the vicinity of the pumped well (including wells CPW-1A, CPW-1, and Monitor 3) were approximately 3 to 9 times lower than transmissivity measured elsewhere within the test area.

7.6.4 Summary of Analytical Results

Transmissivities calculated from the drawdown and recovery data using the Theis (1935) and Theis (1935) Recovery methods ranged from 230 ft²/day to 2,469 ft²/day with an representative average value of 1,012 ft²/day over the test area. The transmissivities for the recovery data were slightly higher than the drawdown data and are considered more representative of the aquifer properties because of the slight variability in the discharge rate during drawdown phase of the test. Based on average net sand thickness of 40 feet, the representative average hydraulic conductivity of the Basal Chadron Sandstone is 25 ft/day. Hydraulic conductivities and transmissivity of the aquifer in the vicinity of wells CPW-1A, CPW-1, and Monitor-3 were approximately 3 to 9 times less than those calculated elsewhere in the test area. The storativity calculated from the drawdown data ranged from 1.7E-03 to 8.32E-05 with an average value of 2.56E-04 for the entire test area.

7.7 Transmissivity Distribution

An isopach of the Basal Chadron Sandstone thickness and spatial distribution of transmissivity is shown on **Figure 20**. Transmissivity values calculated from the recovery data were plotted on the map. In general, higher transmissivities are in areas of thicker sand. However, as discussed previously, lower transmissivities and corresponding lower hydraulic conductivities are present in the vicinity of the pumping well, CPW-1 and Monitor 3. The circular nature of the drawdown cone (**Figure 16**) suggests no significant anisotropic qualities (e.g. directional transmissivity) to the aquifer on a regional scale.

7.8 Radius of Influence (ROI)

Based on the drawdown response of 0.86 feet in distant observation well Monitor-7 (located approximately 6,200 feet south of the pumping well), the ROI of the test was in excess of 6,200 feet. Although not included in the formal test monitoring network, data collected from the most distant observation wells (Monitor-2 and Monitor 8) clearly identify drawdown in excess of 0.4 feet due to pumping, and these data are of sufficient quality to reliably determine aquifer parameters at these locations. Therefore, based on the data collected from Monitor-2 and Monitor-8, the ROI for the test is slightly greater than 8,800 feet.



8. SUMMARY AND CONCLUSIONS

The following are significant results and conclusions of this work:

- The pumping well and all Basal Chadron observation wells exhibited significant and predictable drawdown during the test, demonstrating that the production zone has hydraulic continuity throughout the test area.
- The average transmissivity of the Basal Chadron Sandstone within the Marsland Expansion Area investigated herein is significantly higher than the existing Class III UIC Permit Area and the Three Crow and North Trend Expansion Areas.
- A zone of lower permeability (although not abnormally low by regional standards) is apparent in the
 vicinity of the pumping well (CPW-1A) and observation wells CPW-1 and Monitor-3, with significantly
 higher transmissivity noted elsewhere within the radius of influence of the test.
- Adequate confinement exists between the overlying Brule Formation and the Basal Chadron production zone as evidenced by no discernable drawdown in Brule Formation observation wells.
- The hydrologic properties of the Basal Chadron Sandstone have been adequately characterized to proceed with Class III UIC permitting and a NRC License Amendment Application for the Marsland Expansion Area.



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Tables

Hydrogeology, Water Resources & Data Services

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TABLE 1
GENERALIZED STRATIGRAPHIC SECTION, MARSLAND EXPANSION AREA

Depth (feet bgs)	Geologic Description
0 – 25	Topsoil and alluvial deposits
25 - 150	Arikaree Formation – calcareous sandstone, siltstone and claystone (no wells)
150 - 550	Brule Formation – interbedded siltstone and clayey sandstone (BOW wells)
550 - 1,000	Upper/Middle Chadron Formation – siltstone and claystone confining unit (no wells)
1,000 - 1,050	Basal Chadron Sandstone – CPW and Monitor wells
1,050+	Pierre Shale (no wells)

Note:

1.bgs = below ground surface

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TABLE 2
PREVIOUS TESTING RESULTS, BASAL CHADRON SANDSTONE

Parameter	Class III Permit Area Tests #1 - #3 (mean)	Class III Permit Area Test #4 (south) (mean)	North Trend Tests #5 and #6 (mean)	Three Crow Test # 7 (mean)
Transmissivity (ft²/day)	363	826	60	480
Hydraulic Conductivity (ft/day)	9.3	20.6	2.3	7.5
Storativity	9.7 x 10 ⁻⁵	6.2 x 10 ⁻⁵	5.3 x 10 ⁻⁵	8.8 x 10 ⁻⁵

Note:

- 1. ft²/day = square feet per day
- 2. ft/day = feet per day

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TABLE 3
MARSLAND PUMING TEST #8 WELL COMPLETION DETAILS

Well ID	Northing (ft)	Easting (ft)	Section	Twp/Rng	TOC Elevation (feet amsl)	Total Depth (feet bgs)	Well Diameter (OD) (Inches)	Screen Slot Size (inches)	Top of Screen (feet bgs)	Bottom of Screen (feet bgs)	(feet bas)	Screen Length (feet)
Basal Chadron Sandstone Pumping Well												
CPW-1A	446202	1121450	1	T29N/R51W	4262.7	1,055	4.95	0.015	1022	1052	1022-1052	30
					Basa	al Chadron Sar	ndstone Observation	Wells				
CPW-1	446225	1121528	1	T29N/R51W	4261.85	1,070	4.95	0.020	1015	1048	1015-1048	33
Monitor-2*	439439	1126362	18	T29N/R50W	4198.40	1,027	4.95	0.020	970	1010	970-1010	40
Monitor-3	446288	1121519	1	T29N/R51W	4261.30	1,069	4.95	0.020	1016	1043	1016-1043	27
Monitor-4A	450084	1121344	1	T29N/R51W	4332.10	1,134	4.95	0.020	1088	1110	1088-1110	22
Monitor-5	447734	1119236	1	T29N/R51W	4339.50	1,120	4.95	0.020	1070	1120	1070-1120	50
Monitor-6	442856	1124385	12	T29N/R51W	4215.00	1,050	4.95	0.020	990	1023	990-1023	33
Monitor-7	440358	1120757	12	T29N/R51W	4244.38	1,050	4.95	0.020	1000	1043	1000-1013, 1023-1043	33
Monitor-8*	450974	1117005	2	T29N/R51W	4353.70	1,180	4.95	0.020	1085	1125	1085-1125	40
Brule Formation Observation Wells												
BOW-1	446250	1121572	1	T29N/R51W	4260.10	370	4.95	0.020	285	365	285-305, 325-365	60
BOW-2	450154	1121367	1	T29N/R51W	4323.40	400	4.95	0.020	339	399	339-369, 389-399	40
BOW-3	450974	1117056	2	T29N/R51W	4350.30	415	4.95	0.020	345	415	345-365, 385-415	50

Note:

- 1. * Wells Monitor-2 and Monitor-8 were monitored and analyzed as described in the original Plan, but are not part of the formal monitoring network
- 2. Twp = Township
- 3. Rng = Range
- 4. amsl = above mean sea level
- 5. OD = outer diameter
- 6. bgs = below ground surface



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TABLE 4 MONITORING EQUIPMENT LAYOUT

Well ID	Completion Sand	Monitoring Equipment	Logging Interval		
CPW-1A	Basal Chadron Sandstone	Level Troll 700 (100 PSI)	Linear Event (30 sec if water level changes by		
CFW-IA	Basai Chadron Sandstone	Level 11011 700 (100 F31)	>0.5 ft , 4 min if <0.5 ft of change		
CPW-1	Basal Chadron Sandstone	Level Troll 500 (30 PSI)	Linear Event (30 sec if water level changes by		
CF W-1	Basar Chadron Sandstone	Level 11011 300 (30 F 31)	>0.1 ft , 4 min if <0.1 ft of change		
Monitor-2	Basal Chadron Sandstone	Level Troll 500 (30 PSI)	Linear (4 min)		
Monitor-3	Basal Chadron Sandstone	Level Troll 500 (30 PSI)	Linear (4 min)		
Monitor-4A	Basal Chadron Sandstone	Level Troll 500 (30 PSI)	Linear (4 min)		
Monitor-5	Basal Chadron Sandstone	Level Troll 500 (30 PSI)	Linear (4 min)		
Monitor-6	Basal Chadron Sandstone	Level Troll 500 (30 PSI)	Linear (4 min)		
Monitor-7	Basal Chadron Sandstone	Level Troll 500 (30 PSI)	Linear (4 min)		
Monitor-8	Basal Chadron Sandstone	Level Troll 500 (30 PSI)	Linear (4 min)		
BOW-1	Brule Formation	Level Troll 500 (30 PSI)	Linear (4 min)		
BOW-2	Brule Formation	Level Troll 500 (30 PSI)	Linear (4 min)		
BOW-3	Brule Formation	Level Troll 500 (30 PSI)	Linear (4 min)		
BAR-1	Atmosphere	Baro Troll	Linear (4 min)		

Notes:

- 1. min = minute
- 2. ft = feet
- 3. PSI = pounds per square inch



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TABLE 5
PUMPING FLOW RATE VS. TIME

-		METER 1	METER 2		T	Total Gallons
Date	TIME	GPM	GPM	PSI	AMPS	(meter 1/meter 2)
5/16/2011	5:00	27.90	28.4	50	12	0/0
5/16/2011	6:00	27.10	27.9	49	12	1579/1601
5/16/2011	7:00	26.90	27.1	49	12	3138/3170
5/16/2011	8:00	26.70	27.1	45	12	4824/4880
5/16/2011	9:00	26.70	27.1	45	12	6545/6621
5/16/2011	10:00	26.90	27.1	46	12	8163/8258
5/16/2011	11:00	26.50	26.8	45	12	9720/9831
5/16/2011	12:00	26.40	26.8	46	12	11341/11481
5/16/2011	13:00	26.50	26.8	46	12	12869/13039
5/16/2011	14:00	26.40	26.9	46	12	14518/14713
5/16/2011	15:00	26.40	26.9	46	12	16255/16484
5/16/2011	16:00	26.40	26.9	46	12	17560/18000
5/16/2011	17:00	26.70	27	46	12	19337/19614
5/16/2011	18:00	26.70	27.2	46	12	20933/21240
5/16/2011	19:00	26.60	27.1	46	12	22588/22922
5/16/2011	20:00	26.70	27.3	46	12	24257/24622
5/16/2011	21:00	26.70	27.2	46	12	25814/26206
5/16/2011	22:00	26.70	27.1	46	12	27384/27806
5/16/2011	23:00	26.50	27.2	46	12	29094/29498
5/17/2011	0:00	26.90	27.3	46	12	30660/31136
5/17/2011	1:00	26.80	27.3	46	12	32286/32795
5/17/2011	2:00	26.40	27.2	46	12	33895/34431
5/17/2011	3:00	26.60	27.2	46	12	35533/36107
5/17/2011	4:00	26.70	27.1	46	12	37236/37843
5/17/2011	5:00	26.60	27.3	46	12	38781/39420
5/17/2011	6:00	26.70	27.4	46	12	40434/40997
5/17/2011	7:00	26.80	27.3	46	12	41829/42530
5/17/2011	8:00	26.79	27.25	46	13	43637/44373
5/17/2011	9:00	26.73	27.19	46	13	45229/46012
5/17/2011	10:00	26.73	27.19	46	13	46904/47733
5/17/2011	11:00	26.59	27.12	46	13	48480/49328
5/17/2011	12:00	26.66	27.06	46	13	50184/51061
5/17/2011	13:00	26.66	27.06	46	13	51735/52632
5/17/2011	14:00	26.59	27.19	46	13	53334/54270
5/17/2011	15:00	26.59	27.19	46	13	54968/55945
5/17/2011	16:00	26.53	27.12	46	13	56615/57612
5/17/2011	17:00	26.79	27.25	46	13	58180/59210
5/17/2011	18:00	26.92	27.39	46	13	59728/60788
5/17/2011	19:00	26.99	27.52	46	13	61422/62516
5/17/2011	20:00	26.92	27.58	46	13	63218/64388



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TABLE 5
PUMPING FLOW RATE VS. TIME

		METER 1	METER 2			
Date	TIME	GPM	GPM	PSI	AMPS	Total Gallons (meter 1/meter 2)
5/17/2011	21:00	26.99	27.43	46	13	64670/65839
5/17/2011	22:00	26.92	27.65	46	13	66283/67481
5/17/2011	23:00	26.94	27.45	46	13	67907/69143
5/18/2011	0:00	26.92	27.45	46	13	69508/70780
5/18/2011	1:00	27.06	27.46	46	13	71181/72490
5/18/2011	2:00	26.86	27.45	46	13	72804/74152
5/18/2011	3:00	26.79	27.39	46	13	74443/75824
5/18/2011	4:00	26.79	27.39	46	13	76053/77474
5/18/2011	5:00	26.66	27.32	46	13	77684/79137
5/18/2011	6:00	26.59	27.45	46	13	79283/80777
5/18/2011	7:00	26.46	27.32	46	13	80908/82445
5/18/2011	8:00	26.46	27.32	46	12	82532/84112
5/18/2011	9:00	27.98	27.43	46	12	84302/85927
5/18/2011	10:00	26.59	27.32	46	12	85838/87502
5/18/2011	11:00	26.66	27.32	46	12	87397/89104
5/18/2011	12:00	26.79	27.39	46	12	89019/90769
5/18/2011	13:00	26.53	27.32	46	12	90664/92458
5/18/2011	14:00	26.73	27.19	46	12	92385/94212
5/18/2011	15:00	26.59	27.32	46	12	93845/85706
5/18/2011	16:00	26.92	27.32	46	12	95537/97438
5/18/2011	17:00	26.86	27.52	46	12	97124/99061
5/18/2011	18:00	26.79	27.39	46	12	98727/100302
5/18/2011	19:00	26.79	27.52	46	12	100350/102361
5/18/2011	20:00	26.99	27.65	46	12	101944/104000
5/18/2011	21:00	26.92	27.52	46	12	103574/105667
5/18/2011	22:00	26.86	27.52	46	12	105215/107355
5/18/2011	23:00	26.99	27.58	46	12	106857/108542
5/19/2011	0:00	26.99	27.65	46	12	108521/110734
5/19/2011	1:00	26.99	27.72	46	12	110161/112415
5/19/2011	2:00	26.99	27.65	46	12	111965/114270
5/19/2011	3:00	26.94	27.72	46	12	113333/115667
5/19/2011	4:00	26.94	27.65	46	12	114978/117308
5/19/2011	5:00	26.94	27.58	46	12	116623/118951
5/19/2011	6:00	26.92	27.65	46	12	118246/120689
5/19/2011	7:00	27.06	27.72	46	12	119860/122351
5/19/2011	8:00	27.00	27.65	48	12	121626/124162
5/19/2011	9:00	27.06	27.52	48	12	123245/125826
5/19/2011	10:00	26.86	27.52	48	12	124871/127490
5/19/2011	11:00	26.92	27.58	48	12	126491/129137
5/19/2011	12:00	26.79	27.52	48	12	128125/130828
5/19/2011	13:00	26.59	27.58	48	12	129745/132498
5/19/2011	14:00	26.94	27.65	48	12	131369/134145
5/19/2011	15:00	26.92	27.45	48	12	132973/135792



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TABLE 5
PUMPING FLOW RATE VS. TIME

	i i	METER 1	METER 2			
Date	TIME	GPM	GPM	PSI	AMPS	Total Gallons (meter 1/meter 2)
5/19/2011	16:00	27.45	27.58	48	12	134606/137470
5/19/2011	17:00	26.86	27.52	48	12	136270/139168
5/19/2011	18:00	26.86	27.65	48	12	137893/140832
5/19/2011	19:00	26.79	27.58	48	12	139550/142528
5/19/2011	20:00	26.86	27.58	48	12	141176/144192
5/19/2011	21:00	26.79	27.45	48	12	142803/145861
5/19/2011	22:00	26.86	27.45	48	12	144375/147470
5/19/2011	23:00	26.46	27.58	48	12	146010/149145
5/20/2011	0:00	26.92	27.39	48	12	147643/150817
5/20/2011	1:00	26.73	27.45	48	12	149285/152499
5/20/2011	2:00	26.99	27.58	48	12	150921/154172
5/20/2011	3:00	26.92	27.52	48	12	152550/155837
5/20/2011	4:00	27.06	27.58	48	12	154176/157504
5/20/2011	5:00	26.99	27.39	48	12	155820/159188
5/20/2011	6:00	26.92	27.45	48	12	157422/160827
5/20/2011	7:00	26.79	27.52	48	12	159048/162492
5/20/2011	8:00	26.73	27.32	47	12	160710/164208
5/20/2011	9:00	26.79	27.32	46	12	162426/165960
5/20/2011	10:00	26.59	27.19	46	12	163966/167537
5/20/2011	11:00	26.46	27.12	46	12	165526/169126
5/20/2011	12:00	26.46	27.06	46	12	167215/170855
Avera	ge Flow (GPM)	26.80	27.37			
Combine	d Average Flow (GPM)	27.	.08			

Notes:

- 1. GPM = gallons per minute
- 2. Pumping started at 5:03 am on 5/16/2011 and ended at 12:00 pm on 5/20/11
- 3. PSI = pounds per square inch

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TABLE 6
GROUNDWATER LEVELS, NOVEMBER 12, 2010

Well ID	Measurement Date	Northing (feet)	Easting (feet)	TOC Elevation (feet amsl)	Depth to Water (feet btoc)	Groundwater Elevation (feet amsl)
			Basal Chadron Pu	imping Well		
CPW-1A	NM	446202	1121450	4262.70	NM	NM
			Basal Chadron Obse	ervation Wells		
CPW-1	11/12/2010	446225	1121528	4261.85	551.11	3710.75
Monitor-2	11/12/2010	439439	1126362	4198.40	484.57	3713.83
Monitor-3	11/12/2010	446288	1121519	4261.30	551.03	3710.27
Monitor-4A	11/12/2010	450084	1121344	4327.49	617.80	3709.69
Monitor-5	11/12/2010	447734	1119236	4339.50	628.45	3711.05
Monitor-6	11/12/2010	442856	1124385	4215.00	502.18	3712.83
Monitor-7	11/12/2010	440358	1120757	4244.38	530.99	3713.39
Monitor-8	11/12/2010	450974	1117005	4353.70	644.47	3709.23
			Brule Observat	ion Wells		
BOW-1	11/12/2010	446250	1121572	4260.10	126.13	4133.97
BOW-2	11/12/2010	450154	1121367	4323.40	150.37	4173.04
BOW-3	11/12/2010	450974	1117056	4350.30	137.49	4212.81

Notes:

- 1. TOC = top of casing
- 2. btoc = below top of casing
- 3. amsl = above mean sea level
- 4. NM = not measured



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TABLE 7
DISTANCES TO PUMPING WELL AND OBSERVED DRAWDOWN

Completion Type	Well ID	Distance to Pumping Well (feet)	Completion Sand	Respond to Pumping (Y/N)	Observed Drawdown at End of Pumping (5/20/2011)	Corrected Drawdown at End of Pumping (5/20/2011)
Pumping Well	CPW-1A	0	Basal Chadron Sandstone	Υ	23.40	23.50
Production Zone Observation Wells	CPW-1	67	Basal Chadron Sandstone	Υ	6.22	6.32
	Monitor-3	100	Basal Chadron Sandstone	Υ	4.79	4.89
	Monitor-5	2,800	Basal Chadron Sandstone	Υ	1.29	1.39
	Monitor-4A	4,067	Basal Chadron Sandstone	Υ	1.00	1.10
	Monitor-6	4,667	Basal Chadron Sandstone	Y	1.05	1.15
	Monitor-7	6,200	Basal Chadron Sandstone	Υ	0.76	0.86
	Monitor-8*	6,800	Basal Chadron Sandstone	Υ	0.66	0.76
	Monitor-2*	8,800	Basal Chadron Sandstone	Υ	0.32	0.42
Overlying Observation Wells	BOW-1	133	Brule Formation	N	-	-
	BOW-2	4,167	Brule Formation	N	-	
	BOW-3	6,867	Brule Formation	N	-	

Note:

^{1.*} Wells Monitor-2 and Monitor-8 were monitored and analyzed as described in the original Plan, but are not part of the formal monitoring network used to establish radius of influence.

^{2.} Pumping started at 5:03 am on 5/16/2011 and ended at 12:00 pm on 5/20/11

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Marsland Regional Hydrologic Testing Report - Test # 8

Crow Butte Project, Marsland Expansion Area

TABLE 8
SUMMARY OF TEST RESULTS

		Theis Drawdown			Theis Recovery		
Well ID	Distance to Pumping Well (feet)	Transmissivity (ft²/day)	Hydraulic Conductivity (ft/day)	Storativity	Transmissivity (ft²/day)	Hydraulic Conductivity (ft/day)	Storativity
CPW-1A**	0				573	14	
CPW-1**	67	430	11	8.32E-05	523	13	
Monitor-3	100	230	6	1.70E-03	299	7	
Monitor-5	2,800	915	23	5.50E-05	971	24	
Monitor-4A	4,067	903	23	5.41E-05	1,377	34	
Monitor-6	4,667	901	23	3.44E-05	1,063	27	
Monitor-7	6,200	983	25	3.57E-05	1,315	33	
Monitor-8*	6,800	989	25	3.95E-05	1,596	40	1844 ·
Monitor-2*	8,800	1,781	45	4.72E-05	2,469	62	-24
	Averages	892	22	7.46E-05	1,132	28	

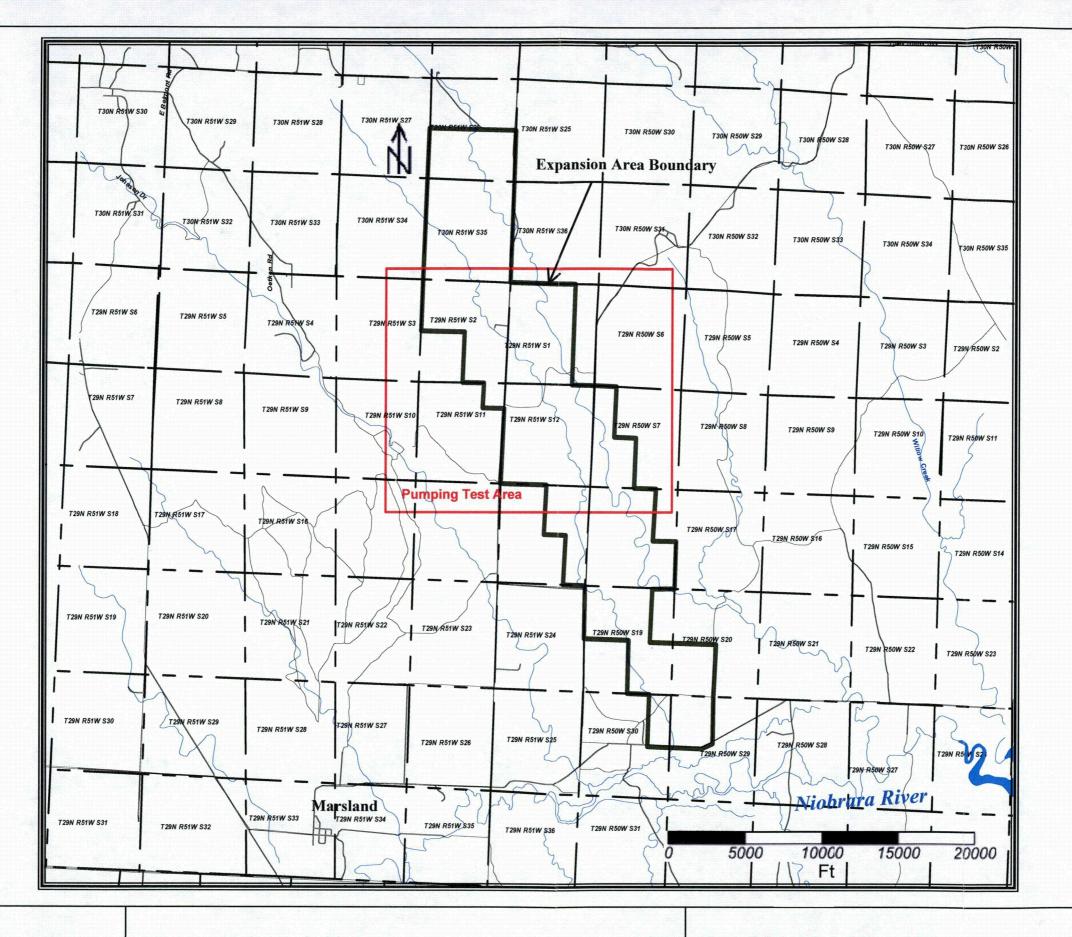
Average Transmissivit (ft²/day)	1,012
Average Hydraulic Conductivity (ft/day)	25
Average Storativity	7.46E-05

Note

- 1. * = Monitor-2 and Monitor-8 were monitored and analyzed as described in the original Plan, but are not part of the formal monitoring network
- 2. ** = Water level data for CPW-1A and CPW-1 were not corrected for barometric variations due to the large drawdowns (greater than 6 feet) relative to much smaller barometric fluctuations
- 2. Pumping started at 5:03 am on 5/16/2011 and ended at 12:00 pm on 5/20/11
- 3. Hydraulic conductivity calculated based on a typical net sand thickness of 40 feet
- 4. ft2/day = square feet per day
- 5. ft/day = feet per day
- 6. -- = not applicable



Figures

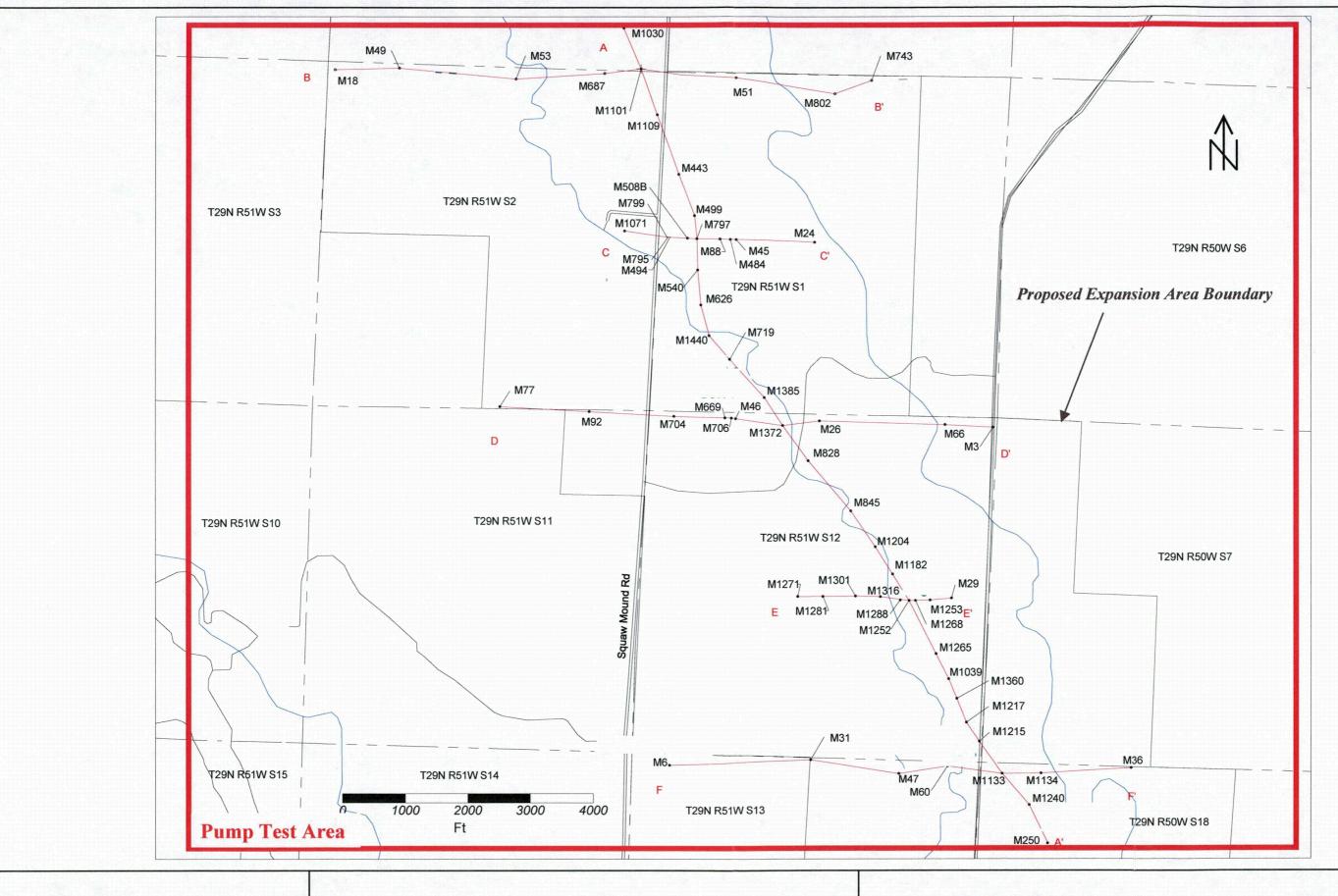


Marsland Expansion Area and Vicinity

Marsland Regional Hydrologic Testing Report – Test # 8
Crow Butte Project, Marsland Expansion Area,
Dawes County, NE



FIGURE:



Hydrogeology, Water Resources & Data Services

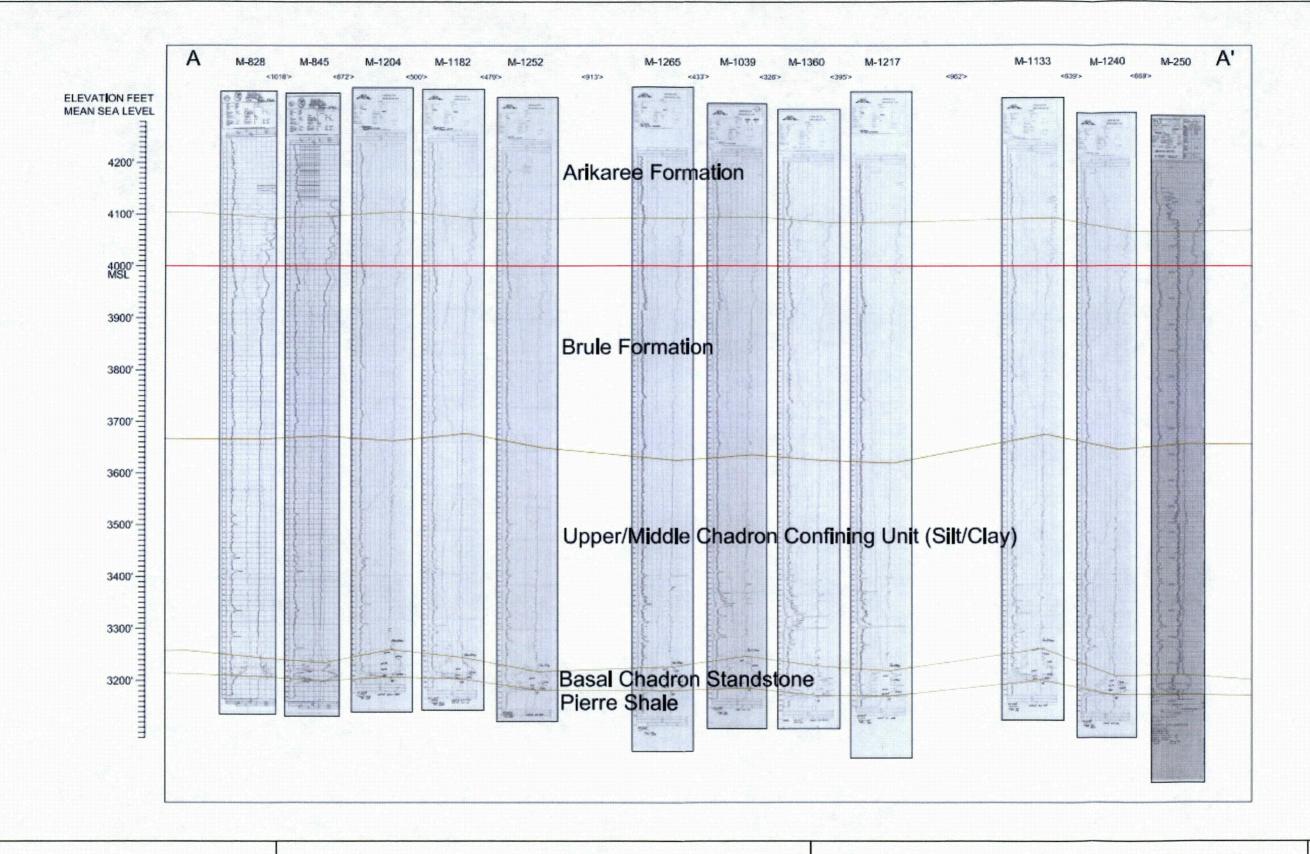
Cross-Section Location Map

Marsland Regional Hydrologic Testing Report – Test # 8
Crow Butte Project, Marsland Expansion Area,
Dawes County, NE



FIGURE:

2



Hydrogeology, Water Resources & Data Services

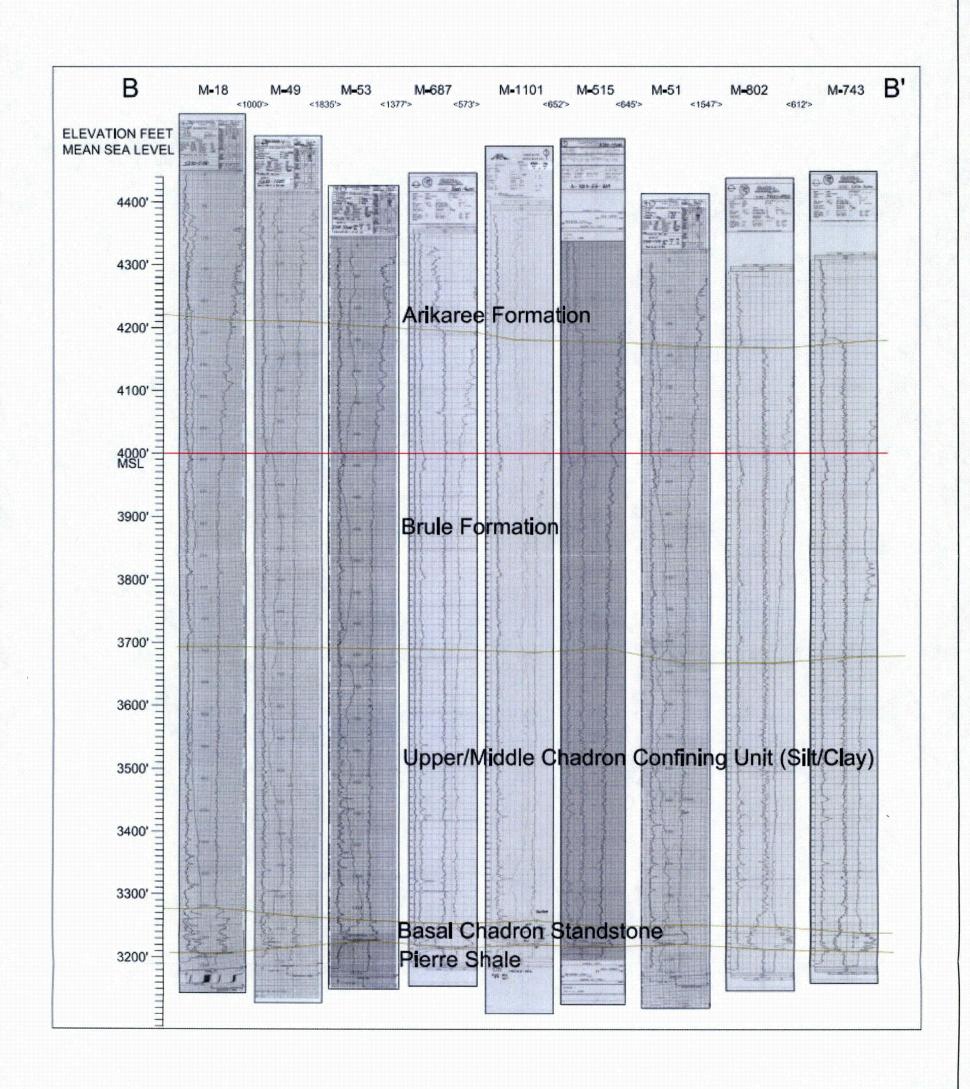
Cross-Section A-A'

Marsland Regional Hydrologic Testing Report – Test # 8
Crow Butte Project, Marsland Expansion Area,
Dawes County, NE

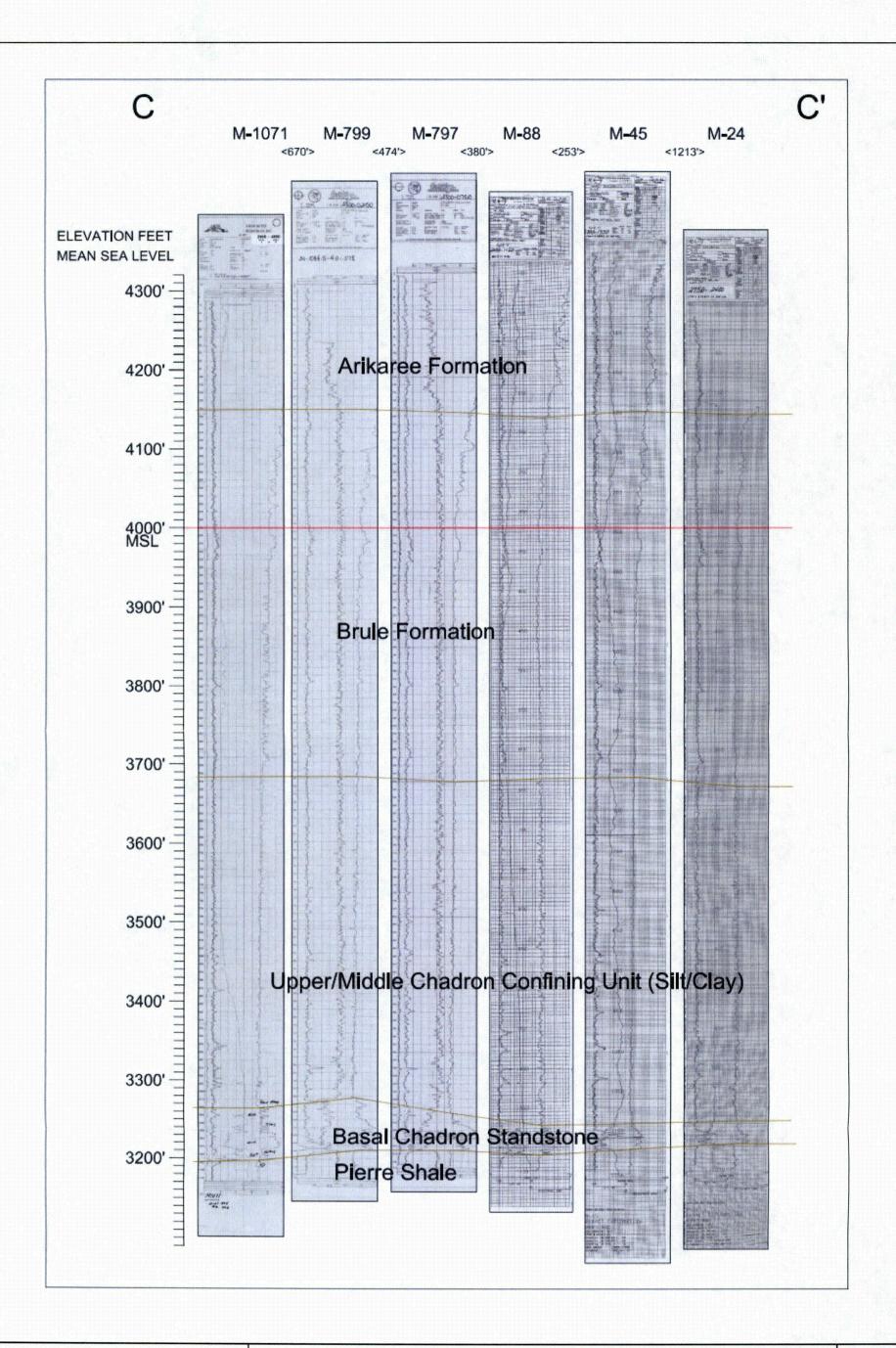


FIGURE:

3

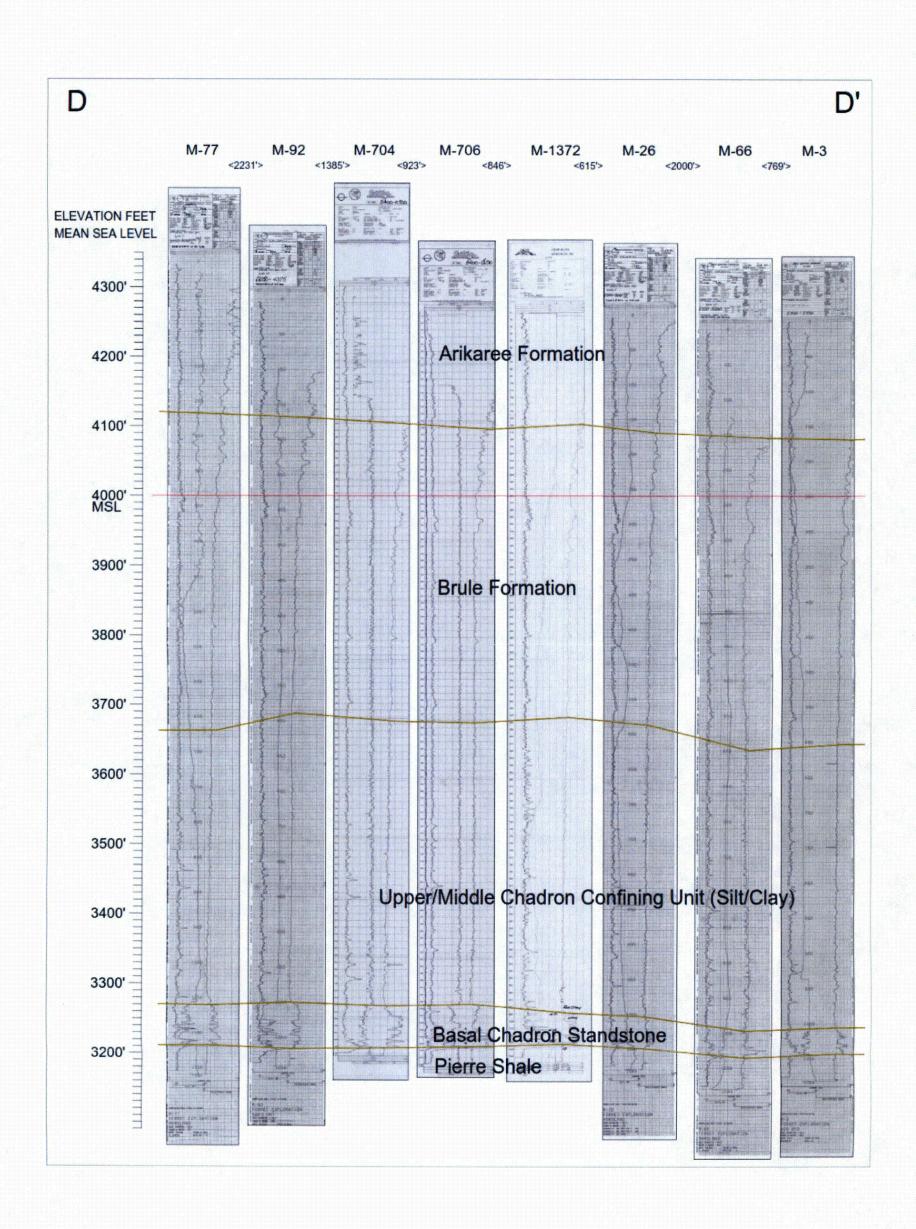




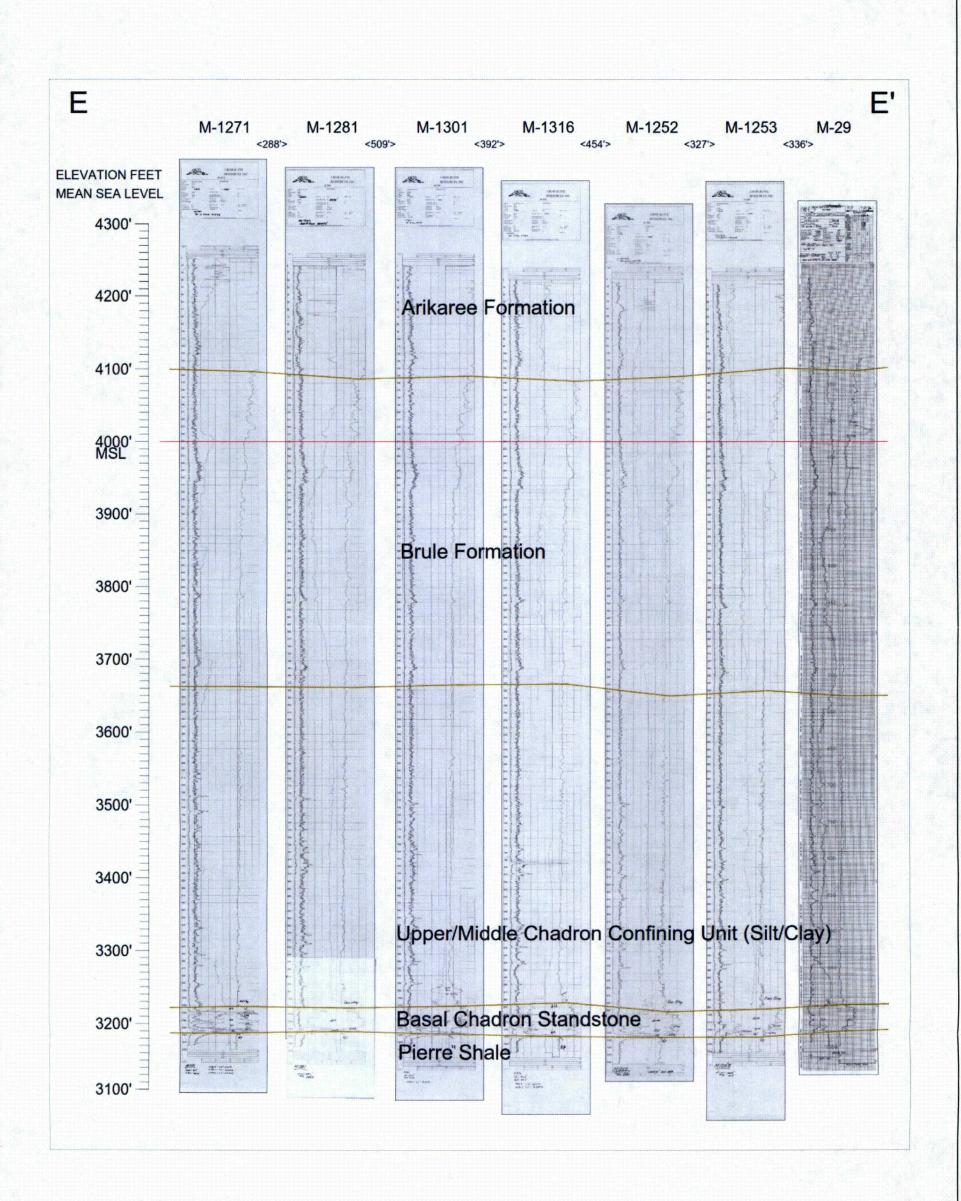




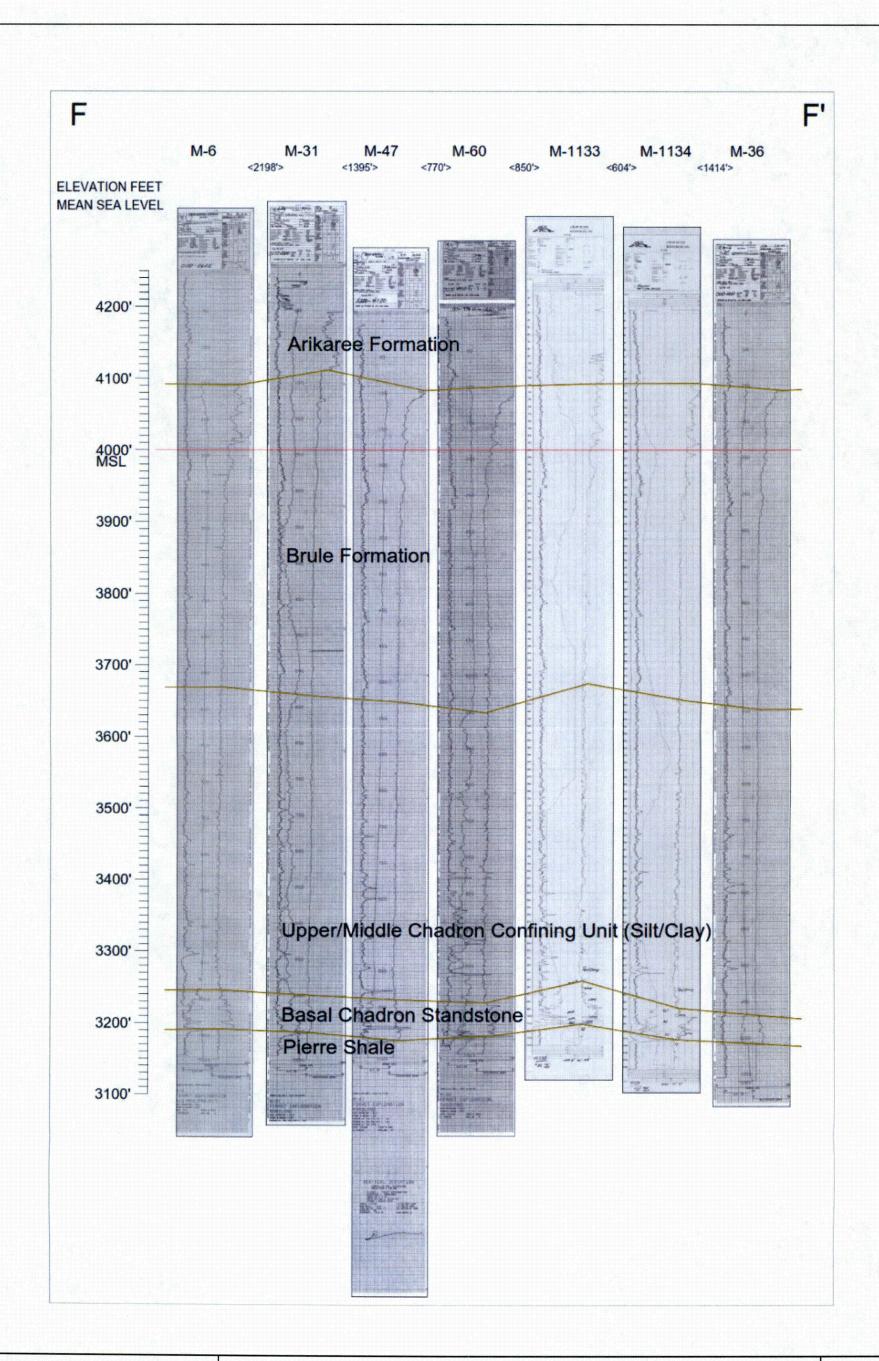




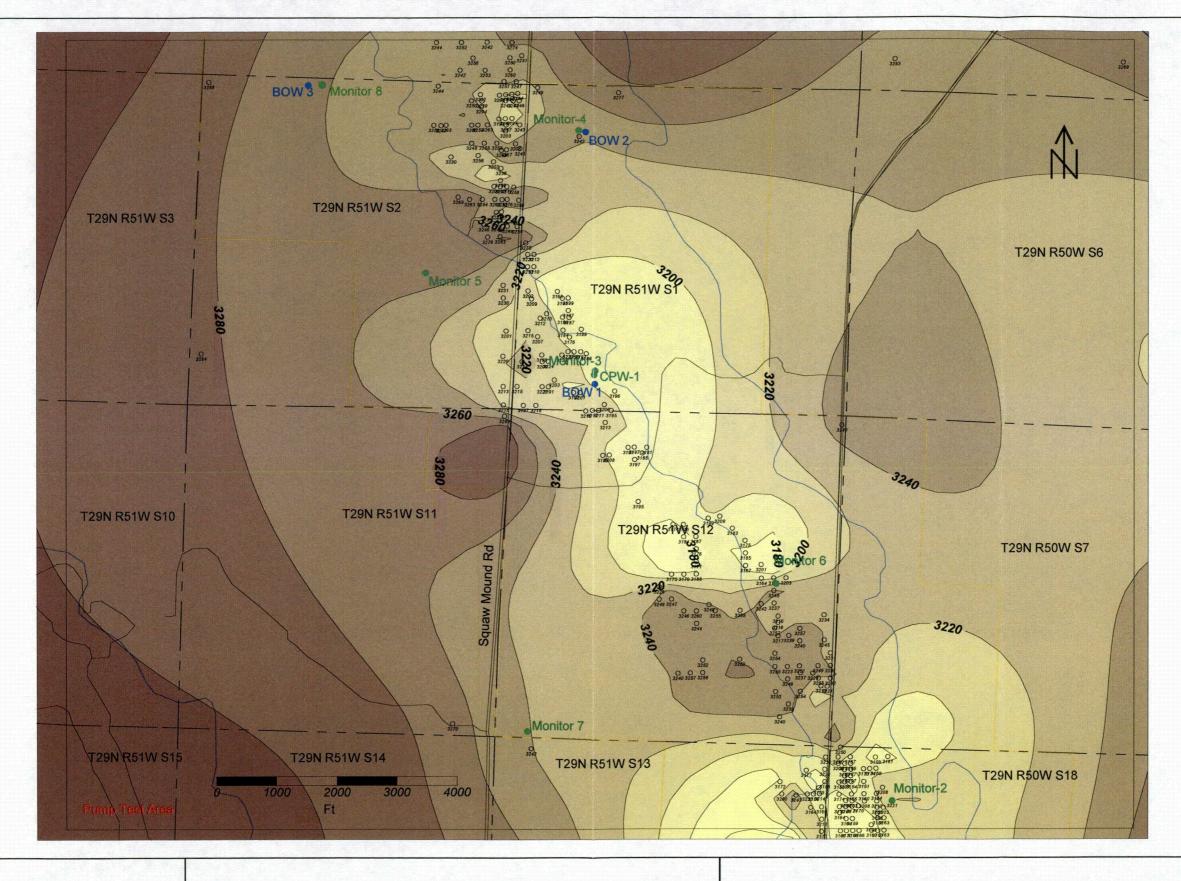




Geologic Cross Section E-E'





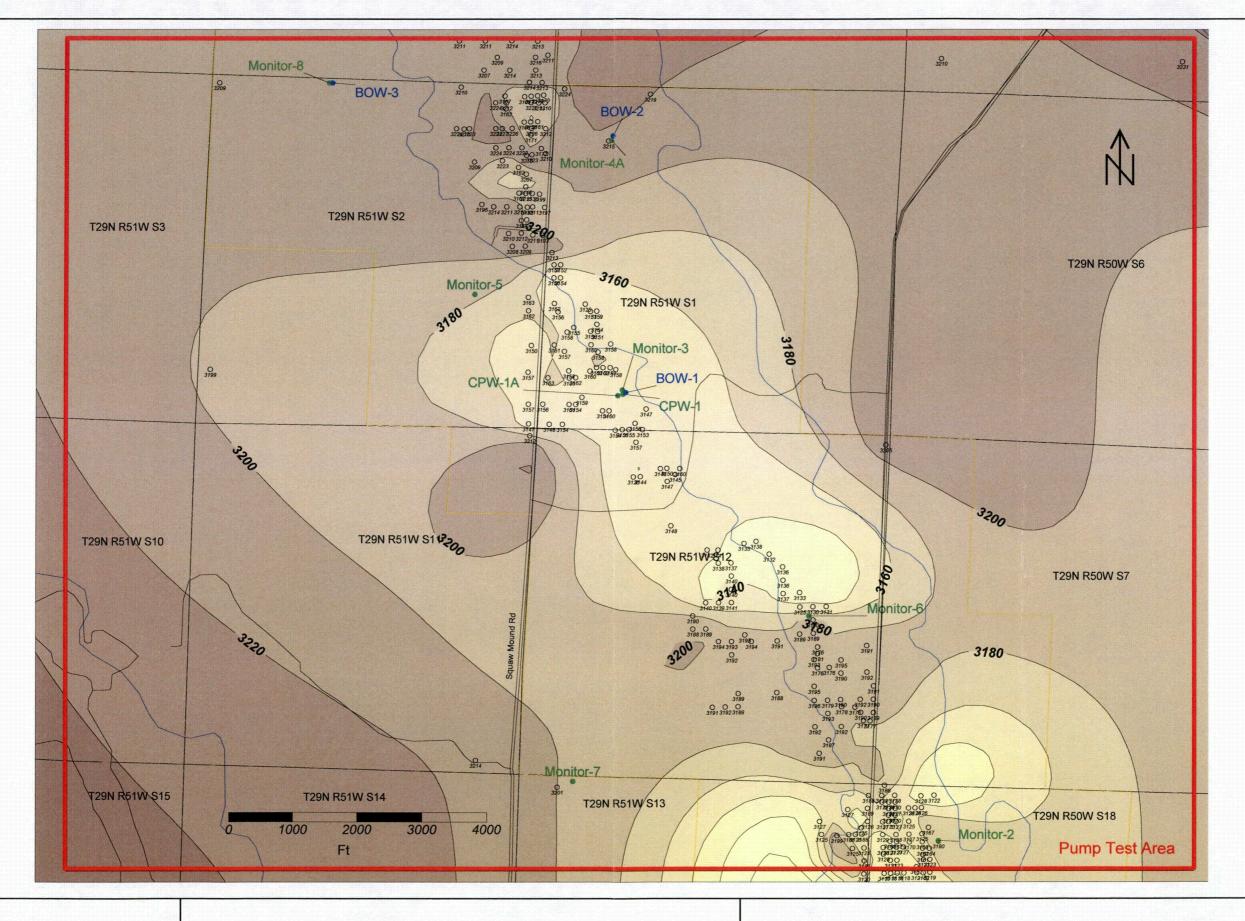


Structure Contour Map
Top of the Basal Chadron Sandstone (ft-MSL)

Marsland Regional Hydrologic Testing Report – Test # 8 Crow Butte Project, Marsland Expansion Area, Dawes County, NE



FIGURE:



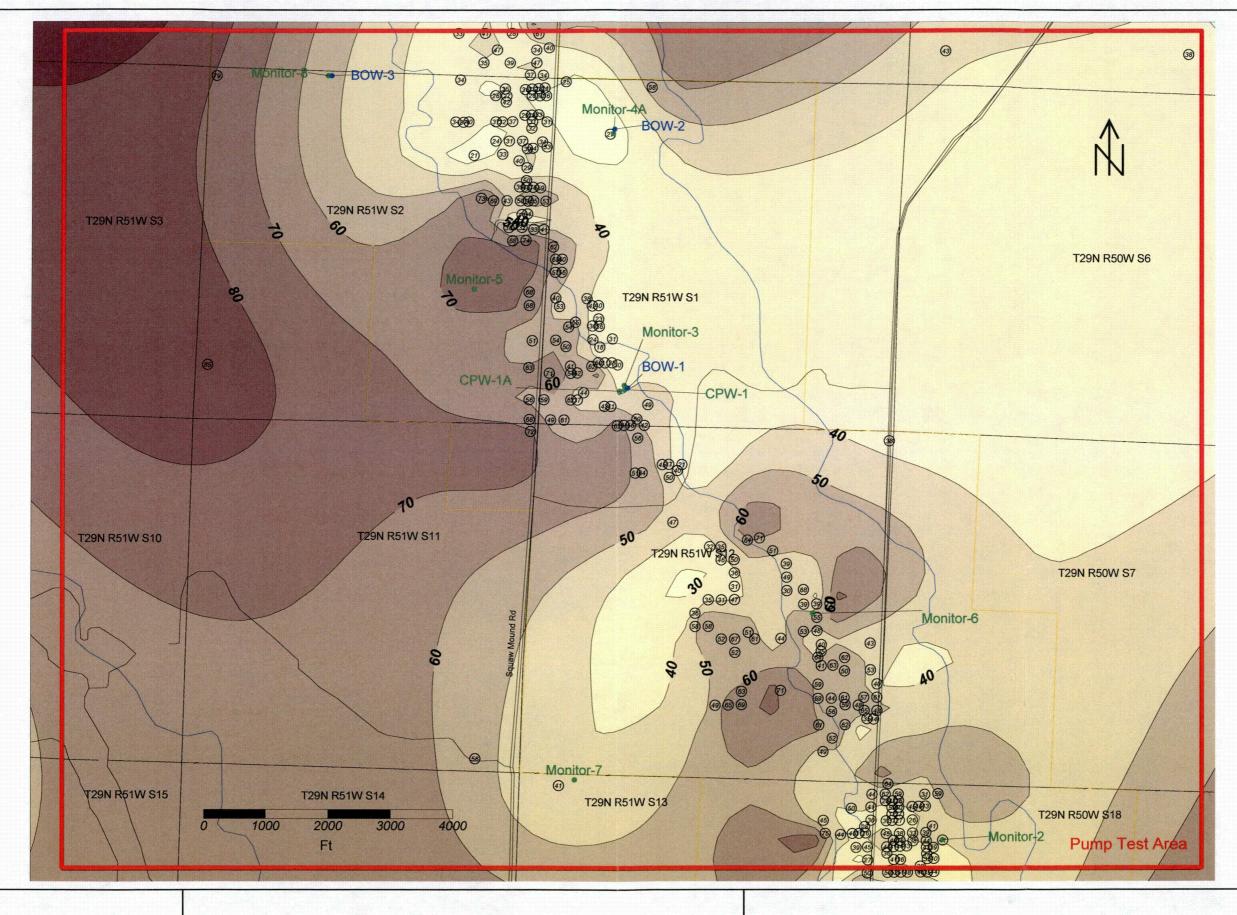
Hydrogeology, Water Resources & Data Services

Structure Contour Map
Top of the Pierre Shale (ft-MSL)

Marsland Regional Hydrologic Testing Report – Test # 8
Crow Butte Project, Marsland Expansion Area,
Dawes County, NE



FIGURE:



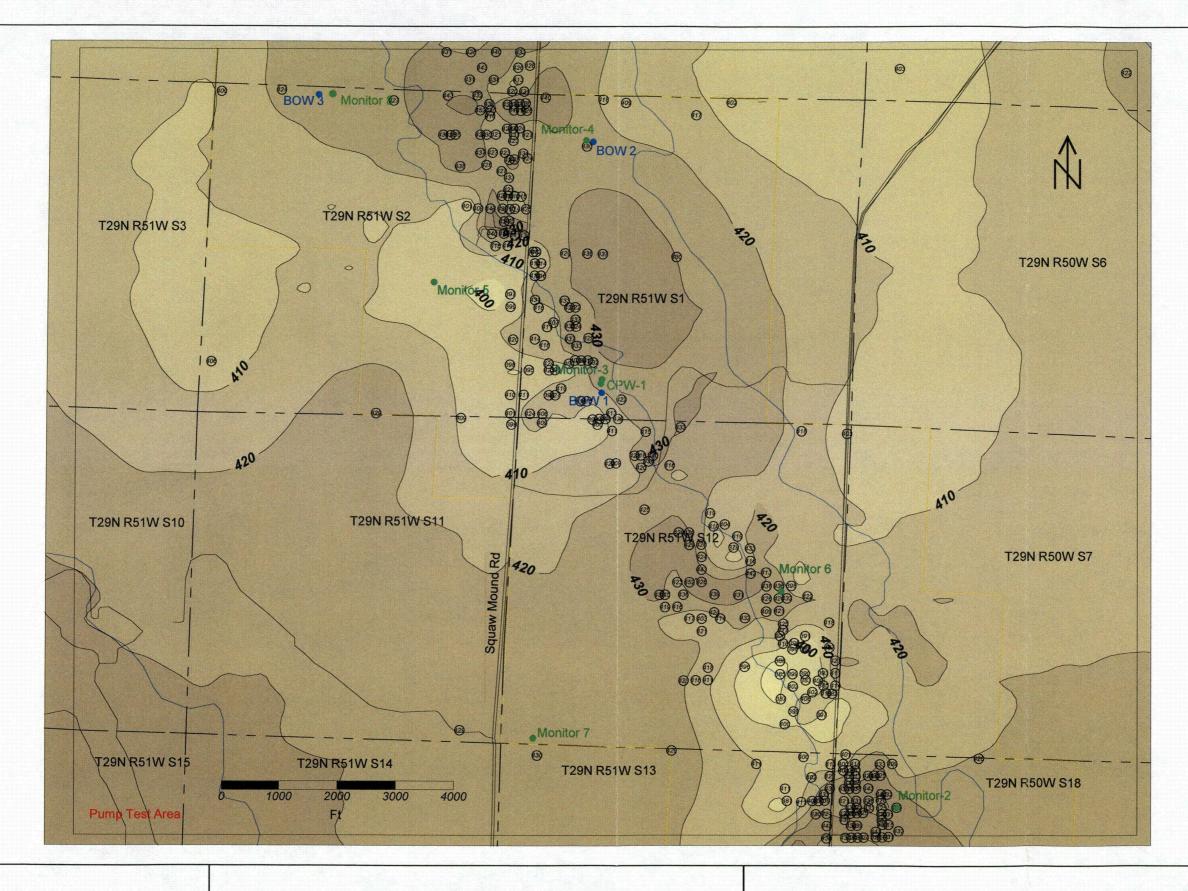
Hydrogeology, Water Resources & Data Services

Isopach (Thickness) Map
Basal Chadron Sandstone (ft-MSL)

Marsland Regional Hydrologic Testing Report – Test # 8
Crow Butte Project, Marsland Expansion Area,
Dawes County, NE



FIGURE:



AQUI-VER, INC.

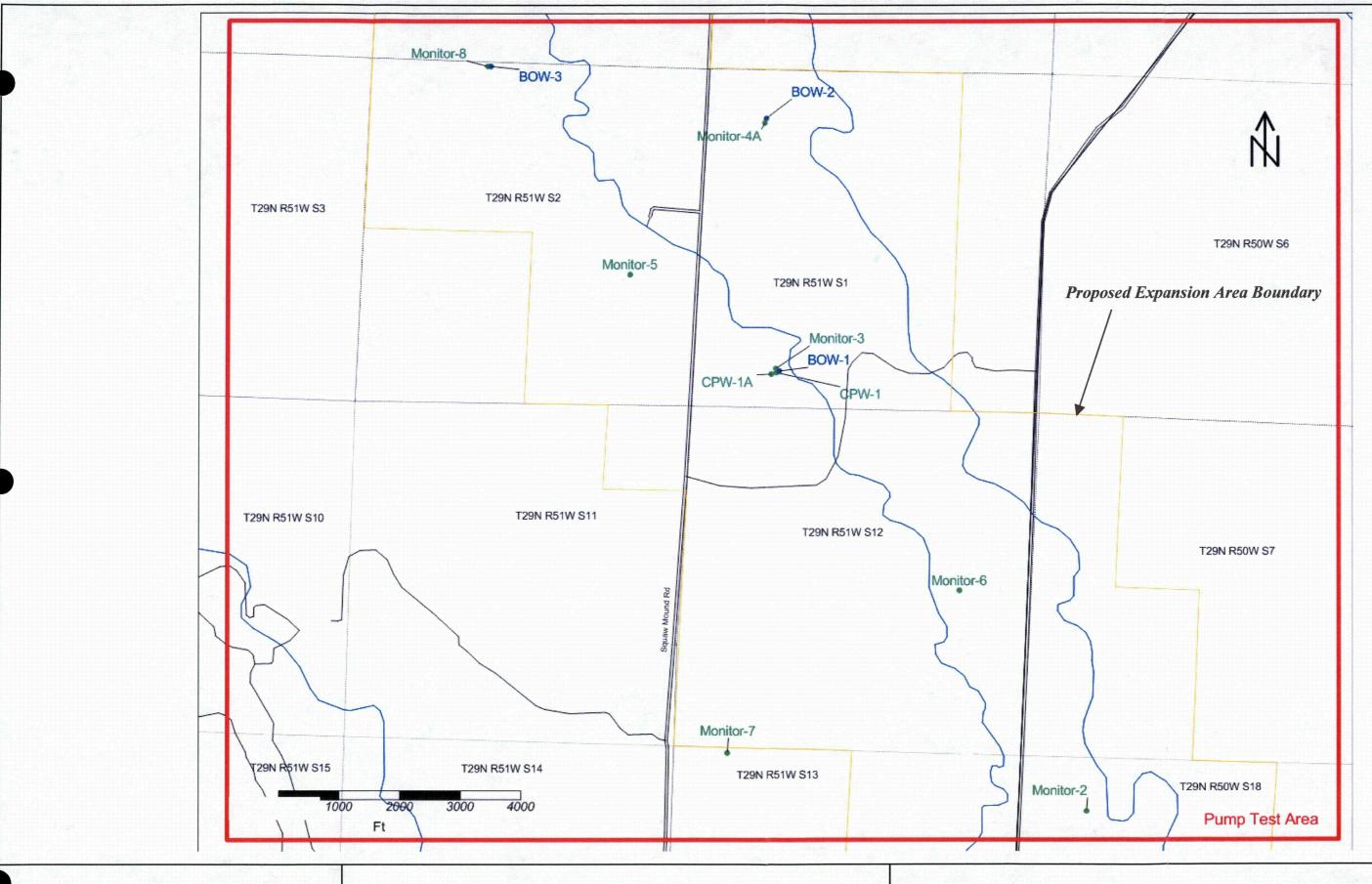
Hydrogeology, Water Resources & Data Services

Isopach (Thickness) Map
Upper/Middle Chadron Confining Unit (ft-MSL)

Marsland Regional Hydrologic Testing Report – Test # 8
Crow Butte Project, Marsland Expansion Area,
Dawes County, NE



FIGURE:



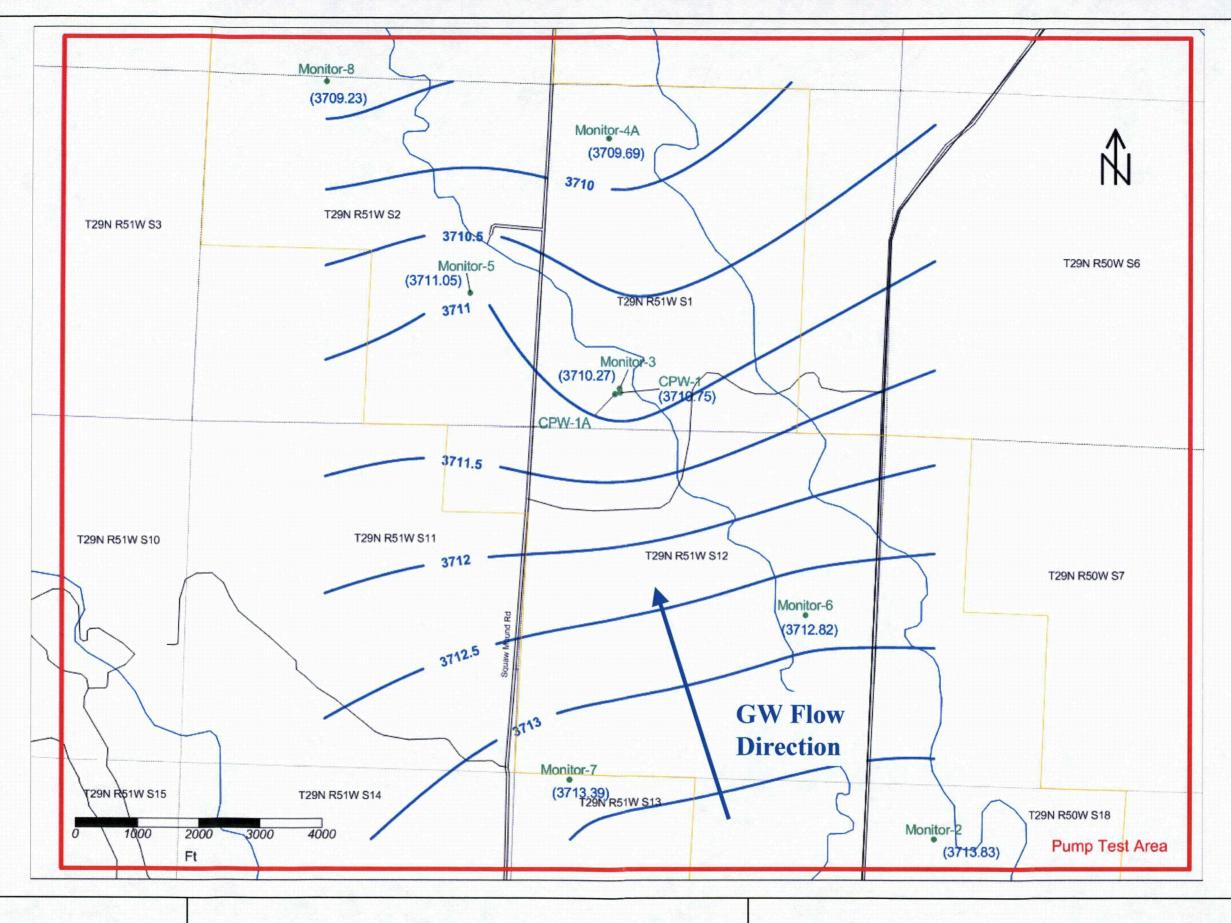
Hydrogeology, Water Resources & Data Services

Marsland Pumping Test #8 Well Locations

Marsland Regional Hydrologic Testing Report – Test # 8
Crow Butte Project, Marsland Expansion Area,
Dawes County, NE



FIGURE:

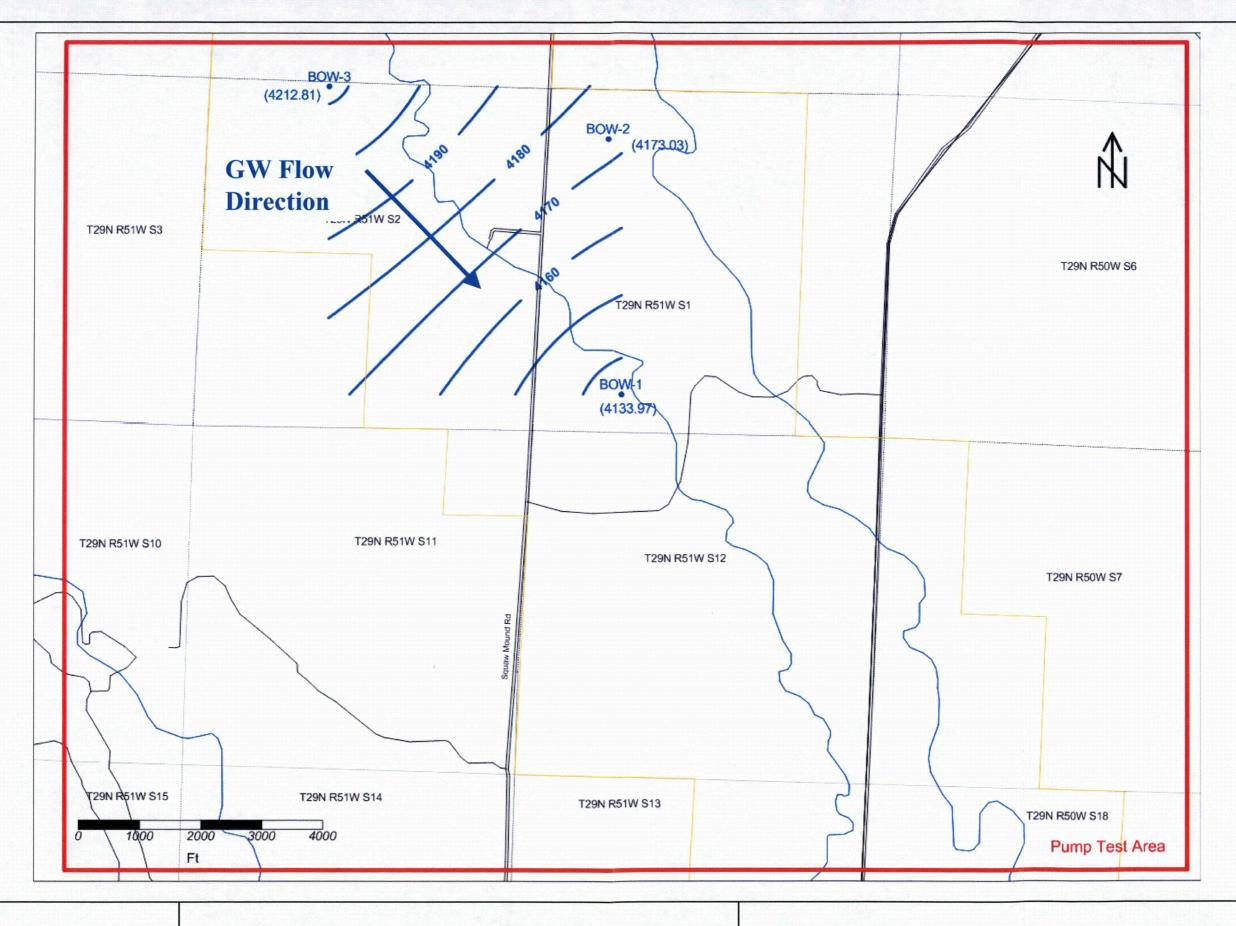


Potentiometric Surface Map – Basal Chadron Sandstone (Production Zone), November 12, 2010

Marsland Regional Hydrologic Testing Report – Test # 8
Crow Butte Project, Marsland Expansion Area,
Dawes County, NE



FIGURE:

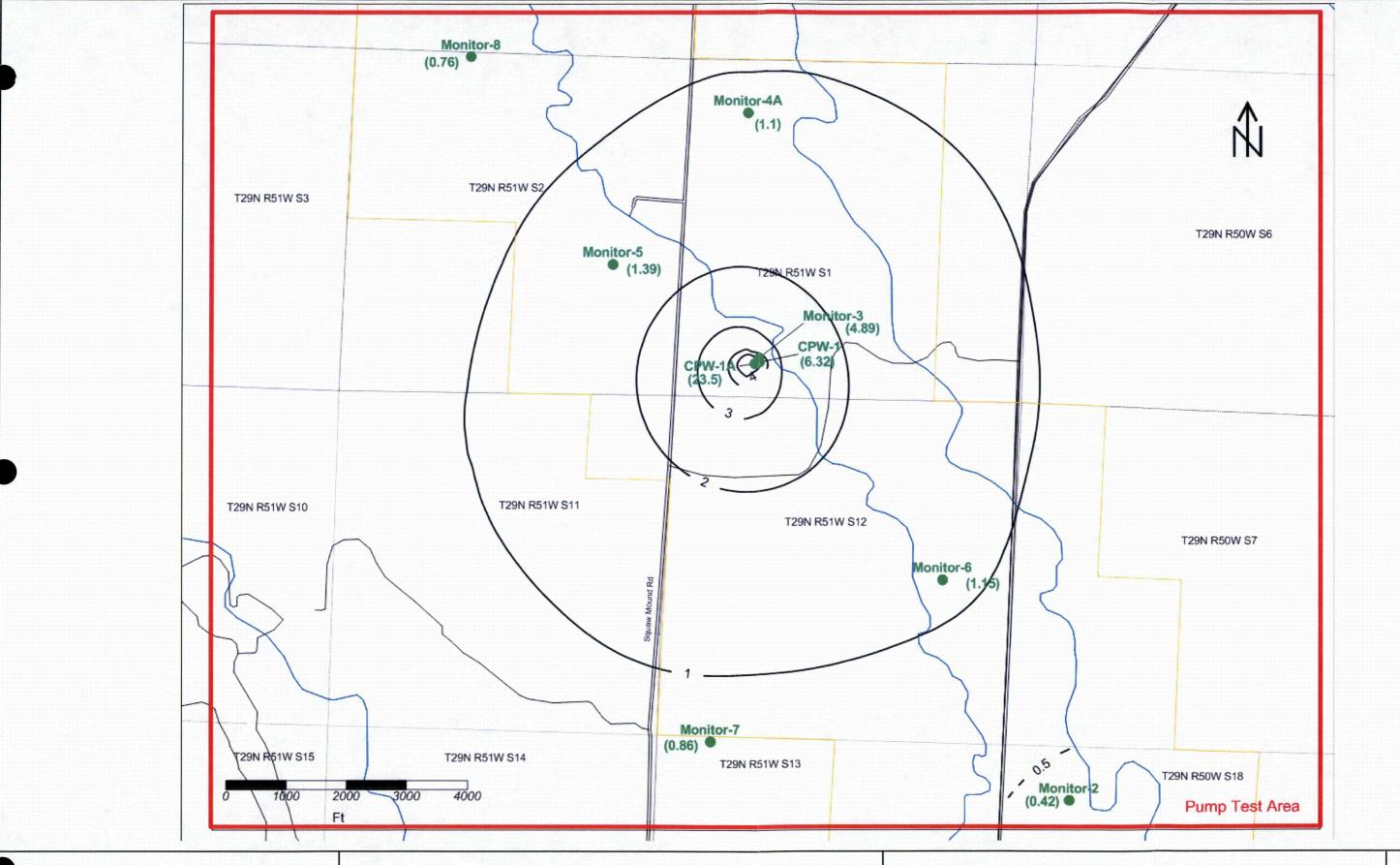


Hydrogeology, Water Resources & Data Services

Potentiometric Surface Map – Brule Formation, November 12, 2010 Marsland Regional Hydrologic Testing Report – Test # 8
Crow Butte Project, Marsland Expansion Area,
Dawes County, NE



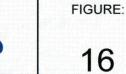
FIGURE:



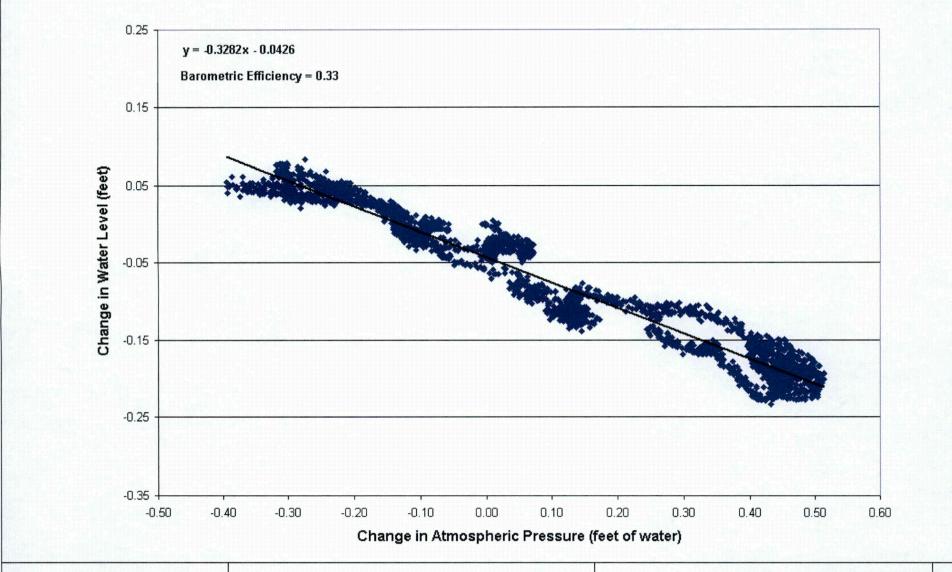
Hydrogeology, Water Resources & Data Services

Drawdown in the Basal Chadron Sandstone at the End of the Test

Marsland Regional Hydrologic Testing Report – Test # 8
Crow Butte Project, Marsland Expansion Area,
Dawes County, NE



8 (Cameco



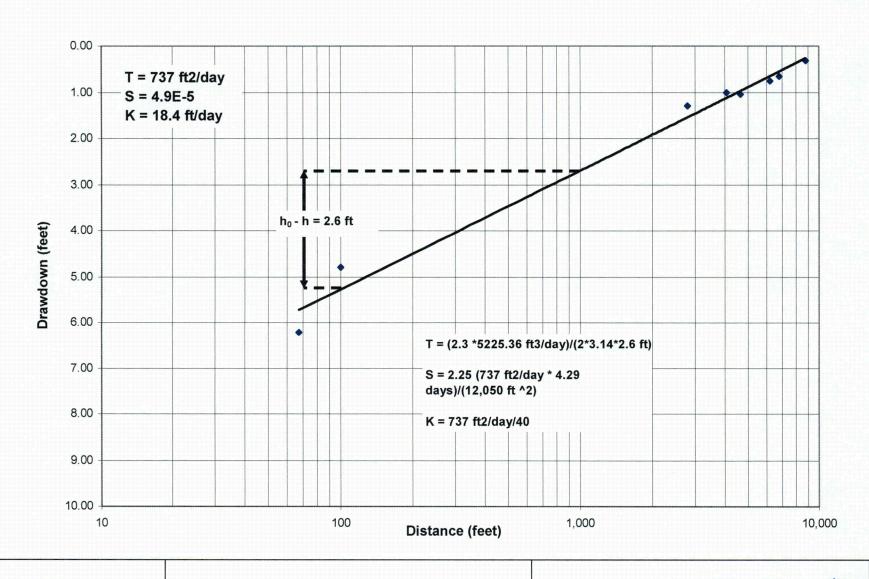
Hydrogeology, Water Resources & Data Services

Change in Barometric Pressure vs. Change in Water Level

Marsland Regional Hydrologic Testing Report – Test # 8
Crow Butte Project, Marsland Expansion Area,
Dawes County, NE



FIGURE:



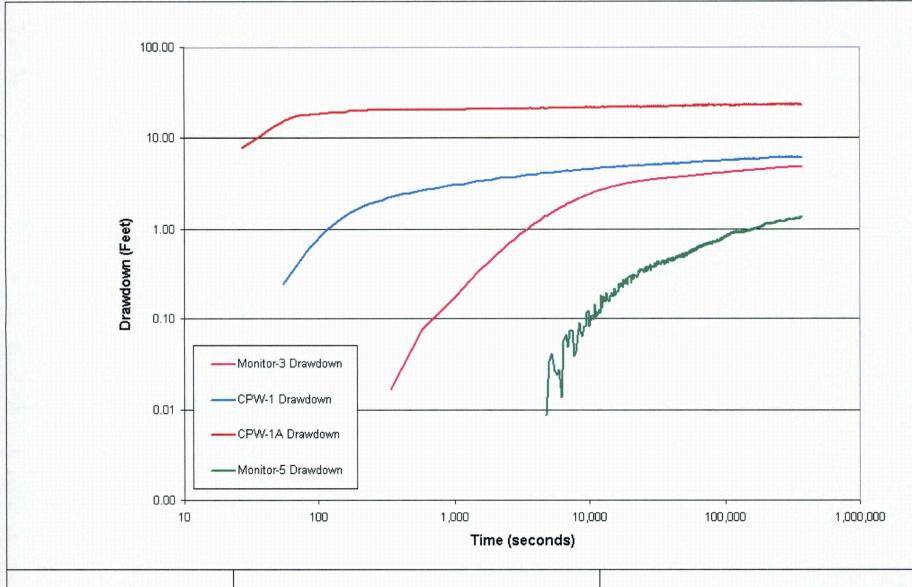
Hydrogeology, Water Resources & Data Services

Distance Drawdown Plot

Marsland Regional Hydrologic Testing Report – Test # 8 Crow Butte Project, Marsland Expansion Area, Dawes County, NE



FIGURE:



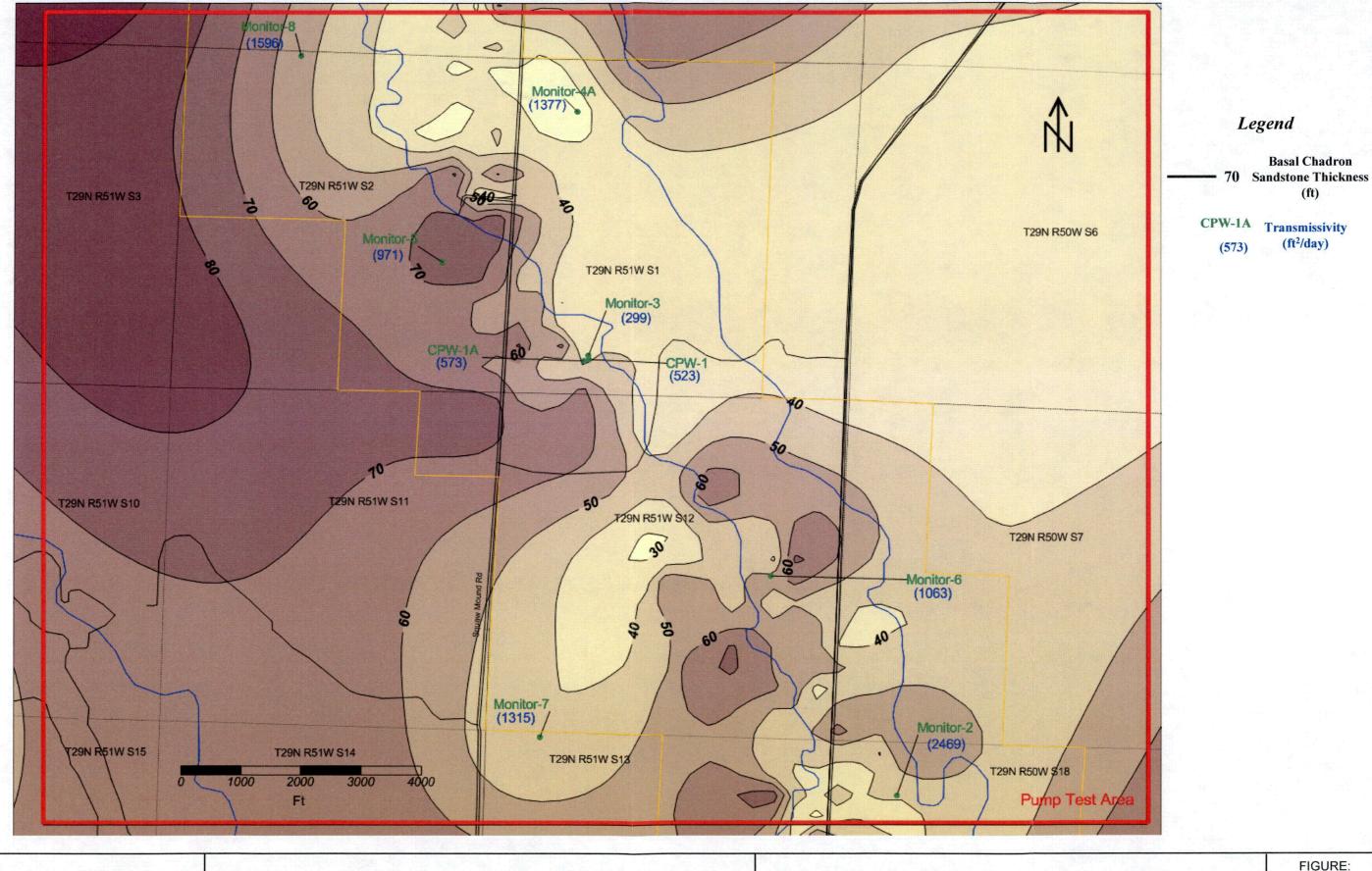
Hydrogeology, Water Resources & Data Services

Drawdown vs. Time for Selected Wells

Marsland Regional Hydrologic Testing Report – Test # 8
Crow Butte Project, Marsland Expansion Area,
Dawes County, NE



FIGURE:



Basal Chadron Sandstone Isopach Showing Transmissivity Distribution

Marsland Regional Hydrologic Testing Report - Test # 8 Crow Butte Project, Marsland Expansion Area, Dawes County, NE





Appendix A

WELL COMPLETION REPORTS

Nebraska Department of Environmental Quality

Well Completion Report

Company: Crow Butte Resources. Inc.

Well Type: Production/Injection

Ground Elevation:

4259 ft.

Drilling Contractor: Landrill Exploration

Mud Products:

6 Bags Super Gel

2 Quart Polymer

Bit Size: 8 Inch

Drilling Begun:

8/24/2010

Completed Formation: Casing Diameter:

Brule 4.95 inch O.D.

Casing Depth:

279 ft.

Packer Type:

Johnson K-packer

Centralizer Depths:

20, 40, 100, 160, 220 Ft

Screen Size:

3 inch by .020 inch

Screened Interval(s):

285 ft. -

ft. -

365 ft. ft.

Completed Formation Upper Boundary:

270 ft.

Cement Contractor: Crow Butte Resources

Estimated Cement Volume: 10.8 bbls.

Cement Density:

12.4 lbs/gal

Cement Type/Class:

I/II API

Cement Circulated to Surface:

0 bbls.

Logging Contractor:

Century Geophysical Corp.

Unit No.: Log Type: 0001

Gamma, SP, Resistance, Deviation

Well Deviation:

1.2 ft. at

342.2 degrees

Remarks:

Tremmied 4 bbls to surface

This report was filled out by:

Wade Beins

Representing:

Crow Butte Resources, Inc.

On:

Certification:

I certify under penalty of law that I have personally examined and am familiar with the information submitted in this form and all its attachments and that, based on inquiry of those individuals immediately responsible for obtaining information, I believe the information is true, accurate, and complete. Further, I certify awareness that there are significant penalties for submitting false information, including the possibility of fine and imprisonment.

By:

Wade Beins

Title: Senior Geologist

May 27, 2011

Wellhead Elevation:

4260 ft.

Driller: J. Lemmon

2 Bags Lost Circulation Material

Crow Butte BOW-2010-1

Drilling Completed On:

8/26/2010

Depth Drilled:

Project:

Well No.

420 ft.

Casing Type:

White Certalok

Basket Depth:

N/A

Packer Depth:

275 ft.

ft.

Gravel Size:

ft. ft.

ft. -

ft.

Lower Boundary:

400 ft.

Operator:

Operator:

Klein

Actual Cement Volume Used: Water Volume Used:

11.6 bbls.

Additives:

500 lbs. Salt 500 lbs. Bentonite 9 lbs/gal

16.2 bbls.

Density At Surface:

Dunn

Probe No.: 9055C

Company: Crow Butte Resources. Inc.

Well Type: Production/Injection

Ground Elevation:

4322 ft.

Drilling Contractor: Landrill Exploration

Mud Products:

7 Bags Super Gel

2 Quart Polymer

Bit Size: 8 Inch

Drilling Begun:

8/25/2010

Completed Formation: Casing Diameter:

Brule 4.95 inch O.D.

Casing Depth:

339 ft.

Packer Type:

Johnson K-packer

20, 40, 100, 160, 220, 280 Ft Centralizer Depths:

Screen Size:

3 inch by .020 inch

Screened Interval(s):

338 ft. -398 ft.

ft. -

ft.

330 ft.

Completed Formation Upper Boundary:

Cement Contractor: Crow Butte Resources

Estimated Cement Volume:

13.1 bbls.

Cement Density: Cement Type/Class: 12.3 lbs/gal I/II API

Cement Circulated to Surface:

0 bbls.

Logging Contractor:

Century Geophysical Corp.

Unit No.:

0001

Log Type: Gamma, SP, Resistance, Deviation

Well Deviation:

2.7 ft. at

300.1 degrees

Remarks:

Tremmied 3 bbls to surface

This report was filled out by:

Wade Beins

Representing:

Crow Butte Resources, Inc.

On:

Certification:

I certify under penalty of law that I have personally examined and am familiar with the information submitted in this form and all its attachments and that, based on inquiry of those individuals immediately responsible for obtaining information, I believe the information is true, accurate, and complete. Further, I certify awareness that there are significant penalties for submitting false information, including the possibility of fine and imprisonment.

By:

Wade Beins

Title:

Senior Geologist

May 27, 2011

Project:

Crow Butte

Well No.

BOW-2010-2

Wellhead Elevation:

4323 ft.

Driller:

J. Lemmon

1 Bags Lost Circulation Material

Drilling Completed On:

8/27/2010

Depth Drilled:

420 ft.

Casing Type:

White Certalok ft.

Basket Depth:

N/A

Packer Depth:

328 ft.

Gravel Size:

ft. ft.

ft. -

ft.

Lower Boundary:

410 ft.

Operator:

Klein

Actual Cement Volume Used:

Water Volume Used:

14.1 bbls. Additives: 500 lbs. Salt 500 lbs. Bentonite

19.6 bbls.

Density At Surface:

9.4 lbs/gal

Operator:

Dunn

Probe No.: 9055C

4350 ft.

8/24/2010

450 ft.

440 ft.

19.6 bbls.

14.1 bbls.

12.2 lbs/gal

ft.

White Certalok

336 ft.

Crow Butte

L. Corbin

2 Bags Lost Circulation Material

N/A

ft.

ft.

Klein

Additives: 500 lbs. Salt 500 lbs. Bentonite

Actual Cement Volume Used:

Dunn

BOW-2010-3

Well Completion Report

Company: Crow Butte Resources. Inc.

Well Type: Production/Injection

Monitor X

ft.

330 ft.

Ground Elevation:

4350 ft.

Drilling Contractor: Landrill Exploration

Mud Products:

6 Bags Super Gel

1 Quart Polymer

Project:

Well No.

Driller:

Wellhead Elevation:

Drilling Completed On:

Depth Drilled:

Casing Type:

Basket Depth:

Packer Depth:

Gravel Size:

Lower Boundary:

Water Volume Used:

Density At Surface:

Probe No.: 9055C

ft. -

ft. -

Operator:

Operator:

Bit Size: 8 Inch

o mei

8/20/2010

Completed Formation:
Casing Diameter:

n: Brule 4.95 inch O.D.

Casing Depth:

Drilling Begun:

339 ft.

Packer Type:

Johnson K-packer

Centralizer Depths:

20, 40, 100, 160, 220, 280 Ft

Screen Size:

3 inch by .020 inch

Screened Interval(s):

: 346 ft. - 416 ft.

ft. -

Completed Formation Upper Boundary:

Cement Contractor: Crow Butte Resources

Estimated Cement Volume:

e: 13.1 bbls.

Cement Density:

12.2 lbs/gal

Cement Type/Class:

I/II API

Cement Circulated to Surface:

Century Geophysical Corp.

Logging Contractor:

Unit No.: 0001

Gamma, SP, Resistance, Deviation

Well Deviation:

3.6 ft. at

320.7 degrees

bbls.

Remarks:

Log Type:

This report was filled out by:

Wade Beins

Representing:

Crow Butte Resources, Inc.

On:

Certification:

I certify under penalty of law that I have personally examined and am familiar with the information submitted in this form and all its attachments and that, based on inquiry of those individuals immediately responsible for obtaining information, I believe the information is true, accurate, and complete. Further, I certify awareness that there are significant penalties for submitting false information, including the possibility of fine and imprisonment.

By:

Wade Beins

Title:

Senior Geologist

Date

Company: Crow Butte Resources. Inc. Project:

Crow Butte

Well Type: Production/Injection

Well No. CPW-2010-1

Ground Elevation:

4260 ft.

Wellhead Elevation:

4262 ft.

Drilling Contractor: Landrill Exploration Mud Products:

11 Bags Super Gel

4 Quart Polymer

Driller: L. Corbin

2 Bags Lost Circulation Material

Bit Size: 8 Inch

Drilling Begun:

8/31/2010

Drilling Completed On:

9/2/2010

Completed Formation:

Chadron

Depth Drilled:

1070 ft.

Casing Diameter:

4.95 inch O.D.

Casing Type:

White Certalok N/A ft.

ft.

ft.

Klein

Casing Depth:

1009 ft.

Basket Depth:

Packer Type:

Johnson K-packer

Packer Depth:

995 ft.

Centralizer Depths:

20, 40, 100, 160, 220, 280, 340, 400, 460, 520, 580, 640, 700, 760, 820, 880, 940 Ft

Screen Size:

3 inch by .020 inch

Gravel Size:

Screened Interval(s):

1015 ft. -1048 ft. ft. -

ft. -

ft. -Lower Boundary:

1046 ft.

Completed Formation Upper Boundary: 1016 ft.

Operator:

Water Volume Used:

Dunn

9055C

Cement Contractor: Crow Butte Resources

Estimated Cement Volume: 38.8 bbls. Actual Cement Volume Used:

58.2 bbls.

Cement Density: Cement Type/Class: 12.4 lbs/gal I/II API

Additives:

41.7 bbls. 500 lbs. Salt 500 lbs. Bentonite

Cement Circulated to Surface:

5 bbls. Density At Surface:

11.6 lbs/gal

Logging Contractor:

0001

Century Geophysical Corp.

ft.

Operator: Probe No.:

Unit No.: Log Type:

Gamma, SP, Resistance, Deviation

Well Deviation:

4.1 ft. at

203.5 degrees

Remarks:

This report was filled out by:

Wade Beins

Representing:

Crow Butte Resources, Inc.

On:

Certification:

I certify under penalty of law that I have personally examined and am familiar with the information submitted in this form and all its attachments and that, based on inquiry of those individuals immediately responsible for obtaining information, I believe the information is true, accurate, and complete. Further, I certify awareness that there are significant penalties for submitting false information, including the possibility of fine and imprisonment.

By:

Wade Beins

Title:

Senior Geologist

Nebraska Department of Environmental Quality

Well Completion Report

Company: Crow Butte Resources. Inc. Project:

Crow Butte

Well Type: Production/Injection

CPW-2010-1A Well No.

4263 ft.

Ground Elevation:

4261 ft.

Wellhead Elevation:

Drilling Contractor: Landrill Exploration

Driller: S. Osmotherly

Mud Products:

Drilling Begun:

7 Bags Super Gel

2 Quart Polymer

3 Bags Lost Circulation Material

Bit Size: 8 Inch

3/14/2011

Drilling Completed On:

3/16/2011

Completed Formation: Chadron

Depth Drilled:

1080 ft.

4.95 inch O.D. Casing Diameter:

Casing Type:

White Certalok

Casing Depth:

1019 ft.

Basket Depth:

N/A ft.

ft.

ft.

Klein

Packer Type:

Johnson K-packer

Packer Depth:

1005 ft.

Centralizer Depths:

20, 40, 100, 160, 220, 280, 340, 400, 460, 520, 580, 640, 700, 760, 820, 880, 940 Ft

Screen Size:

3 inch by .020 inch

Gravel Size:

Screened Interval(s):

1025 ft. -1055 ft. ft. -

ft. ft.

ft. -

1050 ft.

Completed Formation Upper Boundary:

1024 ft.

Lower Boundary:

Cement Contractor: Crow Butte Resources

Estimated Cement Volume:

39.2 bbls.

Operator:

Actual Cement Volume Used: 58.8 bbls.

Cement Density:

12.3 lbs/gal

Water Volume Used:

42.1 bbls.

Cement Type/Class:

Logging Contractor:

I/II API

Additives: 500 lbs. Salt 500 lbs. Bentonite

11 lbs/gal

Cement Circulated to Surface:

bbls.

Century Geophysical Corp.

Density At Surface: Operator:

Unit No.:

0001

Dunn Probe No.: 9055C

Log Type:

Gamma, SP, Resistance, Deviation

Well Deviation:

24.9 ft. at

153.3 degrees

Remarks:

This report was filled out by:

Wade Beins

Representing:

Crow Butte Resources, Inc.

On:

Certification:

I certify under penalty of law that I have personally examined and am familiar with the information submitted in this form and all its attachments and that, based on inquiry of those individuals immediately responsible for obtaining information, I believe the information is true, accurate, and complete. Further, I certify awareness that there are significant penalties for submitting false information, including the possibility of fine and imprisonment.

By:

Wade Beins

Title:

Senior Geologist

Company: Crow Butte Resources. Inc.

Well Type: Production/Injection

Crow Butte Monitor 2

Wellhead Elevation:

4198 ft.

Drilling Contractor: Landrill Exploration

4197 ft.

Driller:

Project:

Well No.

G. Land

Mud Products:

Ground Elevation:

Bit Size: 8 Inch

4/7/1989

Drilling Begun: Completed Formation: Chadron

Casing Diameter:

4.95 inch O.D.

Casing Depth:

974 ft.

Packer Type:

Centralizer Depths:

Johnson K-packer

###

Drilling Completed On: Depth Drilled:

4/9/1989

Casing Type:

1030 ft. White Certalok

ft.

1015 ft.

56.2 bbls.

bbls.

Not Availa lbs/gal

Basket Depth:

N/A

ft.

ft.

Klein

Additives: 500 lbs. Salt 500 lbs. Bentonite

Actual Cement Volume Used:

Dunn

9055C

Packer Depth:

Gravel Size:

Lower Boundary:

Water Volume Used:

Density At Surface:

ft. -

ft. -

Operator:

Operator:

Probe No.:

974 ft.

Screen Size:

3 inch by .020 inch

Screened Interval(s):

980 ft. -1015 ft.

ft. -

ft.

Completed Formation Upper Boundary:

974 ft.

Cement Contractor: Crow Butte Resources

Estimated Cement Volume:

37.5 bbls.

Cement Density:

Not Avai lbs/gal

Cement Type/Class:

I/II API

Cement Circulated to Surface:

Not Avai bbls.

Logging Contractor:

0001

Century Geophysical Corp.

Unit No.: Log Type:

Gamma, SP, Resistance, Deviation

Well Deviation:

14.6 ft. at

128 degrees

Remarks:

This report was filled out by:

Wade Beins

Representing:

Crow Butte Resources, Inc.

On:

Certification:

I certify under penalty of law that I have personally examined and am familiar with the information submitted in this form and all its attachments and that, based on inquiry of those individuals immediately responsible for obtaining information, I believe the information is true, accurate, and complete. Further, I certify awareness that there are significant penalties for submitting false information, including the possibility of fine and imprisonment.

By:

Wade Beins

Title:

Senior Geologist

Nebraska Department of Environmental Quality

Permit No. NE0122611

Well Completion Report

Company: Crow Butte Resources. Inc.

Well Type: Production/Injection

Ground Elevation: 4260 ft.

Drilling Contractor: Landrill Exploration

Mud Products:

Bit Size: 8 Inch

Drilling Begun:

4/14/1989

Completed Formation: Chadron 4.95 inch O.D. Casing Diameter:

Casing Depth: 1008 ft. Packer Type: Johnson K-packer

Centralizer Depths: ###

Screen Size: 3 inch by .020 inch

Screened Interval(s): 1015 ft. -1050 ft.

ft. -

ft.

Completed Formation Upper Boundary: 1014 ft.

Cement Contractor: Crow Butte Resources Estimated Cement Volume: 38.8 bbls.

Cement Density: Not Avai lbs/gal

Cement Type/Class: I/II API

Cement Circulated to Surface: Not Avai bbls.

Logging Contractor: Century Geophysical Corp.

Unit No.: 0001

Log Type: Gamma, SP, Resistance, Deviation

Well Deviation:

13.8 ft. at

72 degrees

Remarks:

This report was filled out by: Wade Beins

Representing: Crow Butte Resources, Inc.

On:

Certification:

I certify under penalty of law that I have personally examined and am familiar with the information submitted in this form and all its attachments and that, based on inquiry of those individuals immediately responsible for obtaining information, I believe the information is true, accurate, and complete. Further, I certify awareness that there are significant penalties for submitting false information, including the possibility of fine and imprisonment.

By: Wade Beins Title: Senior Geologist

May 27, 2011

Project: Well No. Crow Butte Monitor 3

Wellhead Elevation:

4261 ft.

Driller:

G. Land

Drilling Completed On:

4/18/1989

Depth Drilled: Casing Type:

1070 ft.

Basket Depth:

N/A

ft.

White Certalok

Packer Depth:

1008 ft.

Gravel Size:

ft. ft.

ft. ft.

Lower Boundary:

1046 ft.

Operator: Klein

Actual Cement Volume Used:

58.1 bbls.

Water Volume Used:

bbls.

Additives: 500 lbs. Salt 500 lbs. Bentonite

Density At Surface:

Not Availa lbs/gal

Operator: Dunn Probe No.: 9055C

Crow Butte Resources. Inc. Company:

Project:

Crow Butte

Well Type: Production/Injection

х

Well No. Monitor 4A

Ground Elevation:

4326 ft.

Wellhead Elevation:

4328 ft.

Drilling Contractor: Landrill Exploration

Driller:

Mud Products:

L. Corbin

6 Bags Super Gel

3 Quart Polymer

Bit Size:

8 Inch

Drilling Begun:

11/3/2010

Drilling Completed On:

11/5/2010

Completed Formation:

Chadron

Depth Drilled:

Casing Diameter:

4.95 inch O.D.

Casing Type:

1140 ft.

Casing Depth:

1079 ft.

Basket Depth:

White Certalok N/A ft.

Packer Type:

Centralizer Depths:

Johnson K-packer

Packer Depth:

1060 ft.

20, 40, 100, 160, 220, 280, 340, 400, 460, 520, 580, 640, 700, 760, 820, 880, 940, 1000 Ft

Screen Size:

3 inch by .020 inch

Gravel Size:

ft. -

Screened Interval(s):

1080 ft. ft. - 1110 ft.

ft.

ft. -

ft.

Completed Formation Upper Boundary:

1081 ft. Lower Boundary: 1109 ft.

Cement Contractor: Crow Butte Resources

Operator:

Klein

ft.

Estimated Cement Volume:

41.5 bbls.

Actual Cement Volume Used:

9055C

62.2 bbls.

Cement Density:

12.5 lbs/gal

Water Volume Used:

44.6 bbls.

Cement Type/Class:

I/II API

Additives:

500 lbs. Salt 500 lbs. Bentonite

Cement Circulated to Surface:

8 bbls. Density At Surface:

11.9 lbs/gal

Logging Contractor:

Century Geophysical Corp.

Operator: Dunn

Probe No.:

Unit No.: Log Type: 0001

Gamma, SP, Resistance, Deviation

Well Deviation:

11.3 ft. at

53.7 degrees

Remarks:

This report was filled out by:

Wade Beins

Representing:

Crow Butte Resources, Inc.

On:

Certification:

I certify under penalty of law that I have personally examined and am familiar with the information submitted in this form and all its attachments and that, based on inquiry of those individuals immediately responsible for obtaining information, I believe the information is true, accurate, and complete. Further, I certify awareness that there are significant penalties for submitting false information, including the possibility of fine and imprisonment.

By:

Wade Beins

Title: Senior Geologist

Company: Crow Butte Resources. Inc. Project:

Crow Butte

Well Type: Production/Injection

Well No.

Monitor 5

Ground Elevation:

4337 ft.

Wellhead Elevation:

4340 ft.

Drilling Contractor: Landrill Exploration

Driller:

Mud Products:

8 Bags Super Gel

7 Quart Polymer

J. Lemmon 3 Bags Lost Circulation Material

Bit Size:

8 Inch

8/30/2010

Drilling Completed On:

9/1/2010

Drilling Begun: Completed Formation:

Chadron

Depth Drilled:

Casing Diameter:

4.95 inch O.D.

Casing Type:

1140 ft. White Certalok

Casing Depth:

1069 ft.

Basket Depth:

ft. N/A

Packer Type:

Johnson K-packer

Packer Depth:

1060 ft.

Centralizer Depths:

20, 40, 100, 160, 220, 280, 340, 400, 460, 520, 580, 640, 700, 760, 820, 880, 940, 1000 Ft

Screen Size:

3 inch by .020 inch

Gravel Size:

Screened Interval(s):

1070 ft. -1120 ft. ft. -

ft.

ft. -

Completed Formation Upper Boundary:

ft.

1066 ft.

Lower Boundary:

1116 ft.

Cement Contractor: Crow Butte Resources

Operator:

ft. -

Klein

ft.

Estimated Cement Volume:

41.1 bbls.

Actual Cement Volume Used:

Dunn

9055C

61.7 bbls.

Cement Density:

12.2 lbs/gal

Water Volume Used:

44.2 bbls. 500 lbs. Salt 500 lbs. Bentonite

Cement Type/Class:

I/II API

Additives:

Density At Surface:

Logging Contractor:

3 Century Geophysical Corp.

Operator:

11.5 lbs/gal

Unit No.:

0001

Cement Circulated to Surface:

Probe No.:

Log Type:

Gamma, SP, Resistance, Deviation Well Deviation: 27 ft. at

142.1 degrees

bbls.

Remarks:

This report was filled out by:

Wade Beins

Representing:

Crow Butte Resources, Inc.

On:

Certification:

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By:

Wade Beins

Senior Geologist

Nebraska Department of Environmental Quality

Well Completion Report

Crow Butte Resources. Inc. Company:

Project:

Crow Butte

Well Type: Production/Injection

Well No. Monitor 6

4215 ft.

Ground Elevation:

4214 ft.

Wellhead Elevation:

Drilling Contractor: Landrill Exploration

Driller: L. Corbin

Mud Products:

13 Bags Super Gel

8 Quart Polymer

4 Bags Lost Circulation Material

Bit Size: 8 Inch

Drilling Begun:

8/16/2010

Drilling Completed On:

8/18/2010

Completed Formation:

Chadron

Depth Drilled:

Casing Diameter:

Casing Type:

1050 ft.

Casing Depth:

4.95 inch O.D. 989 ft.

Basket Depth:

White Certalok N/A ft.

Packer Type:

Johnson K-packer

Packer Depth:

982 ft.

Centralizer Depths:

20, 40, 100, 160, 220, 280, 340, 400, 460, 520, 580, 640, 700, 760, 820, 880, 940 Ft

Screen Size:

3 inch by .020 inch

Gravel Size:

Screened Interval(s):

992 ft. -

1025 ft.

ft. -

ft.

ft. -Lower Boundary:

1023 ft.

Completed Formation Upper Boundary: Cement Contractor: Crow Butte Resources

982 ft.

Operator:

Klein

ft.

ft.

Estimated Cement Volume:

38.1 bbls.

ft. -

Actual Cement Volume Used:

57.1 bbls.

Cement Density: Cement Type/Class:

12 lbs/gal I/II API

Water Volume Used: Additives: 500 lbs. Salt 500 lbs. Bentonite

40.9 bbls.

Cement Circulated to Surface:

3 bbls. Density At Surface:

10 lbs/gal

Logging Contractor:

Century Geophysical Corp.

Operator: Dunn

Unit No.:

0001

Probe No.: 9055C

Log Type:

Gamma, SP, Resistance, Deviation

Well Deviation:

17.1 ft. at

37.3 degrees

Remarks:

This report was filled out by:

Wade Beins

Representing:

Crow Butte Resources, Inc.

On:

Certification:

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By:

Wade Beins

Title:

Senior Geologist

Nebraska Department of Environmental Quality

Well Completion Report

Crow Butte Resources. Inc. Company:

Project:

Crow Butte

Well Type: Production/Injection

Well No. Monitor 7

4244 ft.

Ground Elevation:

4243 ft.

Wellhead Elevation:

Drilling Contractor: Landrill Exploration Mud Products:

6 Bags Super Gel

6 Quart Polymer

Driller: L. Corbin

3 Bags Lost Circulation Material

Bit Size: 8 Inch Drilling Begun:

8/20/2010

Drilling Completed On:

8/23/2010

Completed Formation:

Chadron

Depth Drilled:

4.95 inch O.D.

1080 ft.

ft.

Casing Diameter:

999 ft.

Casing Type: Basket Depth: White Certalok

Casing Depth:

N/A

Packer Type:

Johnson K-packer

Packer Depth:

993 ft.

Centralizer Depths:

20, 40, 100, 160, 220, 280, 340, 400, 460, 520, 580, 640, 700, 760, 820, 880, 940 Ft

Screen Size:

3 inch by .020 inch

Gravel Size:

Screened Interval(s):

1003 ft. -1046 ft. ft. -

ft. ft. -

ft. ft.

Completed Formation Upper Boundary:

1007 ft.

ft.

Lower Boundary:

1044 ft.

Cement Contractor: Crow Butte Resources

Operator:

Klein

Estimated Cement Volume:

38.4 bbls.

Actual Cement Volume Used:

57.6 bbls.

Cement Density:

11.7 lbs/gal I/II API

Water Volume Used: Additives: 500 lbs. Salt 500 lbs. Bentonite

41.3 bbls.

Cement Type/Class: Cement Circulated to Surface:

bbls.

Density At Surface:

10.2 lbs/gal

Logging Contractor:

Century Geophysical Corp.

Operator: Dunn

Unit No.: Log Type: 0001

159.9 degrees

Probe No.:

9055C

Well Deviation: Remarks:

This report was filled out by:

Wade Beins

Representing:

Crow Butte Resources, Inc.

Gamma, SP, Resistance, Deviation

32.2 ft. at

On:

Certification:

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By:

Wade Beins

Title:

Senior Geologist

Company: Crow Butte Resources. Inc.

Drilling Contractor: Landrill Exploration

Well Type: Production/Injection

Monitor Х Project: Well No. Crow Butte Monitor 8

4352 ft.

Wellhead Elevation:

Drilling Completed On:

4354 ft.

Ground Elevation:

Driller:

Mud Products:

10 Bags Super Gel

4 Quart Polymer

L. Corbin

4 Bags Lost Circulation Material

Bit Size: 8 Inch

Drilling Begun:

8/27/2010

Depth Drilled:

8/30/2010

Completed Formation: Casing Diameter:

Chadron

1150 ft.

4.95 inch O.D.

Casing Type:

White Certalok

Casing Depth:

1079 ft.

Basket Depth:

N/A ft.

Packer Type:

Packer Depth:

1067 ft.

Centralizer Depths:

Johnson K-packer 20, 40, 100, 160, 220, 280, 340, 400, 460, 520, 580, 640, 700, 760, 820, 880, 940, 1000 Ft

Screen Size:

3 inch by .020 inch

Screened Interval(s):

1087 ft. -

1127 ft.

Gravel Size: ft. -

ft. ft.

Klein

ft.

1085 ft.

ft. -Lower Boundary:

1123 ft.

500 lbs. Salt 500 lbs. Bentonite

Completed Formation Upper Boundary:

Cement Contractor: Crow Butte Resources

ft. -

Operator:

Estimated Cement Volume: Cement Density:

41.5 bbls.

12.8 lbs/gal

Cement Type/Class:

I/II API

Cement Circulated to Surface:

5 bbls.

Density At Surface: Dunn

9055C

Actual Cement Volume Used:

Water Volume Used:

Logging Contractor:

Century Geophysical Corp.

Operator: Probe No.:

Additives:

11.5 lbs/gal

62.2 bbls.

44.6 bbls.

Unit No.:

0001

Log Type:

Gamma, SP, Resistance, Deviation

Well Deviation:

38.5 ft. at

173.6 degrees

Remarks:

This report was filled out by:

Wade Beins

Representing:

On:

Crow Butte Resources, Inc.

Certification:

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By:

Wade Beins

Title:

Senior Geologist