

Figure 2.4-30 thru Figure 2.4-40 Are Not Used

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Figure 2.4-40a Main Plant Site Grading And Drainage System For Flood Studies Sheet 1



Figure 2.4-40a Deleted by Amendment 101

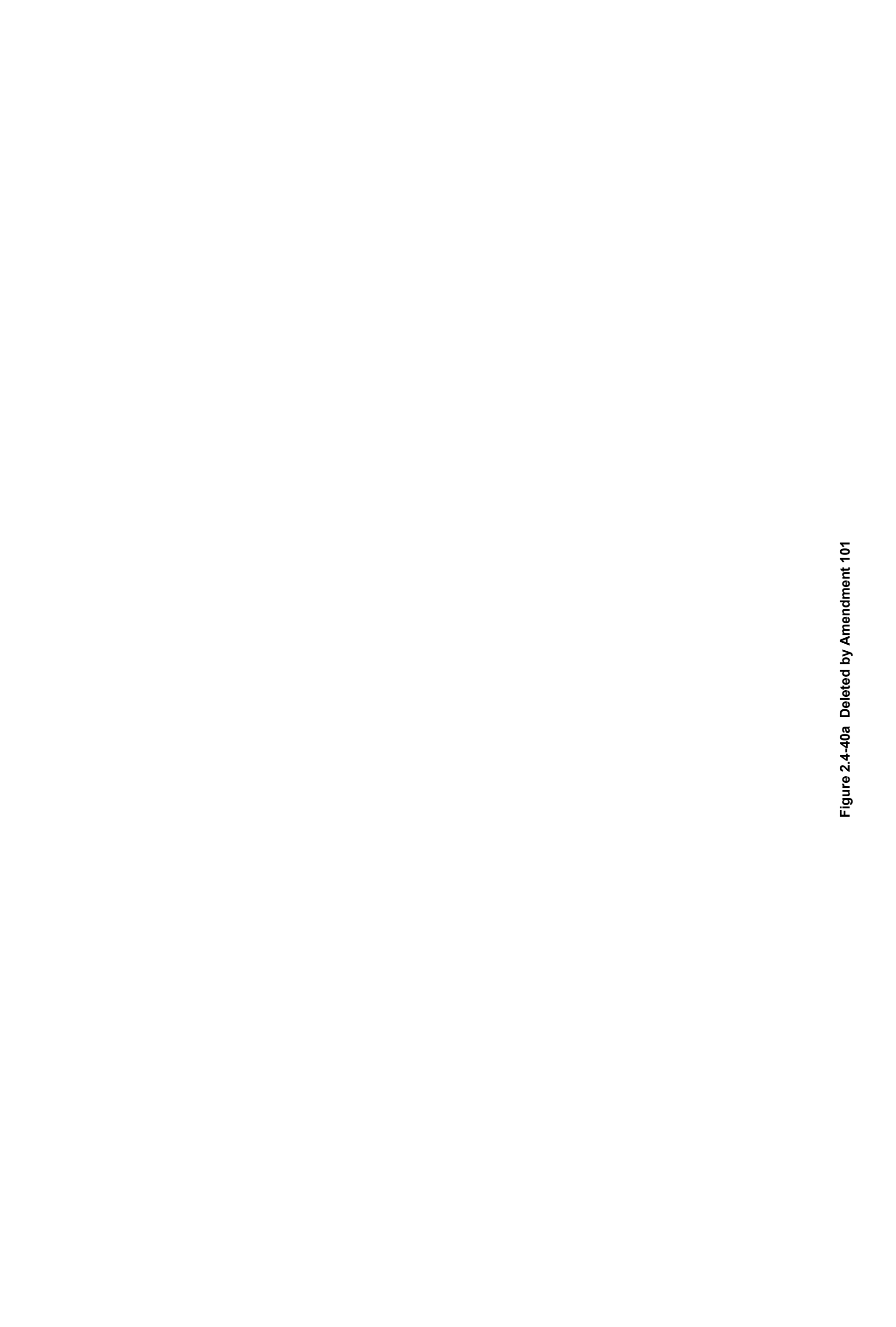


Figure 2.4-40a Deleted by Amendment 101

Figure 2.4-40b Main Plant General Plan

Figure 2.4-40c Yard Site Grading and Drainage System For Flood Studies

Figure 2.4-40d-1 Main Plant Plant Perimeter Roads Plan and Profile Sheet 1

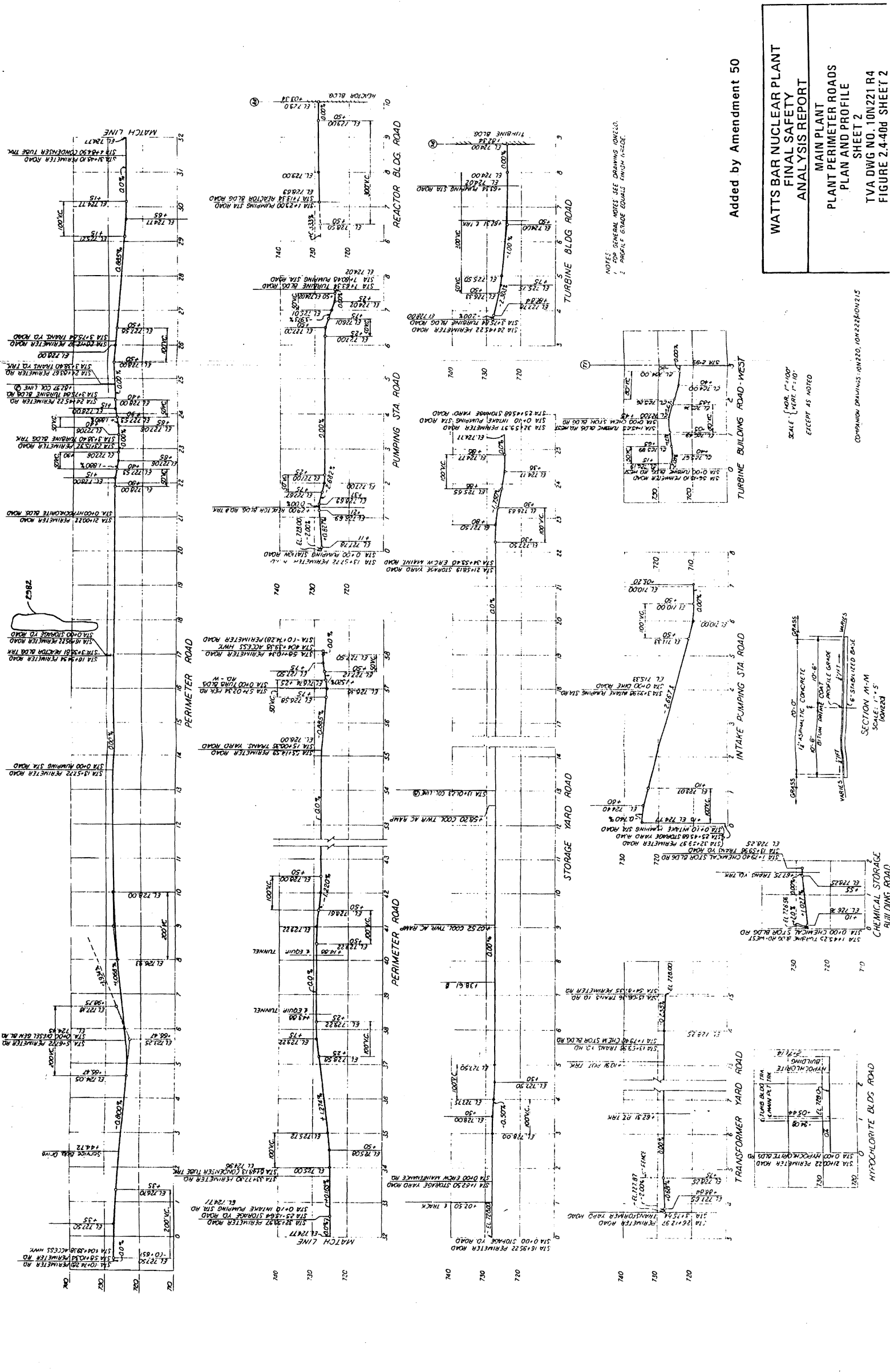


Figure 2.4-40d Main Plant Perimeter Roads Plan and Profile - Sheet 2

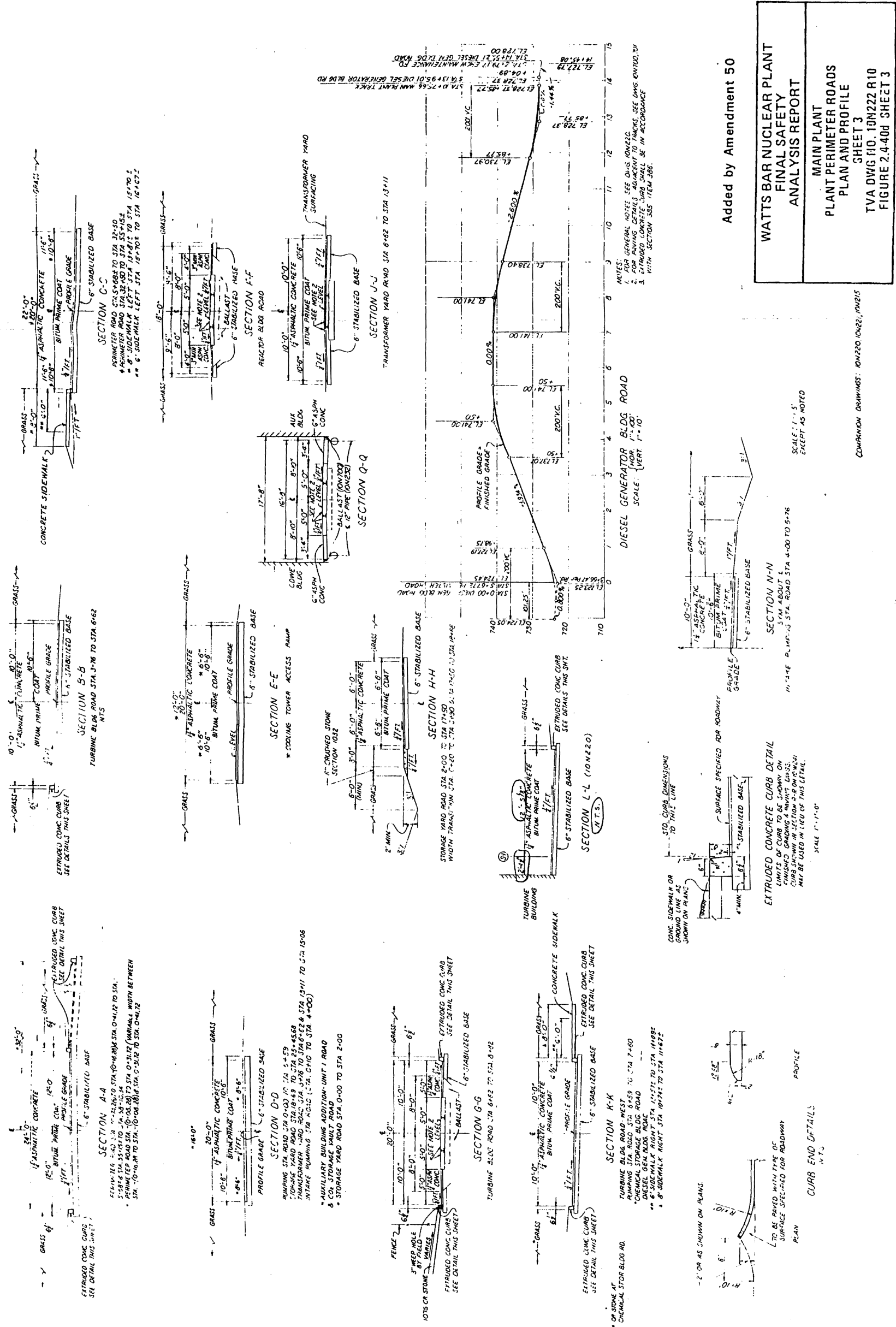
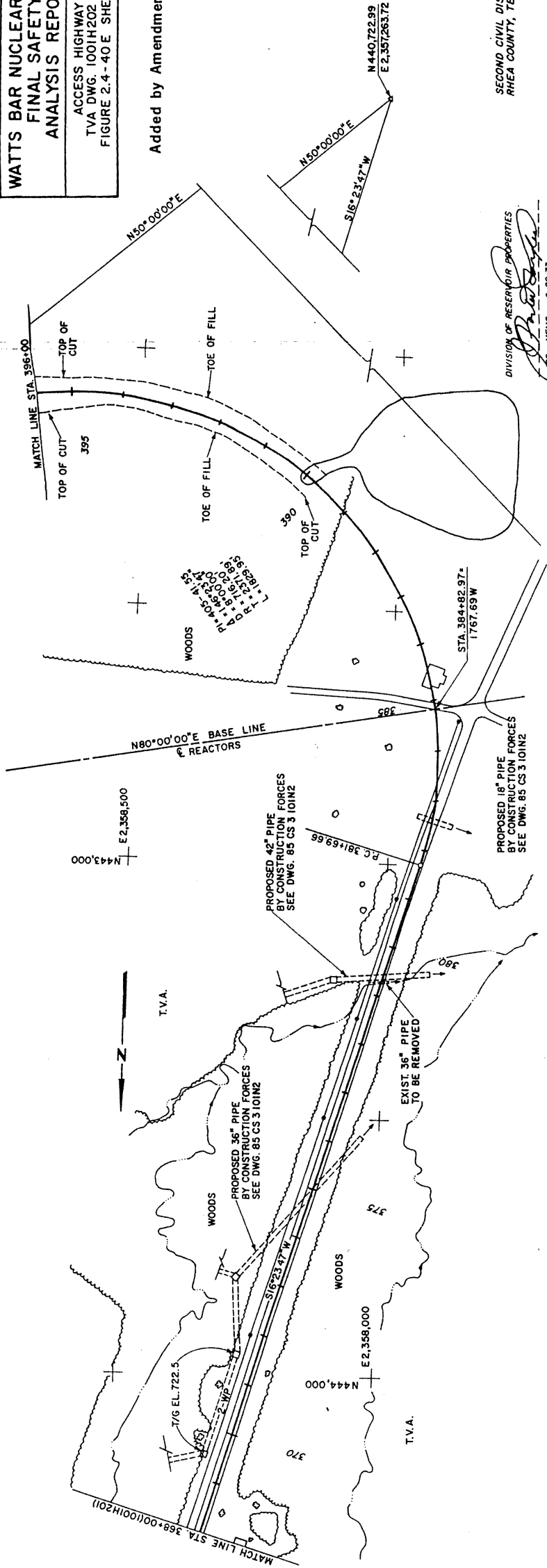


Figure 2.4-40d Main Plant Perimeter Roads Plan and Profile - Sheet 3

WATTS BAR NUCLEAR PLANT
FINAL SAFETY
ANALYSIS REPORT
ACCESS HIGHWAY
TVA DWG. 1001H202 R4
FIGURE 2.4-40 E SHEET 1

Added by Amendment 50



SECOND CIVIL DISTRICT
AREA COUNTY, TENNESSEE

DIVISION OF RESERVING PROPERTIES
MEMO 9-20-73

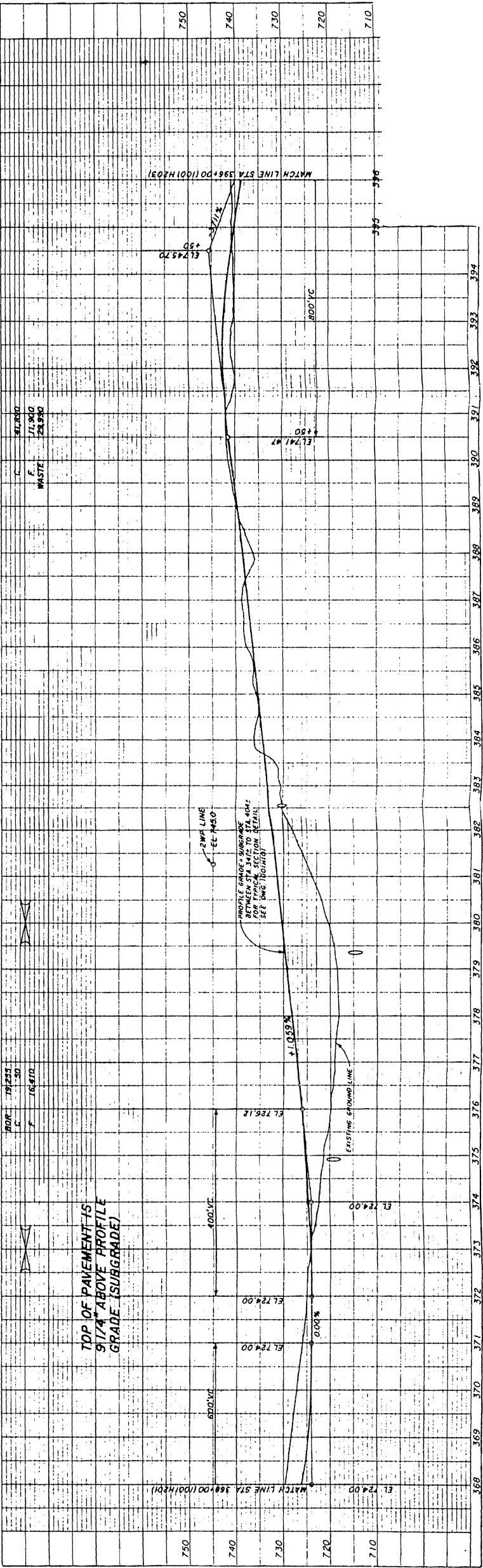
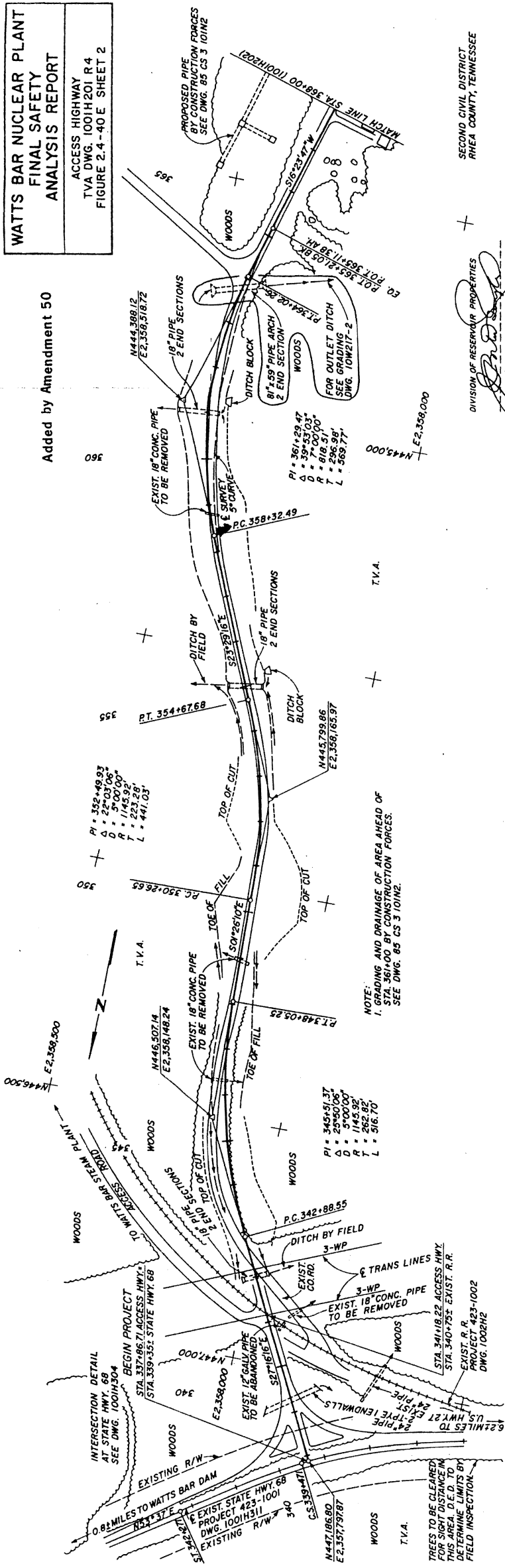


Figure 2.4-40e Access Highway TVA DWG 1001H202 R4 - Sheet 1

WATTS BAR NUCLEAR PLANT
FINAL SAFETY
ANALYSIS REPORT
ACCESS HIGHWAY
TVA DWG. 1001H201 R4
FIGURE 2.4-40E SHEET 2

Added by Amendment 50



SECOND CIVIL DISTRICT
RHEA COUNTY, TENNESSEE

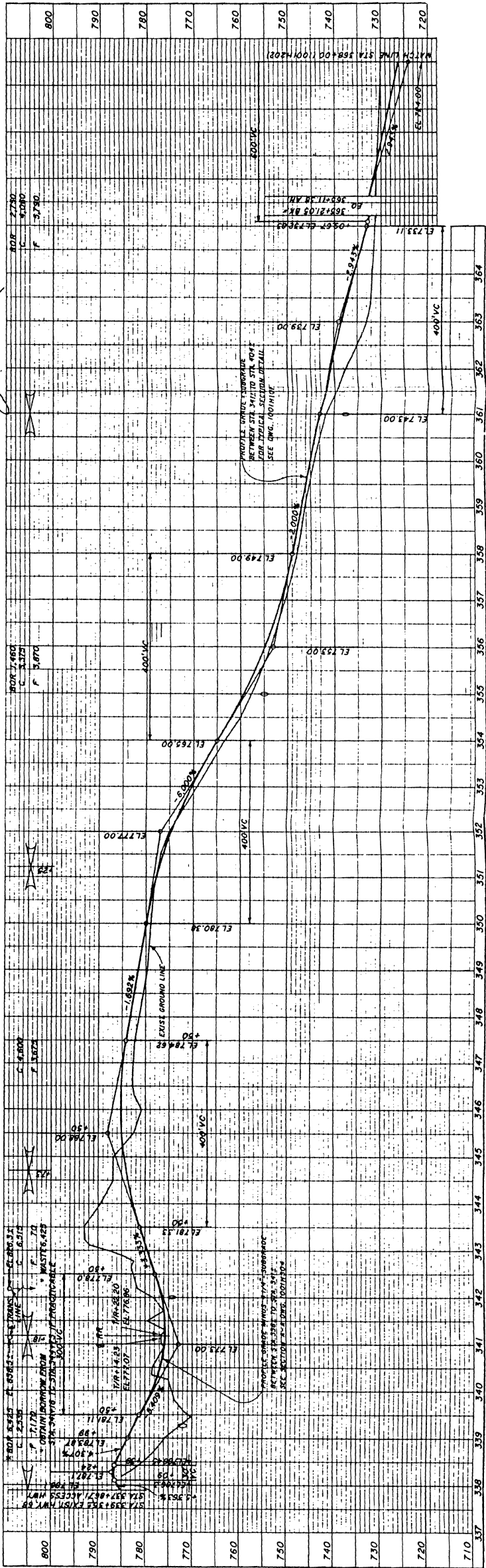
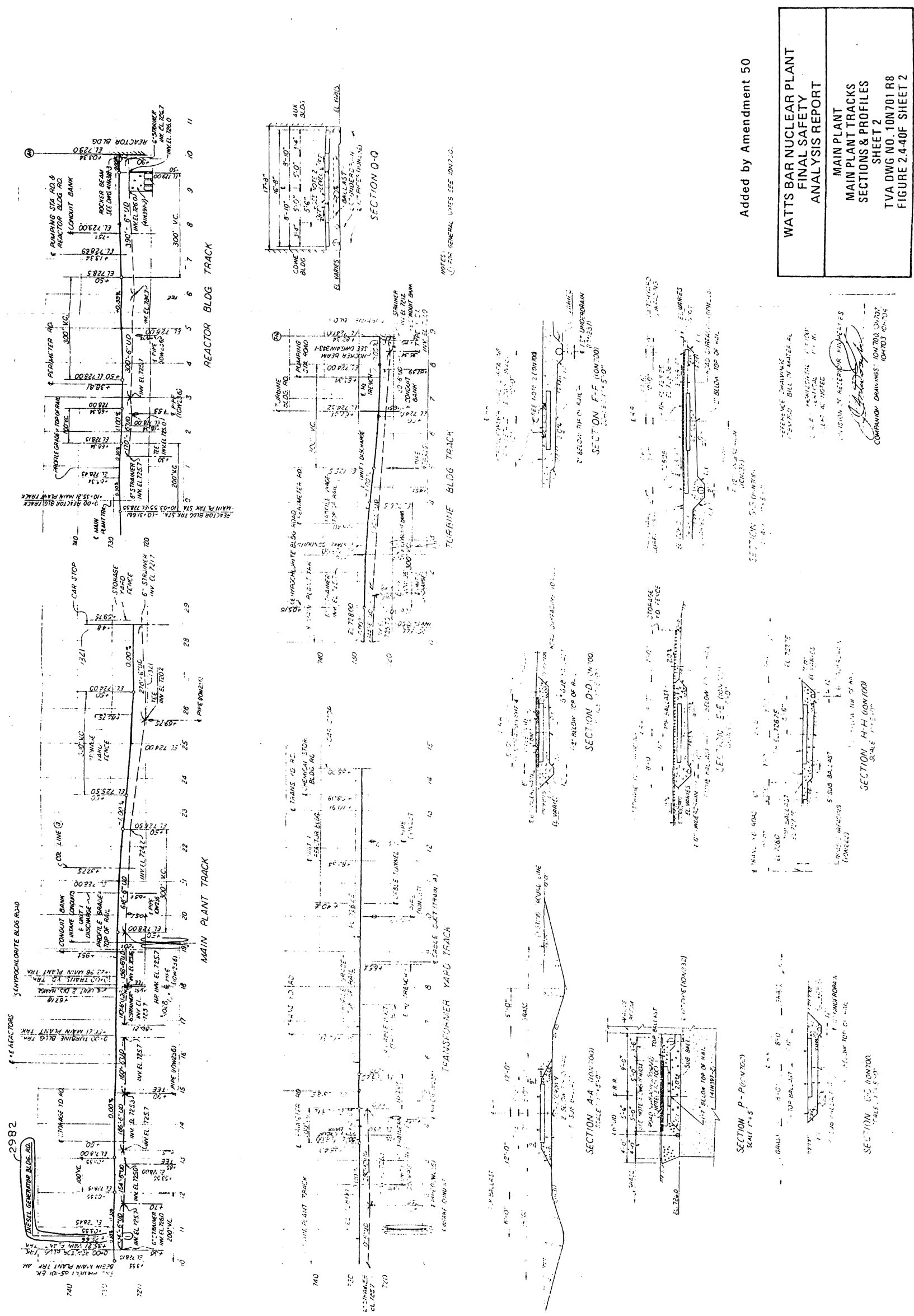


Figure 2.4-40e Access Highway TVA DWG. 1001H201 R4 - Sheet 2

Figure 2.4-40f Main Plant Main Plant Tracks Plan - Sheet 1



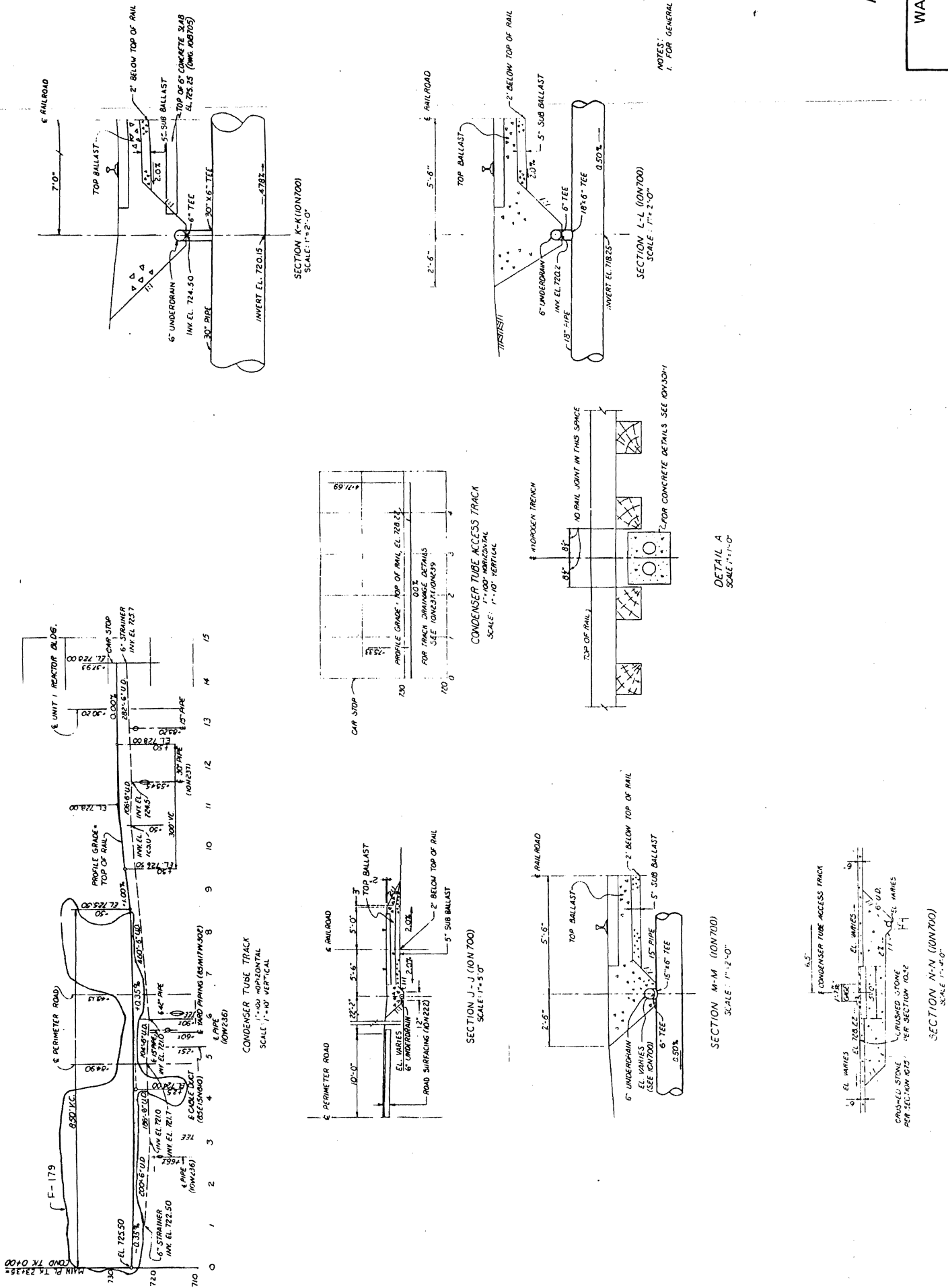


Figure 2.4-40g Yard, Grading Drainage and Surfacing Transformer & Switchyard - Sheet 1



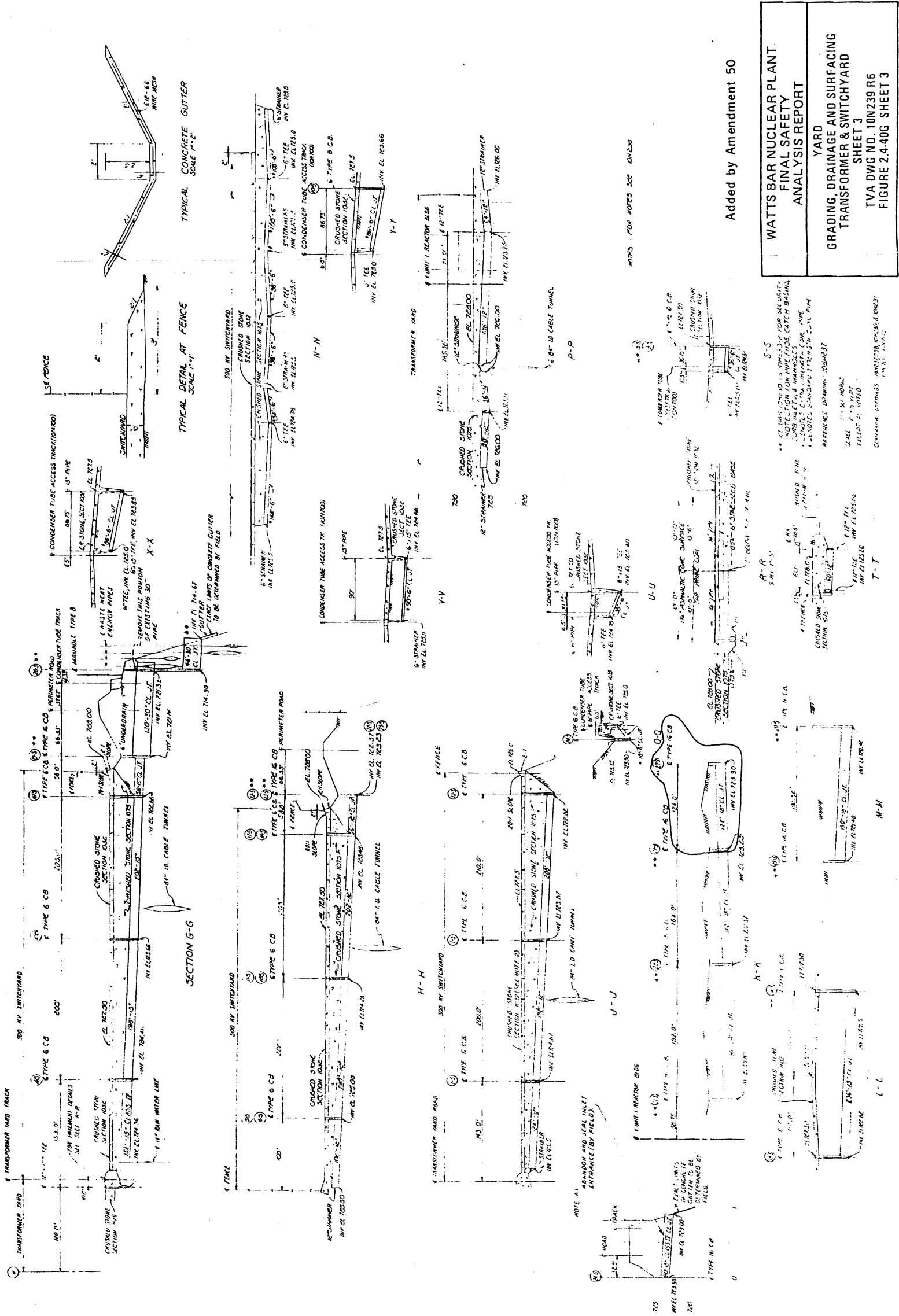
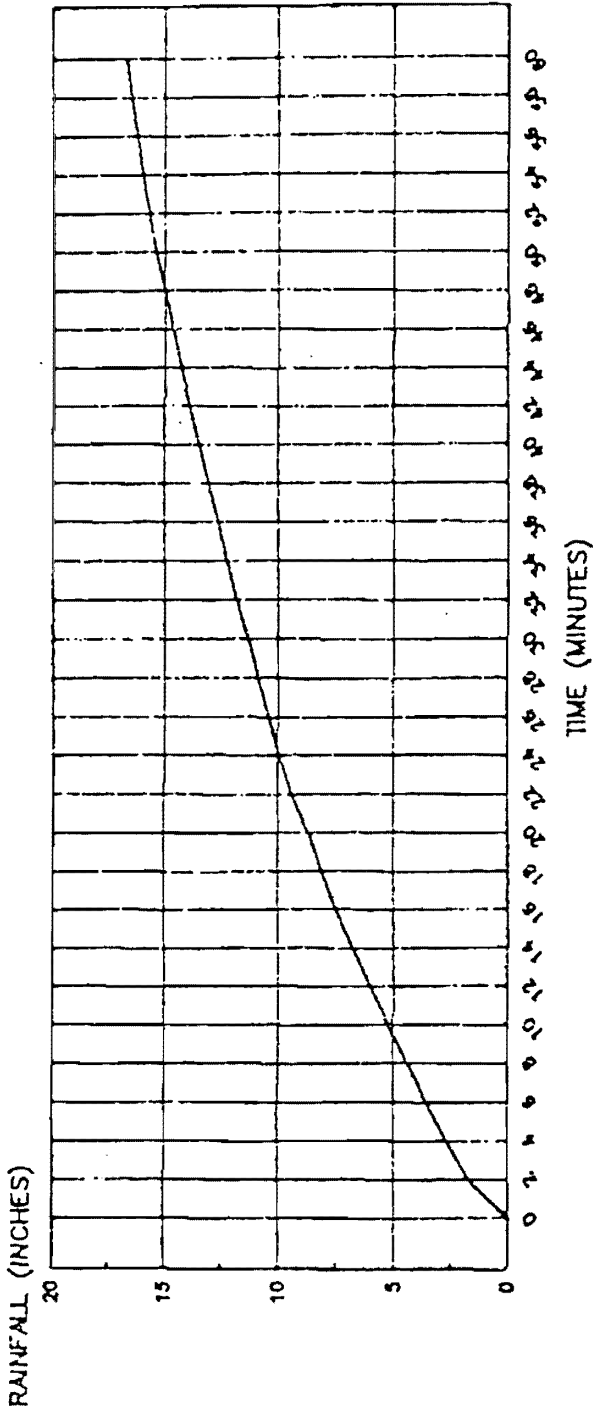


Figure 2.4-40g Yard, Grading Drainage and Surfacing Transformer & Switchyard - Sheet 3

PROBABLE MAXIMUM PRECIPITATION
BASED ON HYDROMETEOROLOGICAL REPORT NO. 56



AMENDMENT 83

WATTS BAR NUCLEAR PLANT
FINAL SAFETY
ANALYSIS REPORT

PROBABLE MAXIMUM PRECIPITATION
• POINT RAINFALL
FIGURE 2.4-40h

SCANNED DOCUMENT
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THE WBNP OPTIGRAPHICS SCANNER DATABASE

Figure 2.4-40h Probable Maximum Precipitation Point Rainfall

Figure 2.4-40i Deleted by Amendment 83

Figure 2.4-40j Deleted by Amendment 83

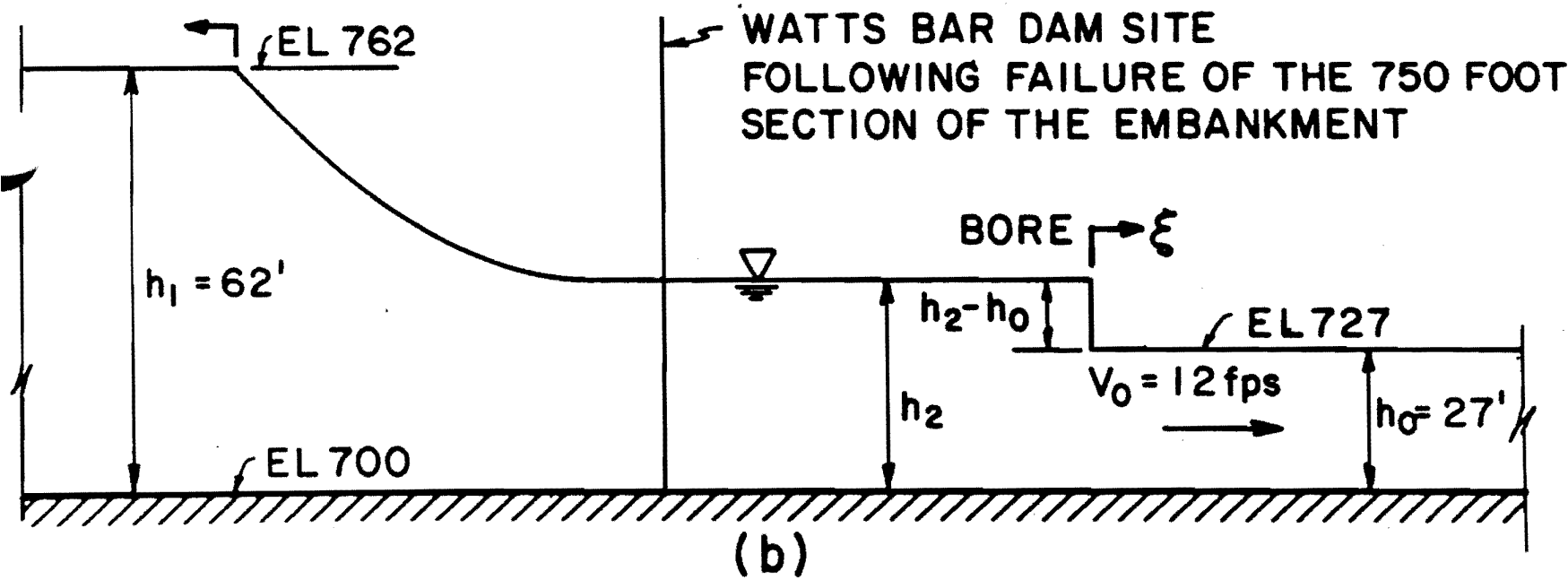
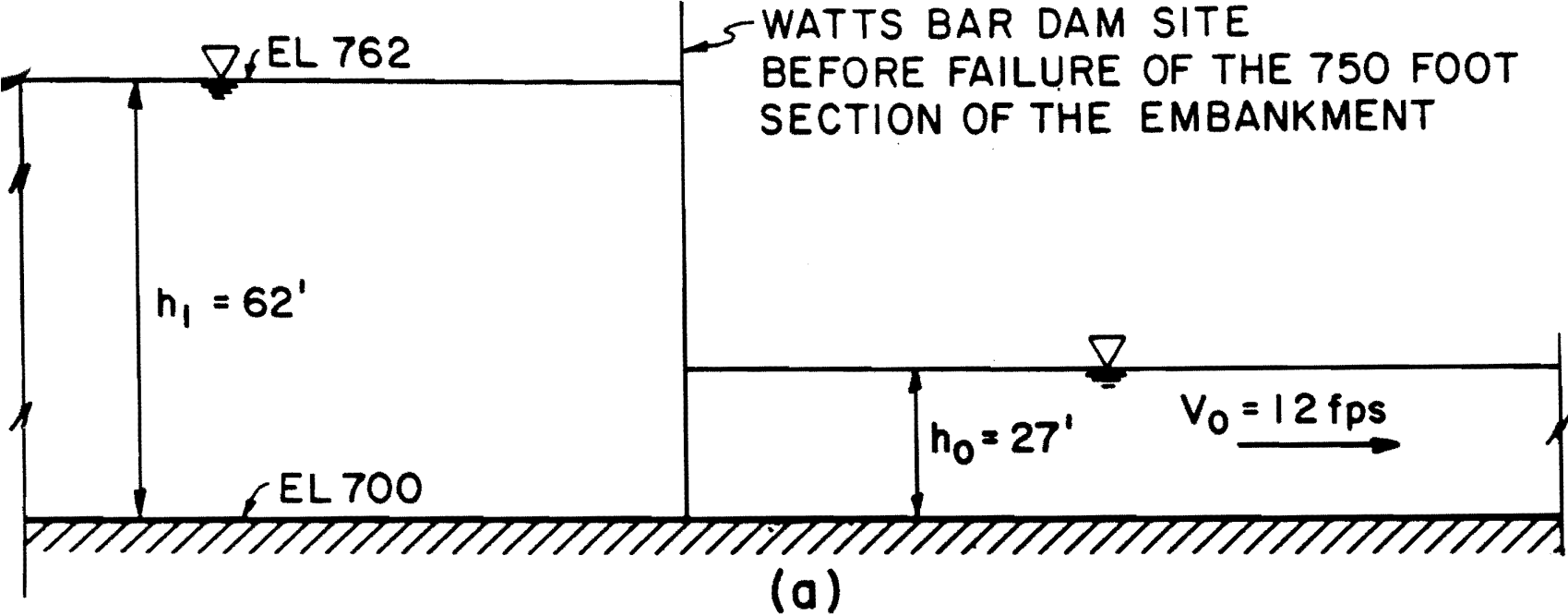
Figure 2.4-40k Deleted by Amendment 83

Figure 2.4-40L Deleted by Amendment 83

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Figure 2.4-41 thru Figure 2.4-60 Are Not Used

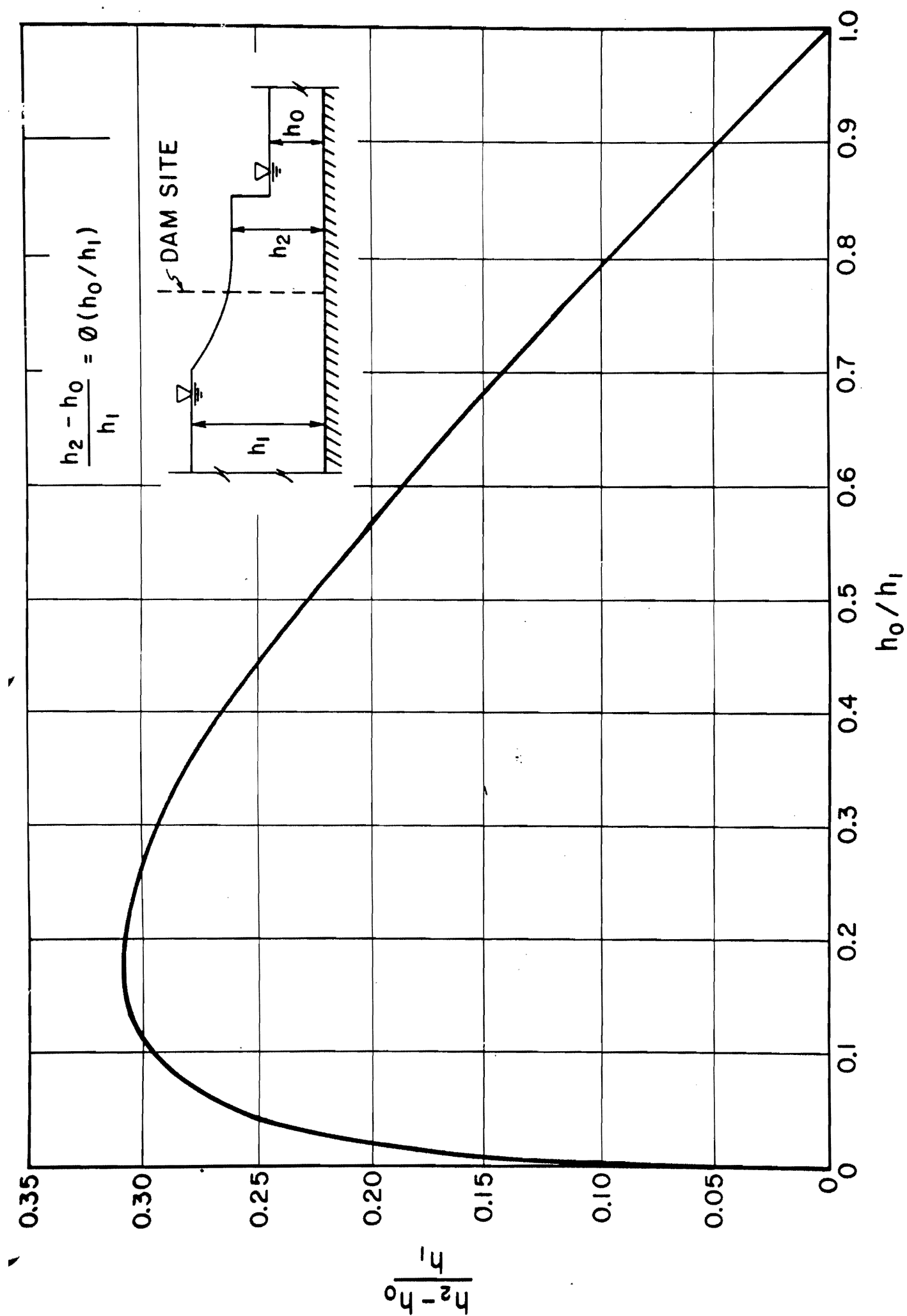
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WATTS BAR PROBABLE MAXIMUM FLOOD
WATER LEVELS BEFORE & AFTER EMBANKMENT FAILURE
FIGURE 2.4-61

Revised by Amendment 39

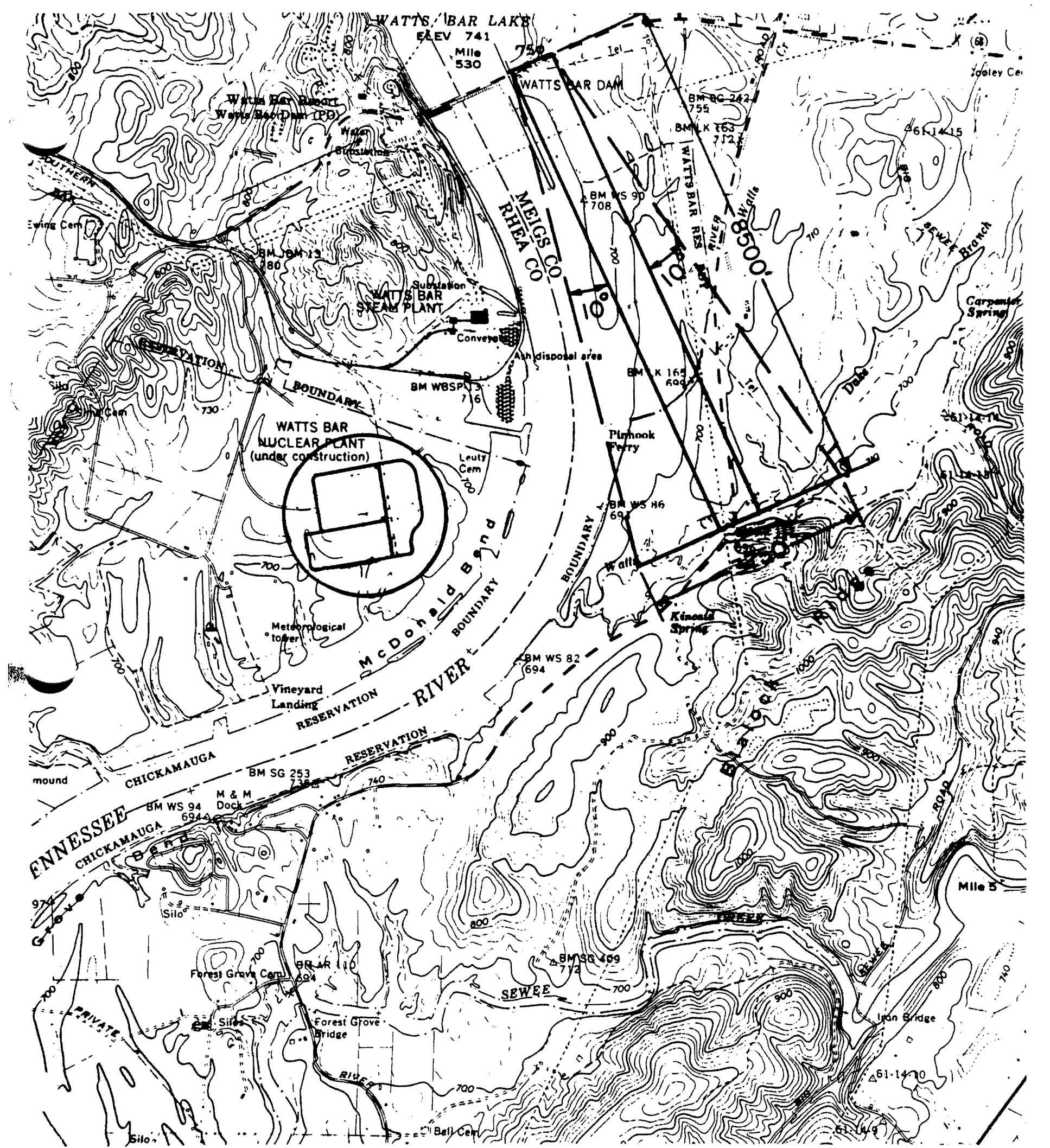
Figure 2.4-61 Watts Bar Probable Maximum Flood Water Levels Before and After Embankment Failure



RELATIVE BORE HEIGHT (AFTER J. J. STROKER, REF. 31)
FIGURE 2.4-62

Revised by Amendment 39

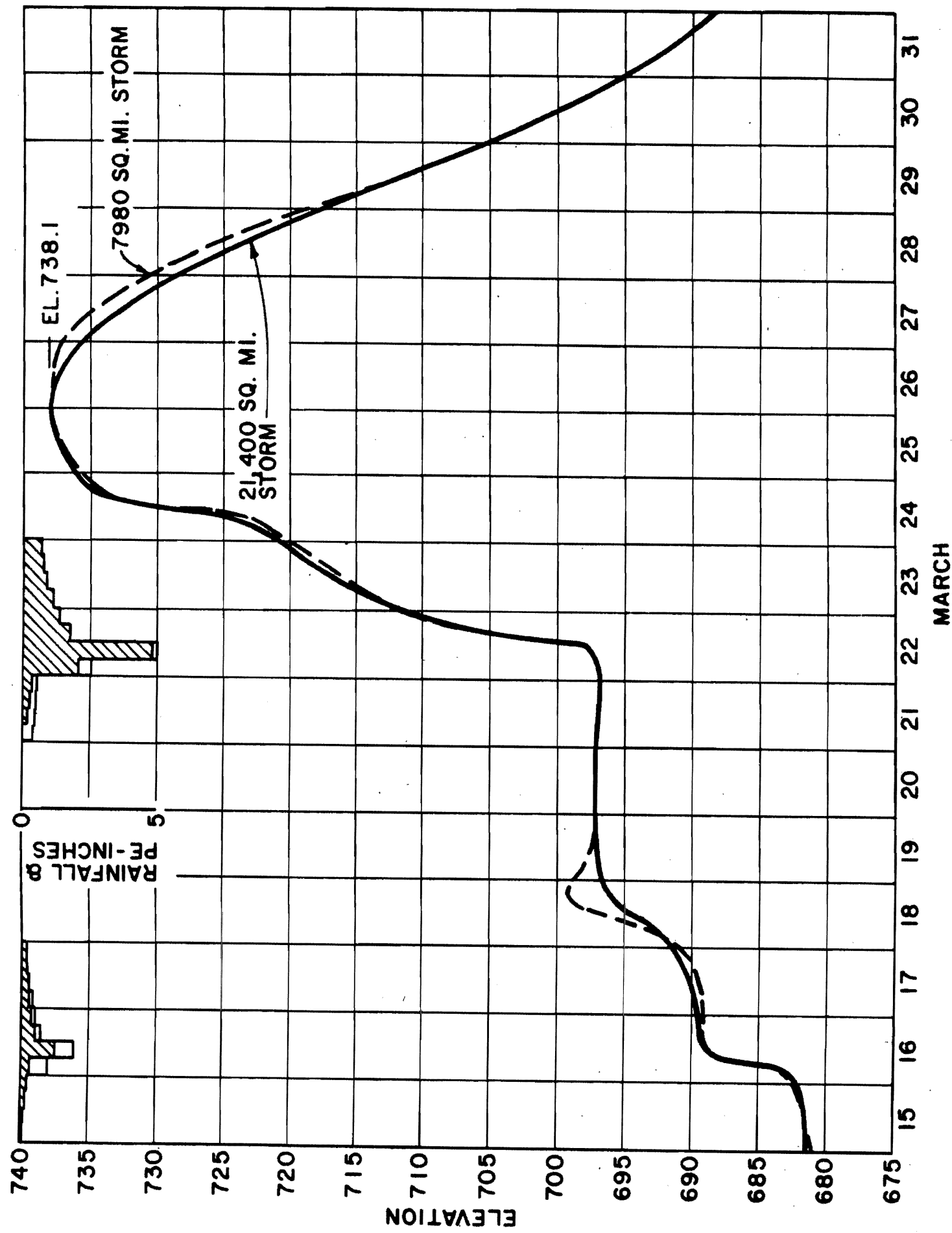
Figure 2.4-62 Relative Bore Height (After J. J. Stroker, REF. 31)



ASSUMED LIMITS OF EMBANKMENT FAILURE
WAVE EXPANSION
FIGURE 2.4-63

Revised by Amendment 39

Figure 2.4-63 Assumed Limits of Embankment Failure Wave Expansion



WATTS BAR NUCLEAR PLANT PROBABLE MAXIMUM FLOOD ELEVATION

FIGURE 2.4 - 64

Revised by Amendment 32

Figure 2.4-64 Watts Bar Nuclear Plant Probable Maximum Flood Elevation

Figure 2.4-65 thru Figure 2.4-67 Are Not Used

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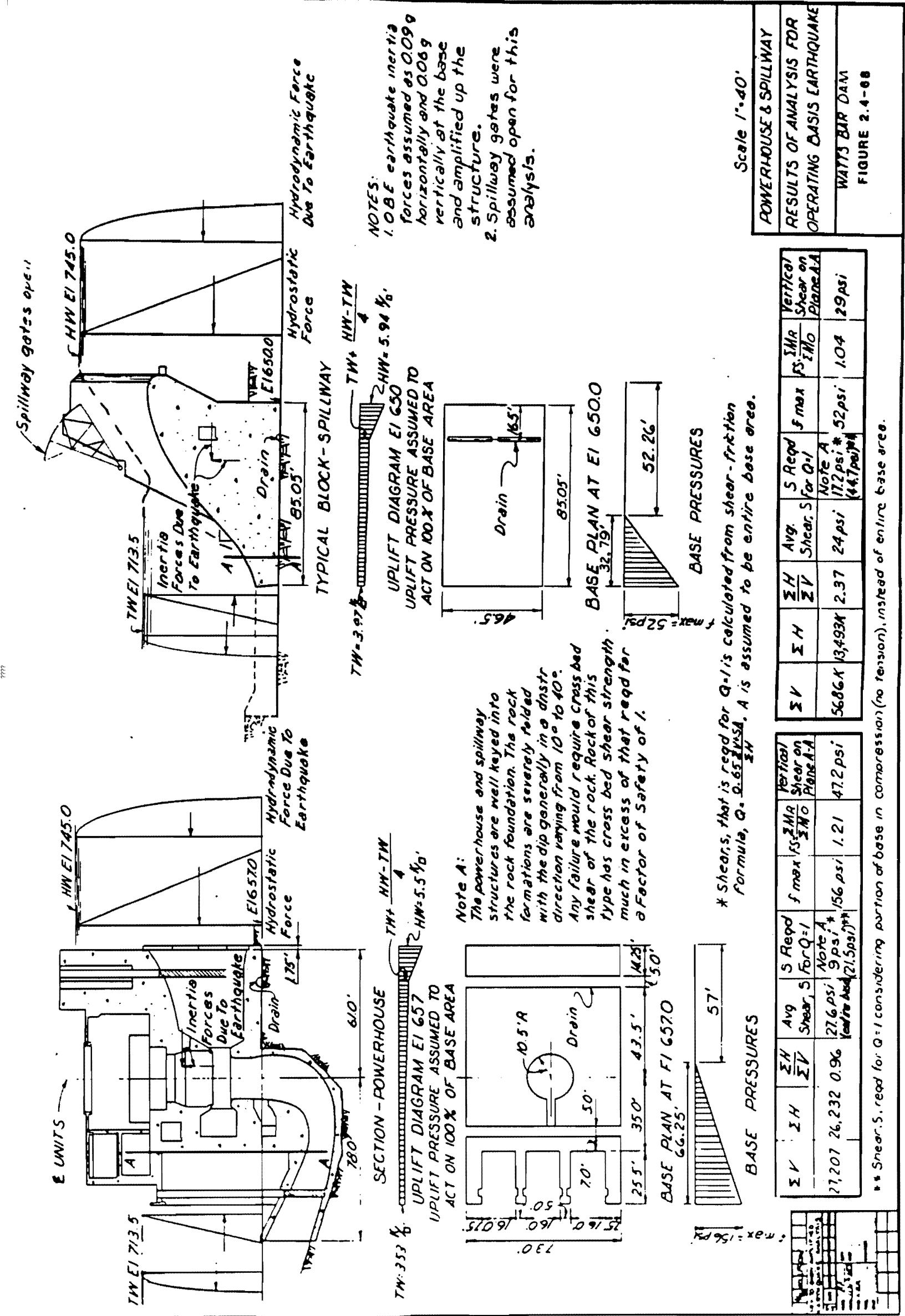


Figure 2.4-68 Powerhouse & Spillway Results of Analysis For Operating Basis Earthquake - Watts Bar Dam

Figure 2.4-69 Deleted by Amendment 103

Figure 2.4-70 Deleted by Amendment 83

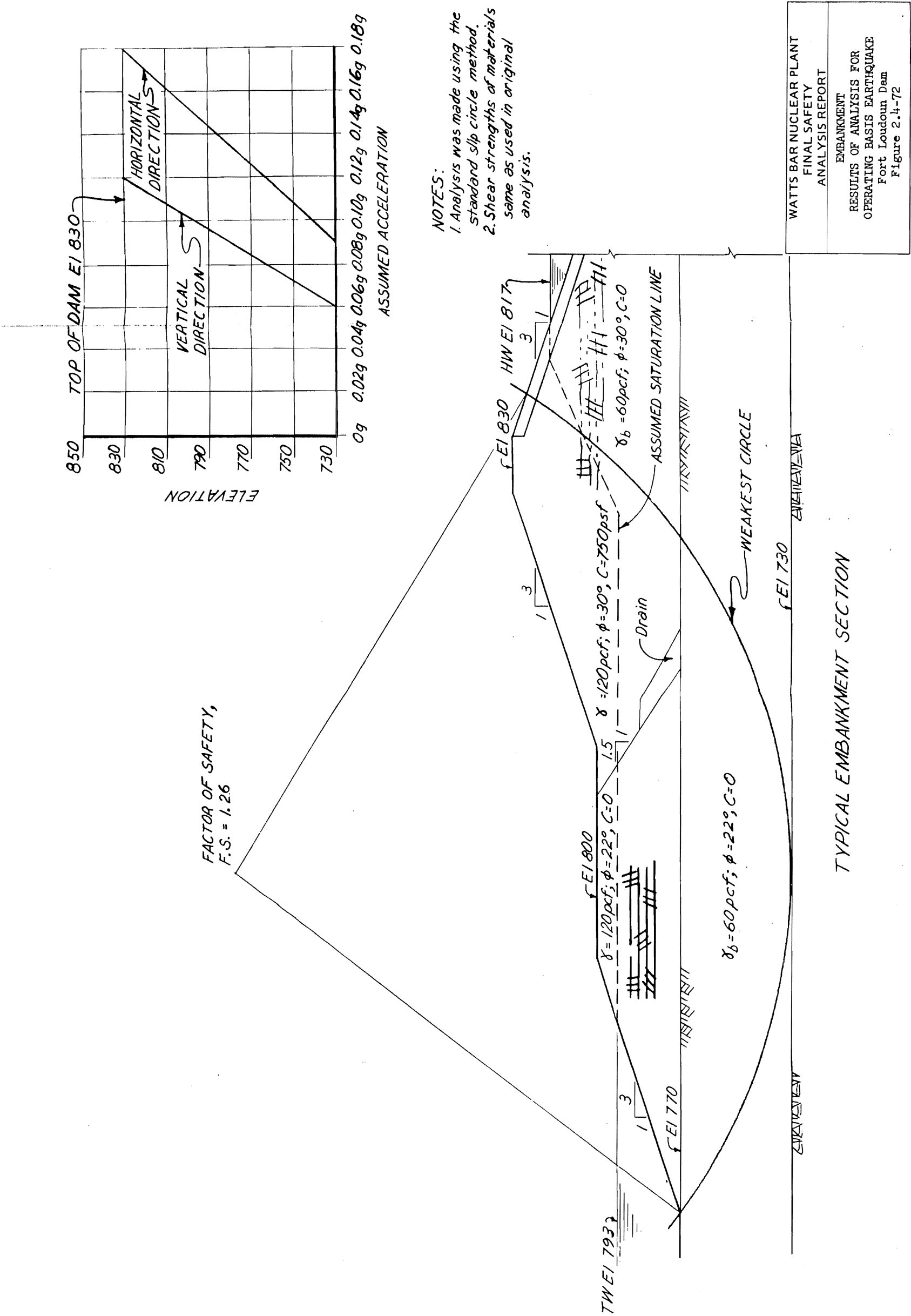


Figure 2.4-72 Embankment Results Of Analysis For Operating Basis Earthquake - Fort Loudoun Dam

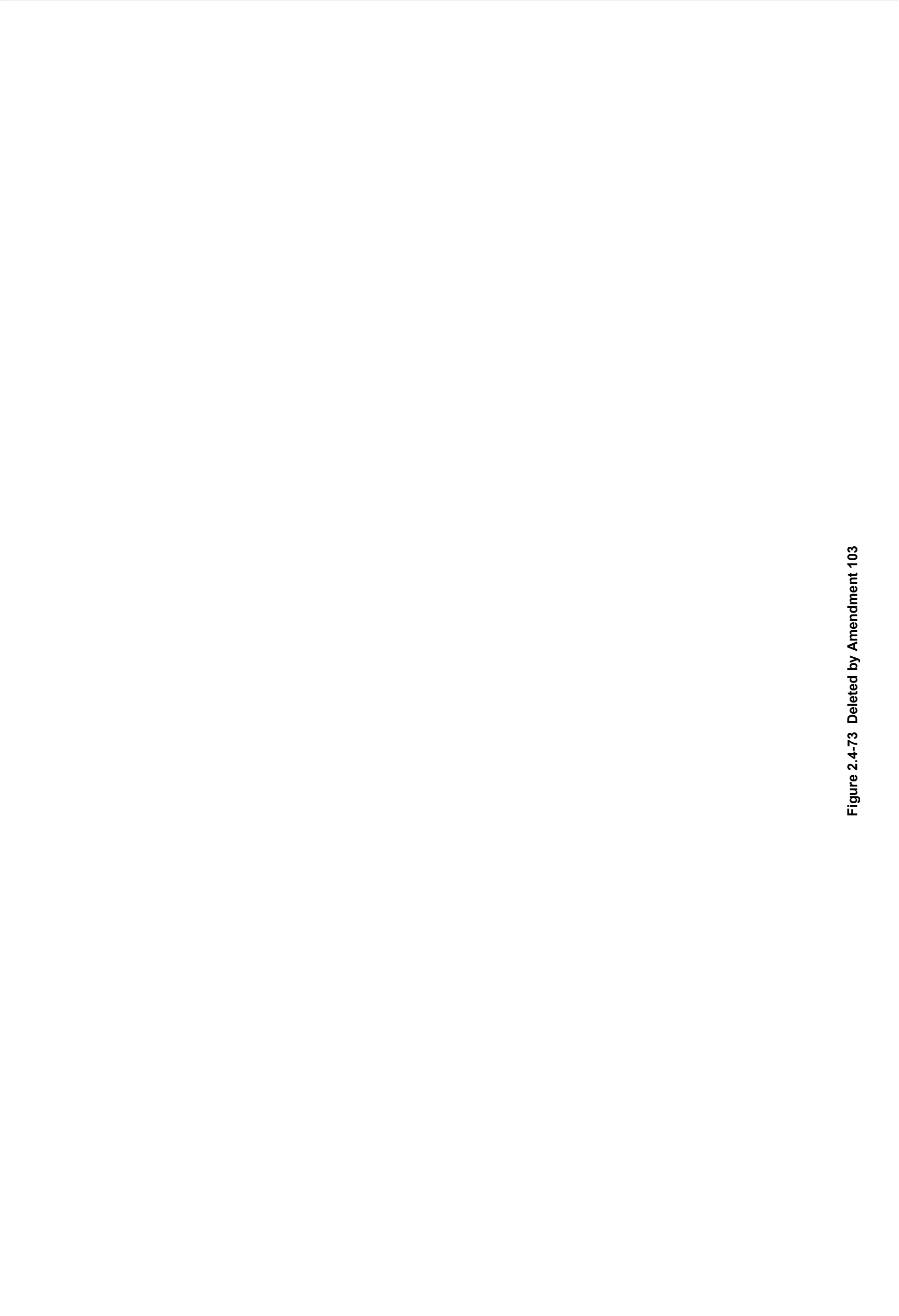


Figure 2.4-73 Deleted by Amendment 103

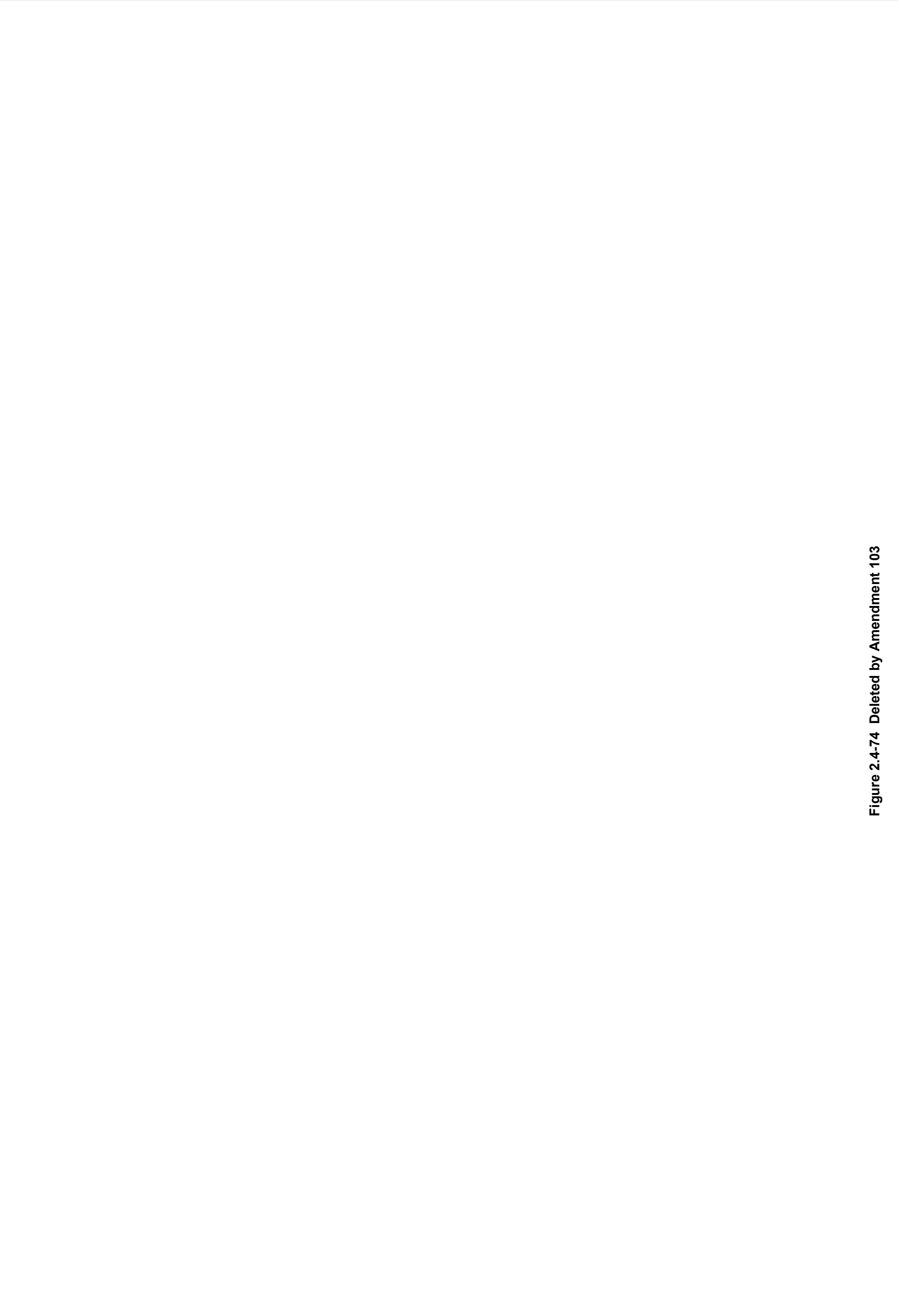


Figure 2.4-74 Deleted by Amendment 103

Figure 2.4-75 Deleted by Amendment 103

Figure 2.4-76 Analysis For OBE & 1/2 PMF Assumed Condition of Dam After Failure Norris Dam

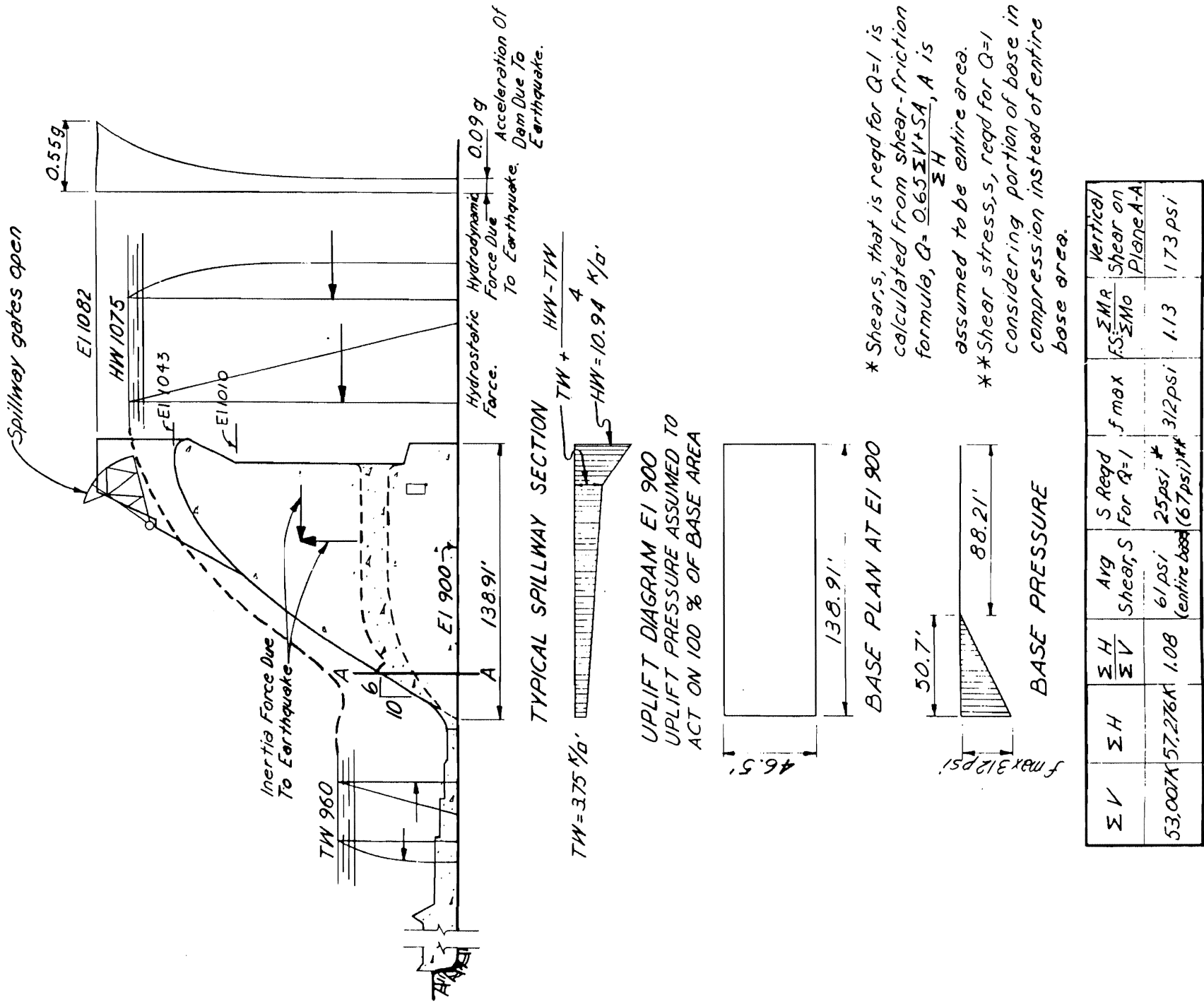


Figure 2.4-77 Spillway & Nonoverflow Results of Analysis For Operating Basis Earthquake -Cherokee Dam

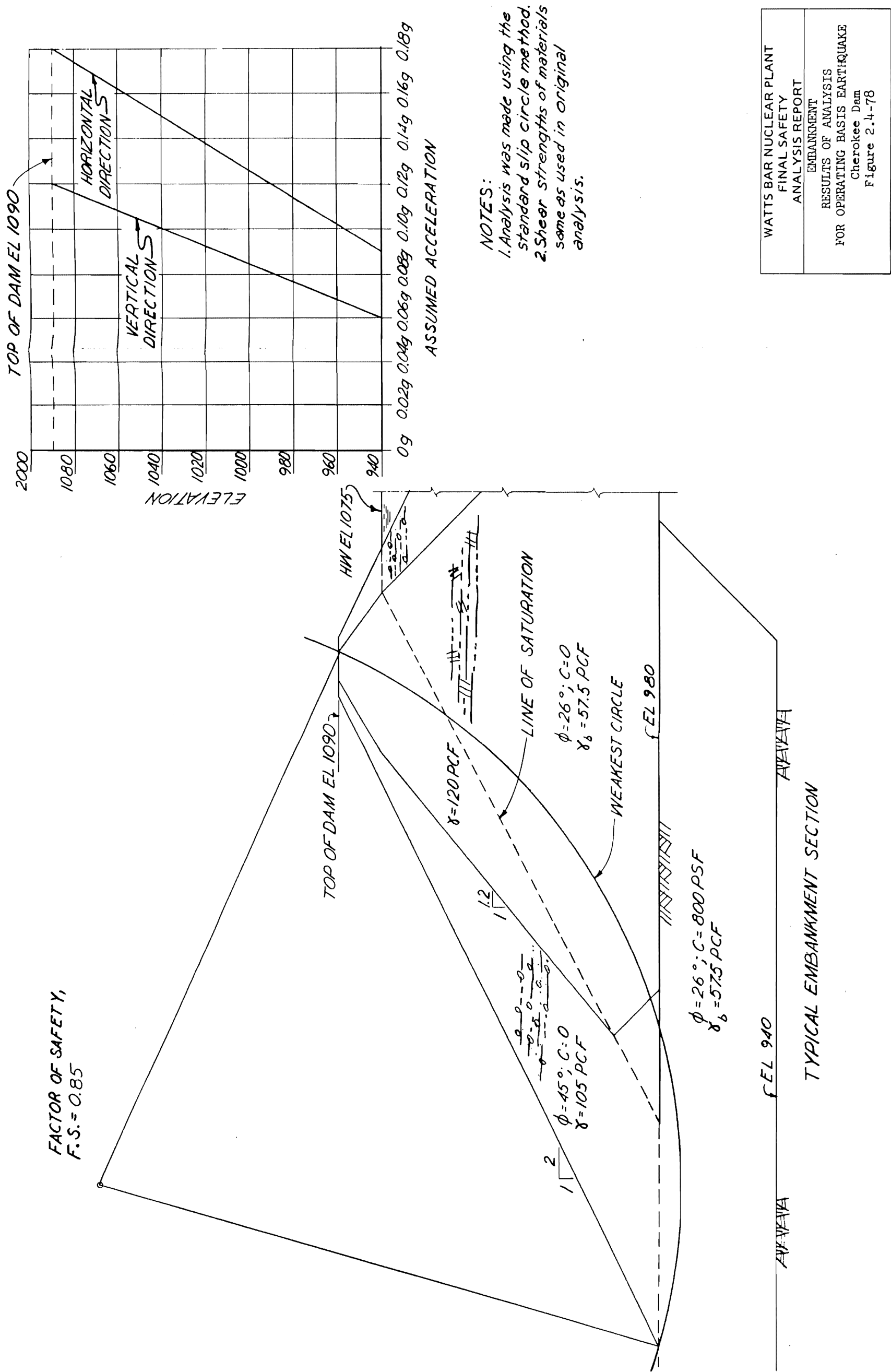
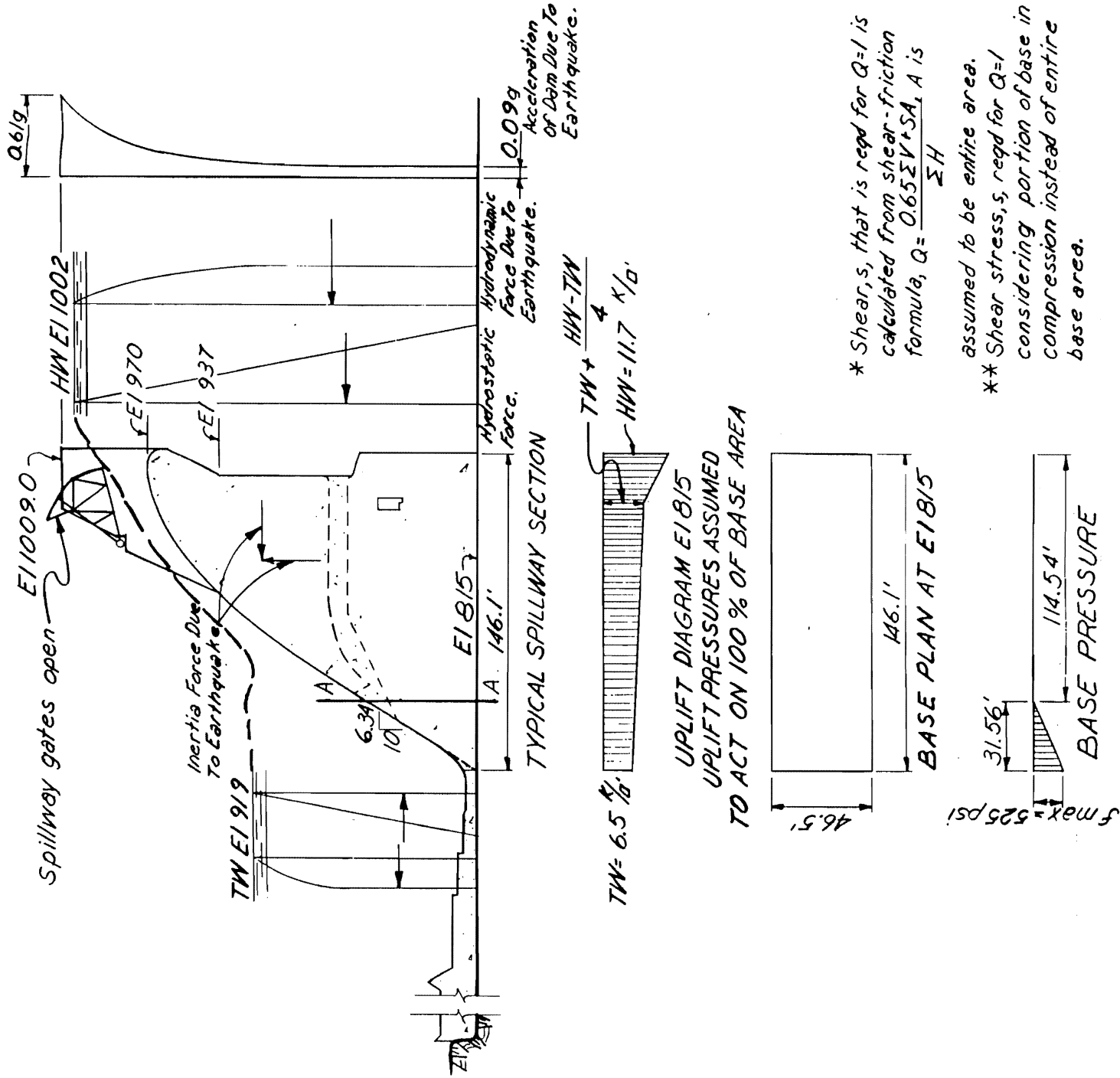


Figure 2.4-78 Embankment Results of Analysis For Operating Basis Earthquake - Cherokee Dam

Figure 2.4-79 Assumed Condition of Dam After Failure PBE And 1/2 Probable Max Flood - Cherokee Dam



NOTES:

1. Vertical acceleration of the spillway at the base assumed to be 0.06 g. By dynamic analysis, amplification of acceleration above the base was determined to be 0.13 g at the top.
2. Horizontal acceleration of the spillway at the base assumed to be 0.09 g. By dynamic analysis, amplification of acceleration above the base was determined to be 0.61 g at the top.
3. Spillway gates assumed open for this analysis.

WATTS BAR NUCLEAR PLANT FINAL SAFETY ANALYSIS REPORT
SPILLWAY & NONOVERFLOW RESULTS OF ANALYSIS FOR OPERATING BASIS EARTHQUAKE Douglas Dam Figure 2.4-80

Figure 2.4-80 Spillway & Nonoverflow Results of Analysis For Operating Basis Earthquake - Douglas Dam

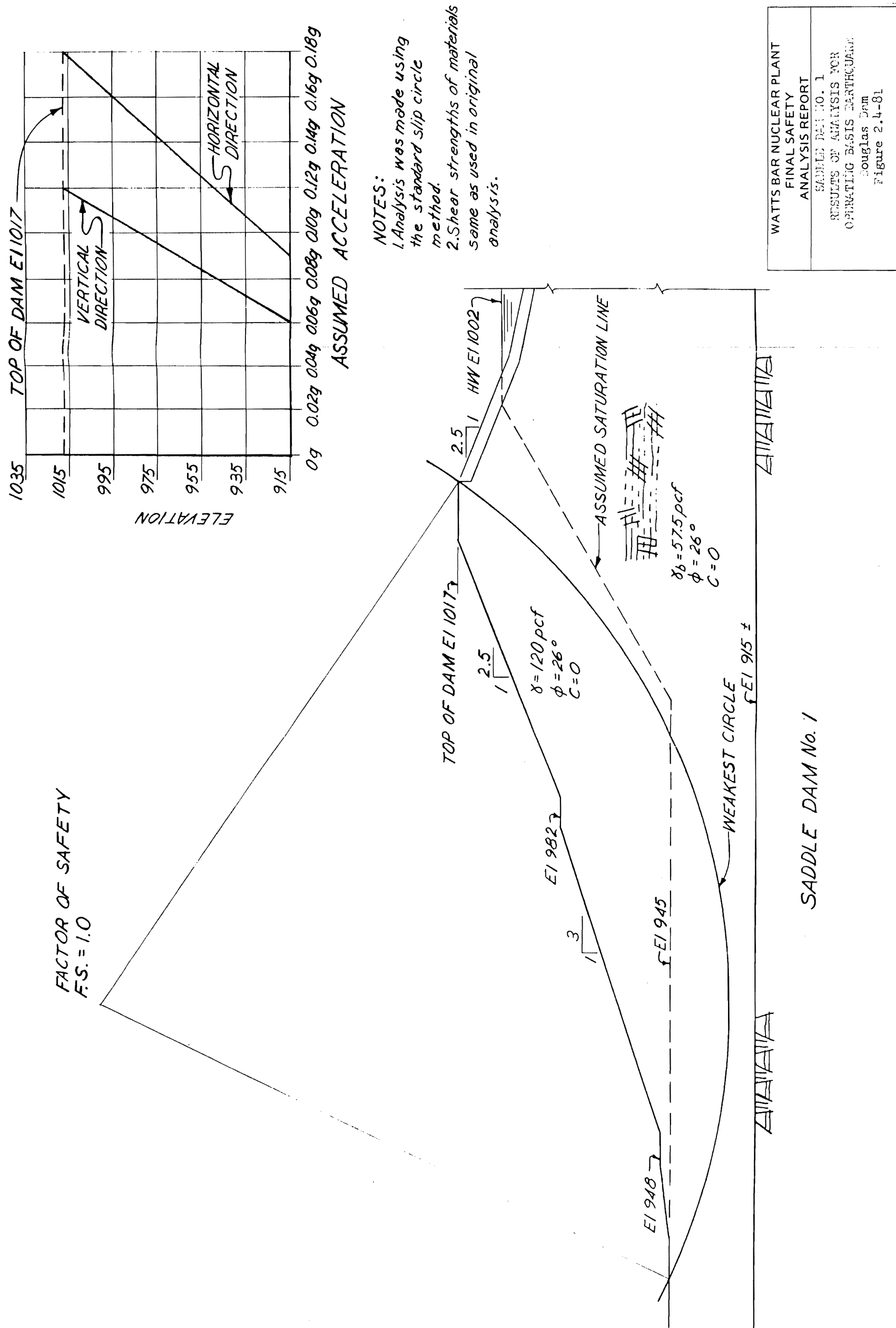


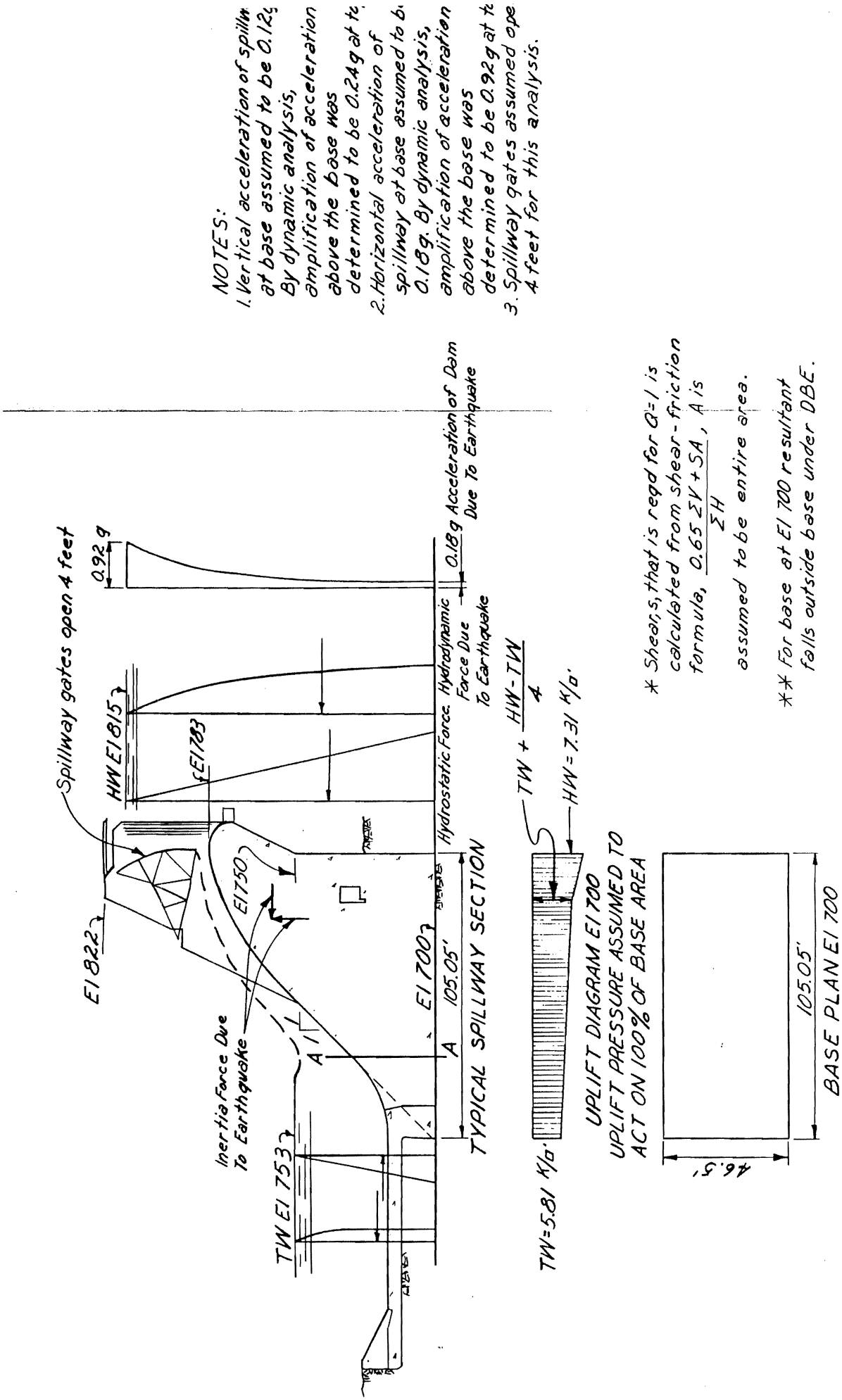
Figure 2.4-81 Saddle Dam No. 1 Results of Analysis For Operating Basis Earthquake - Douglas Dam

Figure 2.4-82 Douglas Dam Assumed Condition of Dam After Failure aBE And 1/2 Probable Maximum Flood - Douglas Project

Figure 2.4-83 Fontana Dam Assumed Condition of Dam after Failure OBE And 1/2 Probable Maximum Flood

Figure 2.4-84 Deleted by Amendment 63

Figure 2.4-85 Deleted by Amendment 63



WATTS BAR NUCLEAR PLANT FINAL SAFETY ANALYSIS REPORT
SPILLWAY RESULTS OF ANALYSIS FOR SSE EARTHQUAKE Fort Loudoun Dam Figure 2.4-86

$\sum V$	$\sum H$	$\frac{\sum H}{\sum V}$	Avg shear	S_{reqd} for $Q=1$	f_{max}	$F.S. \frac{\sum H}{\sum V}$
19,254 K	29,534 K	1.62	42 psi entire base	25 psi *	* *	0.9

BASE PRESSURE **

Figure 2.4-86 Spillway Results of Analysis For SSE Earthquake Fort Loudoun Dam

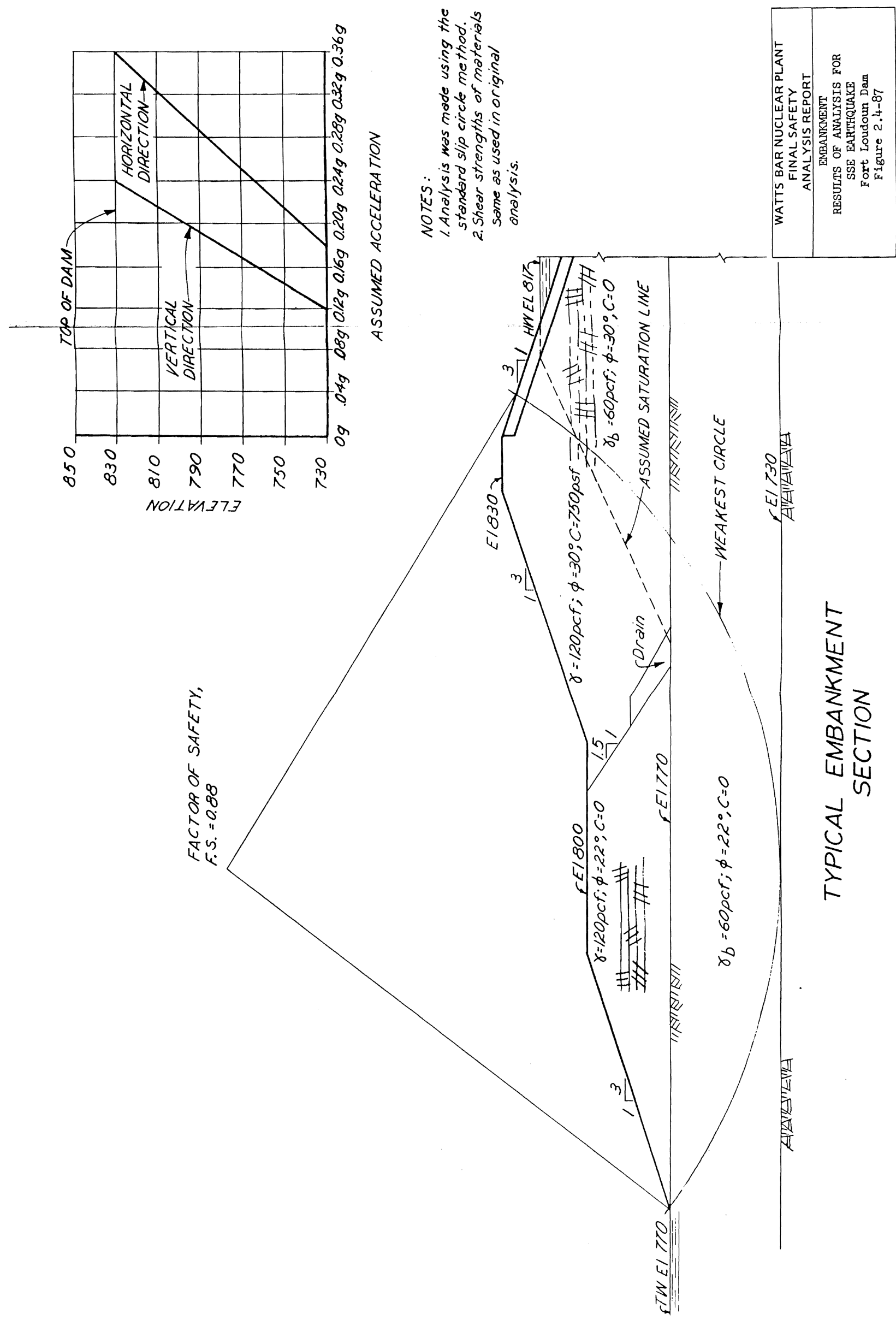


Figure 2.4-87 Embankment Results of Analysis For SSE Earthquake Fort Loudoun Dam

Figure 2.4-88 Fort Loudoun Dam Assumed Condition of Dam After Failure SSE Combined With a 25 Year Flood - Fort Loudoun Dam

Figure 2.4-89 Tellico Dam Assumed Condition of Dam After Failure SSE Combined With a 25 Year Flood Tellico Project

Figure 2.4-90 Norris Dam SSE + 25 Year Flood Judged Condition of Dam After Failure - Norris Dam

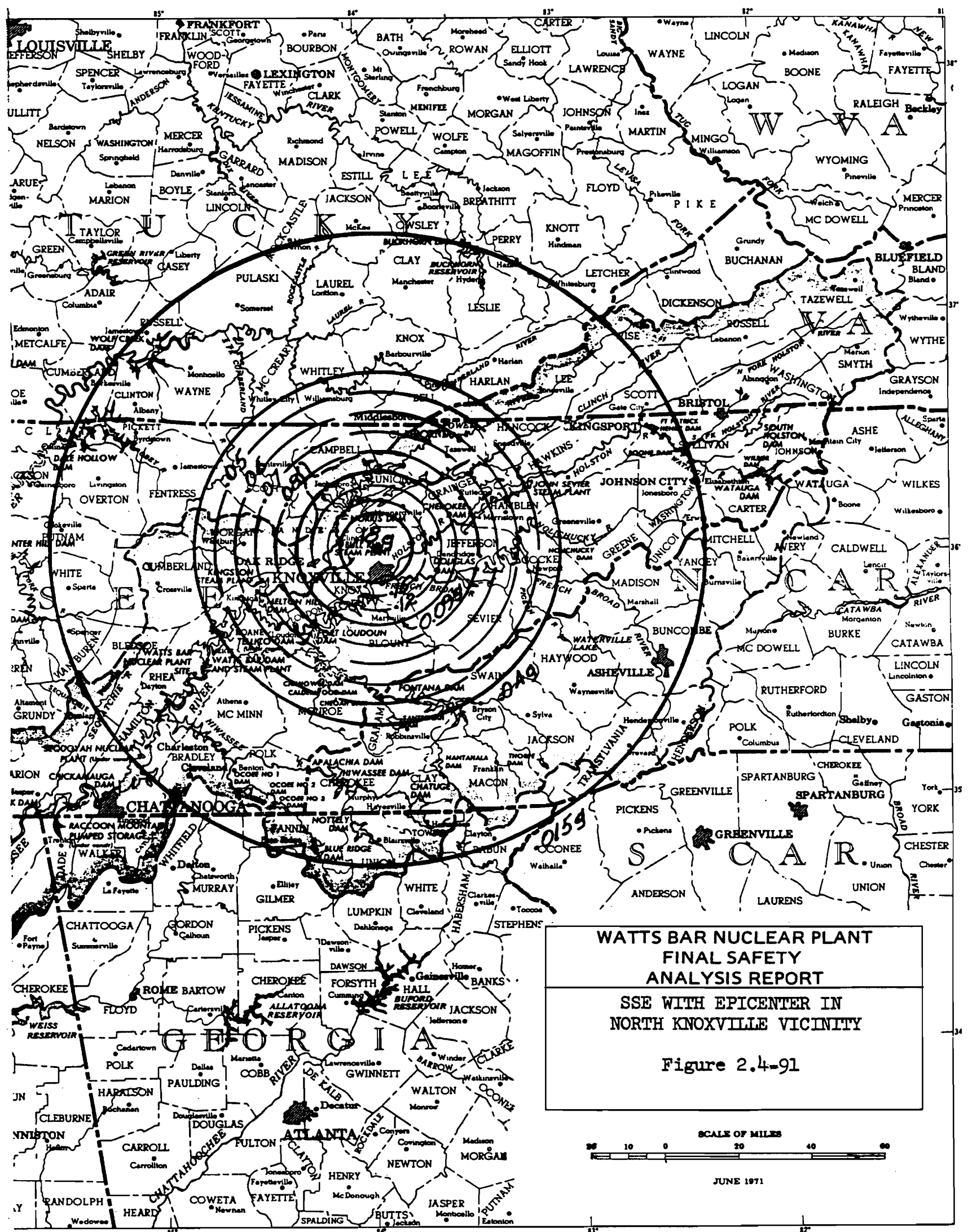


Figure 2.4-91 SSE With Epicenter In North Knoxville Vicinity

Figure 2.4-92 Deleted by Amendment 103

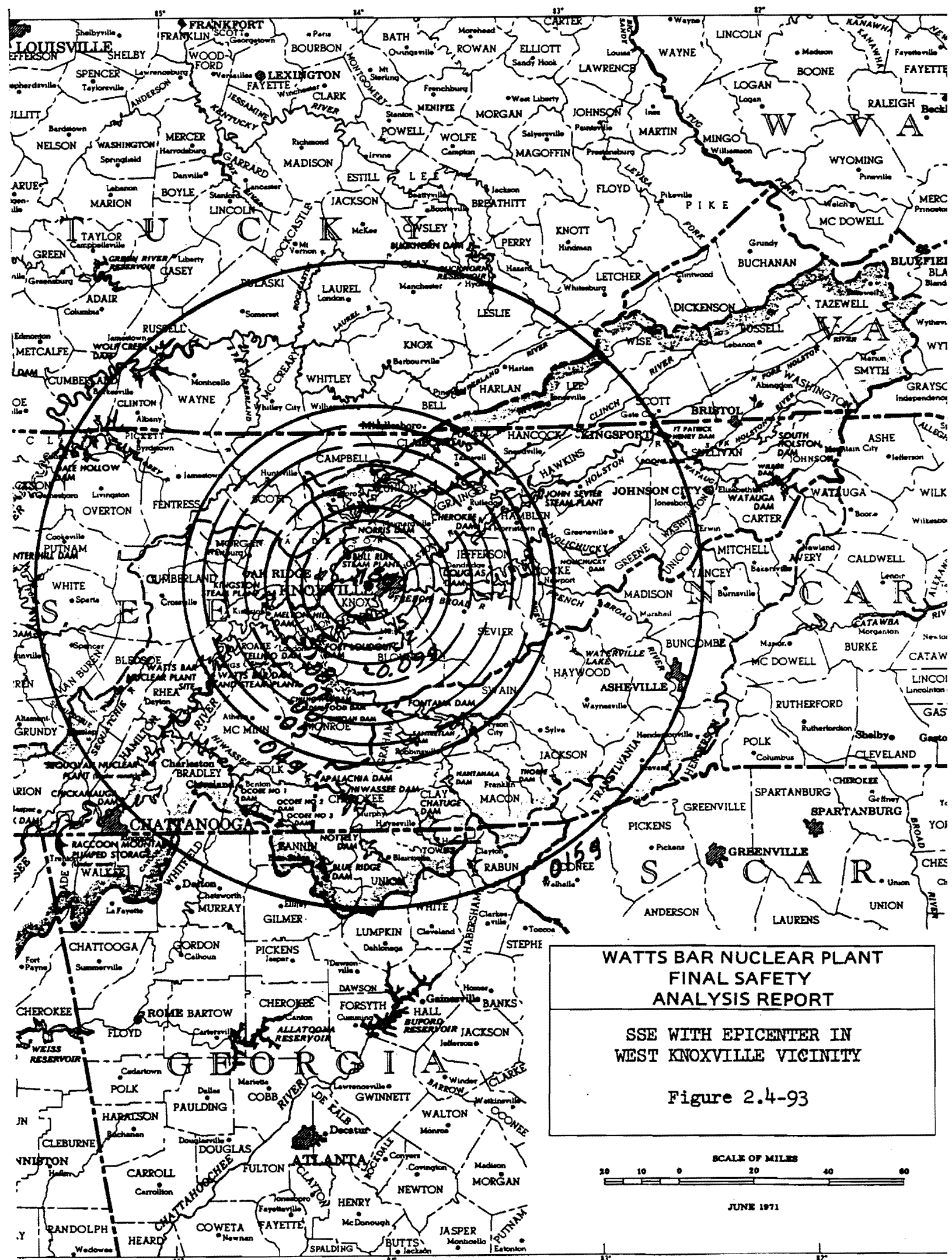


Figure 2.4-93 SSE With Epicenter In West Knoxville Vicinity

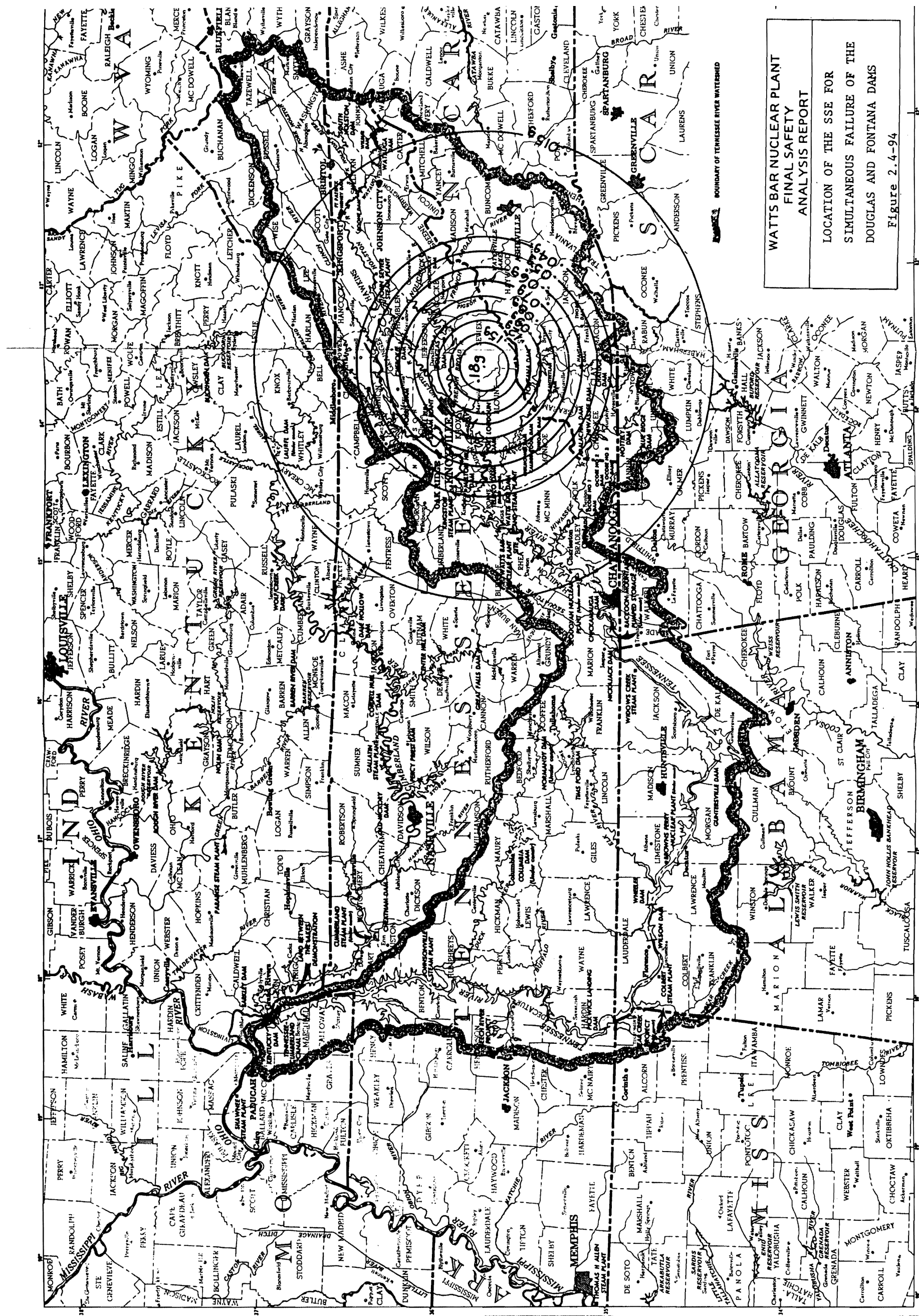


Figure 2.4-94 Location of SSE For Simultaneous Failure of The Douglas and Fontana Dams

Figure 2.4-95 Deleted by Amendment 103

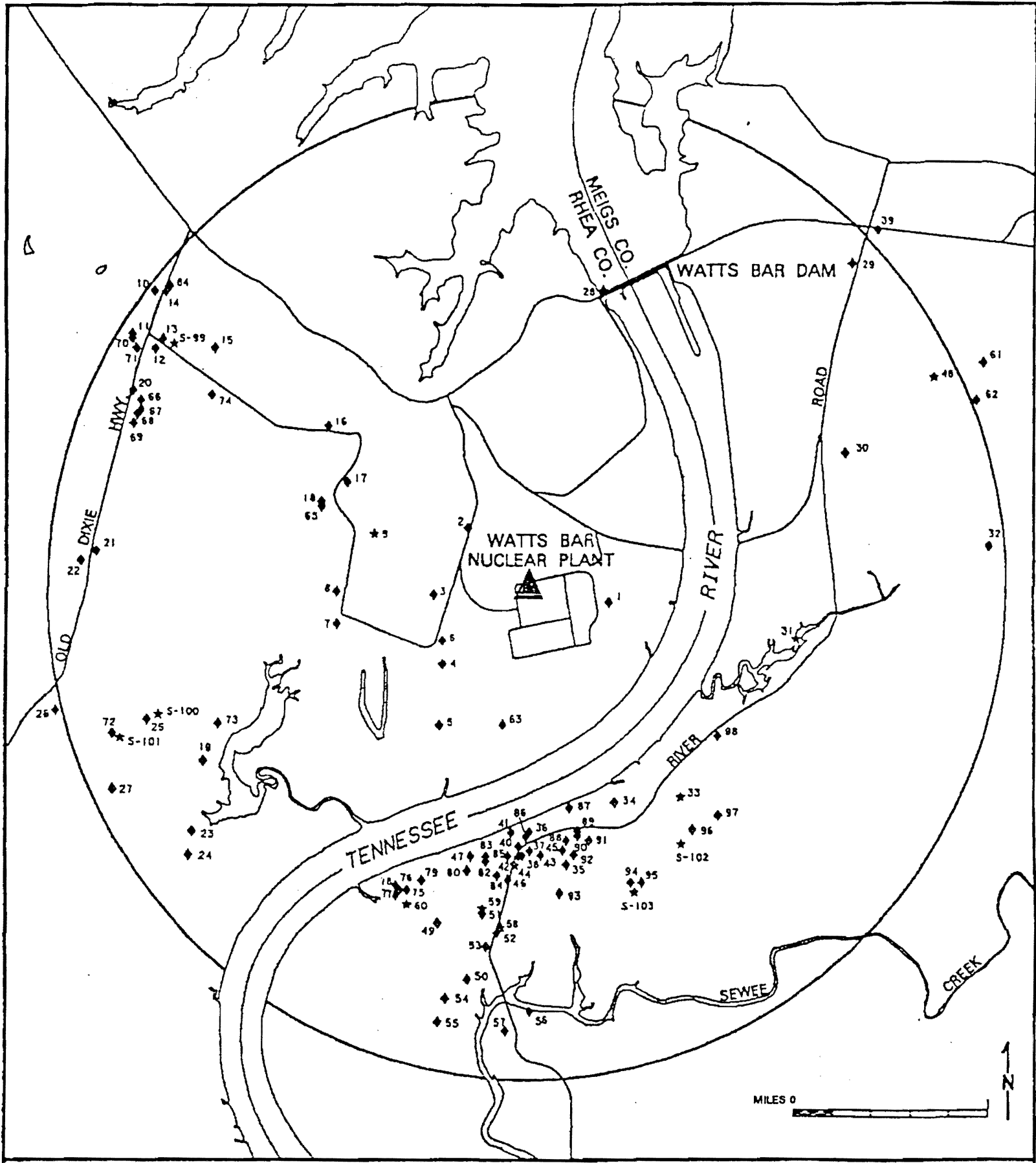
Figure 2.4-96 Deleted by Amendment 103

Figure 2.4-97 Deleted by Amendment 103

Figure 2.4-98 Not Used

Figure 2.4-100 Deleted by Amendment 83

Figure 2.4-101 Deleted by Amendment 33



- LEGEND
- ◆ WELL
 - ★ SPRING
 - ROADS
 - 2 MILE RADIUS OF PLANT SITE

AMENDMENT 83

WATTS BAR NUCLEAR PLANT
FINAL SAFETY
ANALYSIS REPORT

WELL AND SPRING INVENTORY
WITHIN 2 MILE RADIUS OF WATTS BAR
NUCLEAR PLANT SITE
FSAR FIG 2.4-102

SCANNED DOCUMENT
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THE WBNP OPTICGRAPHICS SCANNER DATABASE

Figure 2.4-102 Wells And Spring Inventory Within 2-Mile Radius of Watts Bar Nuclear Plant Site

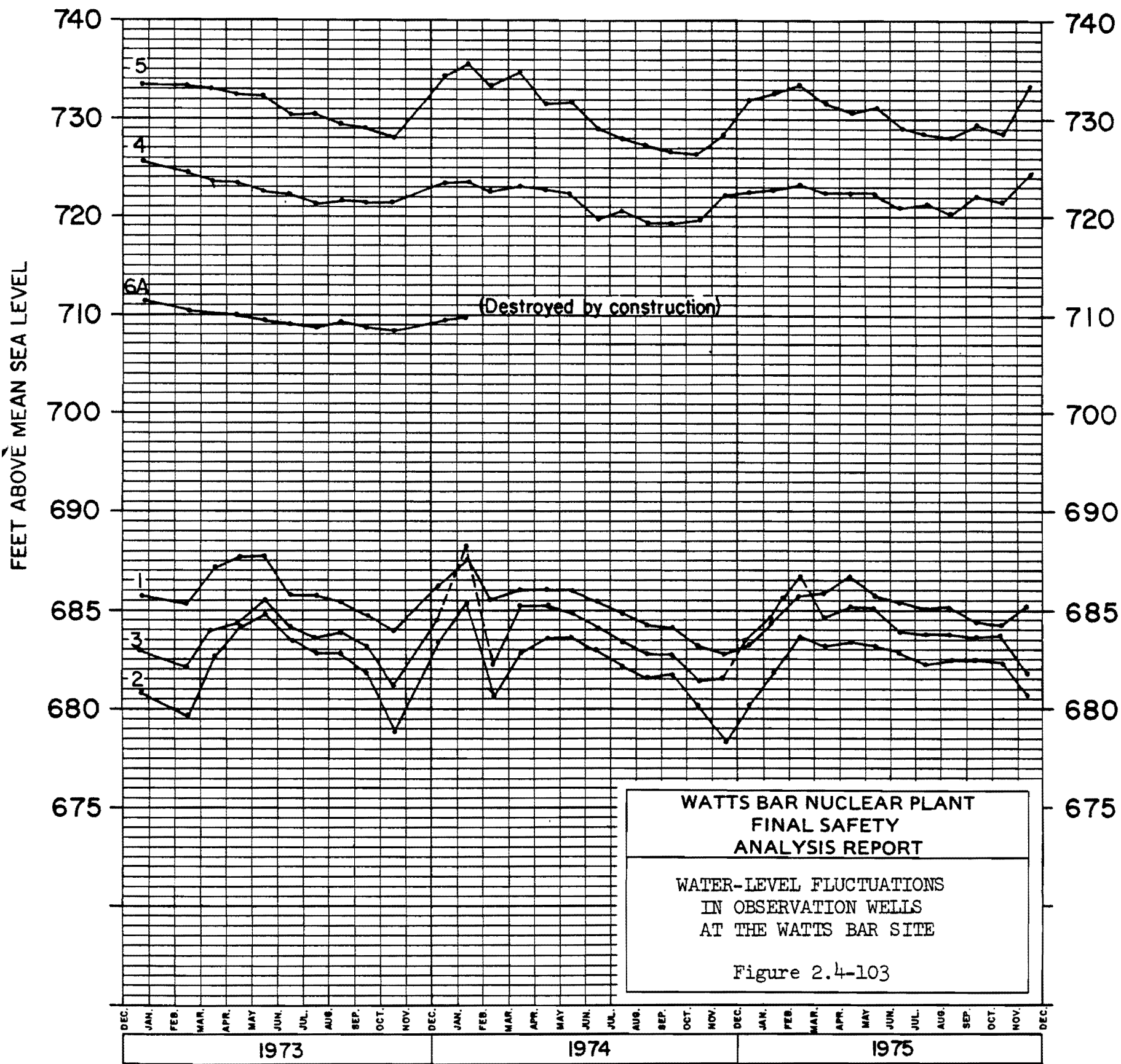
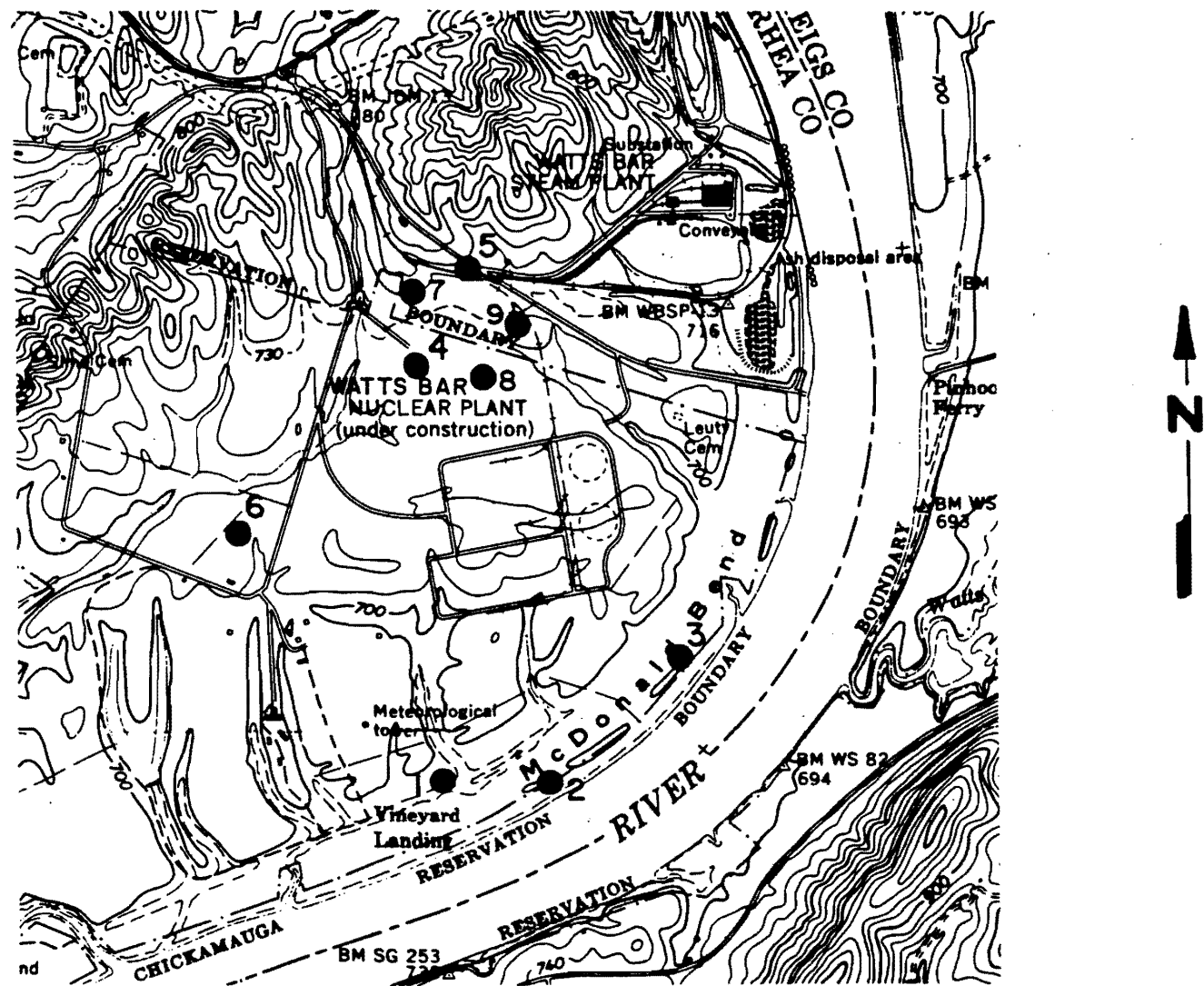


Figure 2.4-103 Water-Level Fluctuations In Observation Wells at The Watts Bar Site



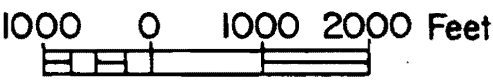
NOTE:

Topographic base from U.S.G.S - T.V.A. 7.5 minute quadrangle, Decatur, Tenn., 118-SE, Contour interval 20 feet.

LEGEND:

●² - Ground-water observation well showing number.

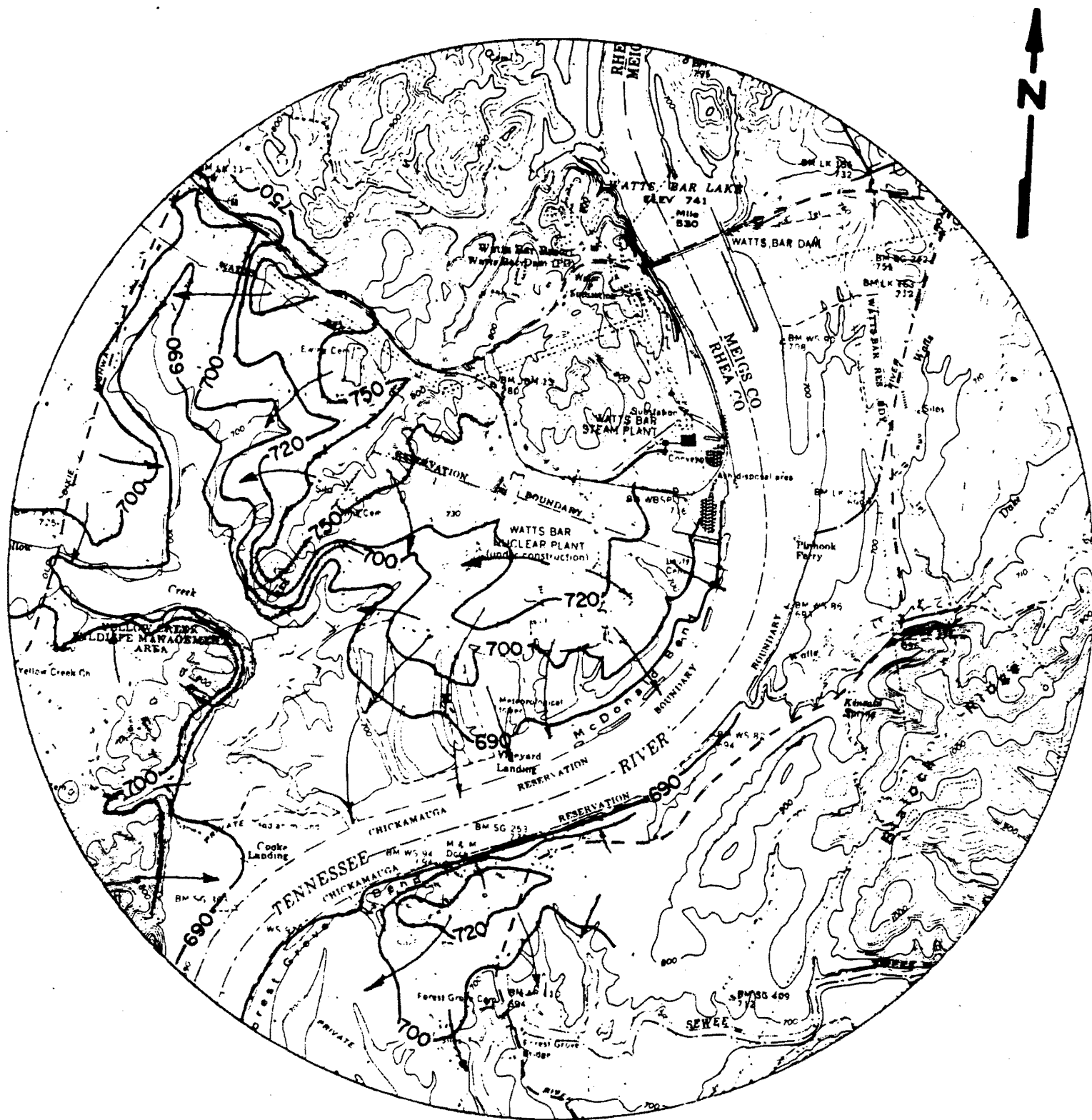
SCALE:



Revised by Amendment 50

WATTS BAR NUCLEAR PLANT FINAL SAFETY ANALYSIS REPORT
LOCATIONS OF GROUND - WATER OBSERVATION WELLS FIGURE 2.4-104

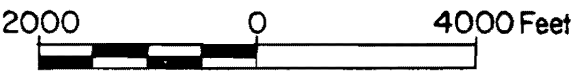
Figure 2.4-104 Locations of Ground - Water Observation Wells



EXPLANATION:

- 700 — Water table contour, in feet above mean sea level.
- General direction of ground-water movement.

SCALE:



Revised by Amendment 50

WATTS BAR NUCLEAR PLANT FINAL SAFETY ANALYSIS REPORT
GENERALIZED WATER-TABLE CONTOUR MAP
Figure 2.4-105

Figure 2.4-105 Generalized Water-Table Contour Map January 1972

DESIGN PRESSURE & TEMPERATURE DATA		
Line Design Pressure (PSI)	Design Temperature (°F)	
1	450	550
2	600	400
3	100	100

1. All design pressures are based on the design temperature of the material.
2. The design pressure is based on the design temperature of the material.
3. The design temperature is based on the design pressure of the material.
4. The design temperature is based on the design pressure of the material.
5. The design temperature is based on the design pressure of the material.
6. The design temperature is based on the design pressure of the material.
7. The design temperature is based on the design pressure of the material.
8. The design temperature is based on the design pressure of the material.
9. The design temperature is based on the design pressure of the material.
10. The design temperature is based on the design pressure of the material.

- NOTES:
1. All design pressures are based on the design temperature of the material.
 2. The design pressure is based on the design temperature of the material.
 3. The design temperature is based on the design pressure of the material.
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 8. The design temperature is based on the design pressure of the material.
 9. The design temperature is based on the design pressure of the material.
 10. The design temperature is based on the design pressure of the material.
- REFERENCE DRAWING:
1. All design pressures are based on the design temperature of the material.

Revised by Amendment

WATTS BAR NUCLEAR PLANT FINAL SAFETY ANALYSIS REPORT POWERHOUSE UNITS 1 & 2 FLOW DIAGRAM RESIDUAL HEAT REMOVAL SYSTEM TVA DWG NO. 47W010-1 R10 FIGURE 2.4-107

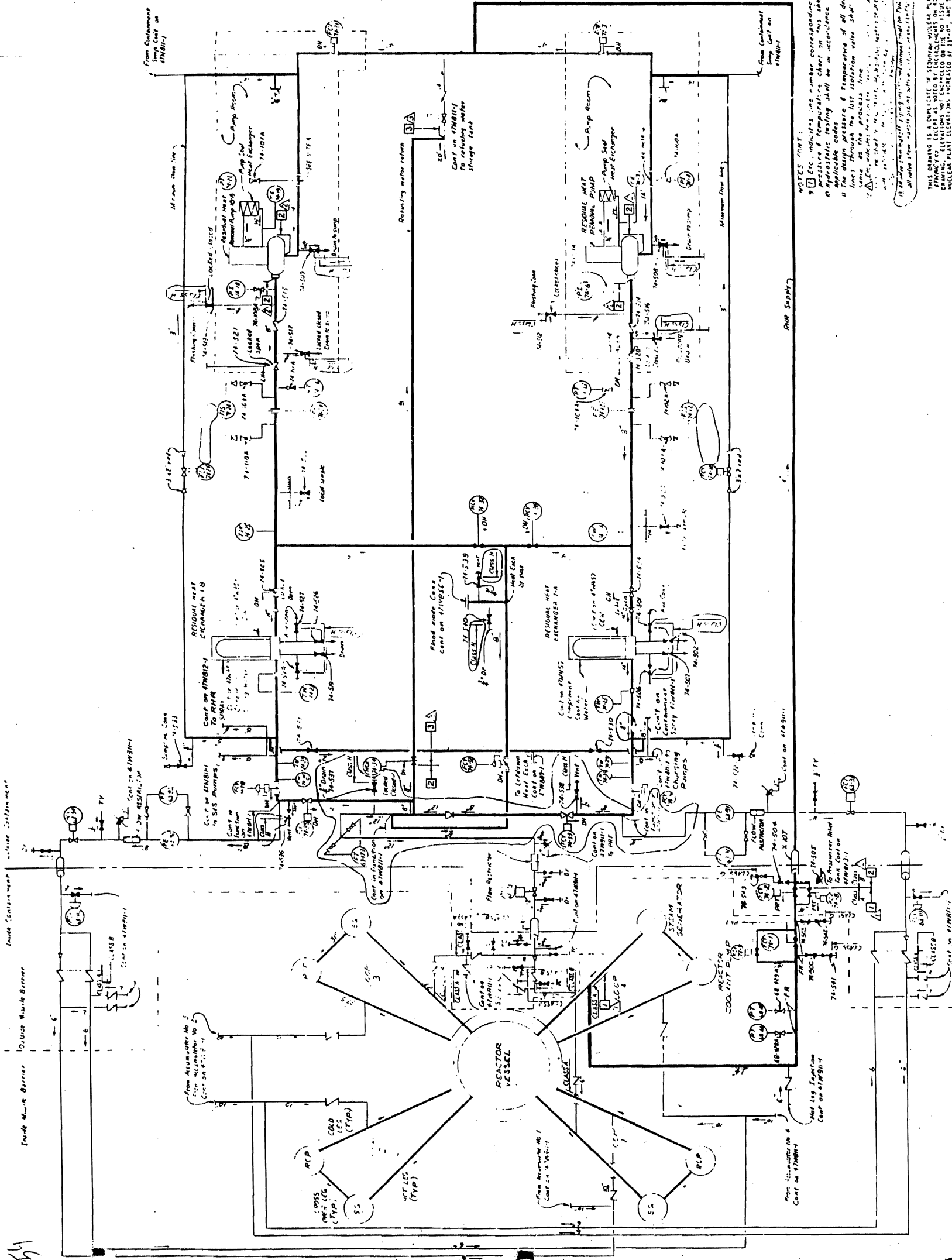
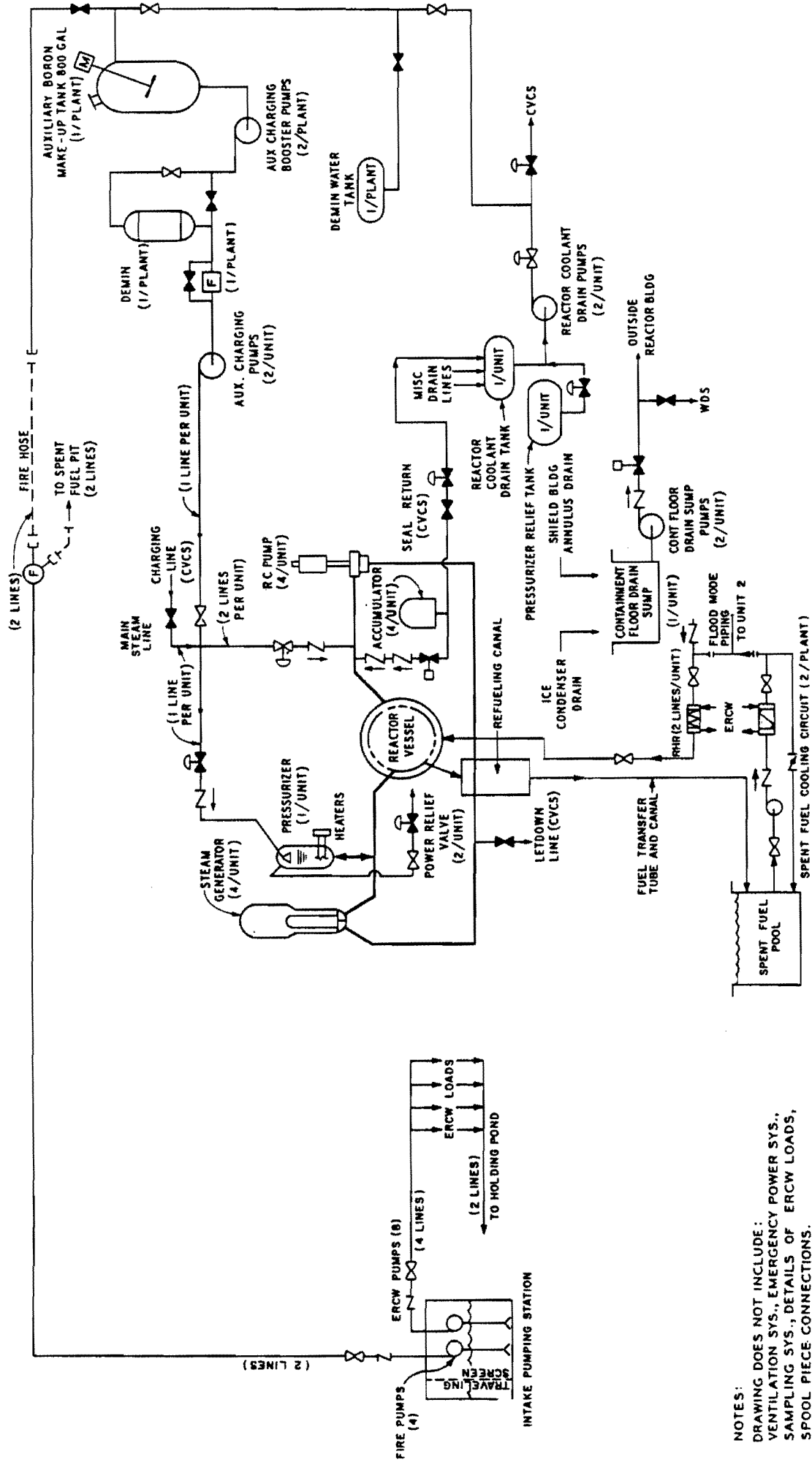


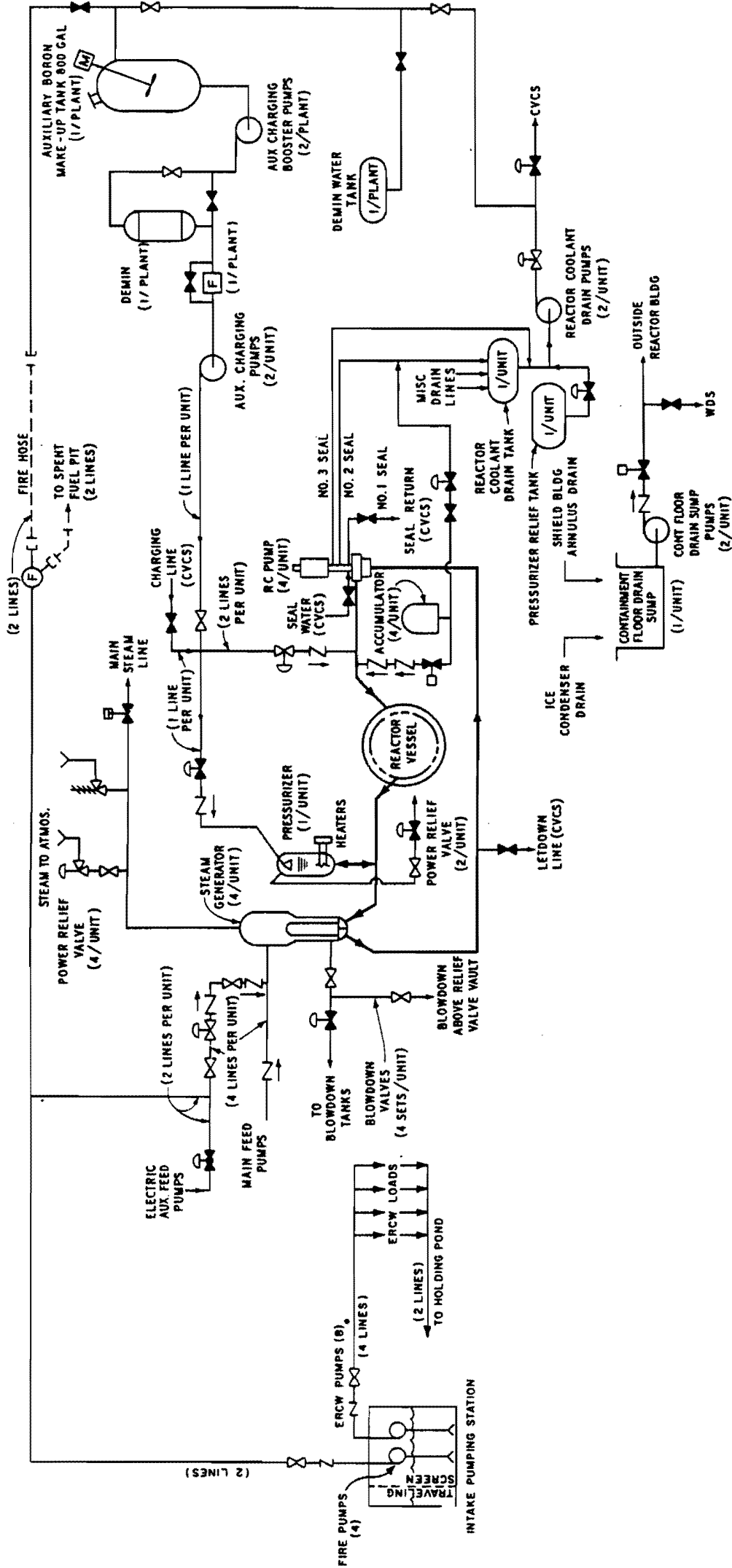
Figure 2.4-107 Powerhouse Units 1 & 2 Flow Diagram - Residual Heat Removal System



WATTS BAR NUCLEAR PLANT
FINAL SAFETY
ANALYSIS REPORT

SCHEMATIC FLOW DIAGRAM
FLOOD PROTECTION PROVISIONS
OPEN REACTOR COOLING
(unit 1 shown, unit 2 similar)
Figure 2.4-108

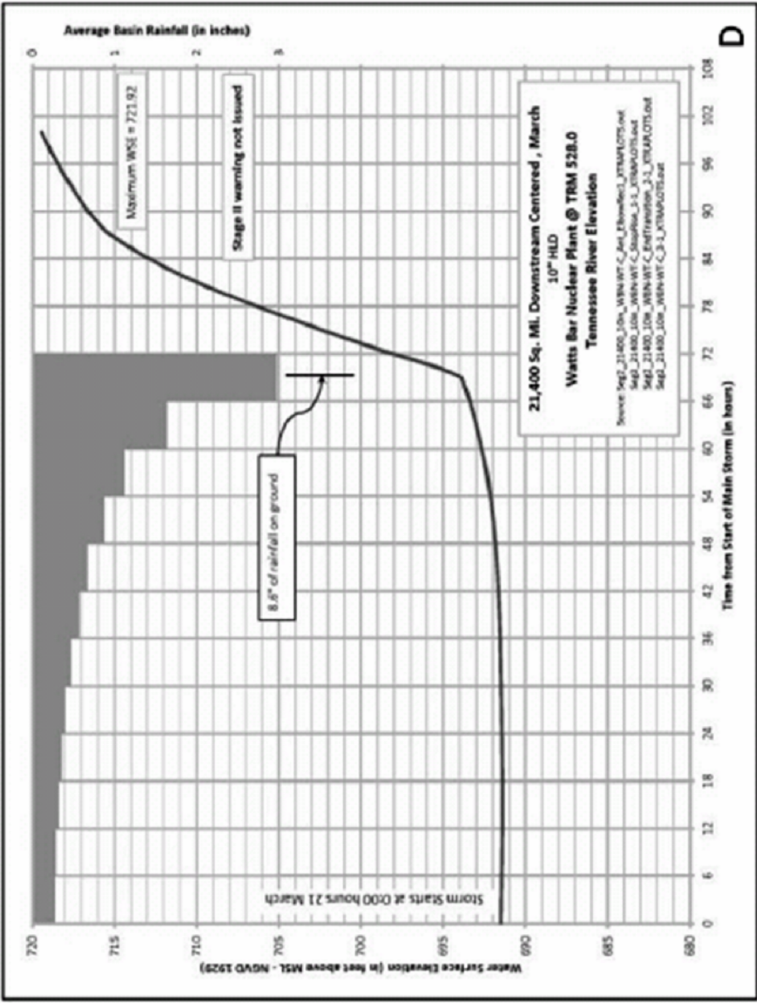
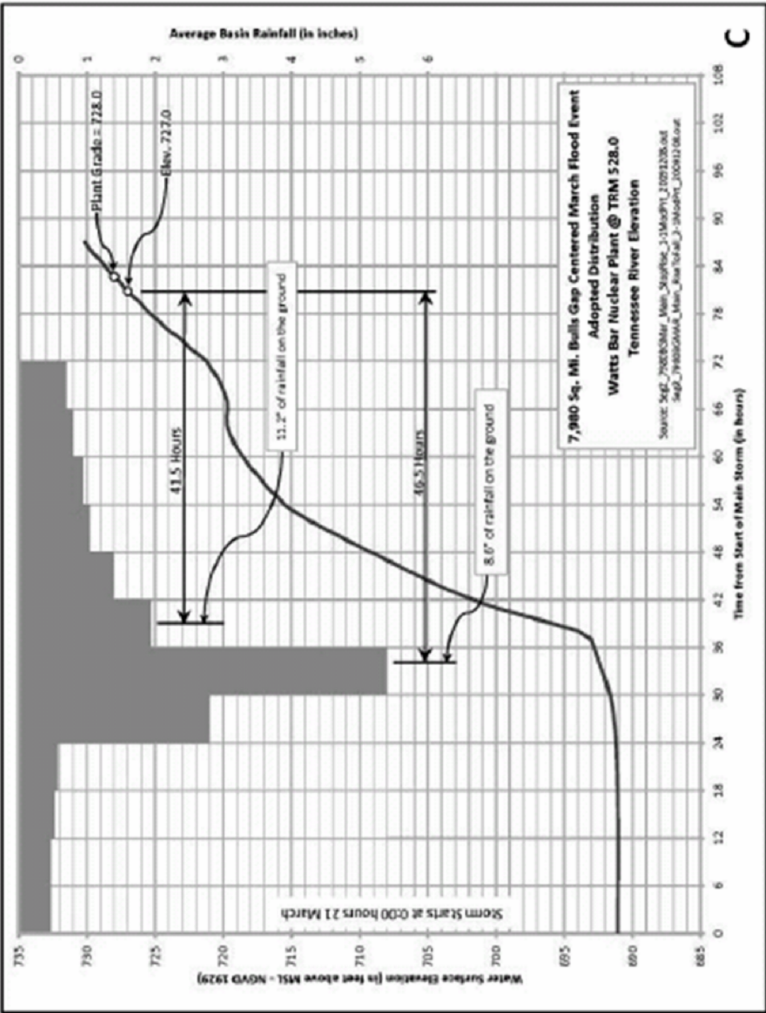
Figure 2.4-108 Schematic Flow Diagram Flood Protection Provisions Open Reactor Cooling (Unit 1 Shown, Unit 2 Similar)



NOTES:
DRAWING DOES NOT INCLUDE:
VENTILATION SYS., EMERGENCY POWER SYS.,
SAMPLING SYS., DETAILS OF ERCW LOADS,
SPOOL PIECE CONNECTIONS.

WATTS BAR NUCLEAR PLANT FINAL SAFETY ANALYSIS REPORT
SCHEMATIC FLOW DIAGRAM FLOOD PROTECTION PROVISIONS NATURAL CONVECTION COOLING (unit 1 shown, unit 2 similar) Figure 2.4-109

Figure 2.4-109 Schematic Flow Diagram Flood Protection Provisions Natural Convection Cooling (Unit 1 Shown, Unit 2 Similar)



NOTE: Times shown allow 4 hours for communications and forecast computations.

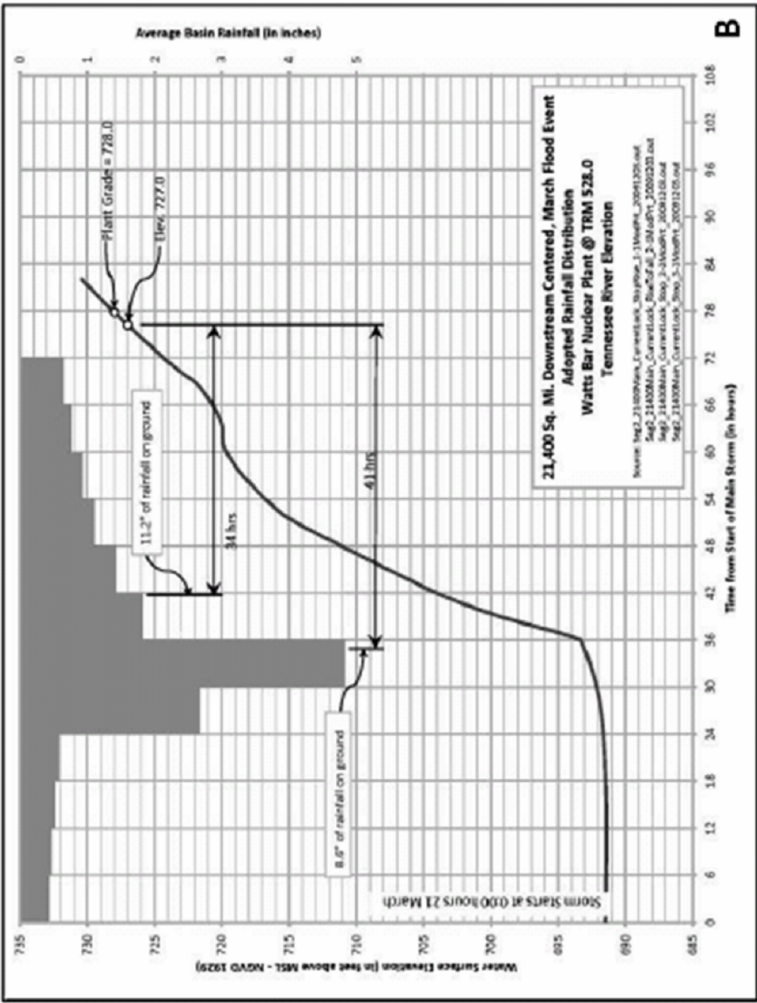
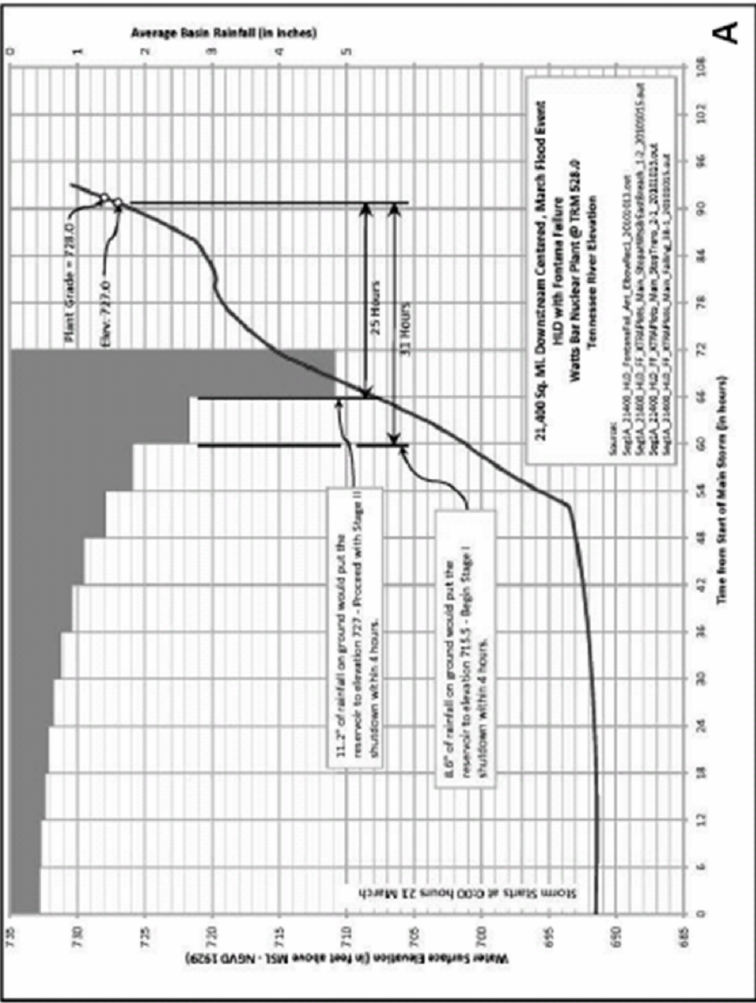
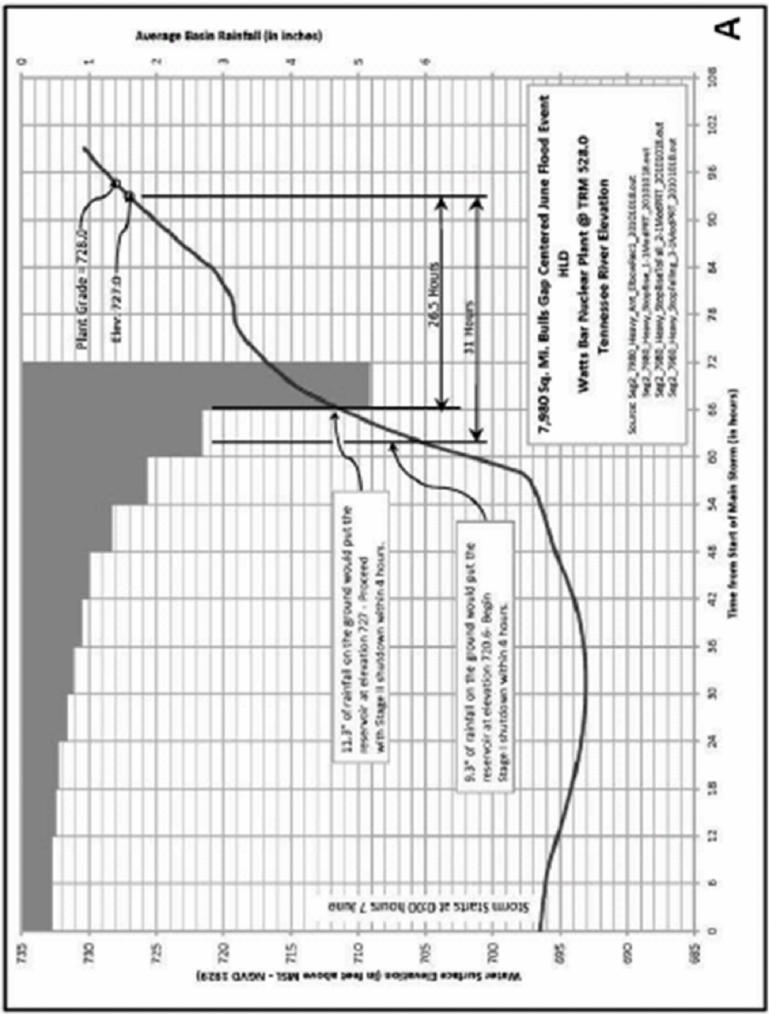
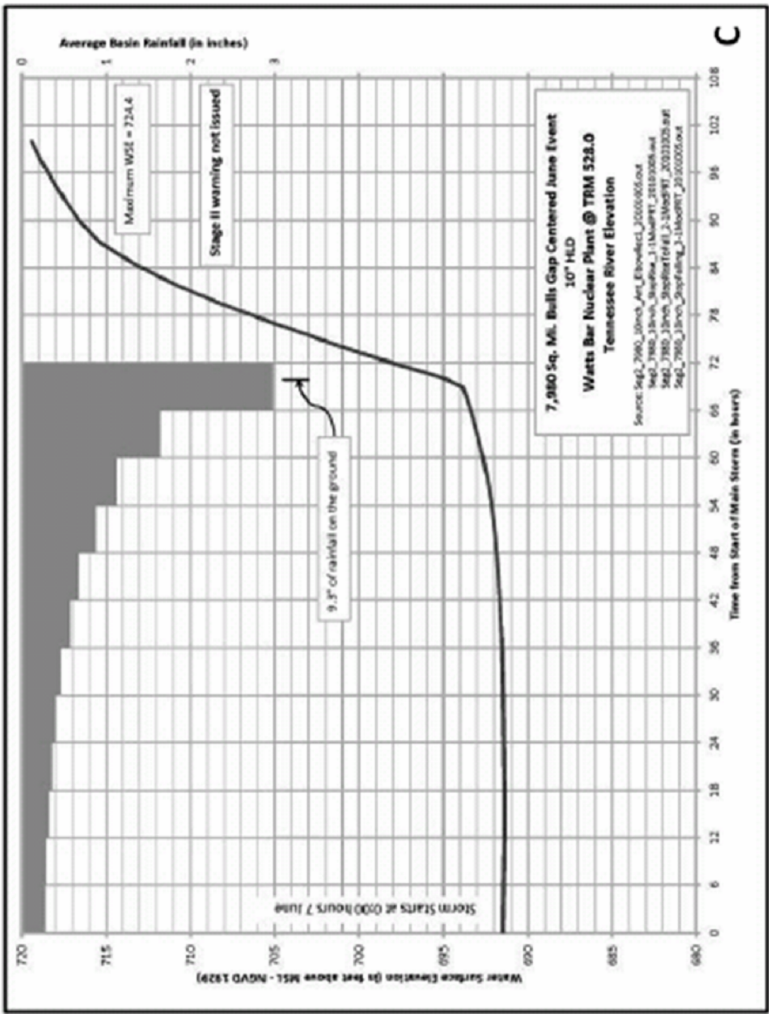


Figure 2.4-110 (Sheet 1) Watts Bar Nuclear Plant Rainfall Flood Warning Time Basis For Safe Shutdown For Plant Flooding - Winter Events



NOTE: Times shown allow 4 hours for communications and forecast computations.

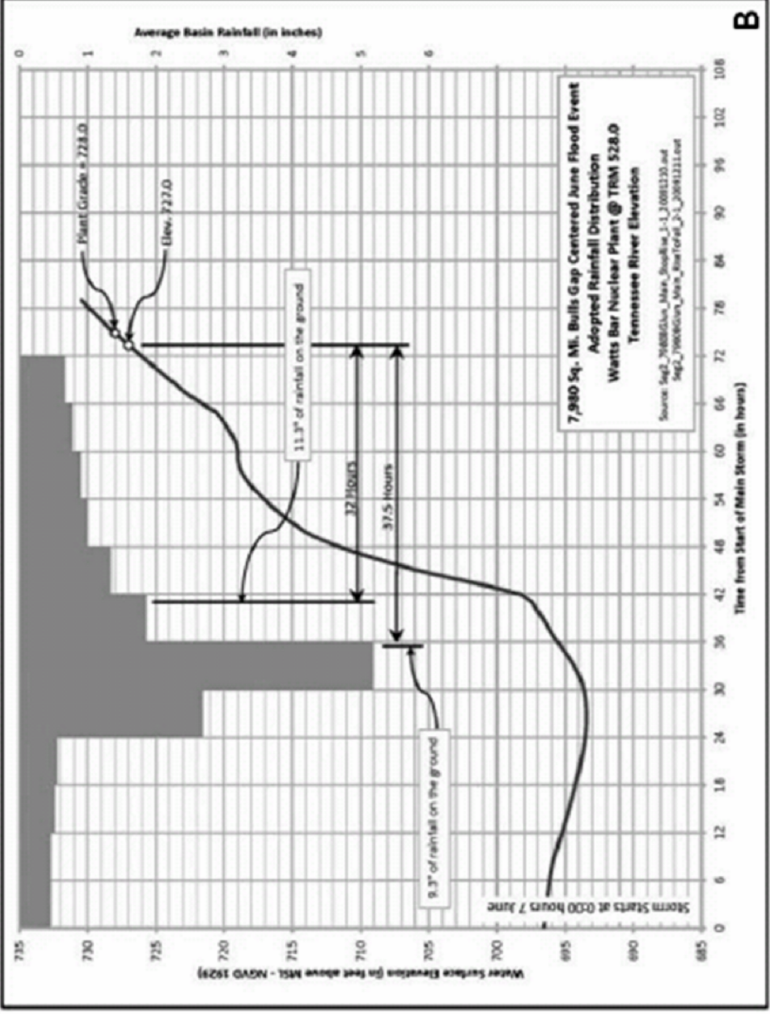


Figure 2.4-110 (Sheet 2) Watts Bar Nuclear Plant Rainfall Flood Warning Time Basis For Safe Shutdown For Plant Flooding - Summer Events

Figure 2.4-111 Deleted by Amendment 103



Figure 2.4-112 OBE with Epicenter Within Area Shown

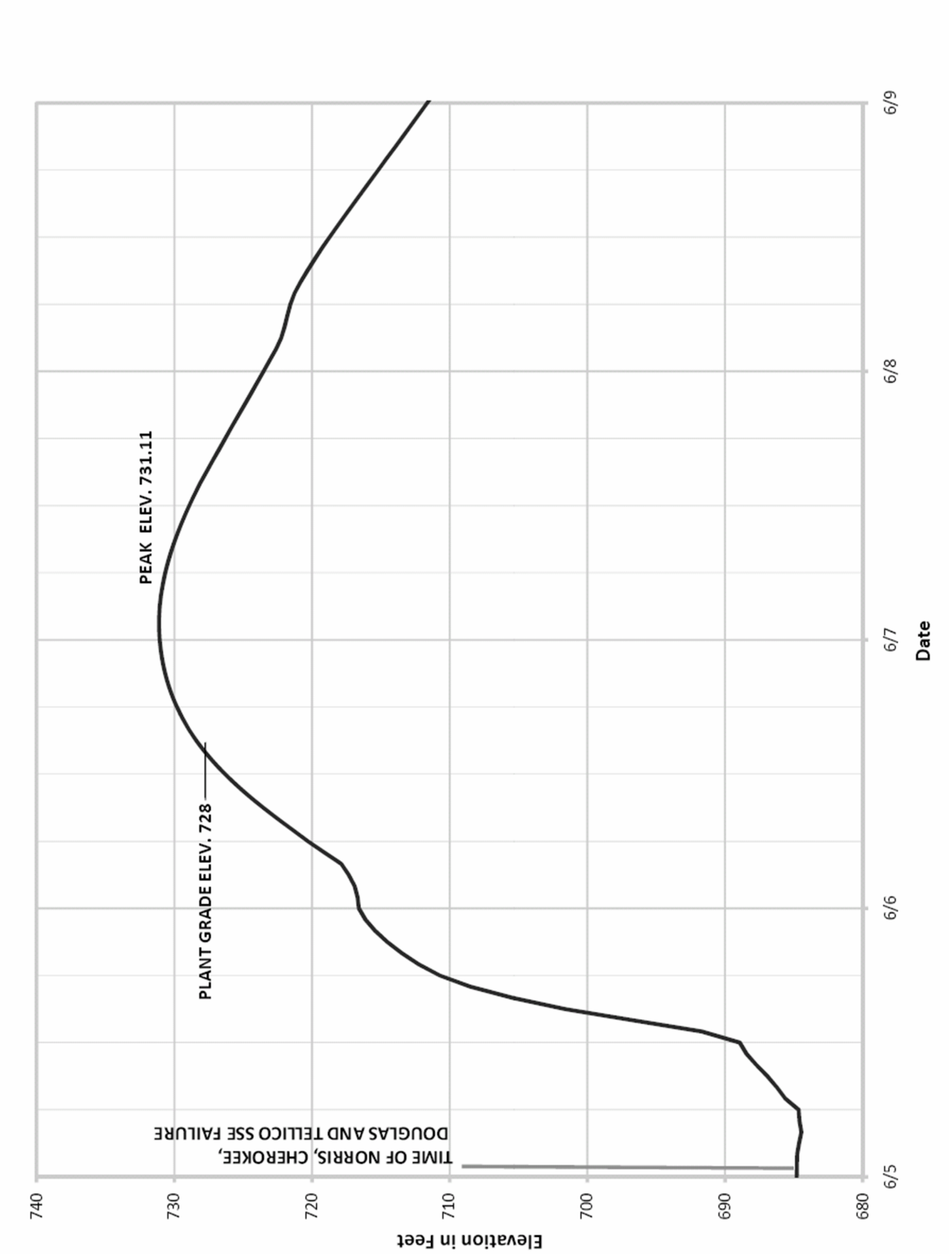


Figure 2.4-113 SSE Failure of Norris, Cherokee, Douglas, and Tellico Dams with 25-Year Flood Failure Wave at Watts Bar Nuclear Plant

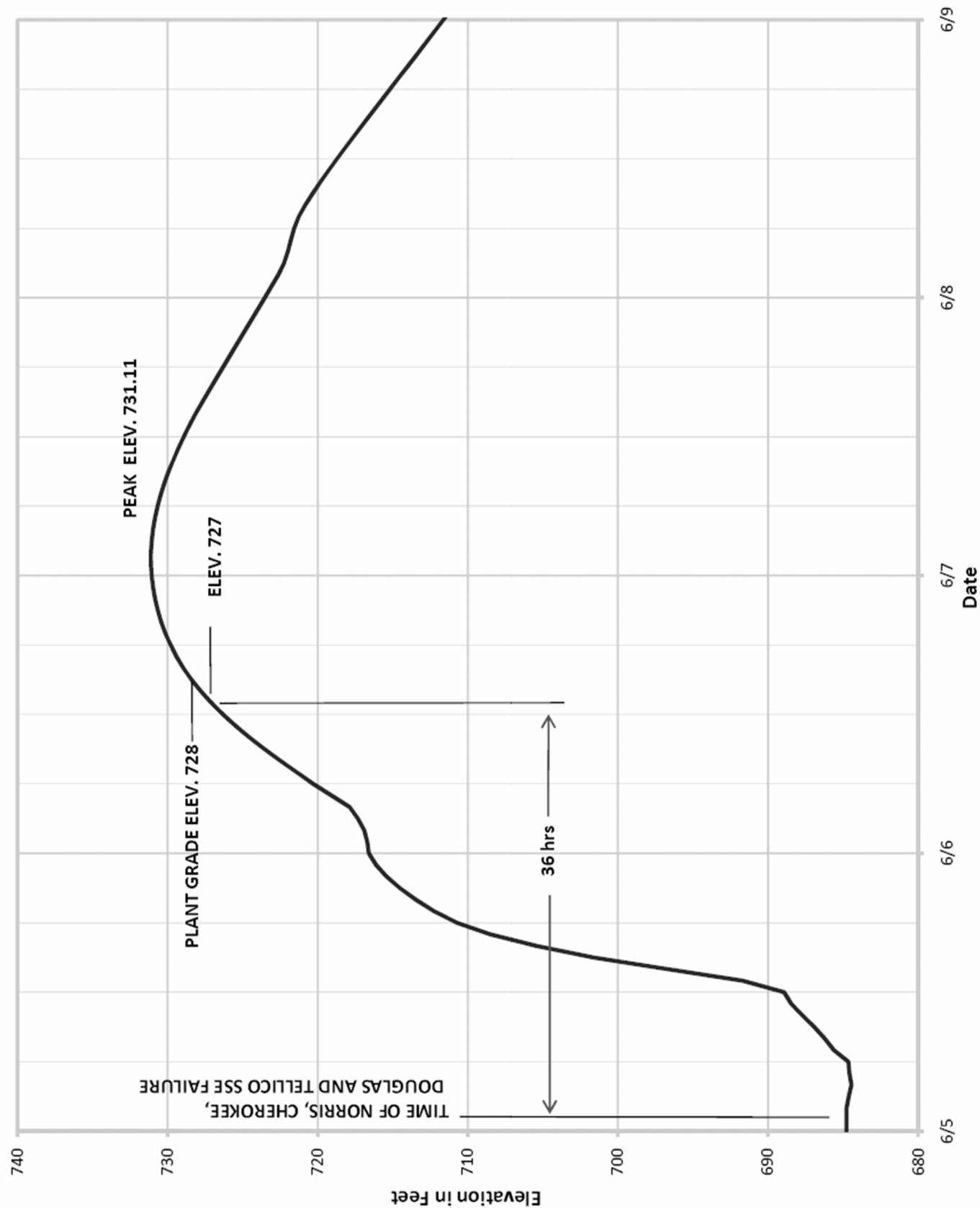


Figure 2.4-114 SSE Failure of Norris, Cherokee, Douglas, and Tellico Dams with 25-Year Flood Failure Wave at Watts Bar Nuclear Plant

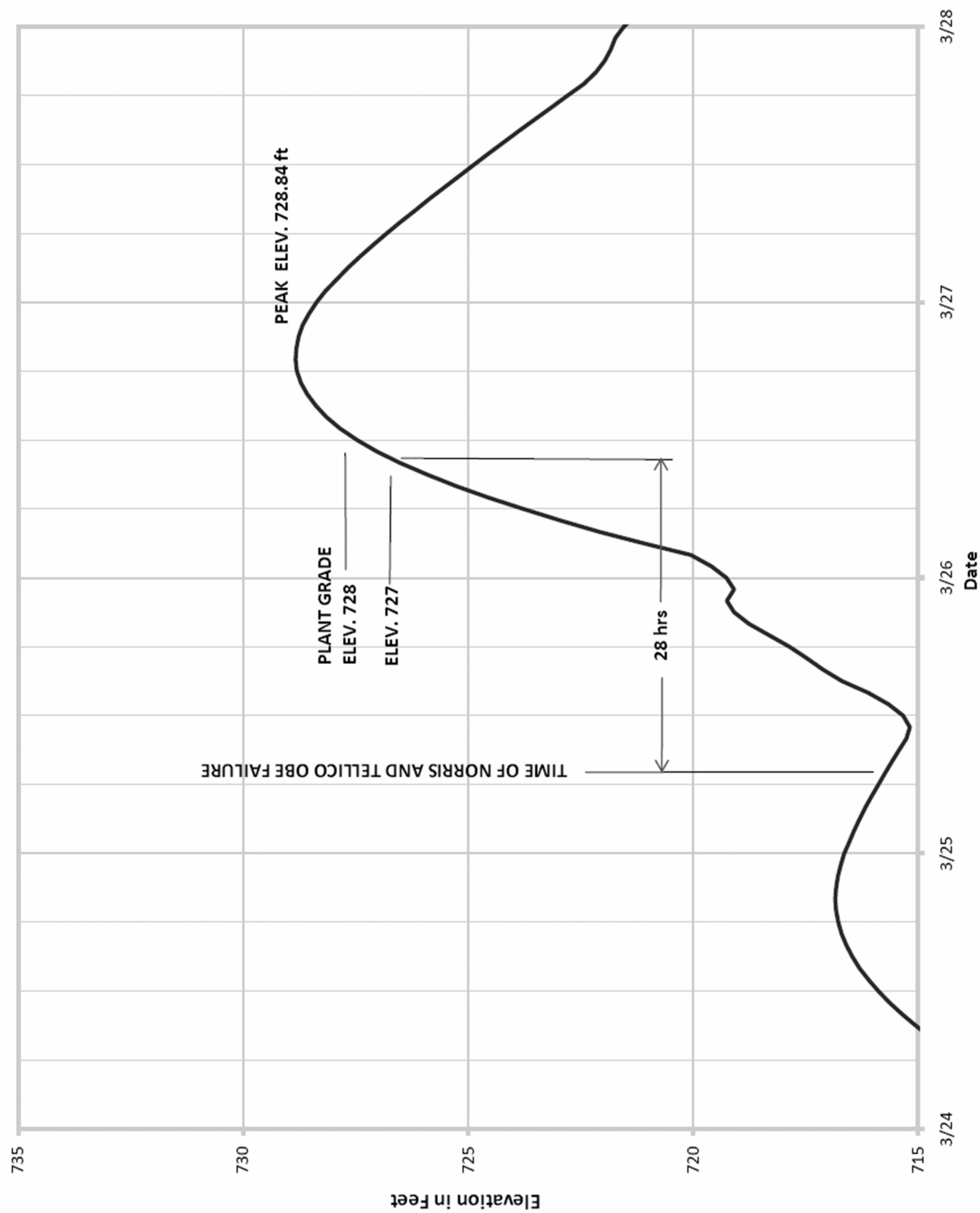


Figure 2.4-115 OBE Failure of Norris and Tellico Dams with 1/2 PMF Event
Failure Wave at Watts Bar Nuclear Plant

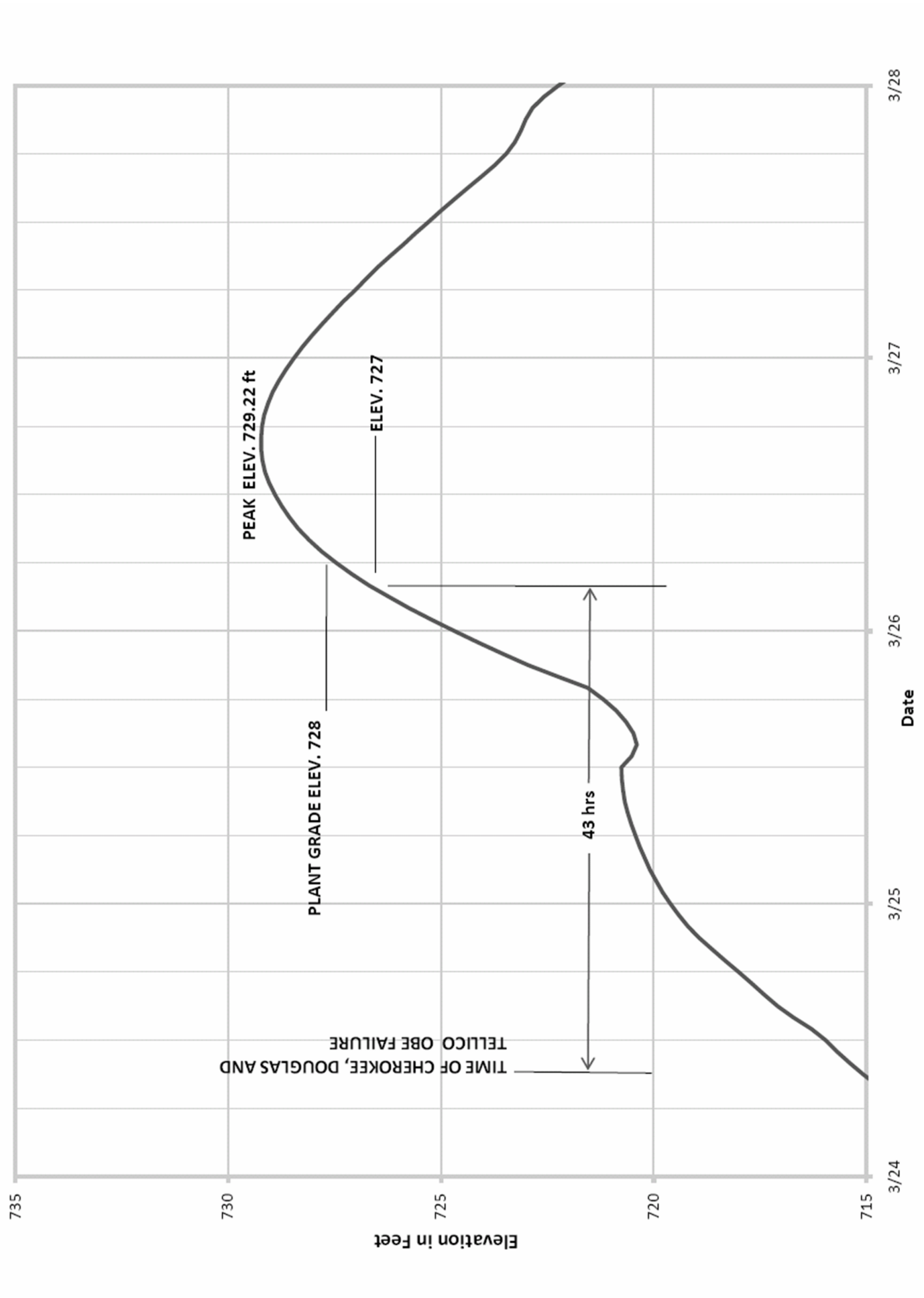


Figure 2.4-116 OBE Failure of Cherokee, Douglas and Tellico Dams with 1/2 PMF Event
Failure Wave at Watts Bar Nuclear Plant